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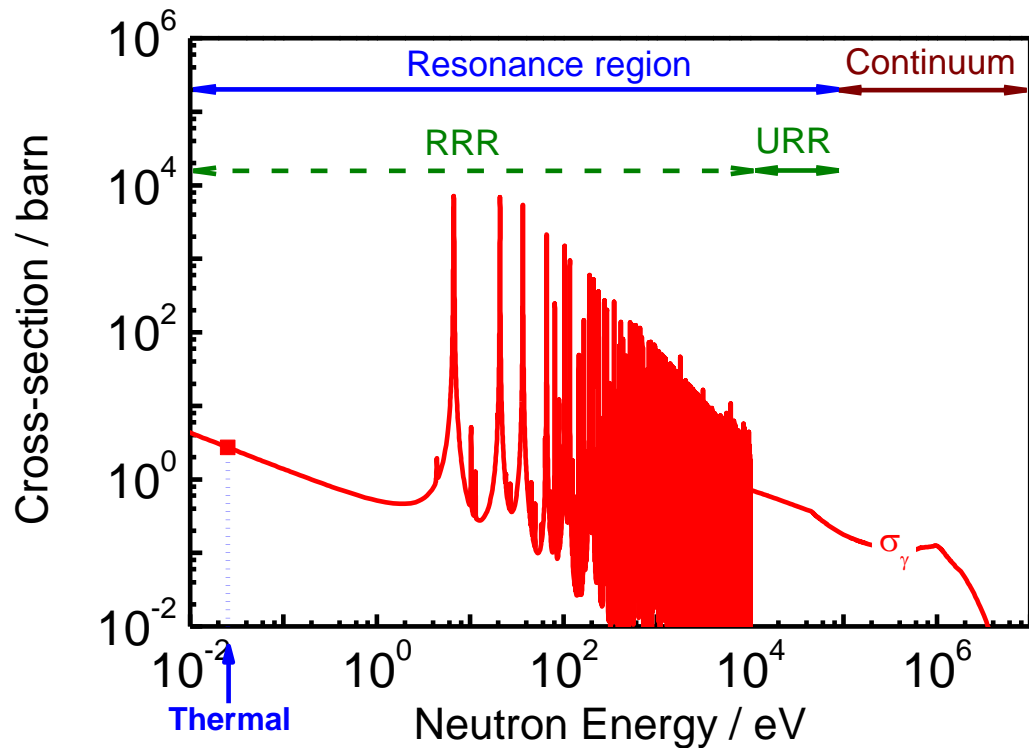
*Serving society
Stimulating innovation
Supporting legislation*

Derivation of resonance
parameters from time-of-
flight measurements

Stefan Kopecky

www.ec.europa.eu/jrc

Neutron induced reaction cross sections

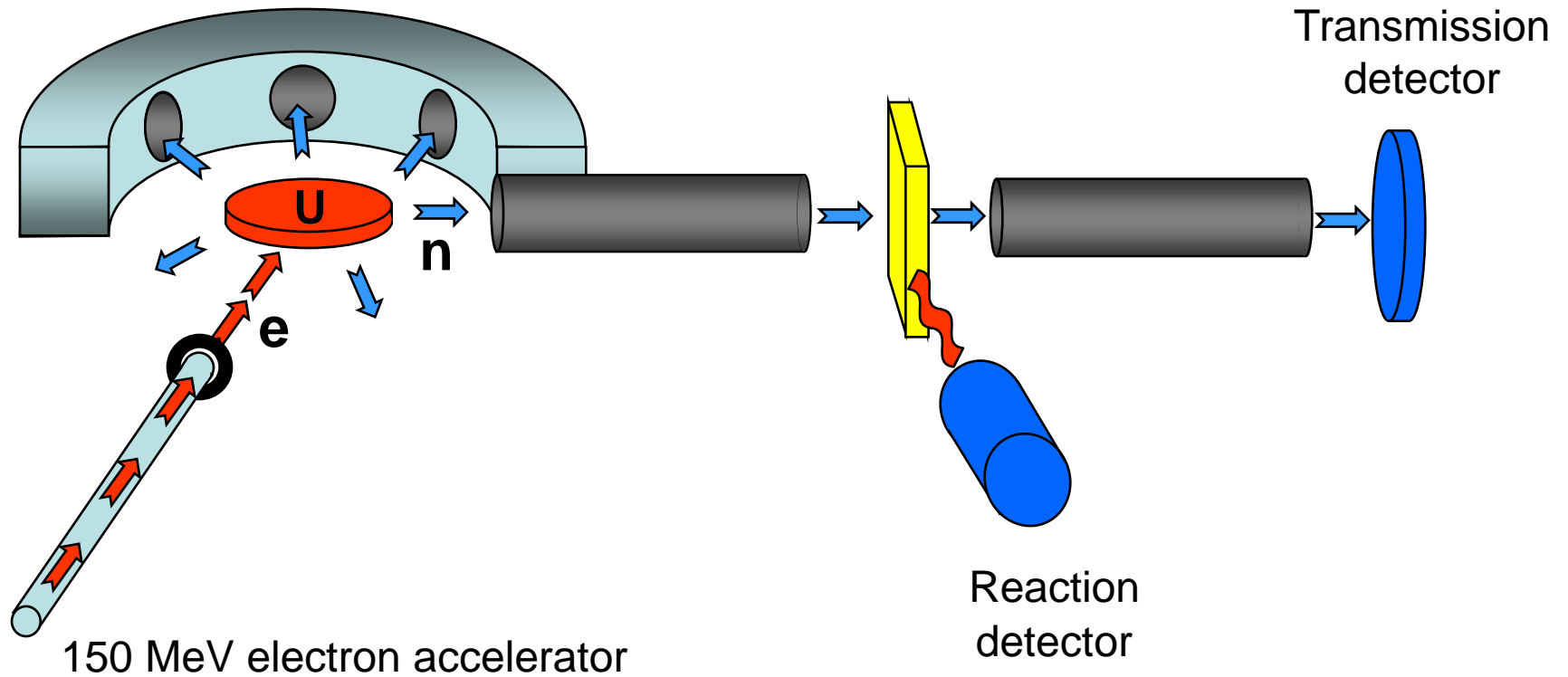


Cross sections cannot be predicted by nuclear theory from first principles

⇒ parameterized by nuclear reaction models

⇒ different models in different energy regions

Time-of-flight measurement



Cross section measurements : transmission + reaction

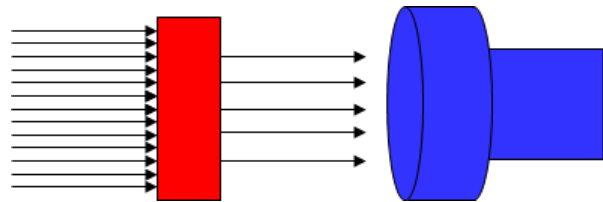
Transmission

$$T = e^{-n \sigma_{\text{tot}}}$$

T : transmission

Fraction of the neutron beam traversing the sample without any interaction

$$T_{\text{exp}} = \frac{C_{\text{in}}}{C_{\text{out}}}$$



Reaction

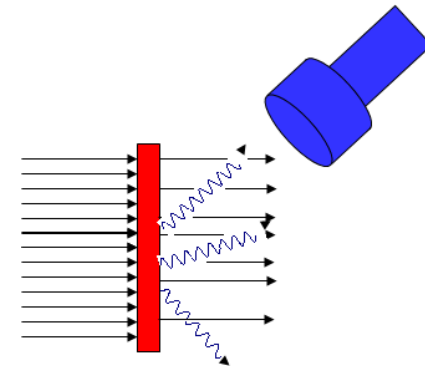
$$Y_r \cong (1 - e^{-n \sigma_{\text{tot}}}) \frac{\sigma_r}{\sigma_{\text{tot}}} + \dots$$

Y_r : reaction yield

Fraction of the neutron beam creating a (n,r) reaction in the sample

Only for thin samples : $Y_r \approx n \sigma_r$

e.g. (n, γ)



Cross section measurements : transmission + reaction

Transmission

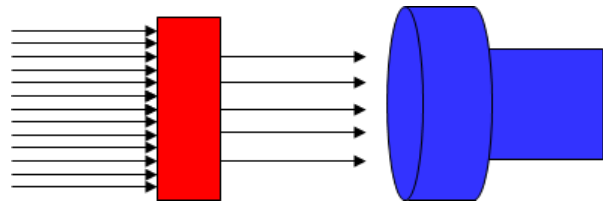
$$T = e^{-n \sigma_{\text{tot}}}$$

T : transmission

Fraction of the neutron beam traversing the sample without any interaction

$$T_{\text{exp}} = \frac{C_{\text{in}}}{C_{\text{out}}}$$

Absolute measurement



Reaction

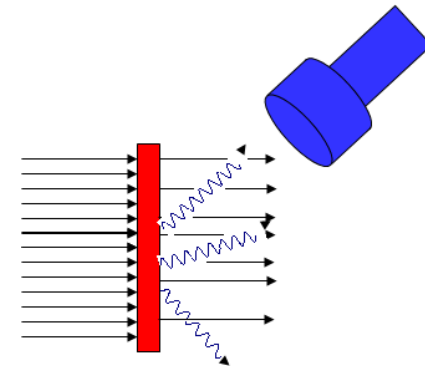
$$Y_r \cong (1 - e^{-n \sigma_{\text{tot}}}) \frac{\sigma_r}{\sigma_{\text{tot}}} + \dots$$

Y_r : reaction yield

Fraction of the neutron beam creating a (n,r) reaction in the sample

$$Y_{r,\text{exp}} = \frac{C_r}{\varepsilon_r \Omega P_r A_r \varphi} = K_r \frac{C_r}{\varphi}$$

e.g. (n, γ)



Experimental observables (resonance region)

$$T_{\text{exp}} = K_T \frac{C_{\text{in}} - B_{\text{in}}}{C_{\text{out}} - B_{\text{out}}}$$

$$\frac{u_T}{T_{\text{exp}}} \approx 0.3\%$$

$$Y_{\text{exp},\gamma} = K_\gamma \frac{C_{\text{in}} - B_{\text{in}}}{C_\varphi - B_\varphi} Y_\varphi$$

$$\frac{u_{Y_\gamma}}{Y_{\text{exp},\gamma}} \approx 2.0\% \quad (\text{without fission})$$

$$Y_{\text{exp},f} = K_f \frac{C_{\text{in}} - B_{\text{in}}}{C_\varphi - B_\varphi} Y_\varphi$$

$$\frac{u_{Y_f}}{Y_{\text{exp},f}} \approx 2.0\%$$

Methodologies to determine $(Z_{\text{exp}}, V_{Z_{\text{exp}}})$ and report them in EXFOR are well established

Nuclear Data Sheets 113 (2012) 3054 - 3100

Becker et al., "AGS-concept", J. of Instrumentation 7 (2012) P11002

⇒ EXFOR Consultants' Meeting, 8 to 10 October 2013, IAEA, INDC(NDS)-0647

Reaction model parameters + covariance (θ, V_θ)



(θ, V_θ) determined by :

- Experimental data and parameters $(Z_{\text{exp}}, V_Z, \kappa, V_\kappa)$
- Model H_M : reaction model (θ) + experiment (κ)
 - Nuclear reaction model $F_M(\theta)$
 - Model to account for experimental parameters κ (i.e. resonance region)
- **Methods or procedures to estimate model parameters (θ, V_θ) from $(Z_{\text{exp}}, V_Z, \kappa, V_\kappa)$**

Reaction model parameters + covariance (θ, V_θ)



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- **Methods or procedures to estimate model parameters (θ, V_θ) from $(Z_{\text{exp}}, V_Z, \kappa, V_\kappa)$**

