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# Calculation of catalytic nuclear reactions induced by reactor neutrons and its applications

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- I spent 3 month in Hokkaido University in Dr.
   Go Chiba's laboratory
- He is a head of reactor physics laboratory in HU



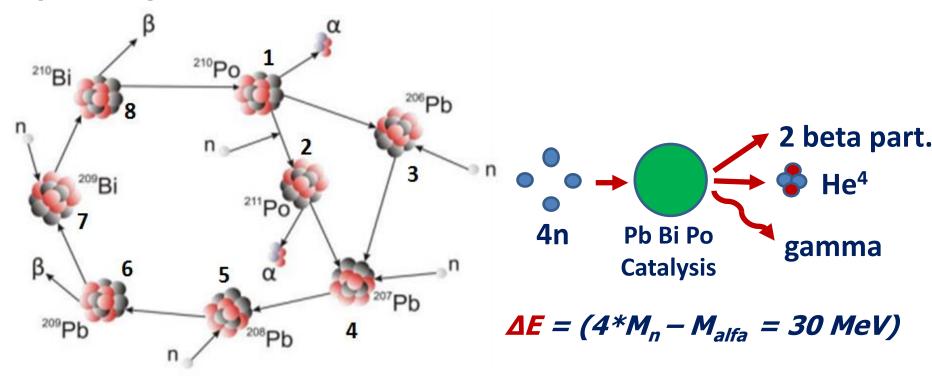
**Prof. Go Chiba** 

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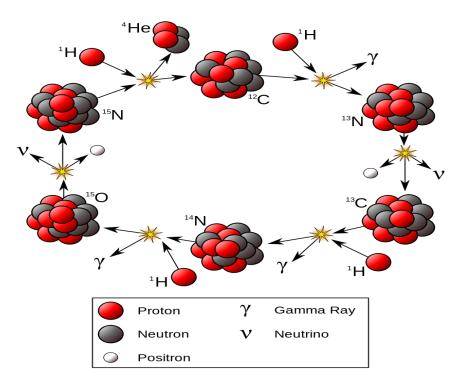
*Neutron catalysis is* a chain reaction based on the reaction of a four neutron capture by catalyst nucleus with the restoration of the initial nucleus

Catalytic cycle reaction - four of neutron capture, two beta decay and alpha decay.



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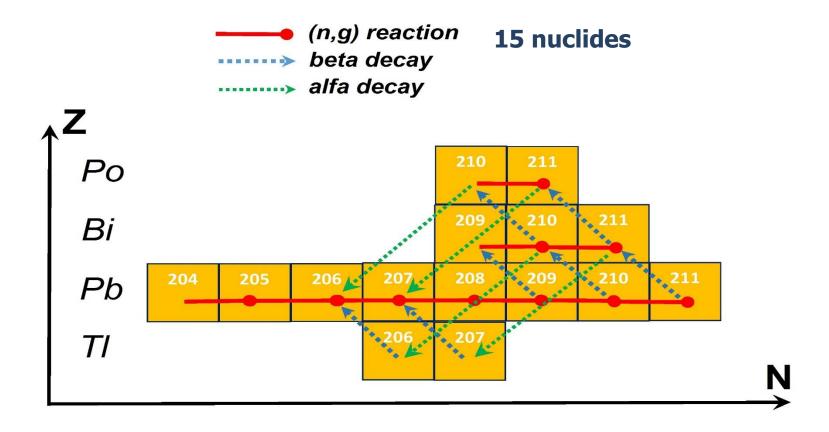
Analog of neutron catalysis is: CNO cycle in massive stars CNO cycle (for carbon-nitrogen-oxygen) is fusion reactions by which stars convert hydrogen to helium



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#### Neutron catalysis is the catalytic chain reaction with *equilibrium state.*



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#### Differential equation for a number density of nuclide *i*

$$\frac{dN_i}{dt} = -\frac{\lambda_i N_i(t) - \sigma_i \phi N_i(t)}{\text{Decrease of } N_i} + \sum_{j \neq i} \lambda_j P_{j \to i} N_j(t) + \sum_{j \neq i} \sigma_j \phi Q_{j \to i} N_j(t)$$

**Increase number density of** N<sub>i</sub>

$$\frac{d}{dt}\mathbf{N} = \mathbf{A}\mathbf{N}$$
$$\mathbf{N} = (N_1, N_2 \dots N_I)$$

A – burn-up matrix N – Nuclide density vector System of linear equations

 $\mathbf{N}(t) = \mathbf{N}(0) \exp(\mathbf{A}t)$ 

The number density in the equilibrium state can be easily obtained if  $t \rightarrow \infty$ 

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$$\mathbf{N}(t) = \mathbf{N}(0) \exp(\mathbf{A}t)$$

## The matrix exponential $\exp(\mathbf{A}t)$ can be numerically calculated with several methods

- 1. Pade approximation
- 2. CRAM (Chebyshev Rational Approximation) developed in VTT technical research center of Finland
- 3. MMPA developed in Hokkaido University

$$N_{pq}(x) = \sum_{k=0}^{p} \frac{(p+q-k)! \, p!}{(p+q)! \, k! \, (p-k)!} x^{k}$$

$$D_{pq}(x) = \sum_{k=0}^{q} \frac{(p+q-k)! \, q!}{(p+q)! \, k! \, (q-k)!} (-x)^{k}$$

$$exp(\mathbf{A}\Delta t) \approx \frac{N_{pq}(\mathbf{A}\Delta t)}{D_{pq}(\mathbf{A}\Delta t)}$$

