

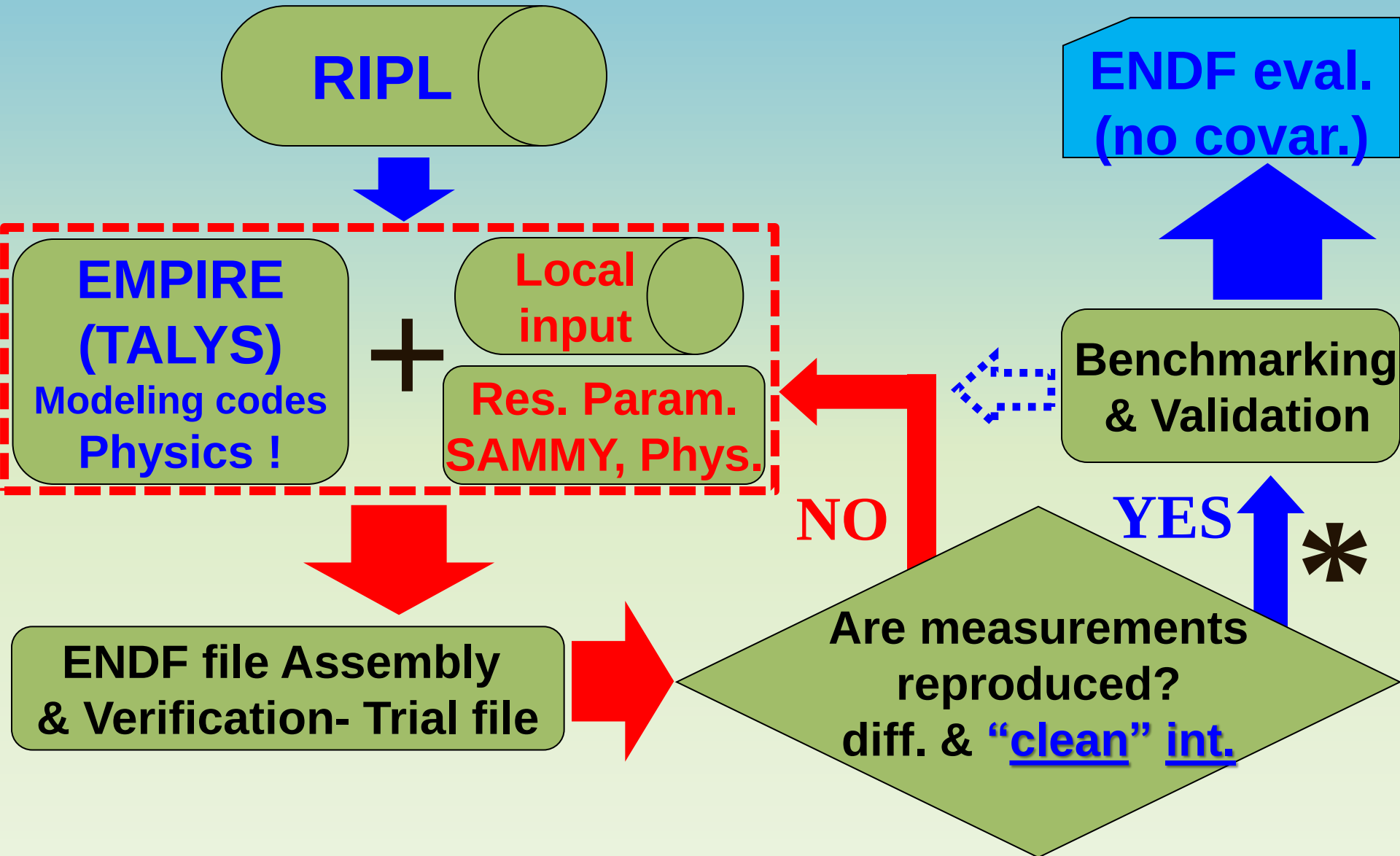
New $n + {}^{235}\text{U}$ evaluation (fast)



**R. Capote, A. Trkov, M. Sin,
M.W. Herman, V.G. Pronyaev**



IAEA evaluation process (no covar.)



$n + {}^{235}\text{U}$ fast region ($E_n > 2.25 \text{ keV}$)

- ❑ (n, f) from 2006 Neutron Standards
(to be updated with new GMA Standard fit)
- ❑ (n, γ) : Adopted from B/VII.1
(Update based on Jandel/RPI ?)
- ❑ (n, f) : 3H barrier with absorption
- ❑ PFNS adopted from IAEA CRP
(incl. Rising-Talou analysis above thermal)



Extended optical model for fission

M. Sin,^{1,*} R. Capote,^{2,†} M. W. Herman,³ and A. Trkov²

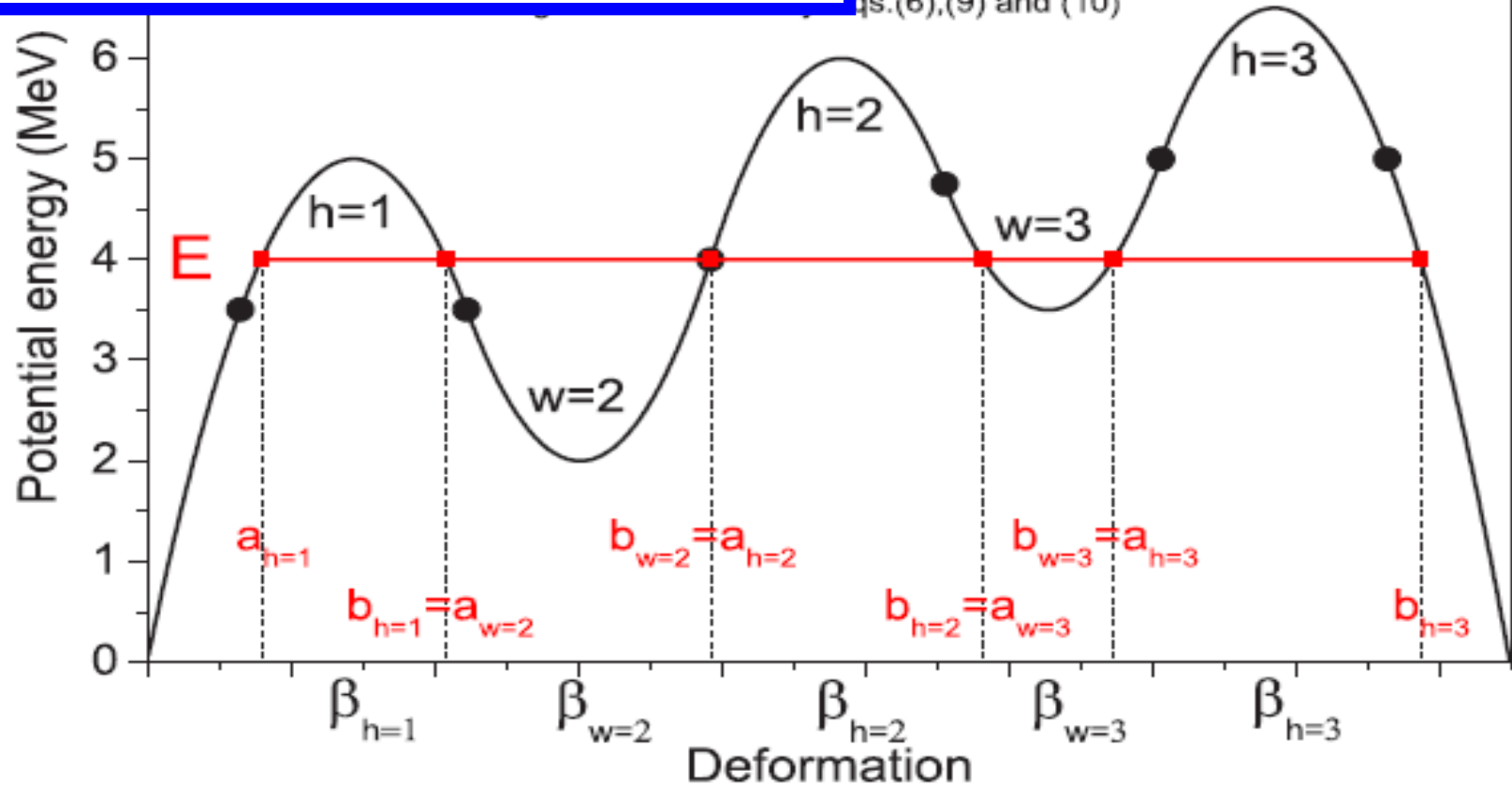


FIG. 1. A triple-humped fission barrier and associated parameters.