Model for experimental parameters

$$T_{\text{exp}} = \int R(t, E) T(E) dE = \int R(t, E) e^{-n\sigma(E)} dE$$

Experimental broadening

$$\frac{\ln(T_{\text{exp}})}{n} \neq \int R(t, E) \sigma(E) dE$$

Sample inhomogeneity

$$Y_{\text{exp}} = K_{\text{exp}} \cdot \int R(t, E) Y_{\text{Mod}}(E) dE$$

$$Y_{\text{Mod}}(E) = \varepsilon_c Y_c(E) + \varepsilon_{ns}(E) Y_s$$

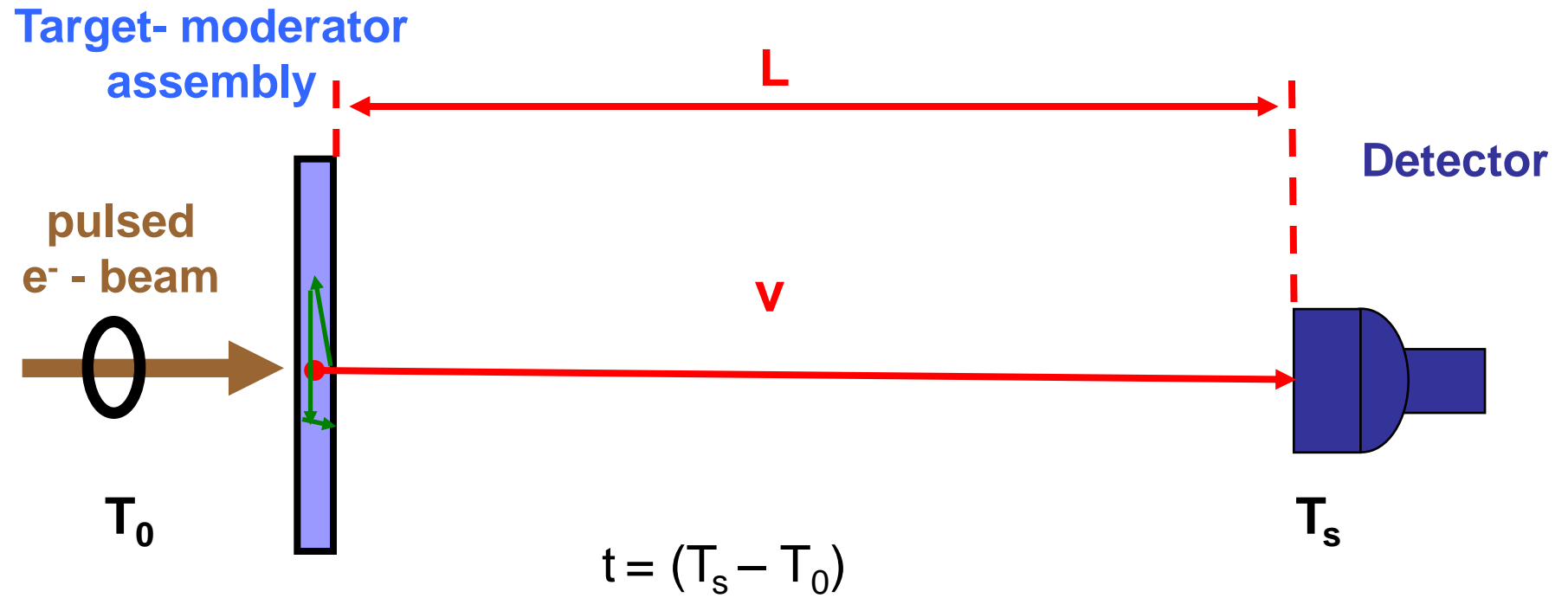
Multiple Scattering

$$Y_c(E) = F_0 Y_0(E) + F_m Y_m(E)$$

Gamma attenuation

Neutron sensitivity

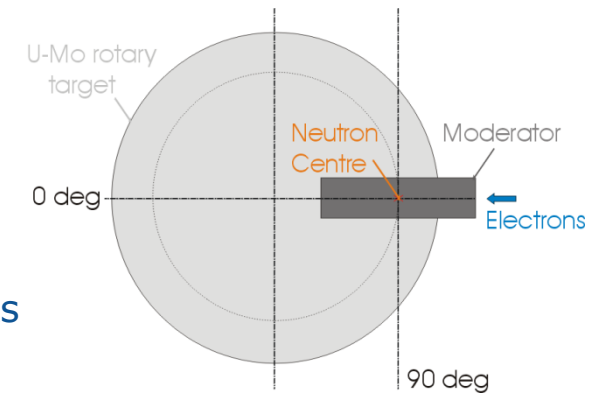
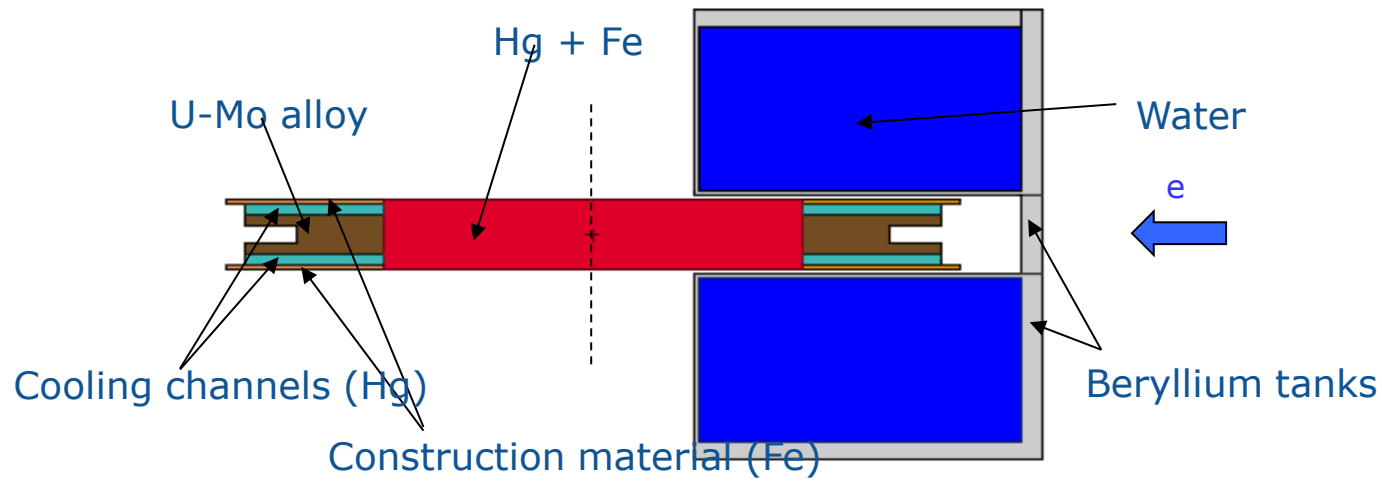
TOF -> Energy



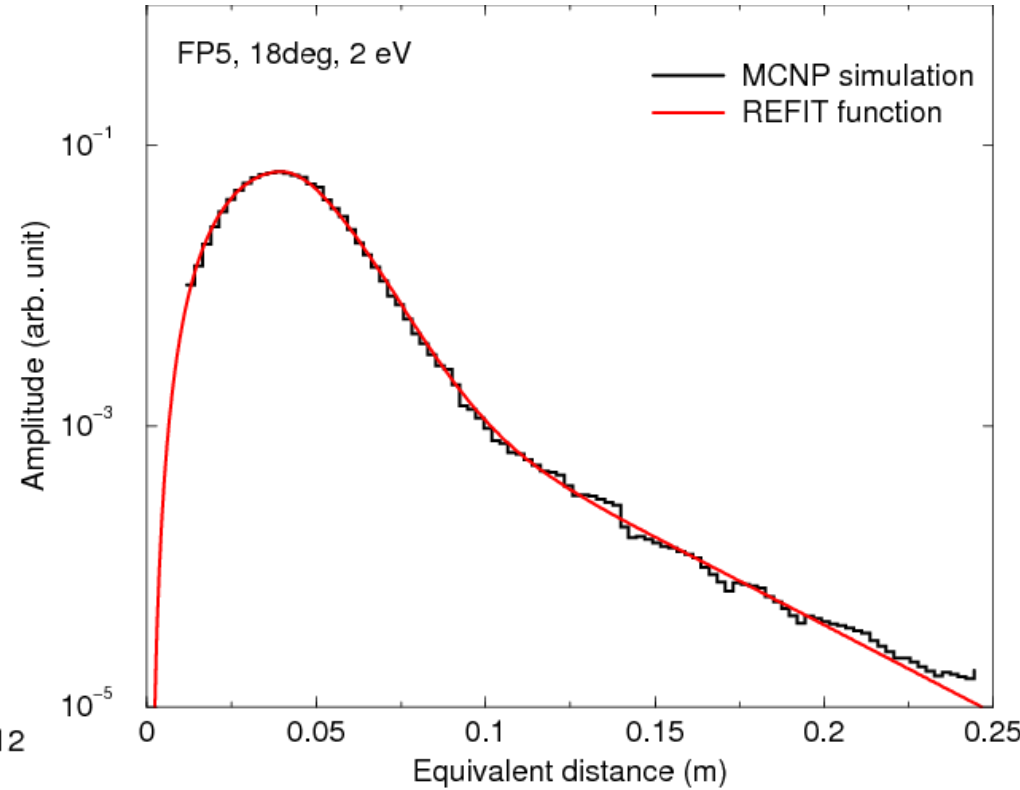
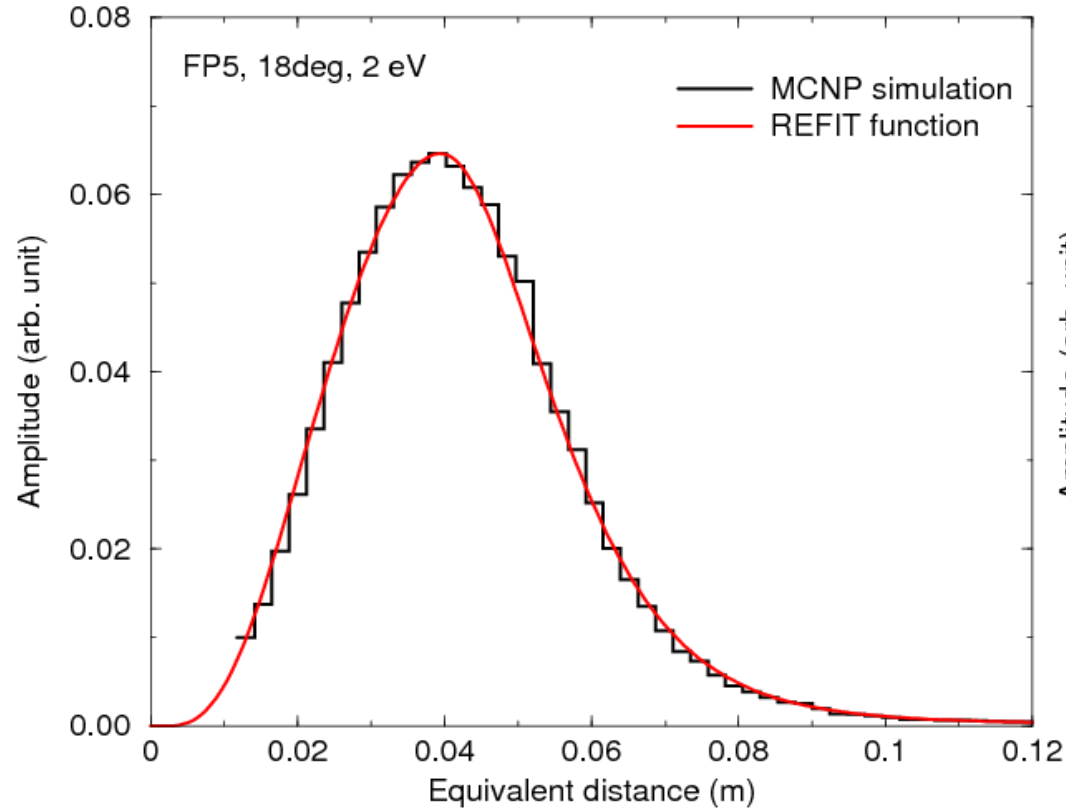
$$v = \frac{L}{t}$$