Optical model for fission: 3H

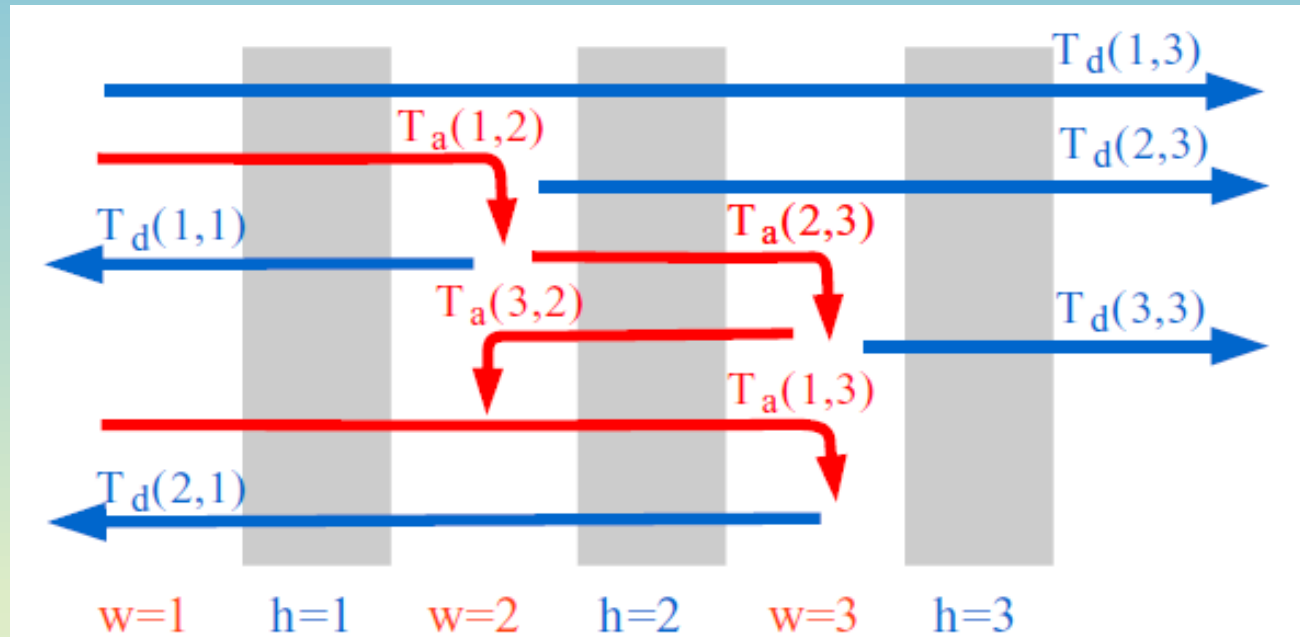
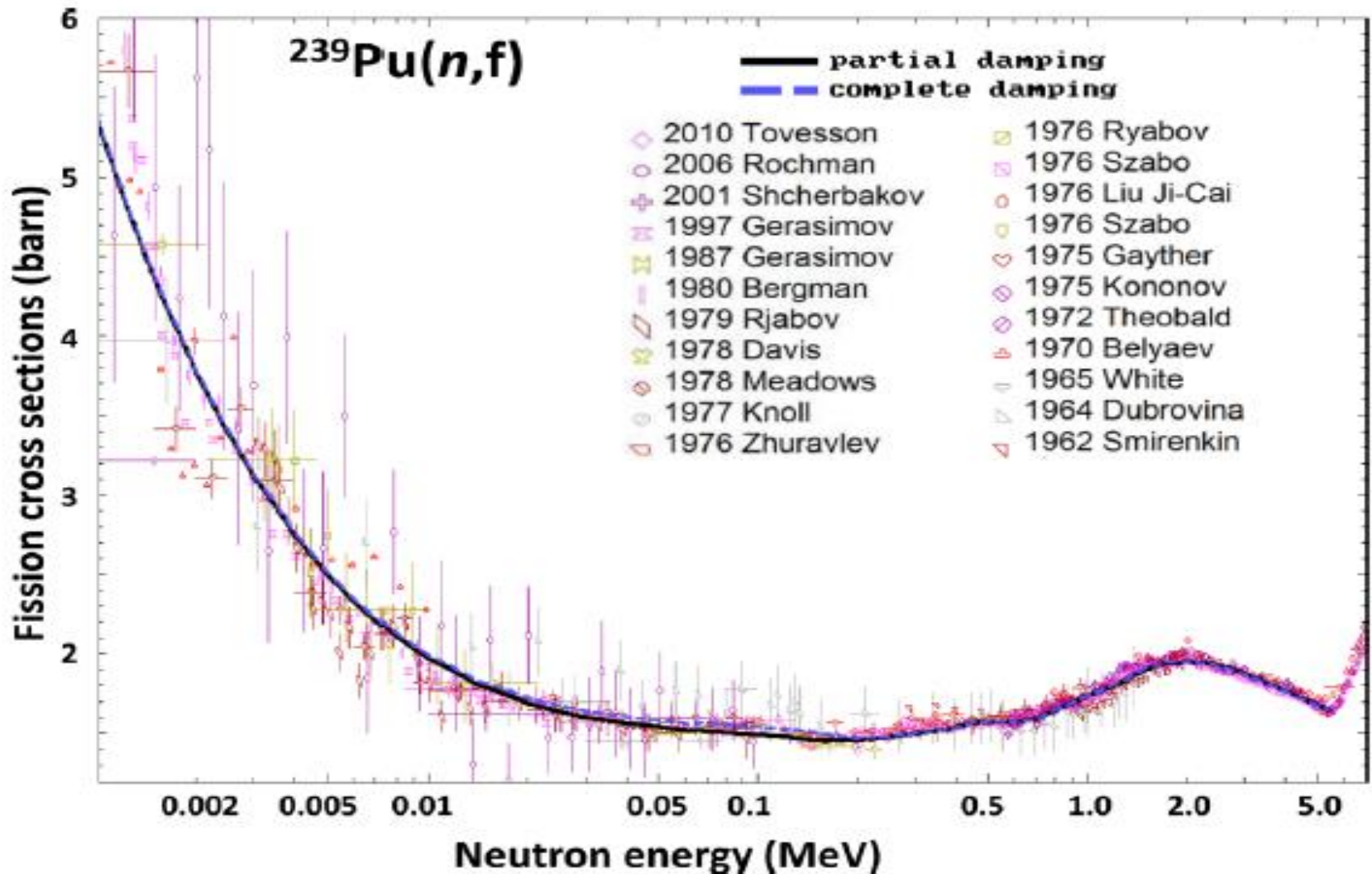