$$\Rightarrow E = \frac{1}{2}mv^2$$

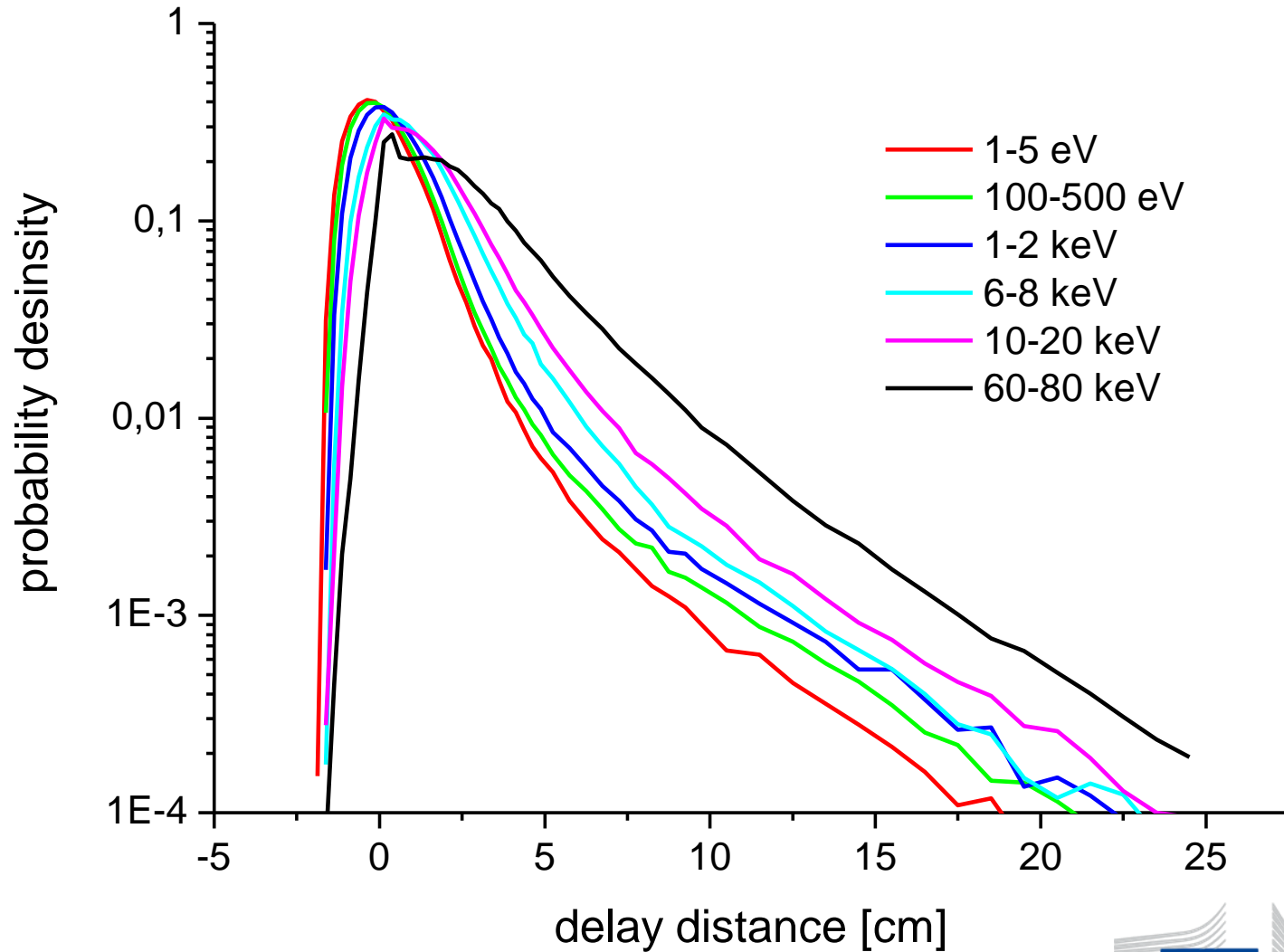
GELINA Target-moderator assembly



GELINA Response function

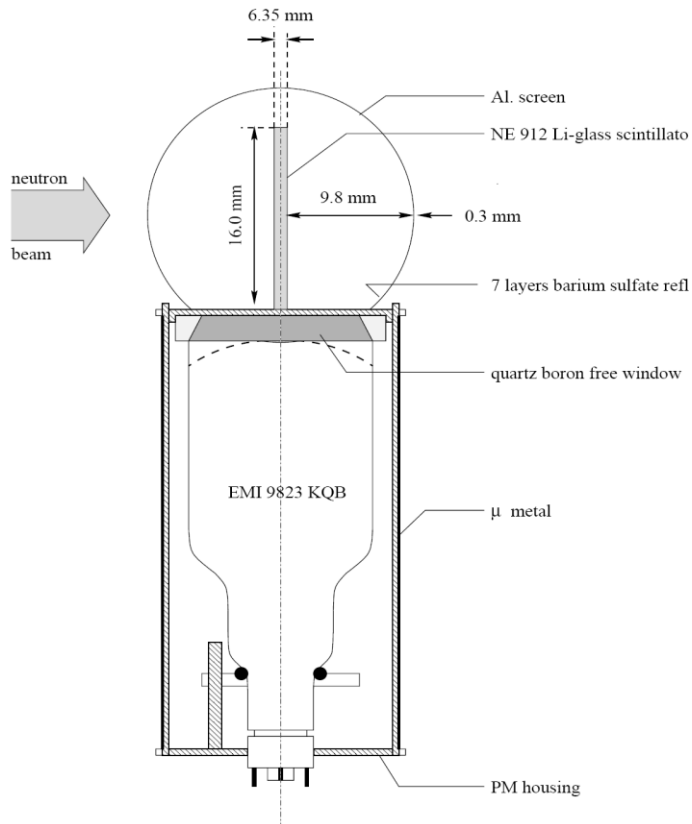


GELINA Response function

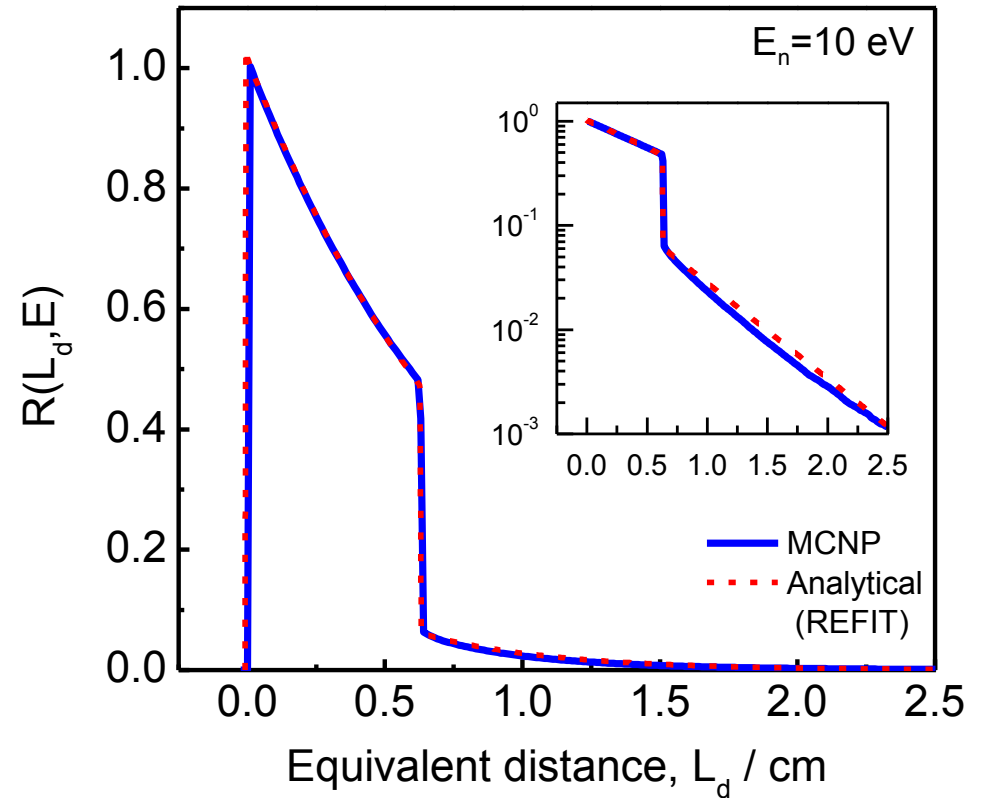


Detector Response

${}^6\text{Li}(n,t)\alpha$ Scintillator + Photomultiplier



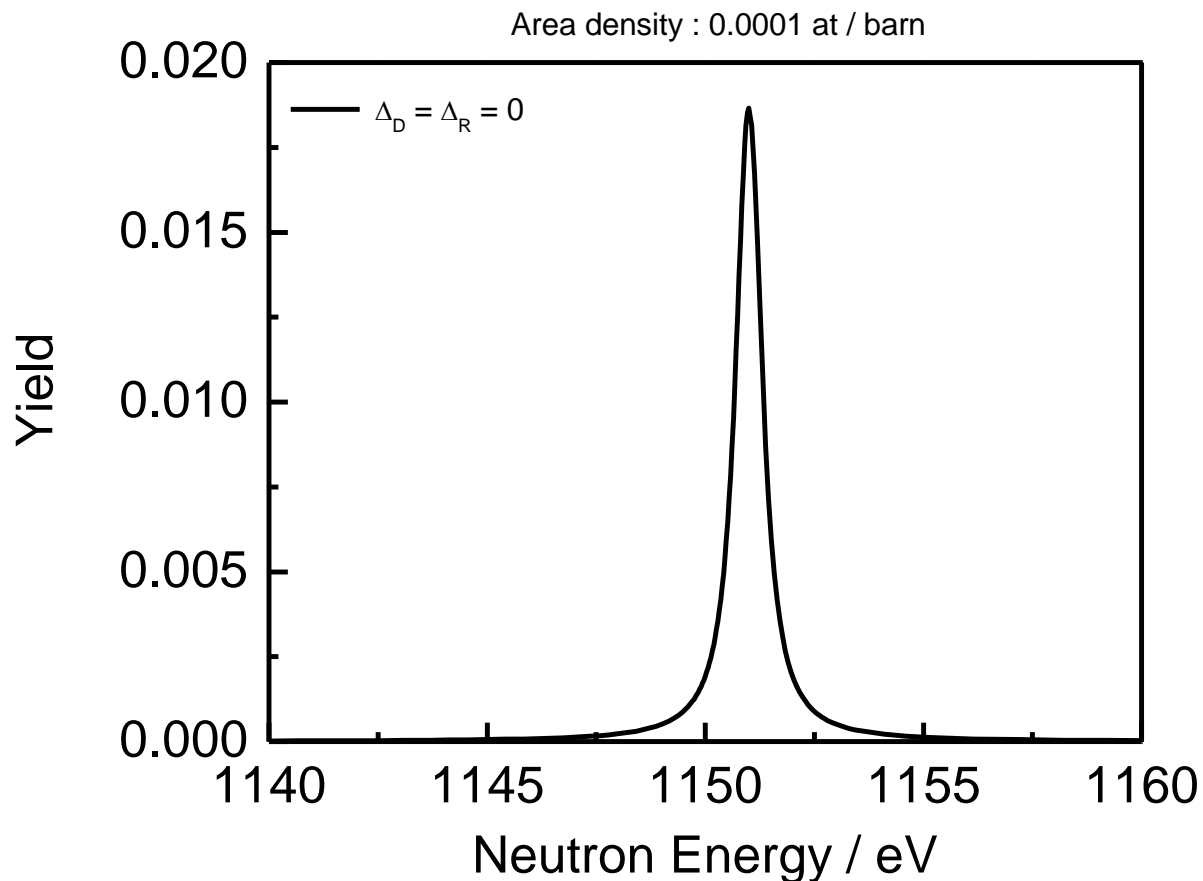
$$R(t_d, E_n)$$



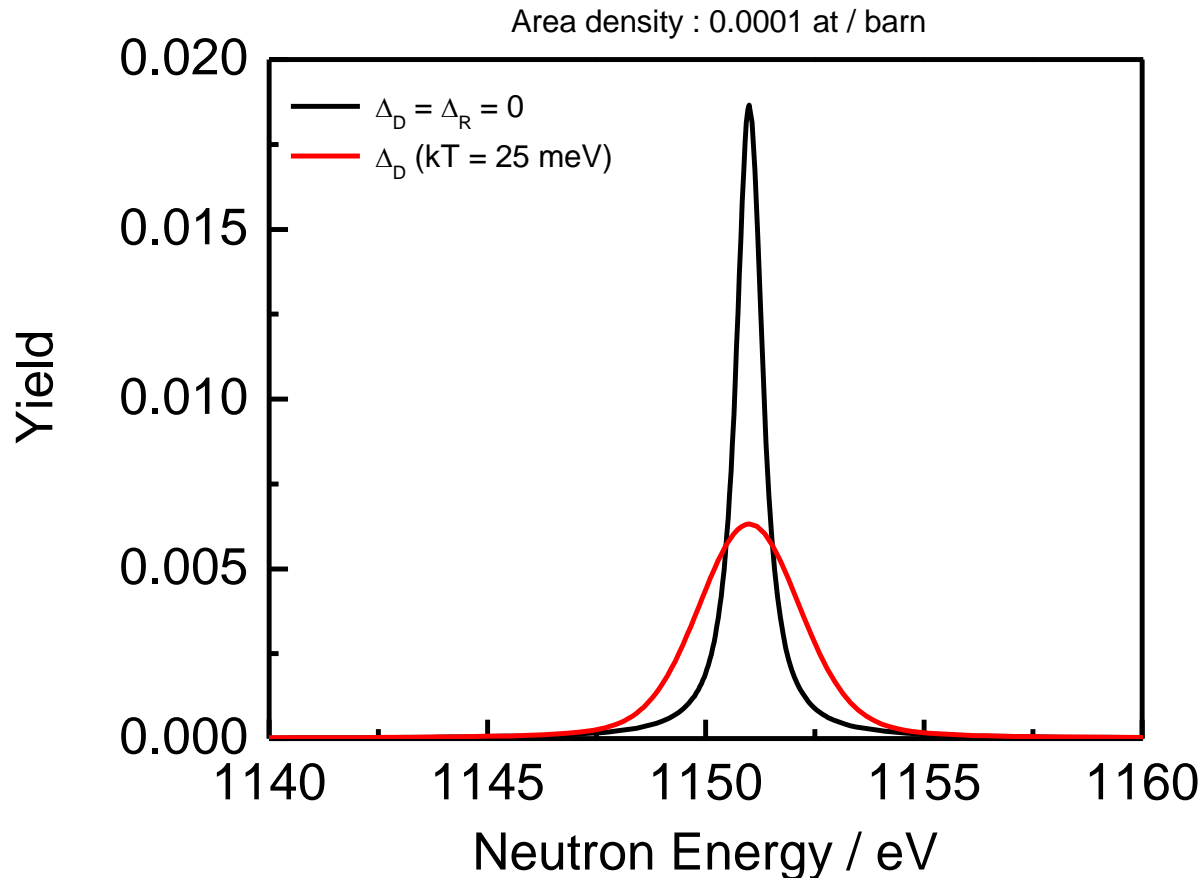
Theoretical yield

^{56}Fe 1.15 keV resonance

$$Y_\gamma \cong \frac{\sigma_\gamma}{\sigma_{\text{tot}}} (1 - e^{-n\sigma_{\text{tot}}}) + \dots$$



^{65}Fe 1.15 keV resonance



$$Y_\gamma \cong \frac{\bar{\sigma}_\gamma}{\bar{\sigma}_{\text{tot}}} (1 - e^{-n\bar{\sigma}_{\text{tot}}}) + \dots$$

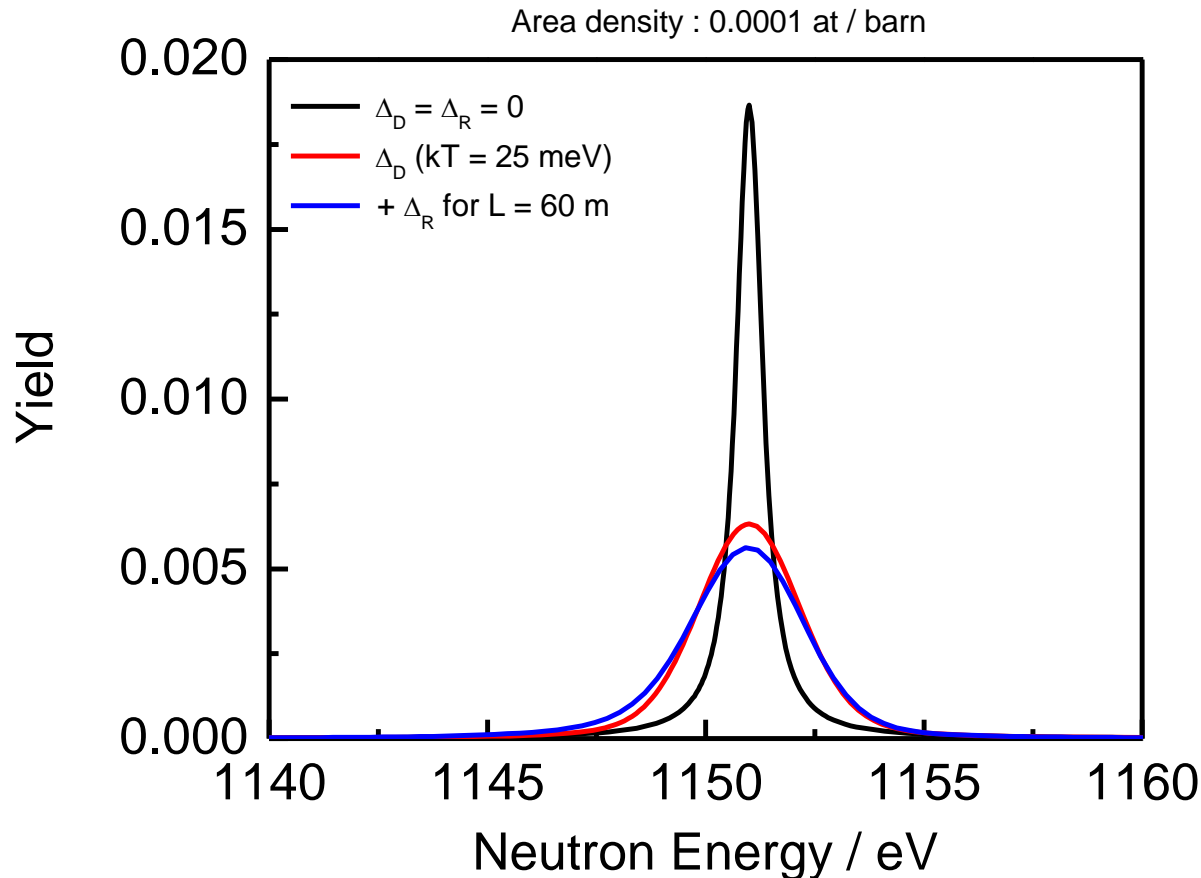
$$\bar{\sigma}(E) = \int dE' S(E') \sigma(E - E')$$

$$\Delta_D = \sqrt{\frac{4 E k_B T}{m_X / m_n}}$$

$$\text{FWHM} = 2\sqrt{\ln 2} \Delta_D$$

+Doppler + Response

^{65}Fe 1.15 keV resonance



$$Y_\gamma \cong \frac{\bar{\sigma}_\gamma}{\bar{\sigma}_{\text{tot}}} (1 - e^{-n\bar{\sigma}_{\text{tot}}}) + \dots$$