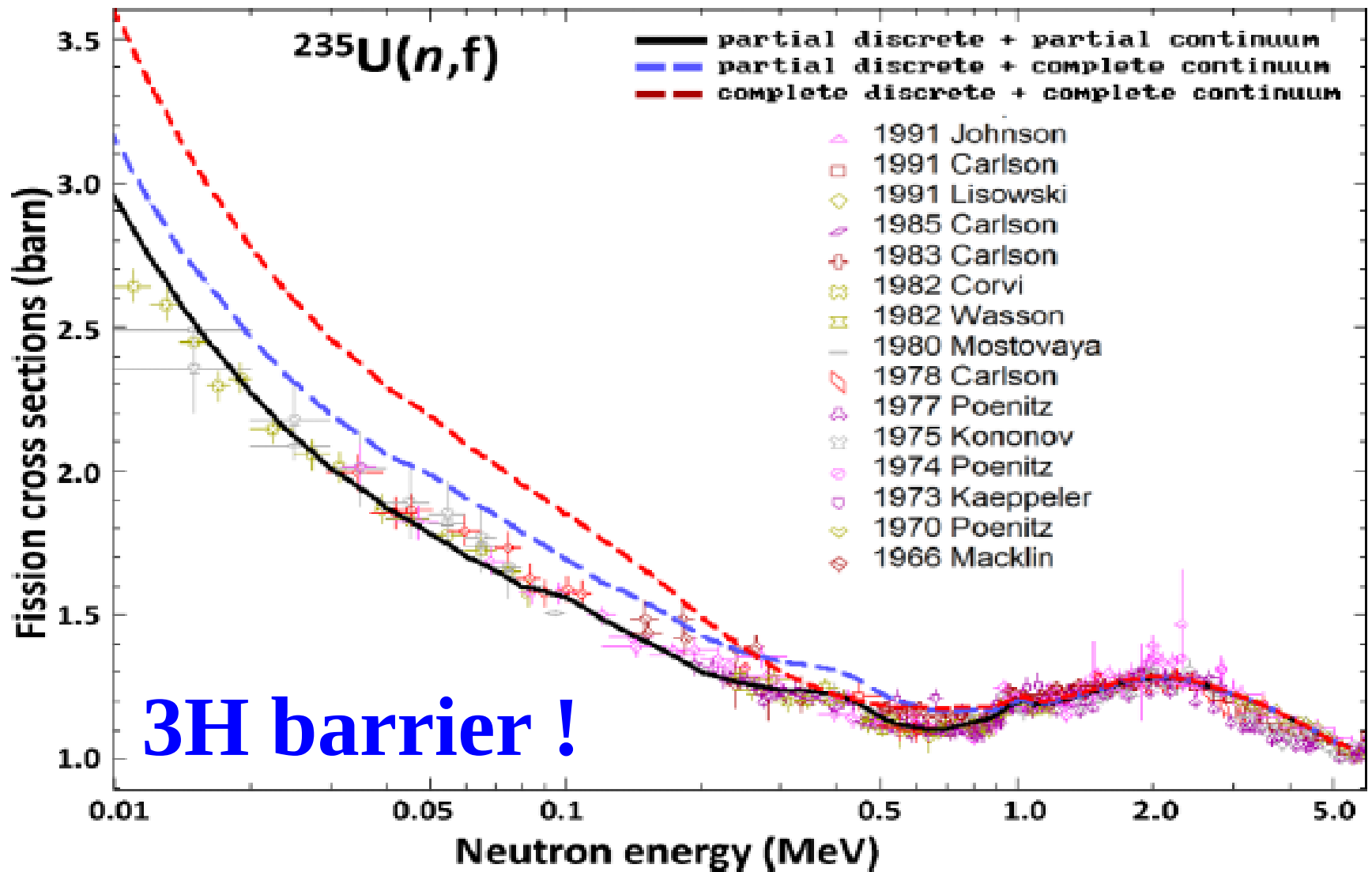
FIG. 2. Schematic representation of the transmission flux for a triple-humped fission barrier. w (h) values indicated below the figure represent the well (barrier) index. The coefficients $T_a(w, w')$ that represents the absorption in a well w of the flux coming from the well w' are shown as bent arrows (in red), the coefficients $T_d(h, h')$ that represent the transmission through the humps h and h' are shown as straight arrows (in blue), and the coefficients $T_d(h, h) \equiv T_h$ represent the transmission through a single hump h . Arrows pointing to the



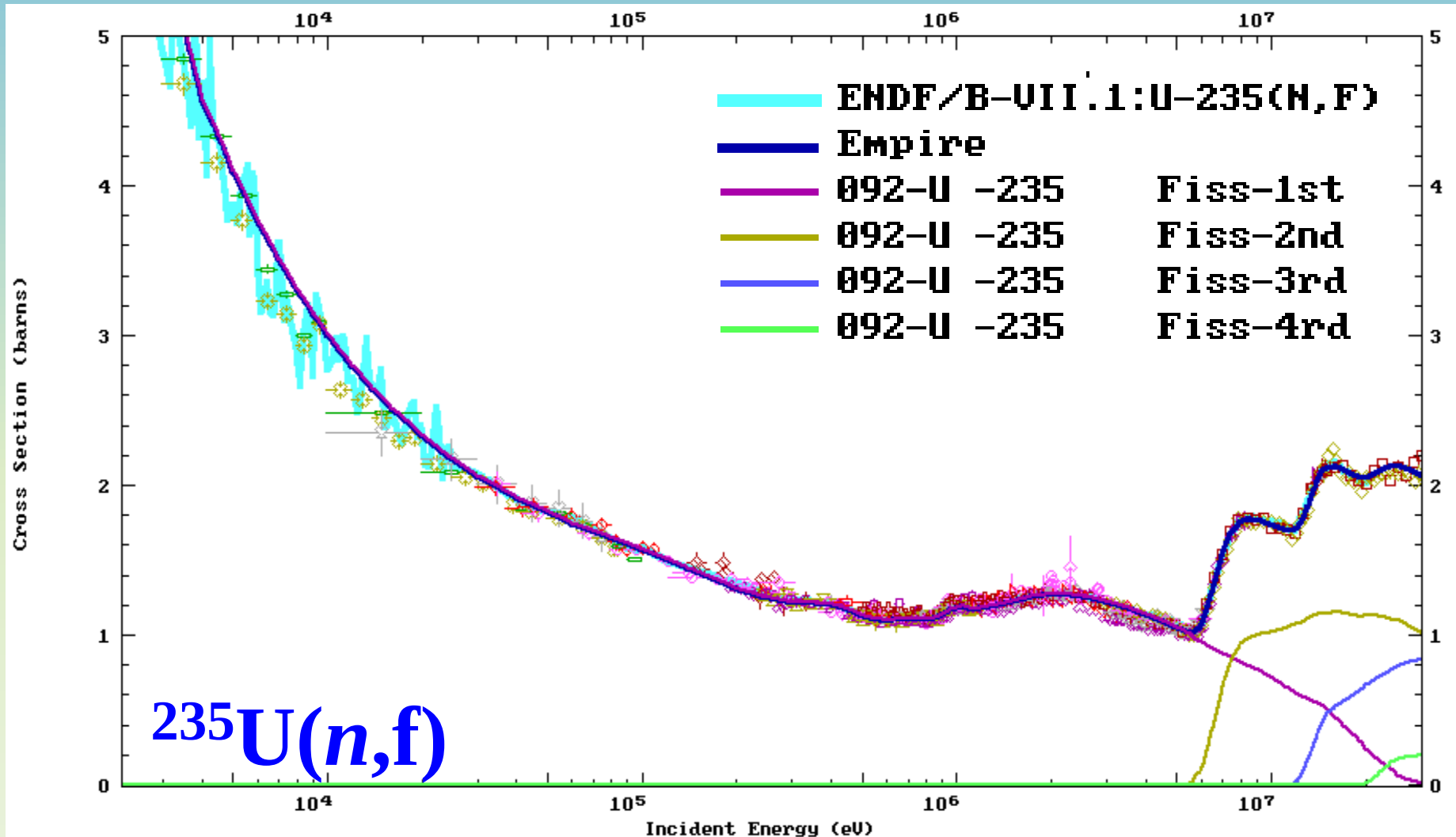
$^{239}\text{Pu}(n,f)$ 2H barrier, independent barriers ok