$$\bar{\sigma}(E) = \int dE' S(E') \sigma(E - E')$$

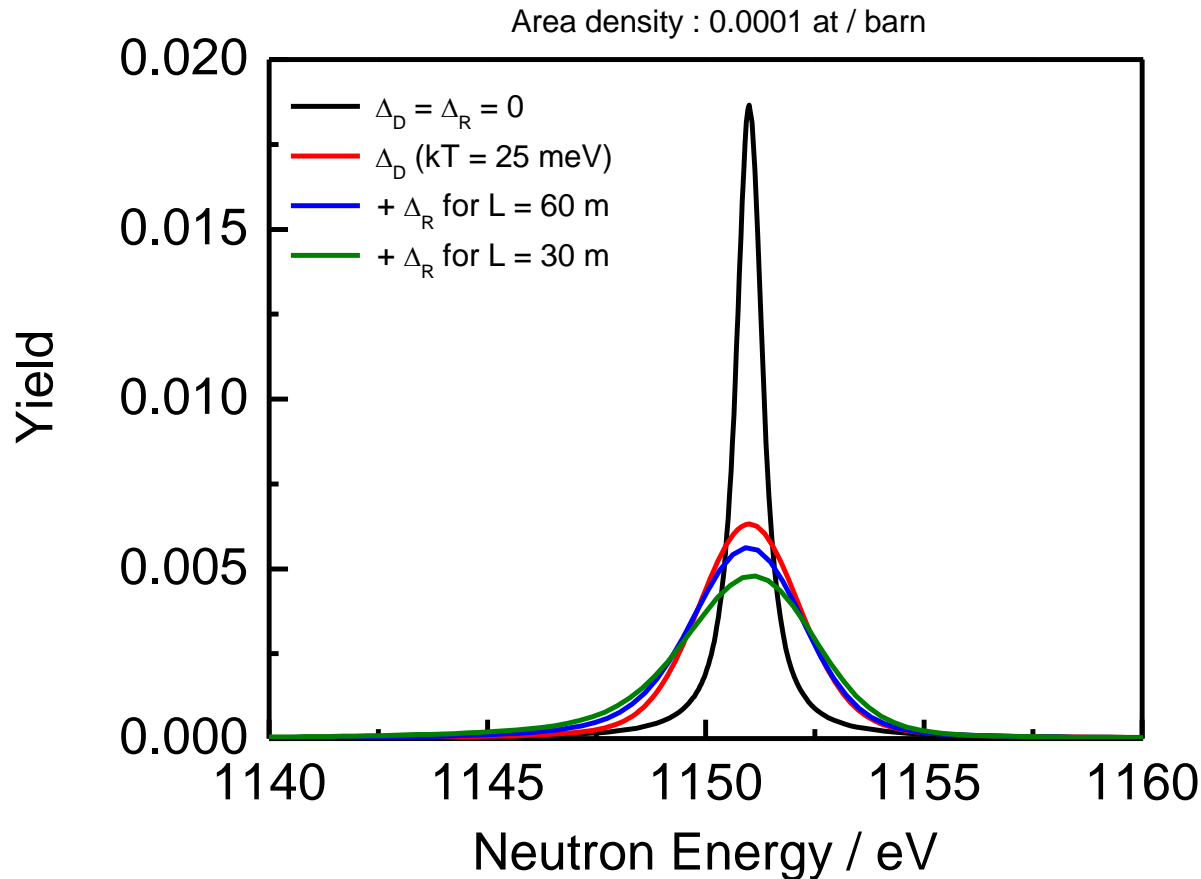
$$Y_{\text{exp}} = \frac{\int R(t, E) Y_\gamma(E) dE}{\int R(t, E) dE}$$

$L = 60 \text{ m}$

$$\frac{\Delta E}{E} = 2 \sqrt{\left(\frac{\Delta L}{L}\right)^2 + \left(\frac{\Delta t}{t}\right)^2}$$

+Doppler + Response

⁶⁵Fe 1.15 keV resonance



$$Y_\gamma \cong \frac{\bar{\sigma}_\gamma}{\bar{\sigma}_{\text{tot}}} (1 - e^{-n\bar{\sigma}_{\text{tot}}}) + \dots$$

$$\bar{\sigma}(E) = \int dE' S(E') \sigma(E - E')$$

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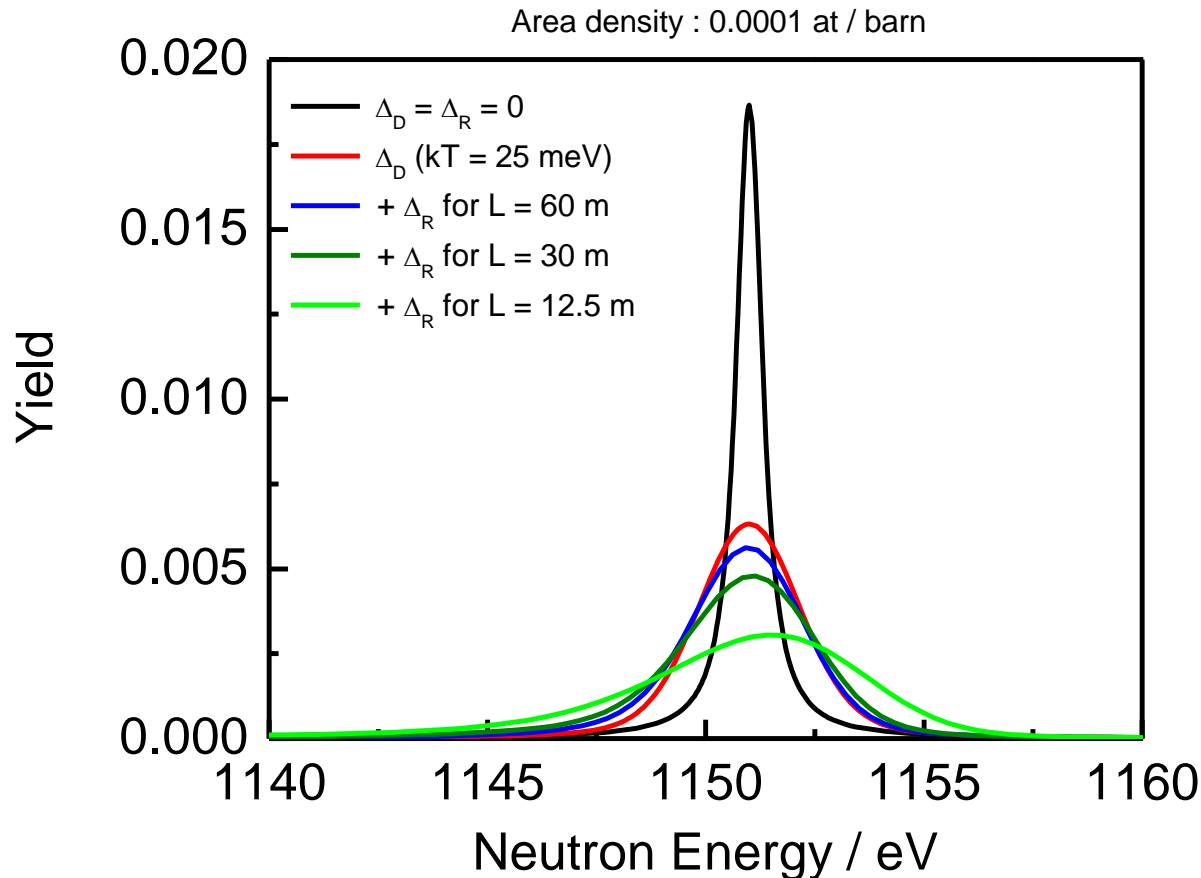
L = 60 m

L = 30 m

$$\frac{\Delta E}{E} = 2 \sqrt{\left(\frac{\Delta L}{L}\right)^2 + \left(\frac{\Delta t}{t}\right)^2}$$

+Doppler + Response

^{65}Fe 1.15 keV resonance



$$Y_\gamma \cong \frac{\bar{\sigma}_\gamma}{\bar{\sigma}_{\text{tot}}} (1 - e^{-n\bar{\sigma}_{\text{tot}}}) + \dots$$

$$\bar{\sigma}(E) = \int dE' S(E') \sigma(E - E')$$

$$Y_{\text{exp}} = \frac{\int R(t, E) Y_\gamma(E) dE}{\int R(t, E) dE}$$

L = 60 m

L = 30 m

L = 12.5 m

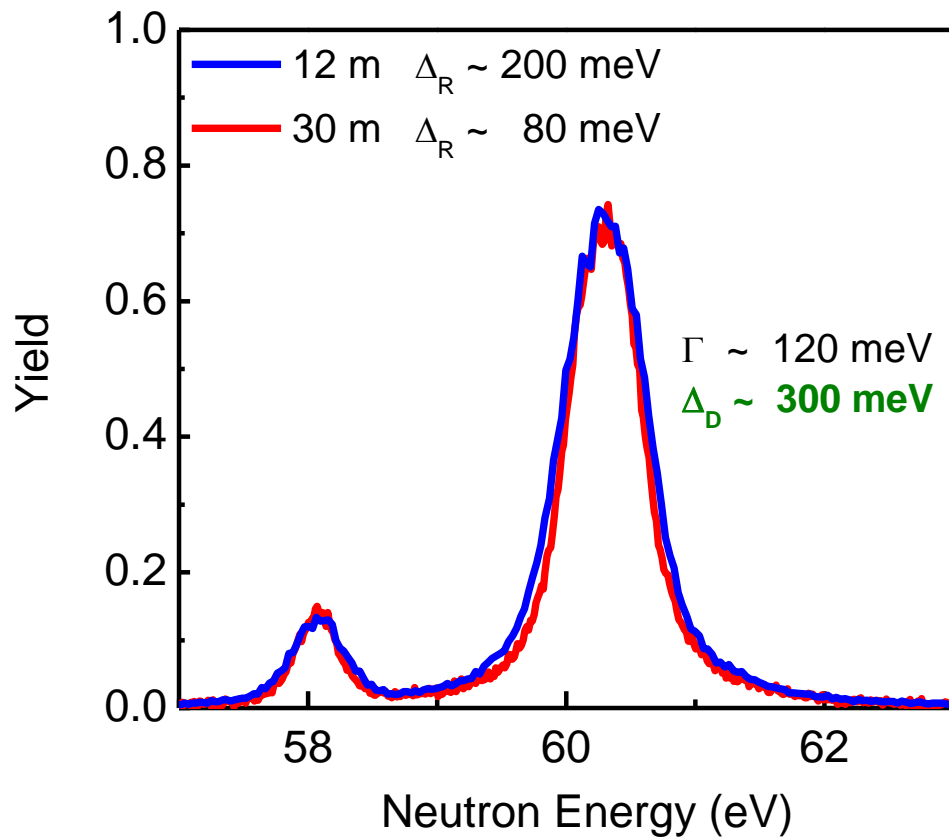
$$\frac{\Delta E}{E} = 2 \sqrt{\left(\frac{\Delta L}{L}\right)^2 + \left(\frac{\Delta t}{t}\right)^2}$$

$^{197}\text{Au}(n,\gamma)$ at L=12m and 30 m

$$\frac{\Delta E}{E} = 2 \sqrt{\left(\frac{\Delta L}{L}\right)^2 + \left(\frac{\Delta t}{t}\right)^2}$$

$$\Delta_D = \sqrt{\frac{4 E k_B T}{m_X / m_n}}$$

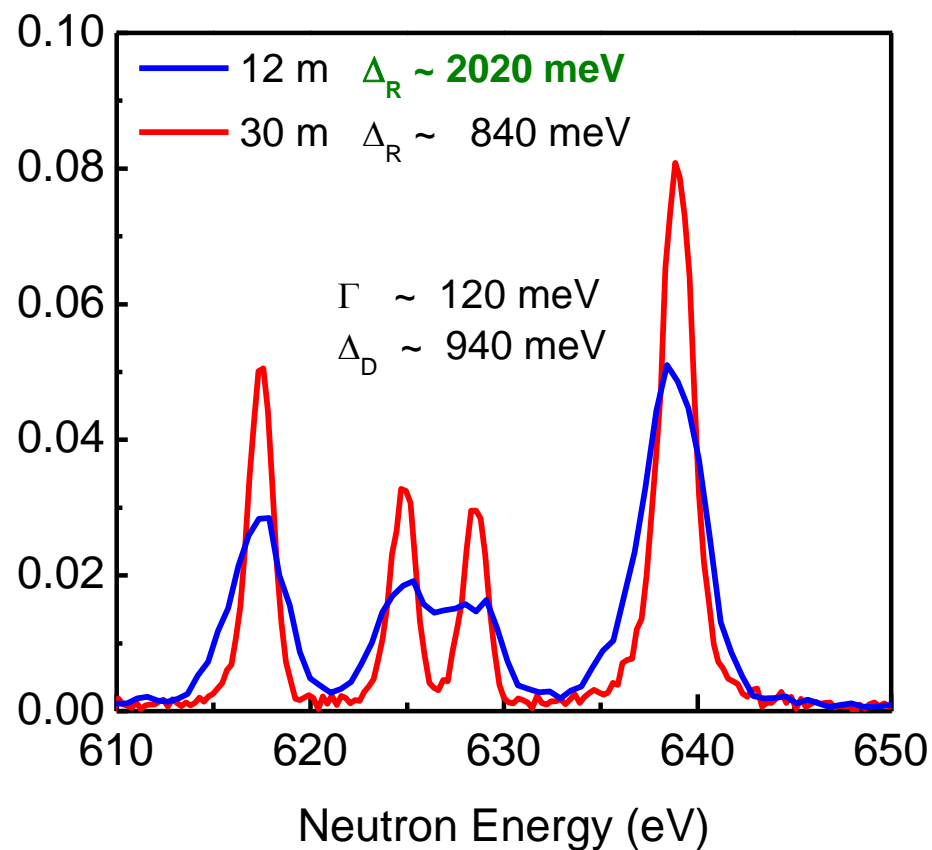
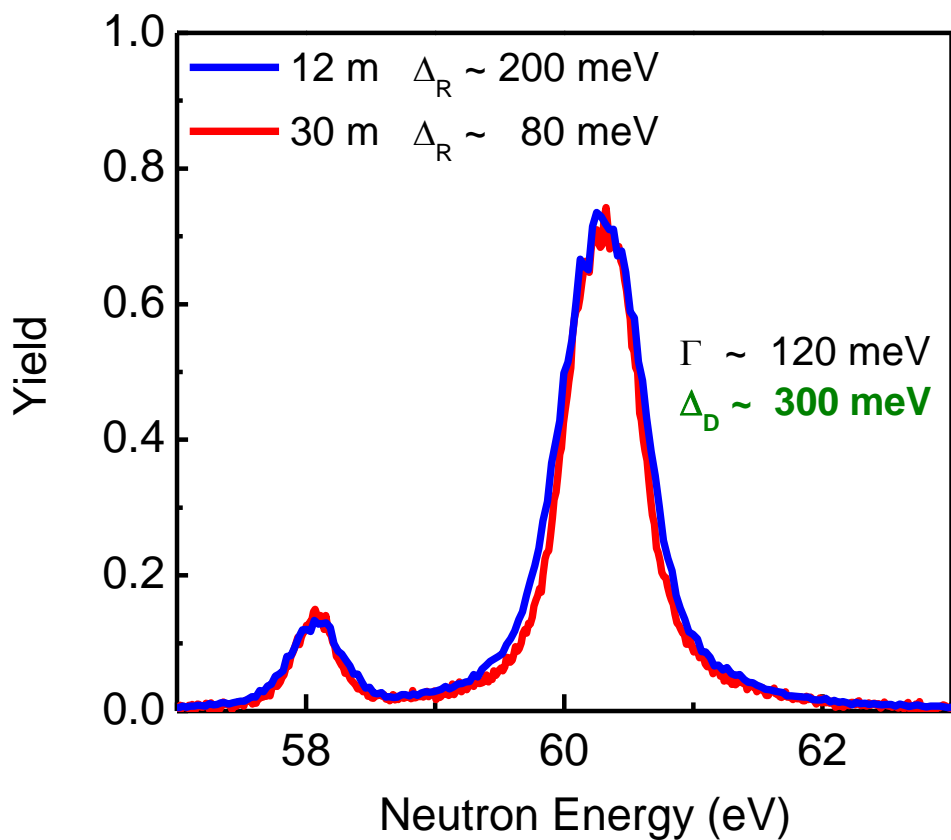
$$\text{FWHM} = 2 \sqrt{\ln 2} \Delta_D$$