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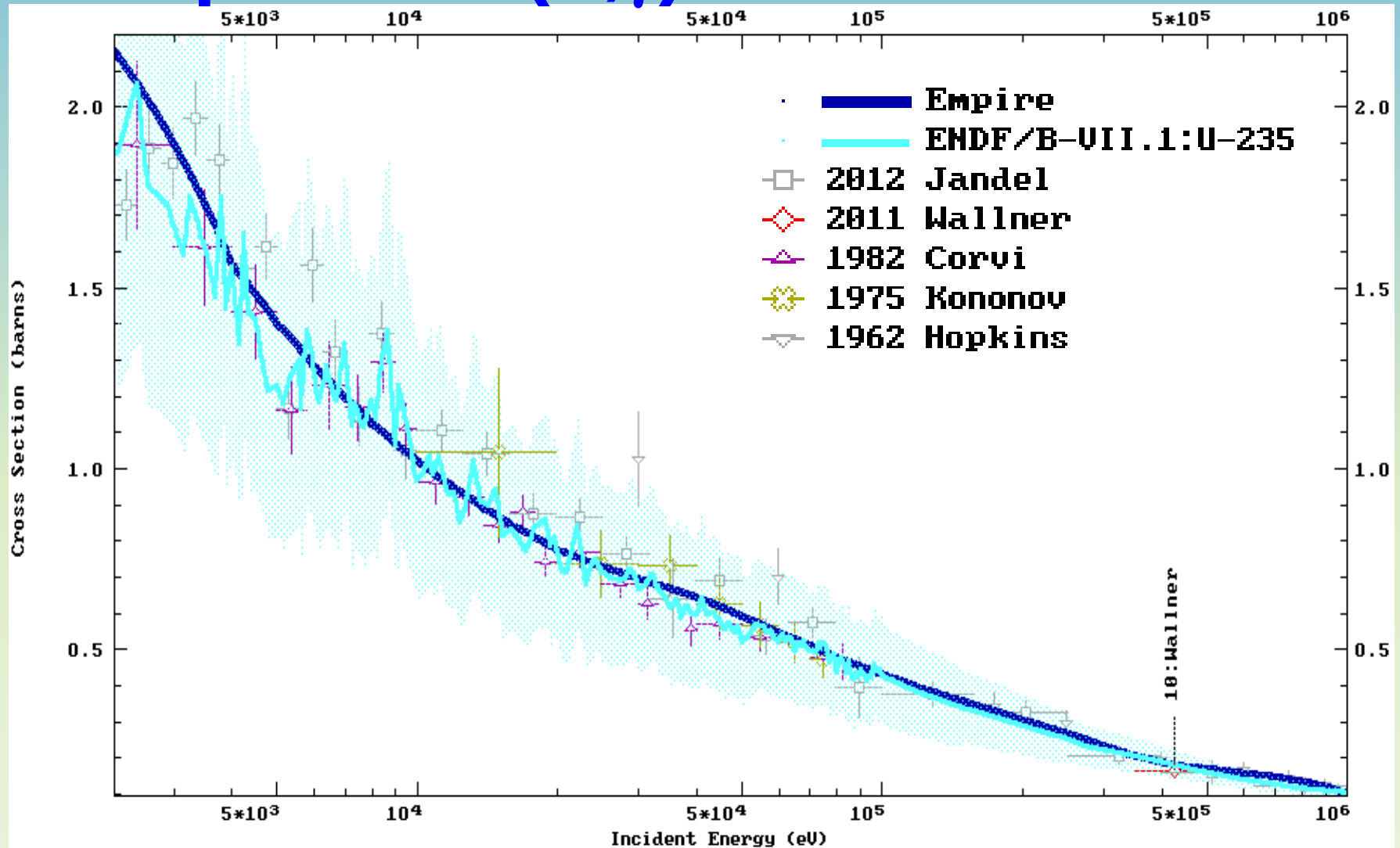
Empire $^{235}\text{U}(n,f)$ vs ENDF/B-VII.1



$^{235}\text{U}(n,f)\text{-ib6a} = \text{ENDF-B/VII.1} = \text{STD}$



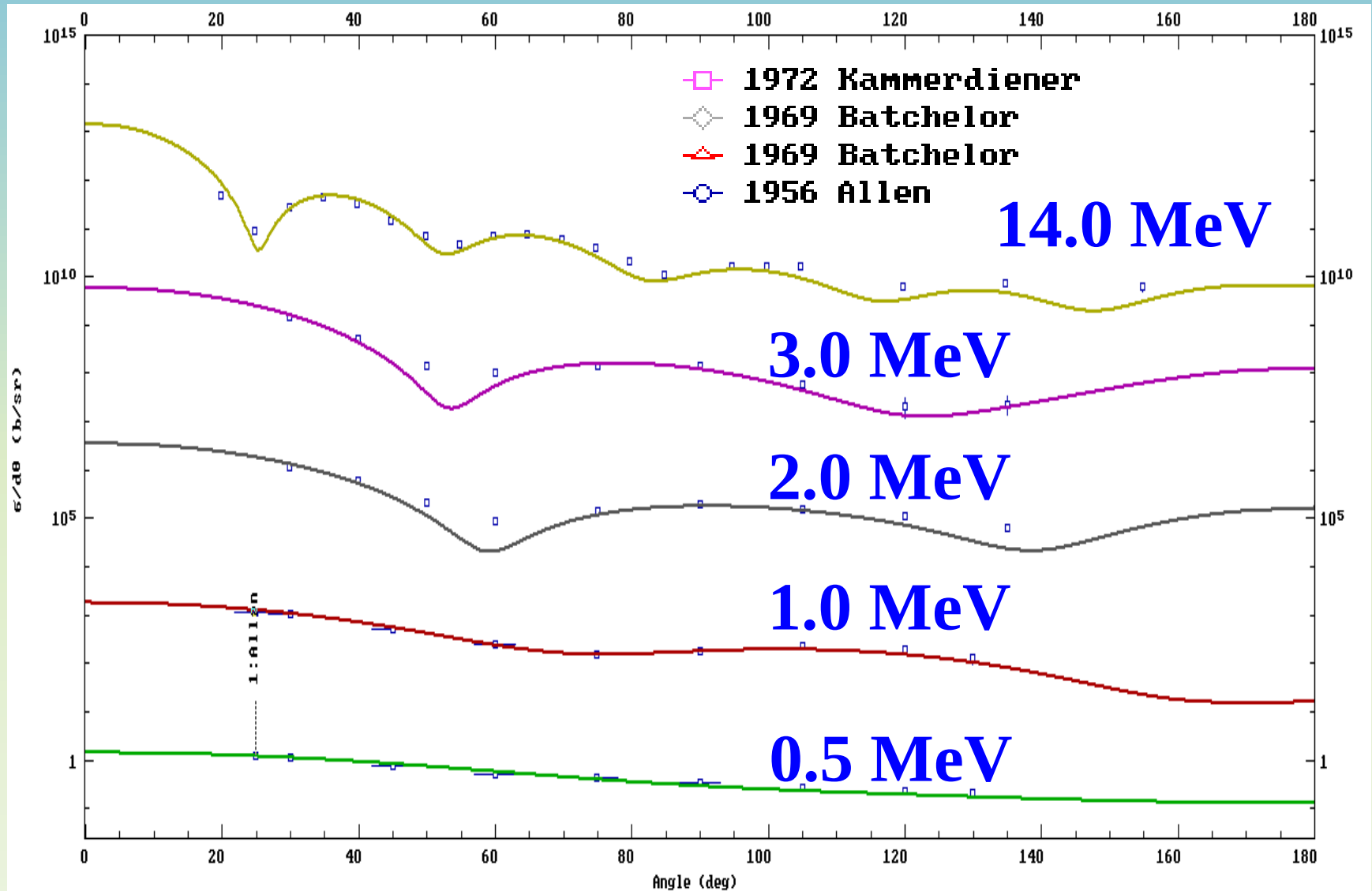
Empire $^{235}\text{U}(n,\gamma)$ vs ENDF/B-VII.1