$^{197}\text{Au}(n,\gamma)$ at L=12m and 30 m

$$\frac{\Delta E}{E} = 2 \sqrt{\left(\frac{\Delta L}{L}\right)^2 + \left(\frac{\Delta t}{t}\right)^2}$$

$$\Delta_D = \sqrt{\frac{4 E k_B T}{m_X / m_n}} \quad \text{FWHM} = 2 \sqrt{\ln 2} \Delta_D$$



$^{56}\text{Fe}(n,\gamma)$ at L= 30 m

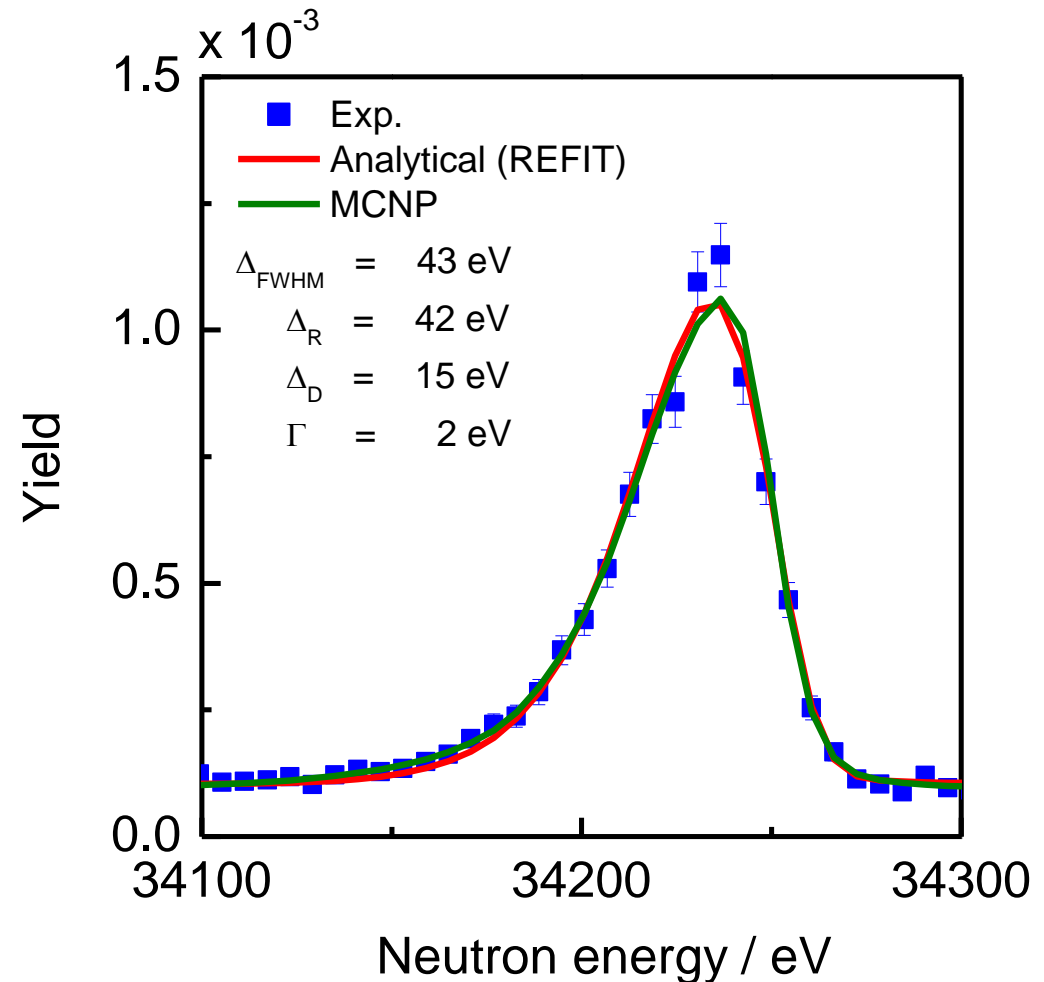
$$\Delta_{\text{FWHM}} = \sqrt{\Gamma^2 + \Delta_{\text{D}}^2 + \Delta_{\text{R}}^2}$$

dominated by Δ_{R} or Δ_{D}

with

- Δ_{R} Experimental resolution
- Δ_{D} Doppler broadening
- Γ Total resonance width

⇒ effective experimental observable is resonance area



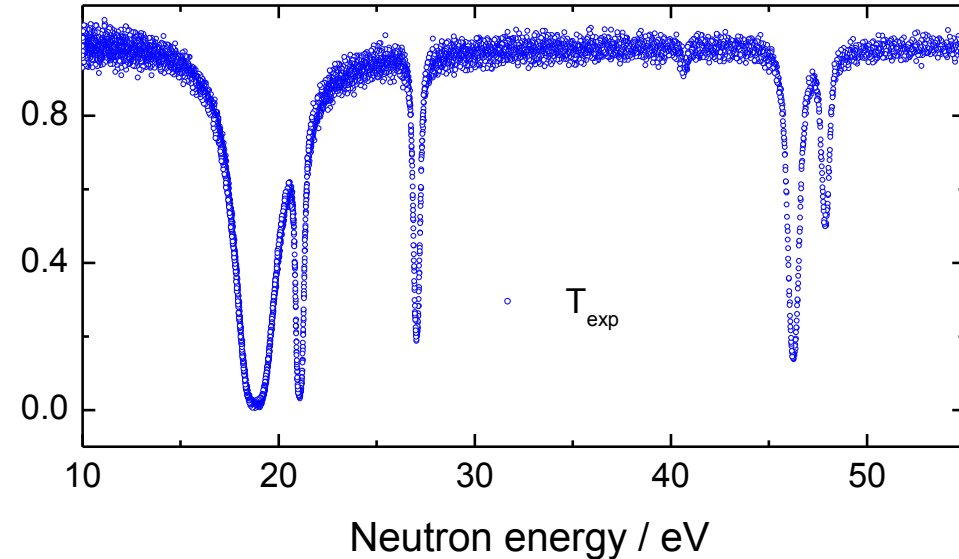
Sample inhomogeneity

^{nat}W -powder mixed with ^{nat}S -powder
(80 cm diameter, 14 g ^{nat}W , 3.5 g ^{nat}S)

Declared : $n_{\text{W}} = (1.084 \pm 0.014) 10^{-3}$ at/b

Heterogeneous sample:

$$\bar{T} = \int T(n')p(n')dn' = \int e^{-n' \sigma_{\text{tot}}} p(n')dn'$$



Transmission measurements

- a 25 m station of GELINA

- ^6Li detector

Sample inhomogeneity

^{nat}W-powder mixed with ^{nat}S-powder
(80 cm diameter, 14 g ^{nat}W, 3.5 g ^{nat}S)

Declared : $n_W = (1.084 \pm 0.014) 10^{-3}$ at/b

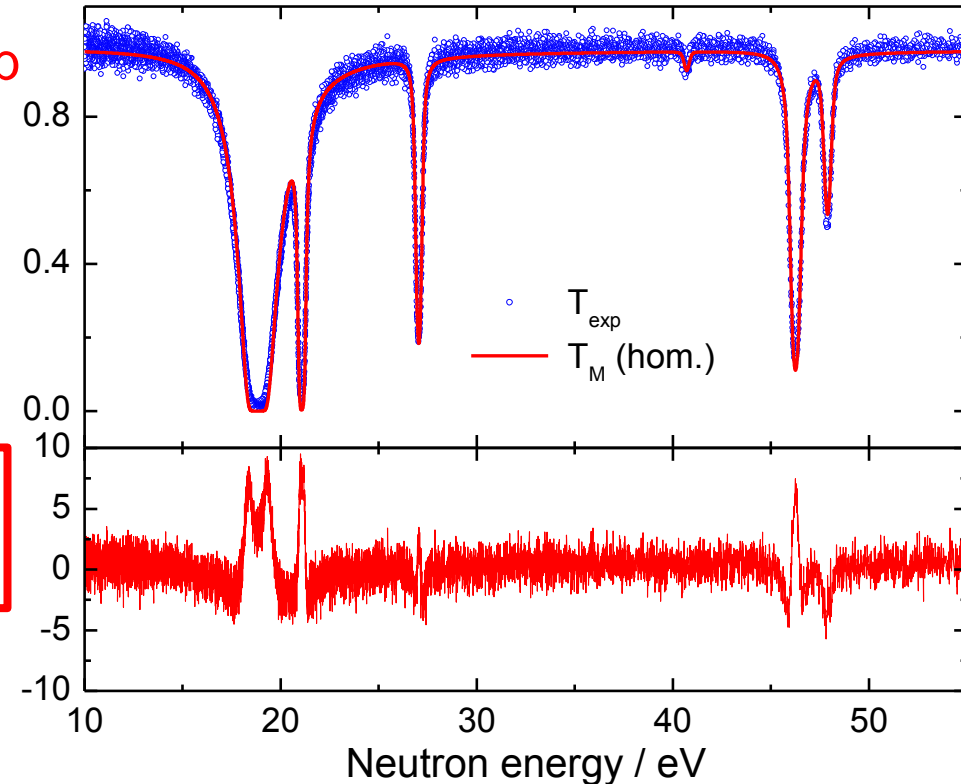
T_M (hom.) : $n_W = (0.939 \pm 0.003) 10^{-3}$ at/b

Heterogeneous sample:

$$\bar{T} = \int T(n') p(n') dn' = \int e^{-n' \sigma_{\text{tot}}} p(n') dn'$$

\neq

$$T(\bar{n}) = e^{-\bar{n} \sigma_{\text{tot}}}$$



T_M : REFIT + JEFF 3.2

Sample inhomogeneity

^{nat}W-powder mixed with ^{nat}S-powder
(80 cm diameter, 14 g ^{nat}W, 3.5 g ^{nat}S)

Declared : $n_W = (1.084 \pm 0.014) 10^{-3}$ at/b

T_M (hom.) : $n_W = (0.939 \pm 0.003) 10^{-3}$ at/b

T_M (inhom.) : $n_W = (1.096 \pm 0.003) 10^{-3}$ at/b

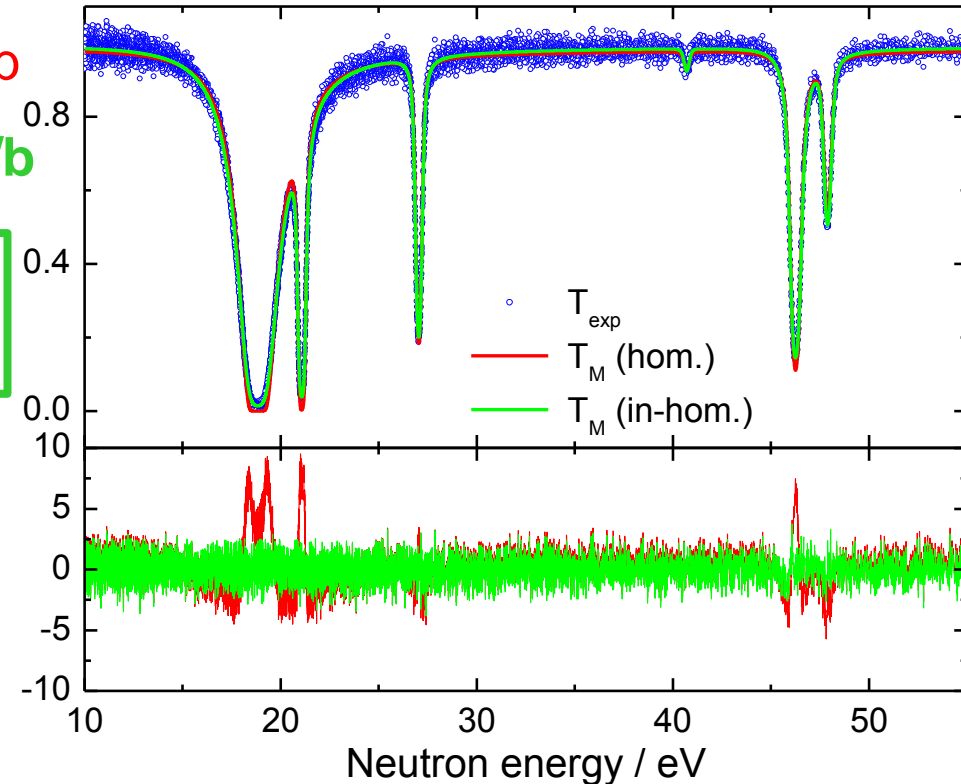
$$\bar{T} = \int T(n') p(n') dn' = \int e^{-n' \sigma_{\text{tot}}} p(n') dn'$$

LP Model

Levermore, Pomraning et al., J. Math. Phys. 27, 2526, 1986

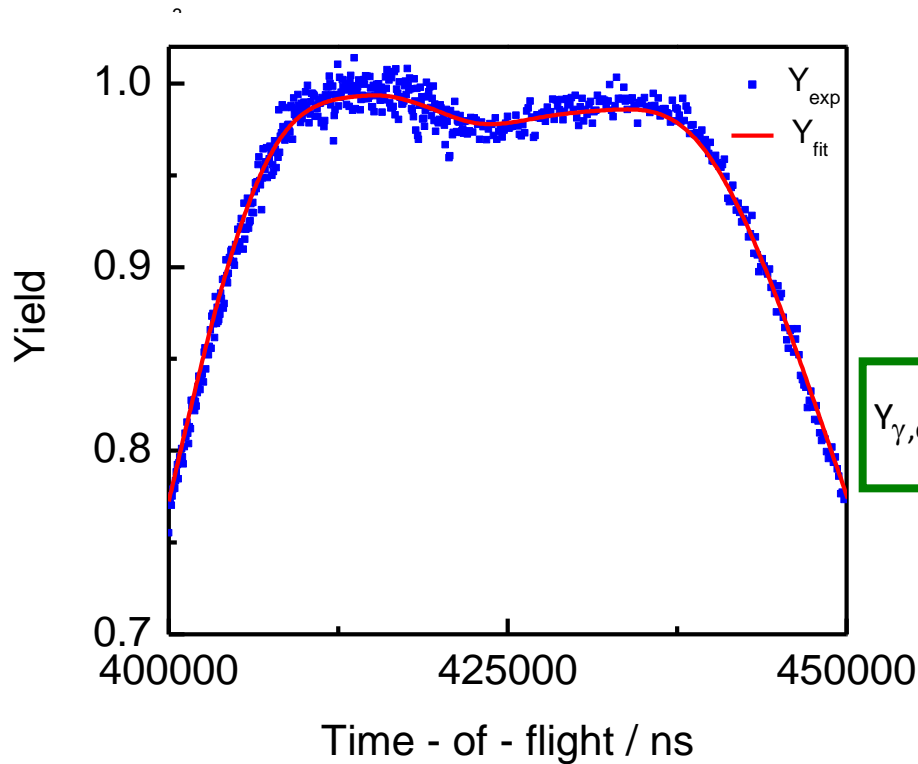
Implemented in REFIT

Becker et al., Eur. Phys. J. Plus 129 (2014) 58 - 9

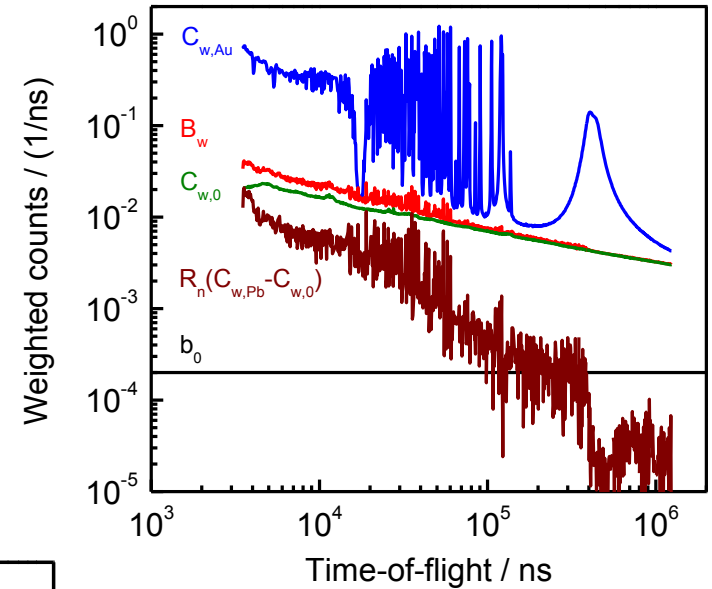
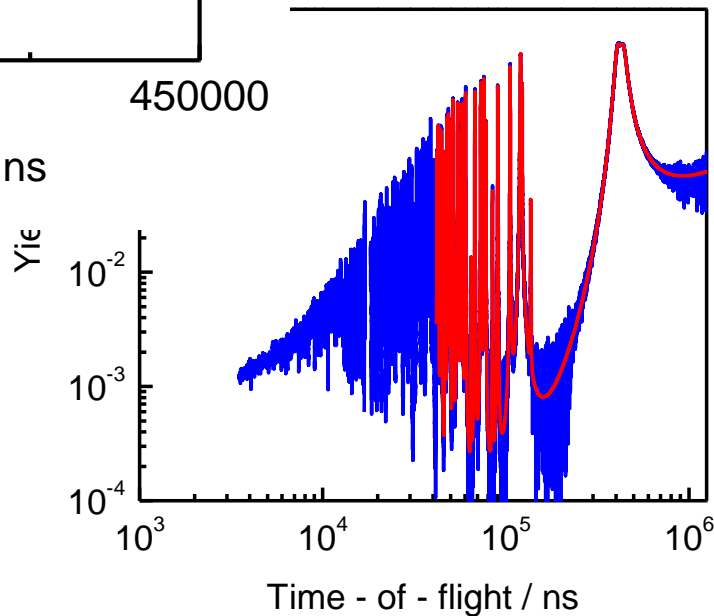


T_M : REFIT + JEFF 3.2

Normalization at saturated resonances



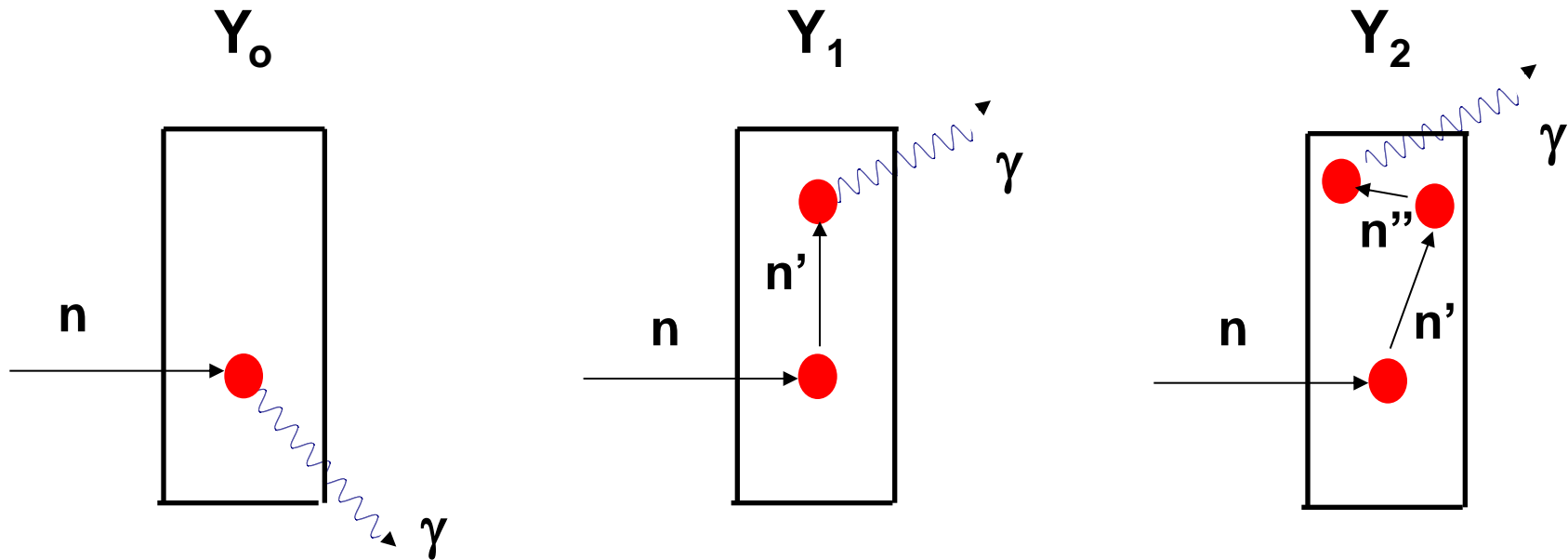
$$Y_{\gamma, \text{exp}} = N_C \frac{C_w - B_w}{C_\varphi - B_\varphi} Y_\varphi$$



Saturated resonance at 4.9 eV
 with $\Gamma_n \ll \Gamma_\gamma$
 \Rightarrow no reference cross section
 except for shape of $^{10}\text{B}(n, \alpha)$

Multiple Scattering

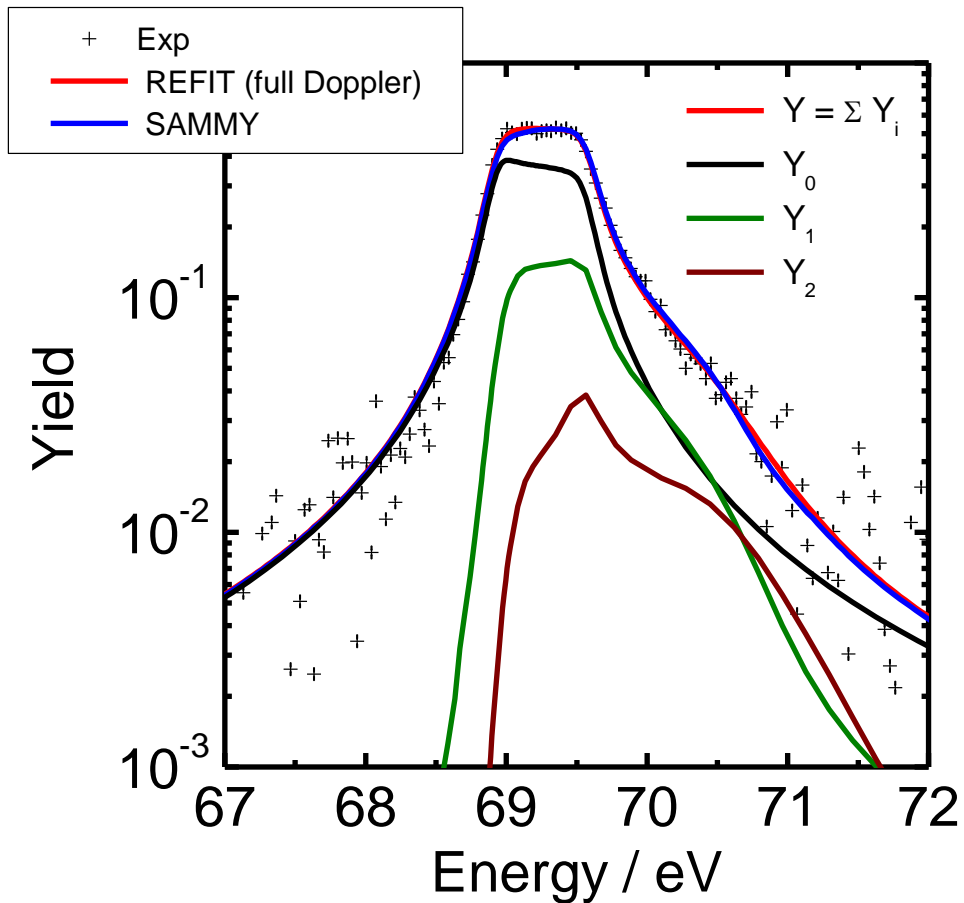
$$Y_r = Y_0 + Y_1 + Y_2 + \dots = Y_0 + Y_m$$



$$Y_0 = (1 - e^{-n \bar{\sigma}_{\text{tot}}}) \frac{\sigma_{\gamma}}{\sigma_{\text{tot}}}$$