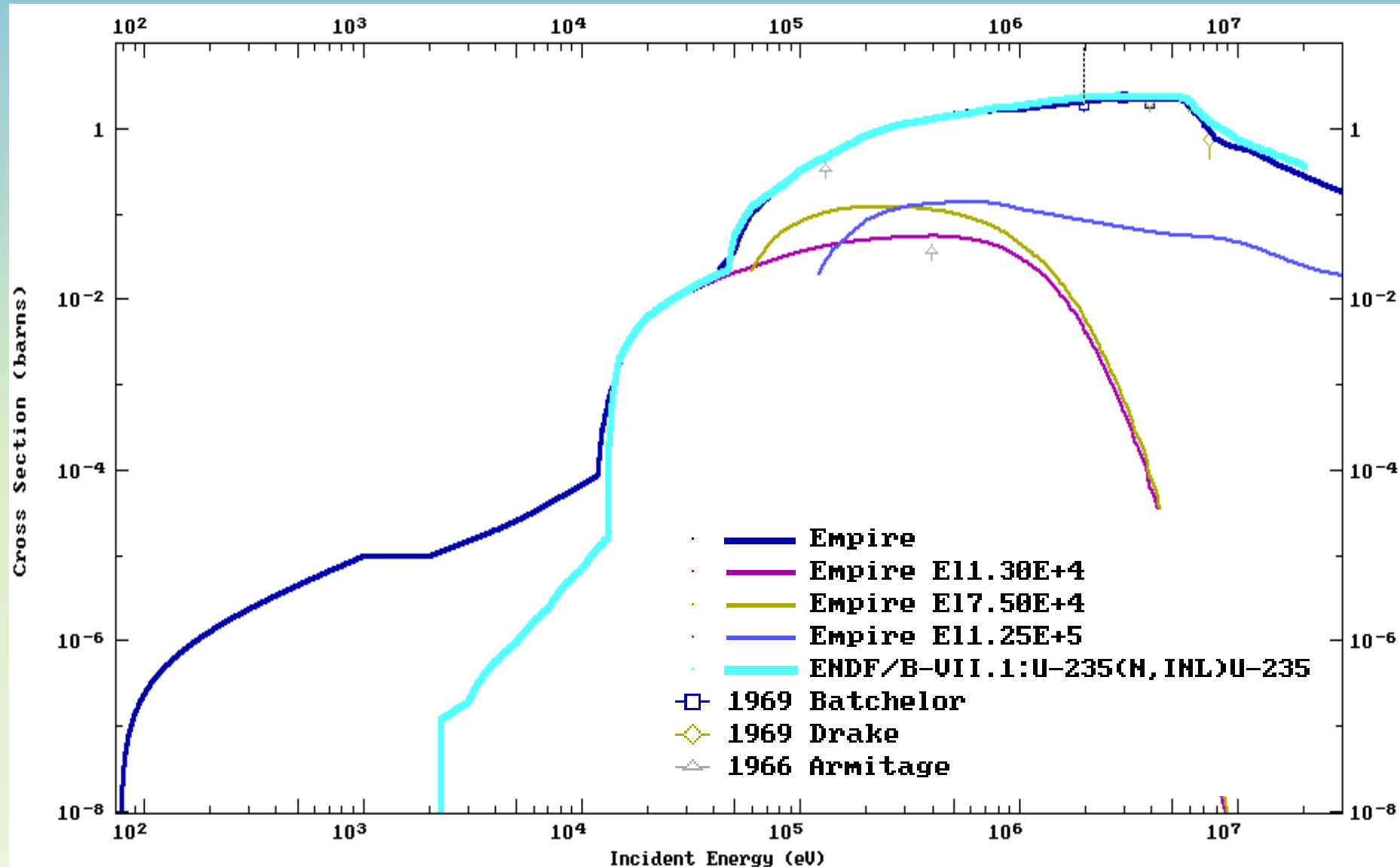
$^{235}\text{U}(n,\gamma) - \text{ib6a} = \text{ENDF-B/VII.1}$



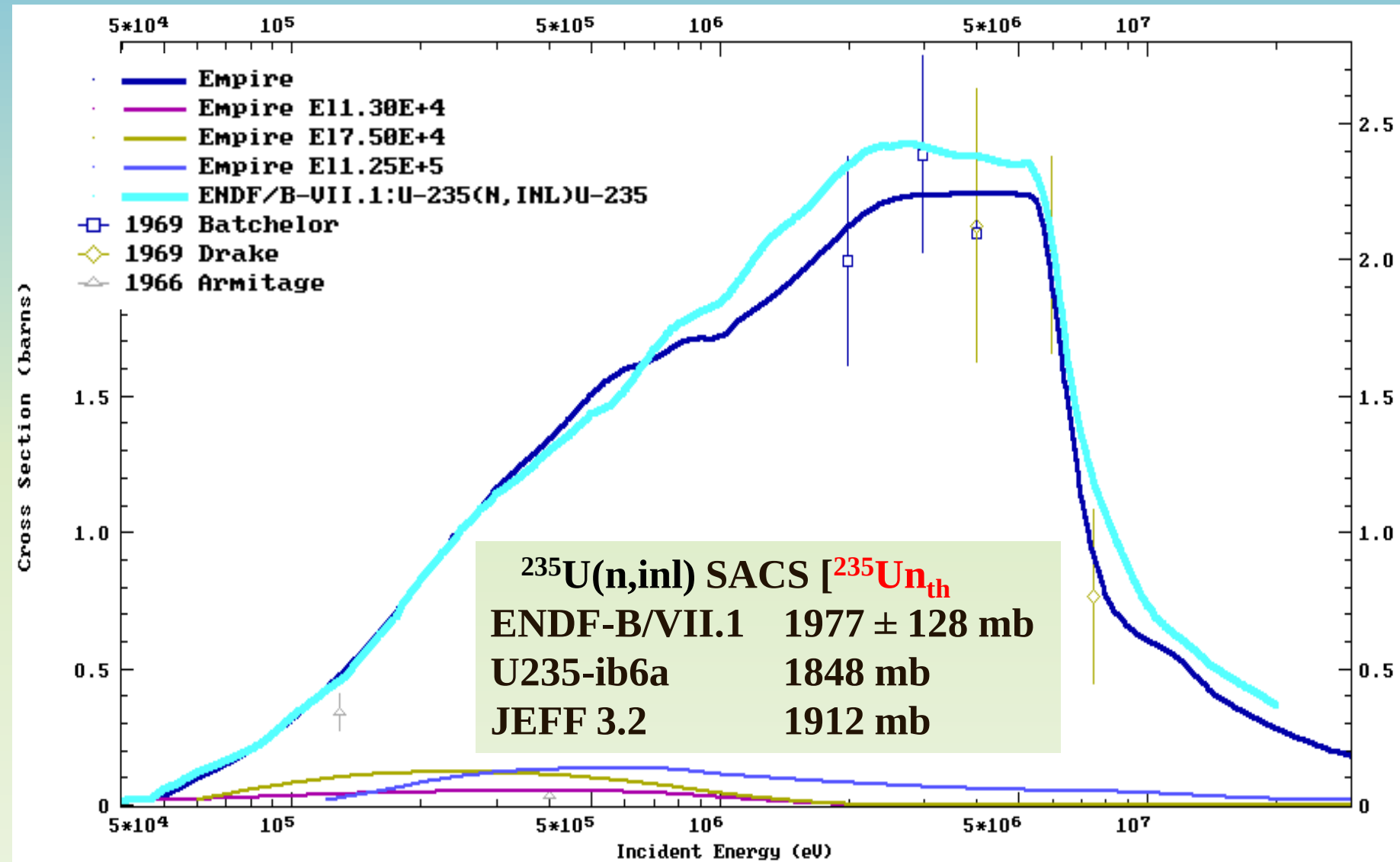
$^{235}\text{U}(\text{n},\text{el}), ^{235}\text{U}(\text{n},\text{sct})$ ang.distributions



$^{235}\text{U}(n,\text{inl})$ (b6a) vs ENDF/B-VII.1



$^{235}\text{U}(n,\text{inl})$ (b6a) vs ENDF/B-VII.1



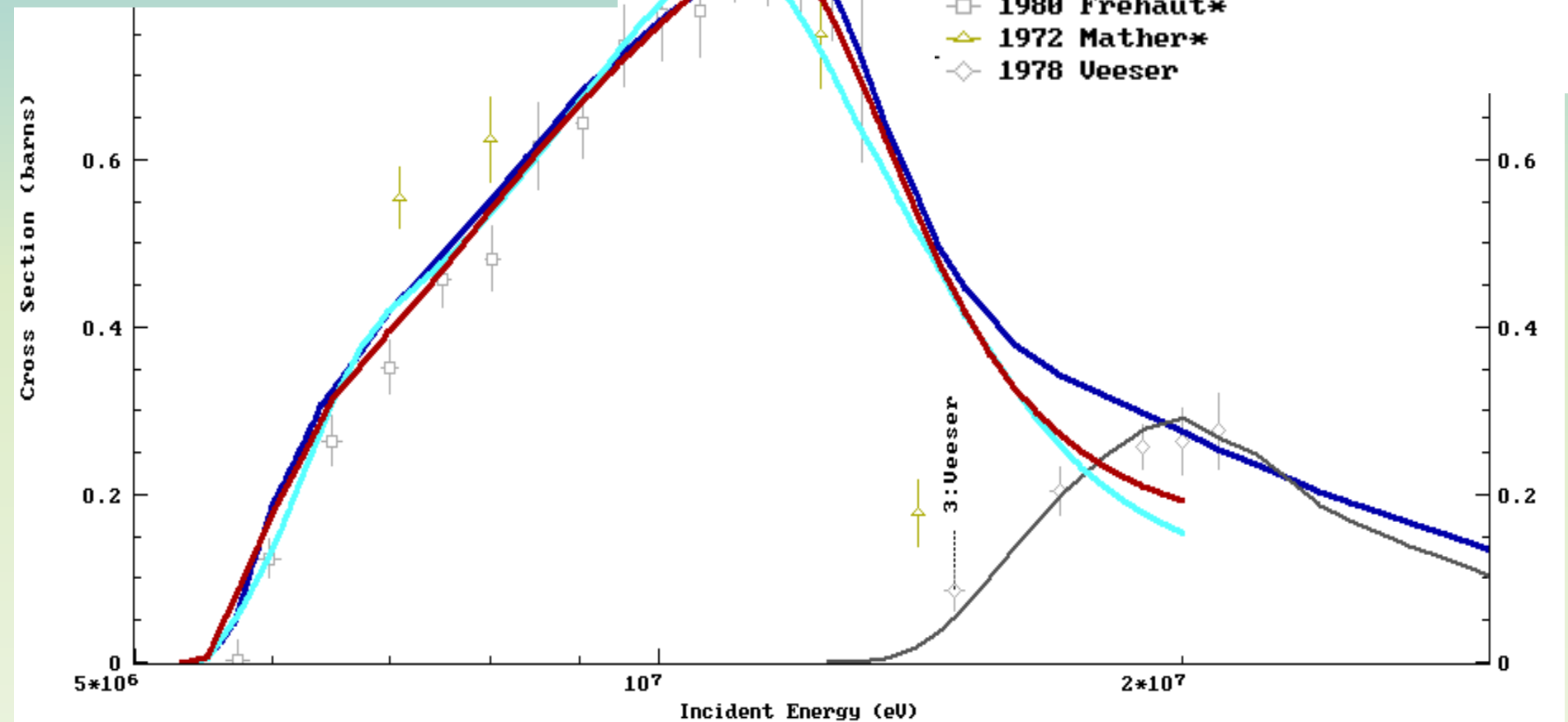
$\sigma(n,2n)$, $\sigma(n,3n)$ vs ENDF/B-VII.1

$^{235}\text{U}(n,2n)$ SACS [$^{235}\text{U}_{\text{nth}}$]