Multiple Scattering

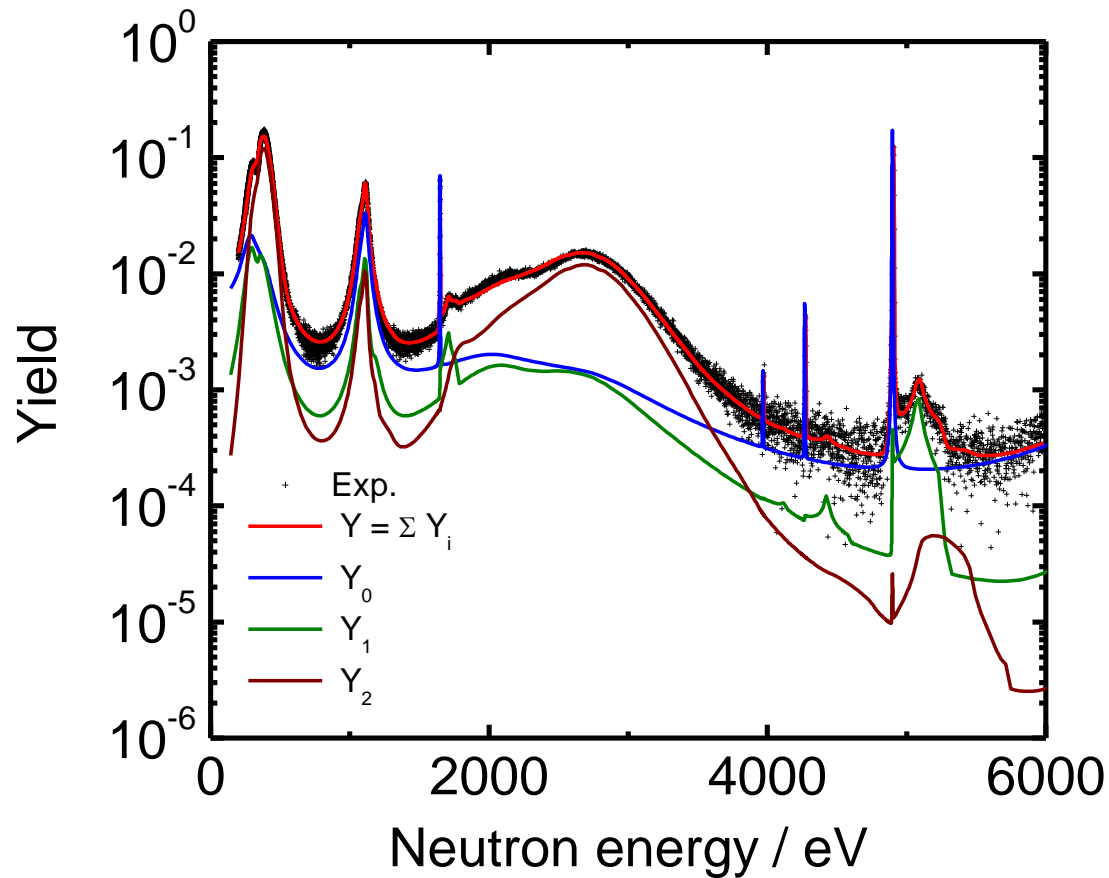
69 eV resonance in $^{232}\text{Th}+n$



Th metal disc
80 mm diameter
1 mm thick

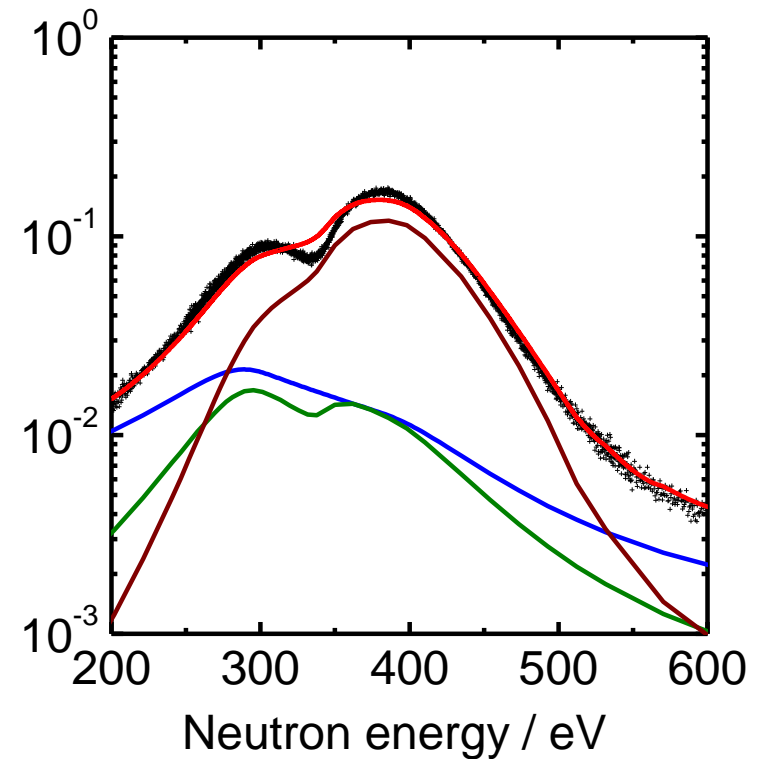
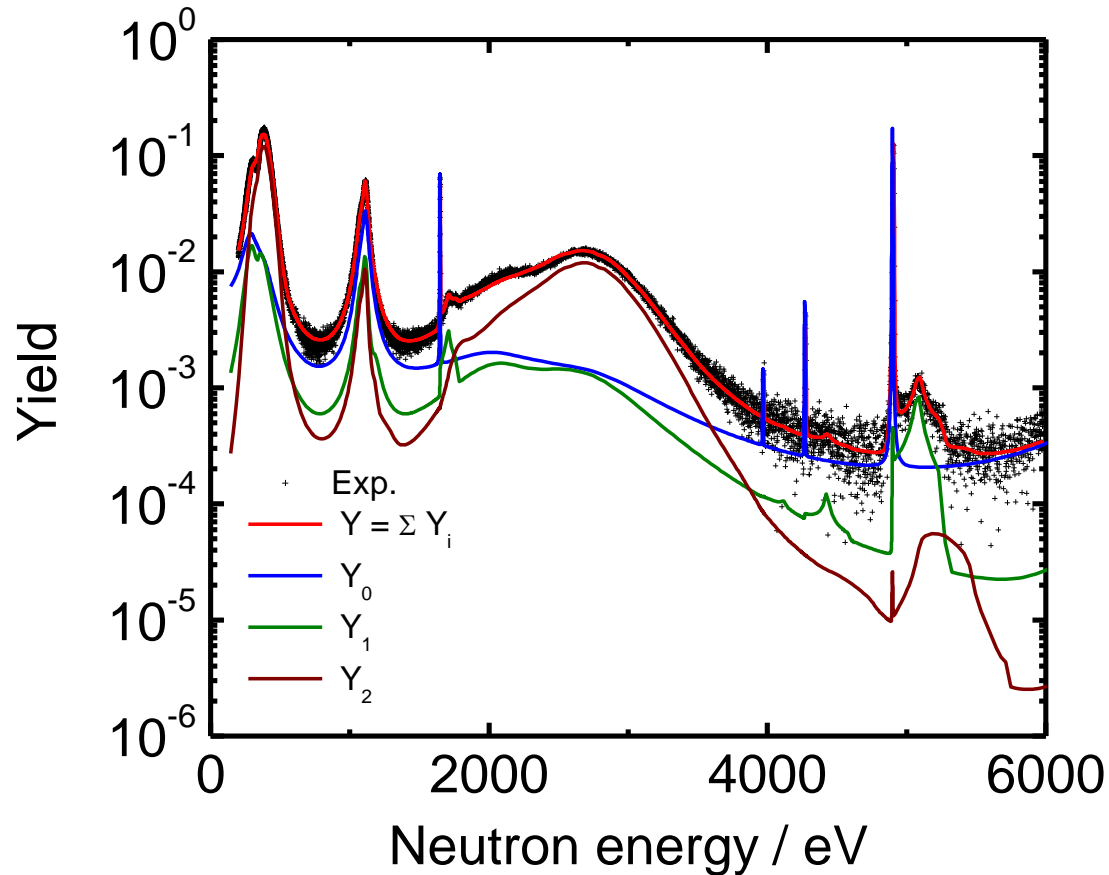
Multiple Scattering

$^{55}\text{Mn} + n$: Sputtering target , 77 mm diameter and 3 mm thick



Multiple Scattering

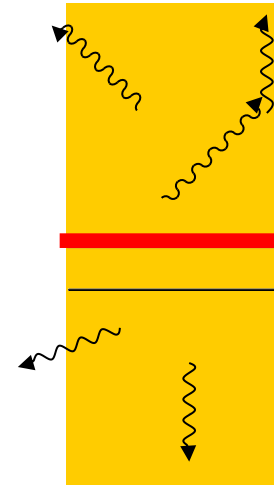
$^{55}\text{Mn} + n$: Sputtering target, 77 mm diameter and 3 mm thick



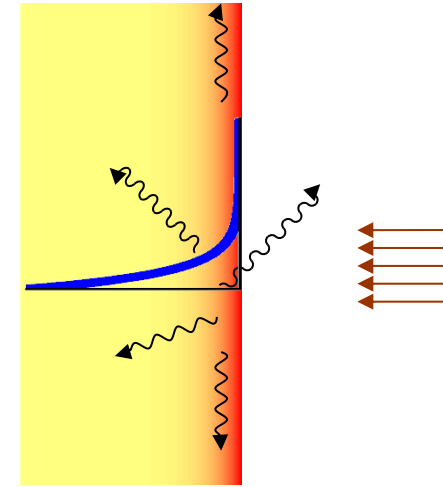
Gamma Attenuation

γ - ray attenuation depends on resonance strength

Each resonance requires special WF



WR
Weak
Resonance

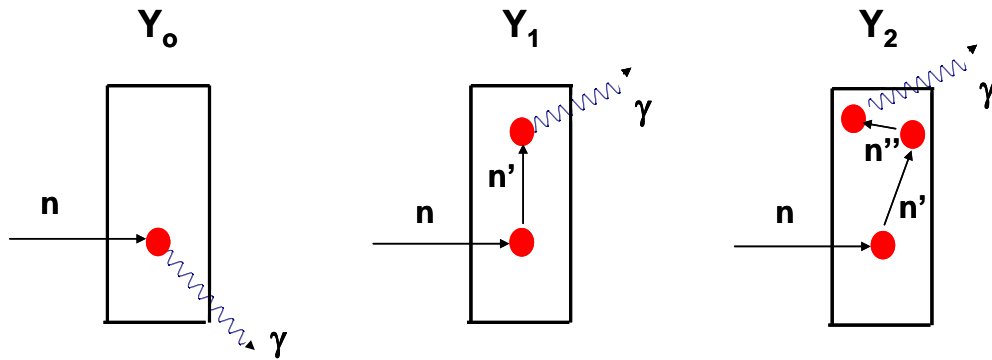


SR
Strong
Resonance

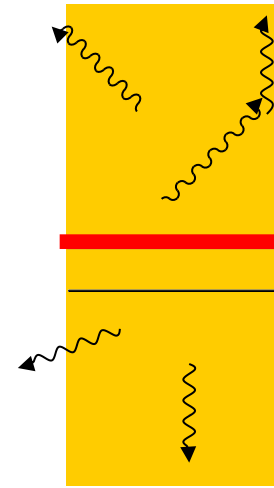
γ - ray attenuation depends on $n\sigma_{\text{tot}}$

γ - ray attenuation depends on resonance strength

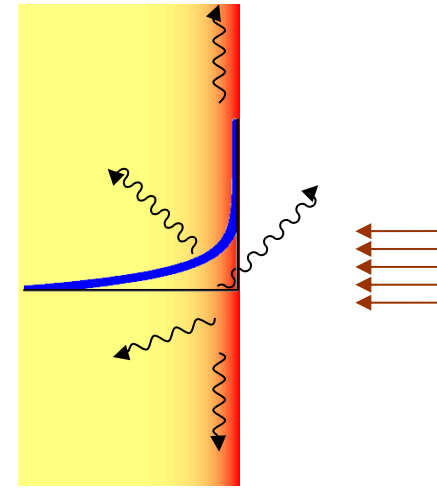
Each resonance requires special WF
+ each component Y_0, Y_1, Y_2



\Rightarrow in practice not possible



WR
Weak
Resonance



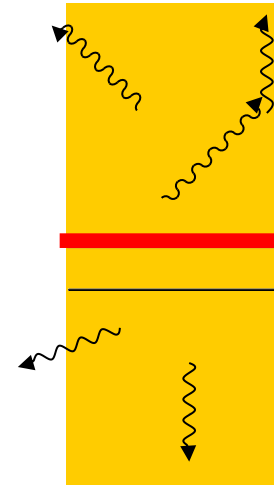
SR
Strong
Resonance

Gamma Attenuation

Procedure:

(1) Analyse experimental data for WR

i.e. supposing homogeneous
distribution of γ -rays



WR
Weak
Resonance

Gamma Attenuation

Procedure:

(1) Analyse experimental data for WR

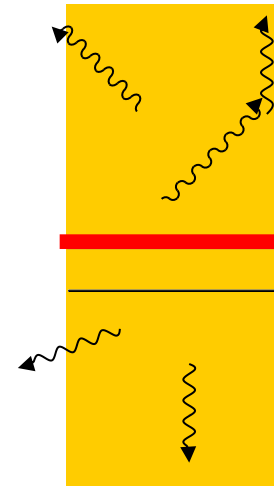
i.e. supposing homogeneous distribution of γ -rays

(2) Correction factor on calculated yield mostly based on calculations

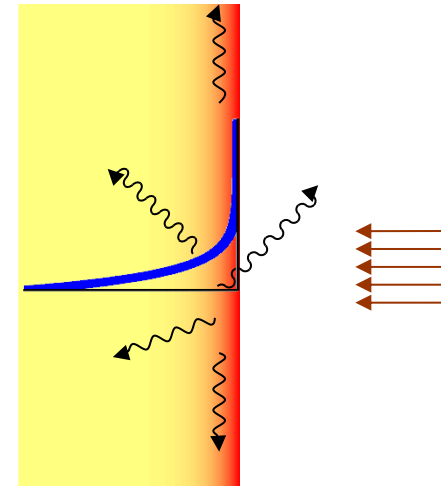
$$F_0(n\sigma_{\text{tot}})$$

$$F_m(n\sigma_{\text{tot}}) \approx 1$$

$$Y_c = F_0 Y_0(E_n) + F_m Y_m(E_n)$$



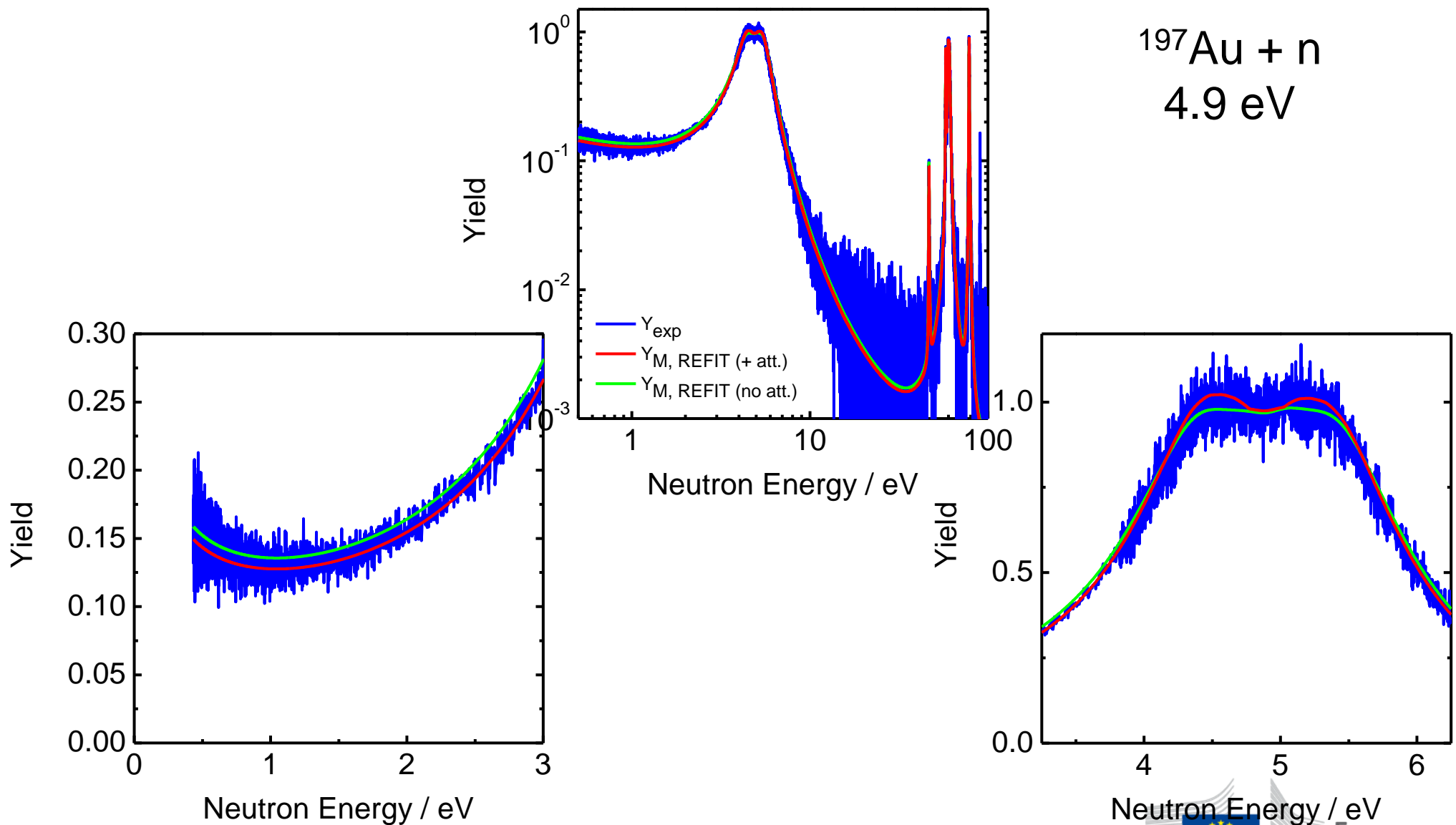
WR
Weak
Resonance



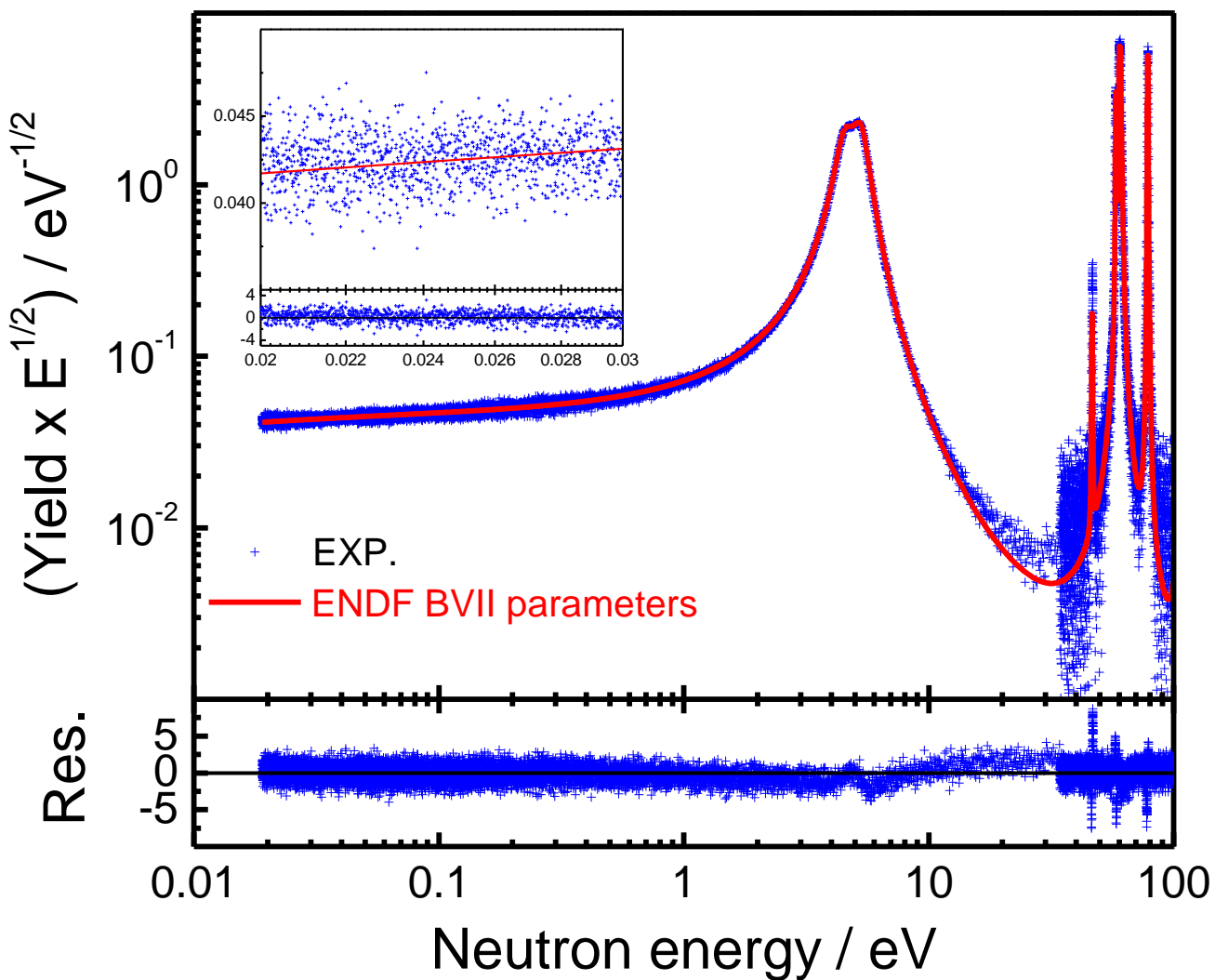
SR
Strong
Resonance

Gamma Attenuation

$^{197}\text{Au} + n$
4.9 eV



Gamma Attenuation

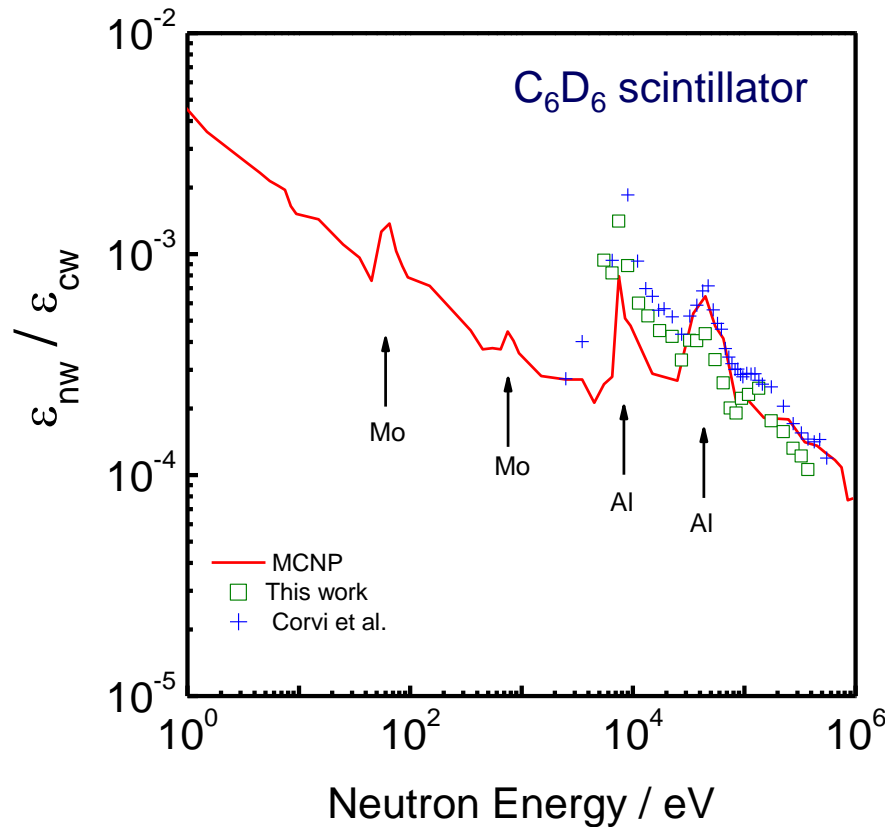
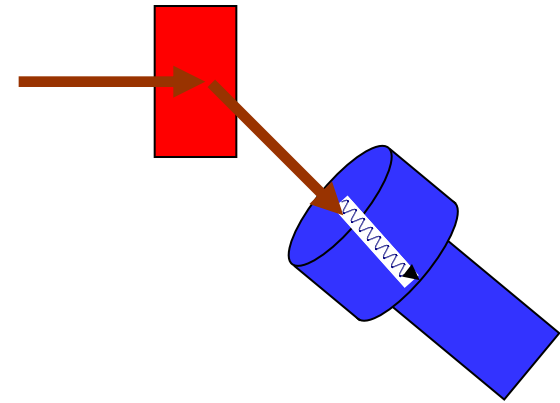


Standard :
From transmission
 $\sigma(n_{th}, \gamma) = (98.7 \pm 0.1) \text{ b}$

GELINA :
From capture
 $\sigma(n_{th}, \gamma) = (99.0 \pm 1.0) \text{ b}$

Schillebeeckx et al., JKPS 59 (2011) 1563

Neutron scattered by the sample creates a capture event in the detector



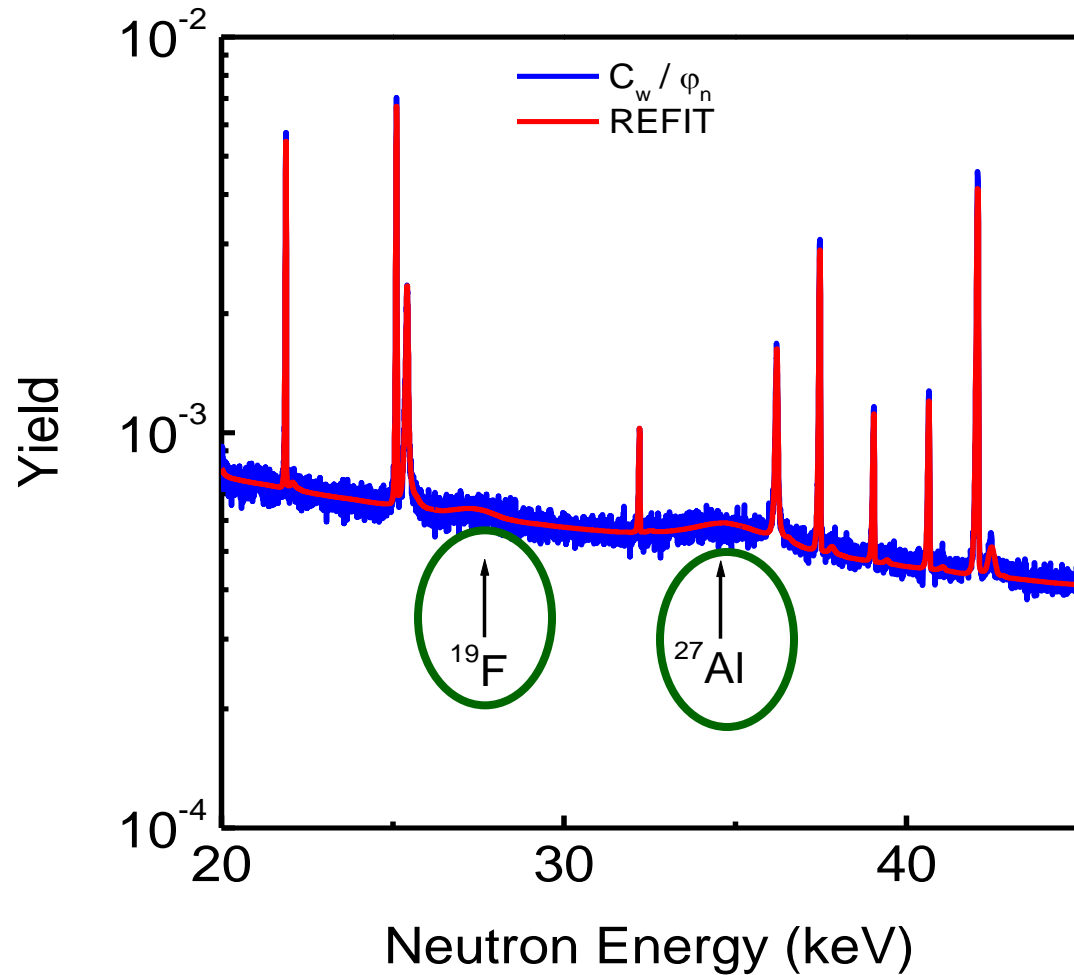
- Mo from μ -metal
- F from teflon in C_6D_6
- Al from
 - Sample holder
 - Detector structure

Neutron Sensitivity

REFIT : correction for NS

$$Y_M = \varepsilon_c Y_c + K_{ns} Y_n$$

$$Y_c = F_0 Y_0(E_n) + F_m Y_m(E_n)$$

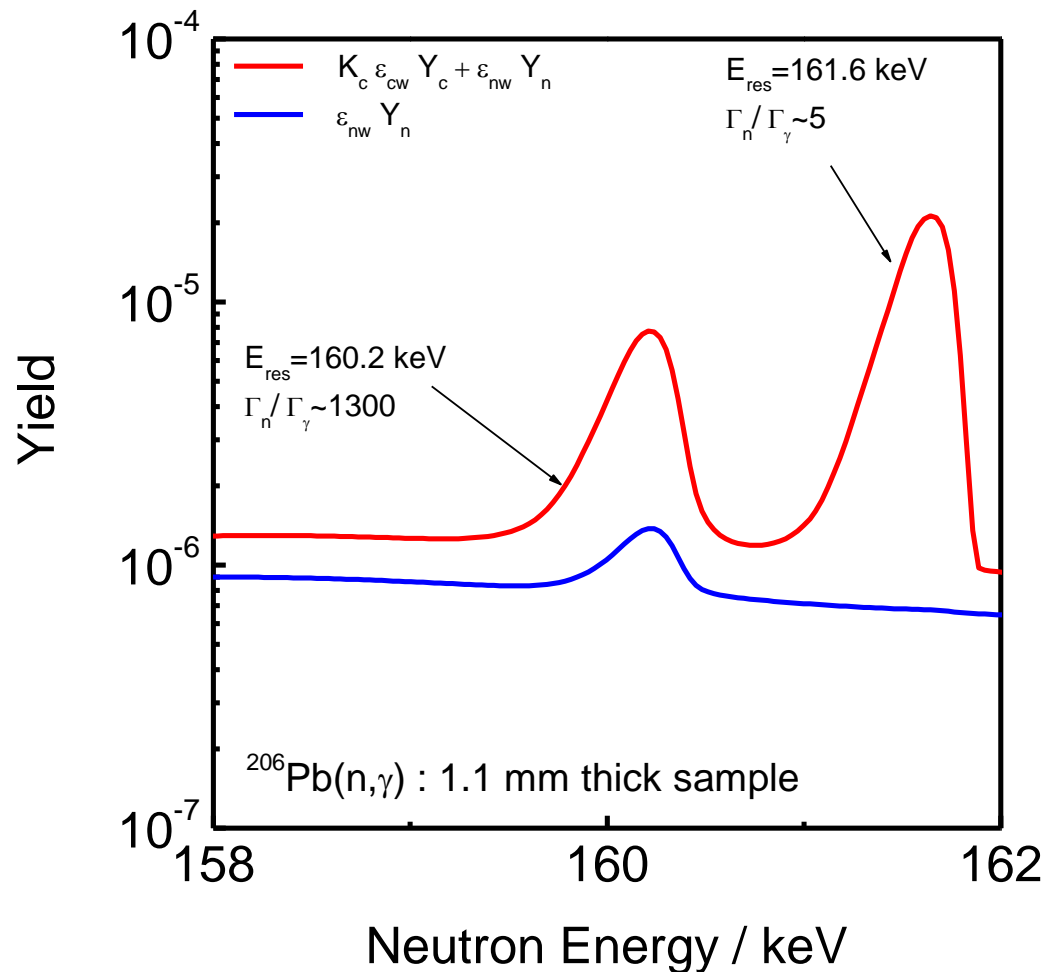


REFIT : correction for NS

$$Y_M = \varepsilon_c Y_c + K_{ns} Y_n$$

$$Y_c = F_0 Y_0(E_n) + F_m Y_m(E_n)$$

includes impact of multiple interaction events



Conclusions

- Modelling of experimental effects
 - Important for reliable determination of nuclear parameters
- The question "How good is the experimental model" remains unanswered
- Uncertainty of nuclear parameters are determined in an interplay between (experimental) model and experimental uncertainties



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