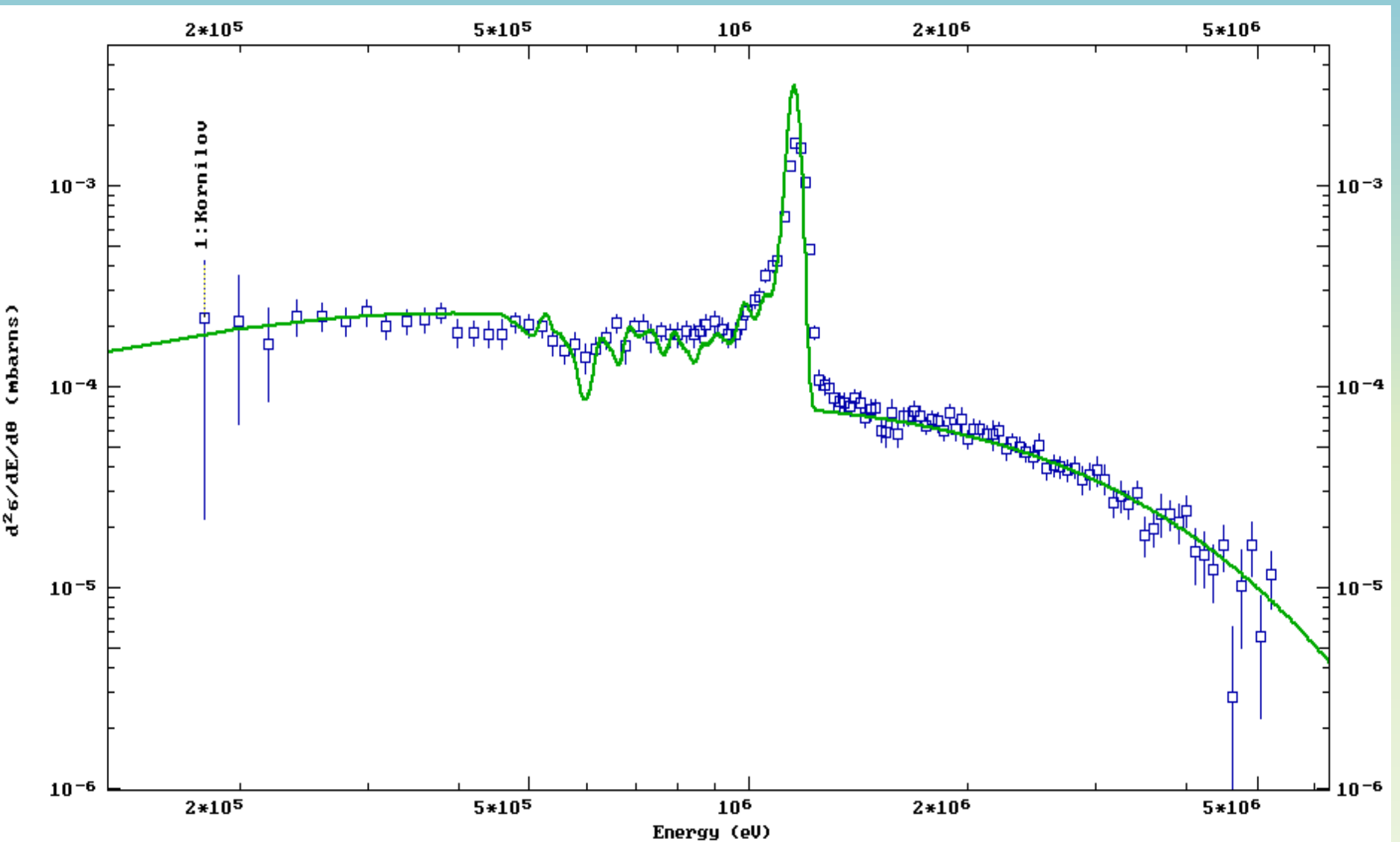
ENDF-B/VII.1 11.6 ± 0.6 mb

U235-ib6a 12.1 mb

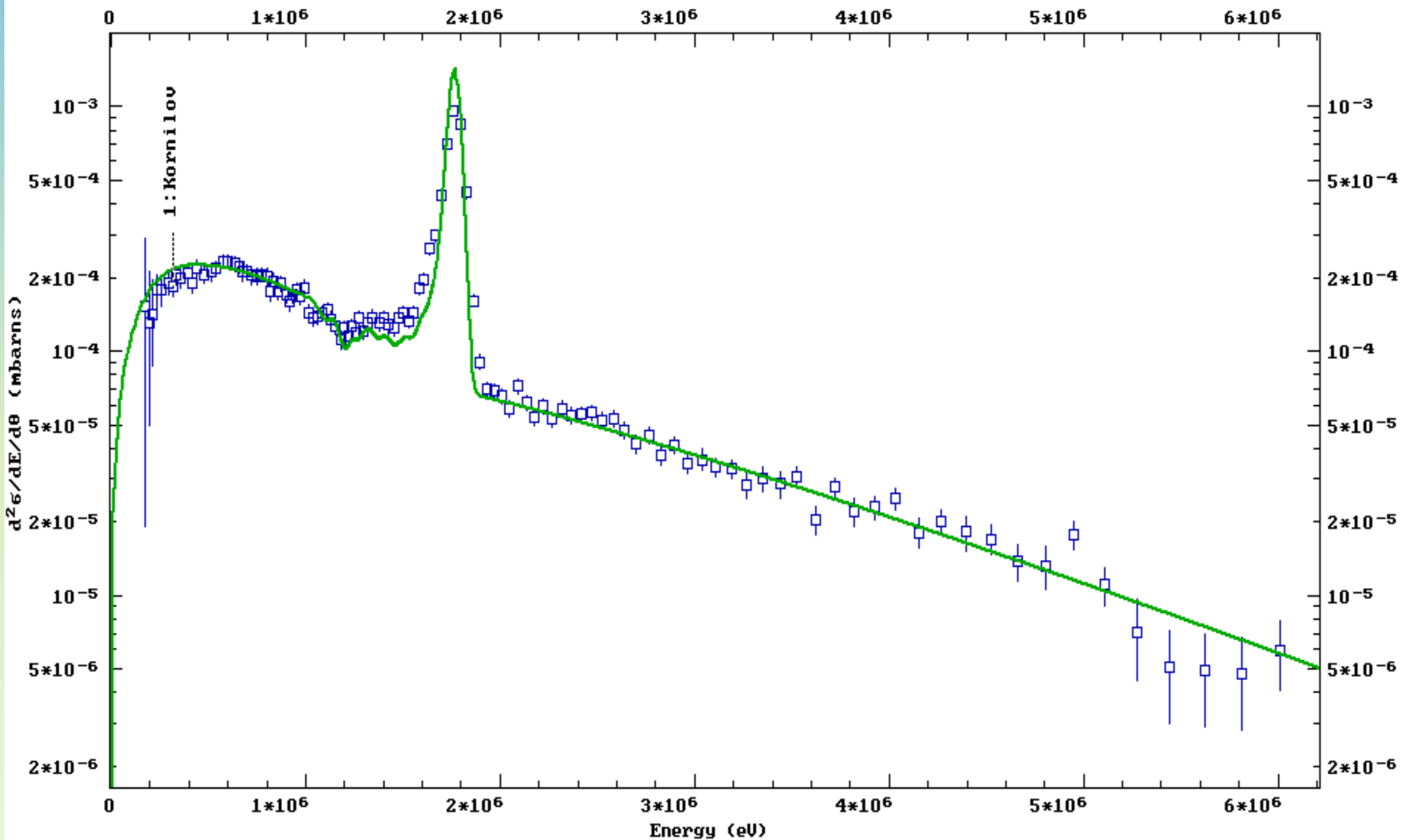
JEFF 3.2 18.2 mb



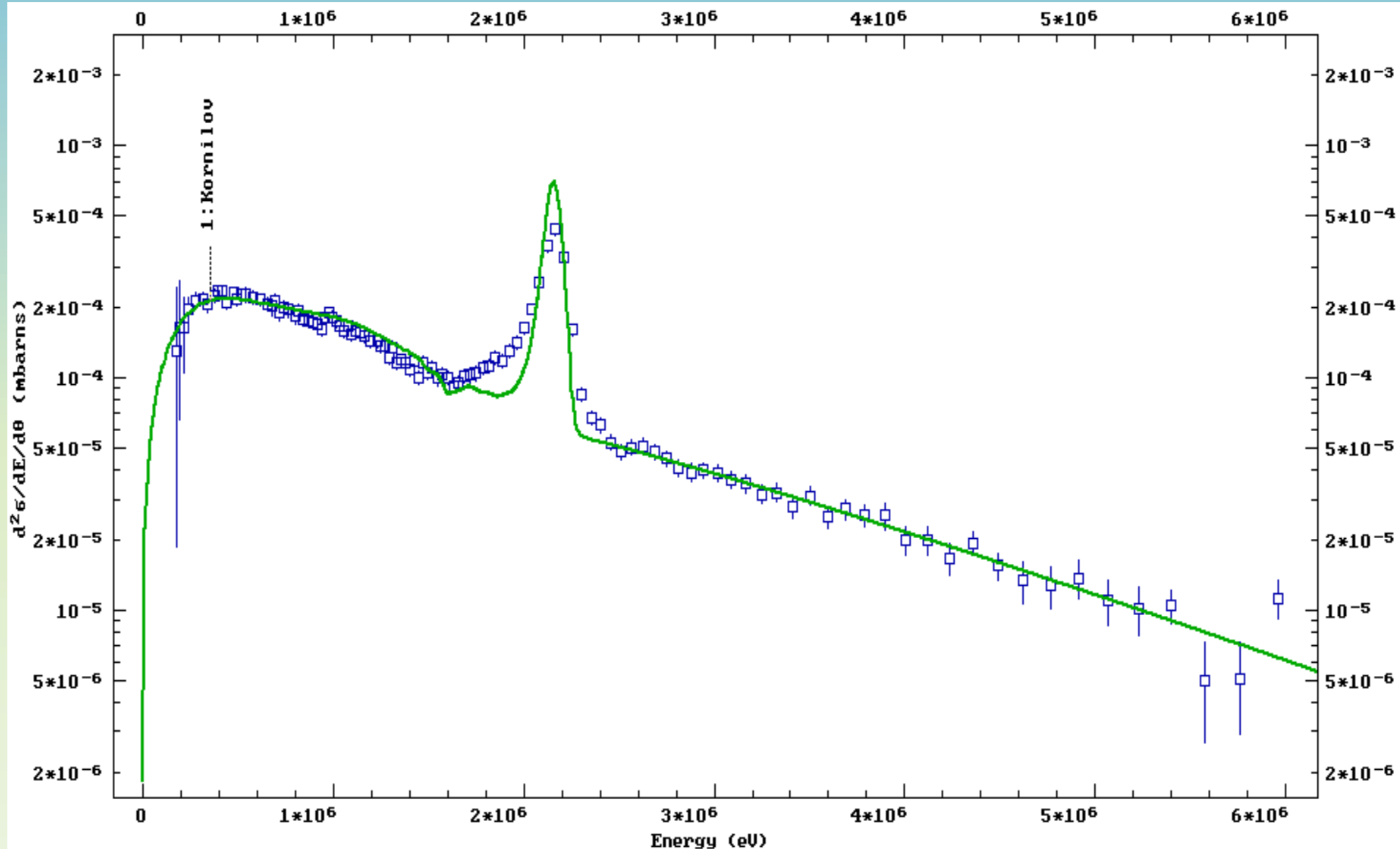
$^{235}\text{U}+n$, DDX yield, $E_n=1.19$ MeV, 120 deg



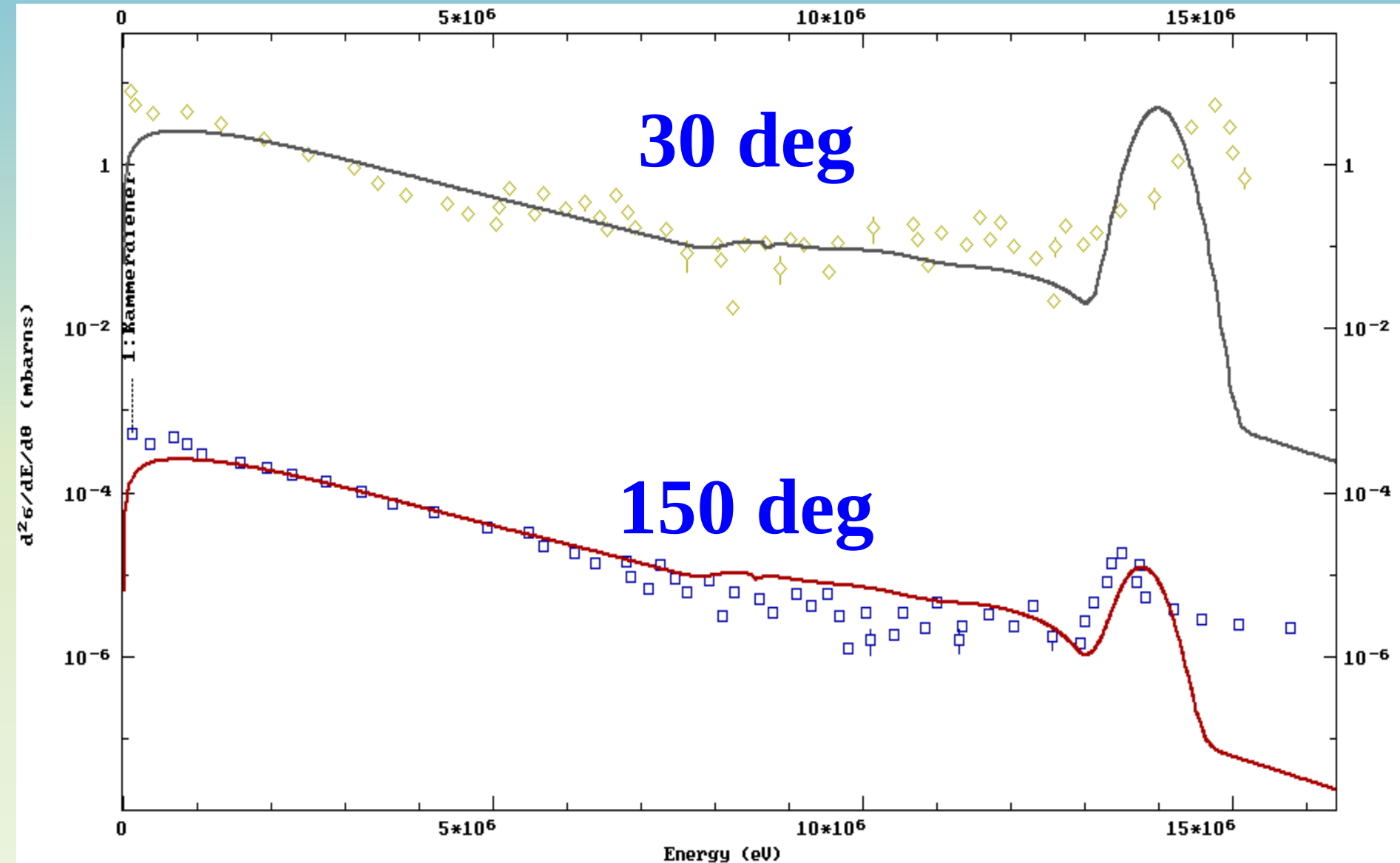
$^{235}\text{U}+n$, DDX yield, $E_n=1.79$ MeV, 120 deg



$^{235}\text{U}+n$, DDX yield, $E_n=2.19$ MeV, 120 deg



$^{235}\text{U}+n$, DDX yield, $E_n=14\text{ MeV}$



Conclusions: ^{235}U fast region

Better physics → improved performance

- ❑ New fast evaluation with **3H fission barriers** leading to elastic/inelastic and (n,xn) **consistent** changes
- ❑ PFNS thermal from IAEA CRP ($E_{av}=2.00(1)$ MeV)
- ❑ PFNS fast adopted from Talou-Rising
- ❑ Fission in fast region from **2006 Neutron Standards**
(to be updated based on new GMA Standard fit)
- ❑ Capture in fast region from **ENDF/B-VII.1**
(update based on Jandel/RPI data ??)
- ❑ Good agreement between B/VII.1 SACS and new eval.