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In burnup calculation it is convenient to use 1-group energy averaged cross sections **1-group cross section** is defined from energy-dependent cross section  $\sigma(E)$  and neutron flux  $\varphi(E)$ . G is the total number of energy groups

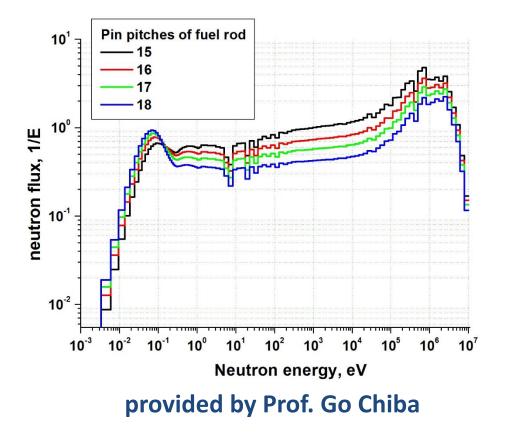
$$\tilde{\sigma} = \frac{\int \sigma(E)\varphi(E)dE}{\int \varphi(E)dE}$$
$$\tilde{\sigma} = \frac{\sum_{g=1}^{G} \sigma_{g}\varphi_{g}}{\sum_{g=1}^{G} \varphi_{g}}$$

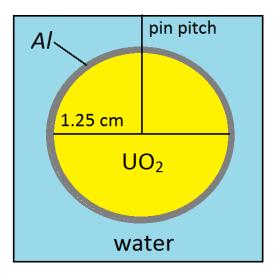
**G** is the total number of energy groups  $\varphi(E)$  is energy spectra of neutron flux

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#### **One group cross section**

## Neutron flux spectra at different pin pitches of the tank-typed critical assembly TCA with CBZ (TCA – is Japanese experimental reactor)





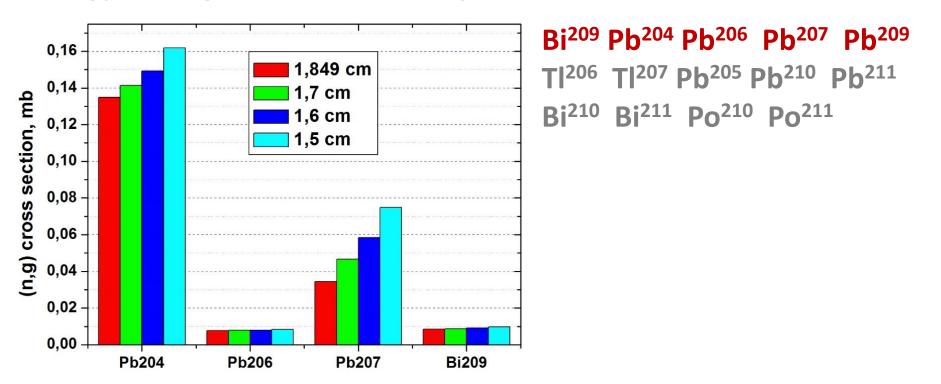
pin cell of TCA

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#### One group cross section

#### (n,g) cross sections were taken from JENDL-4.0 library

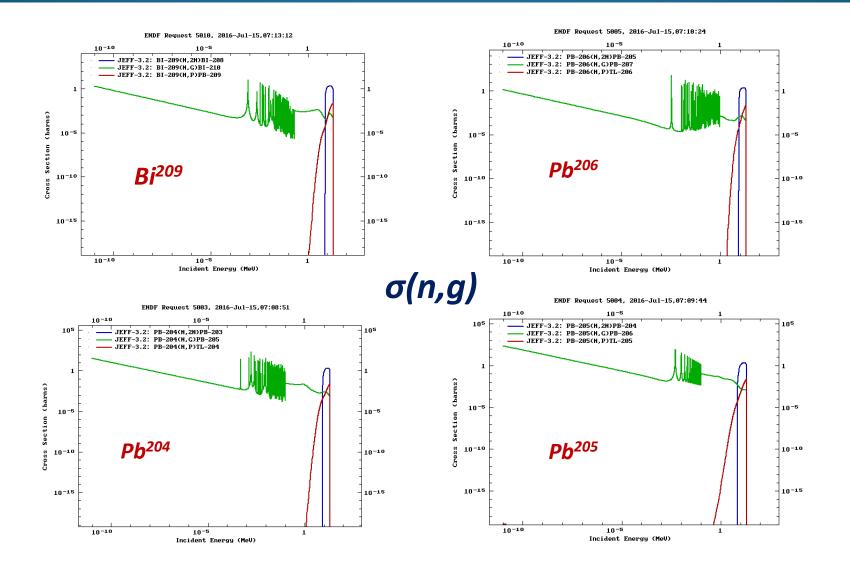
#### **Energy averaged cross sections of stable nuclides**



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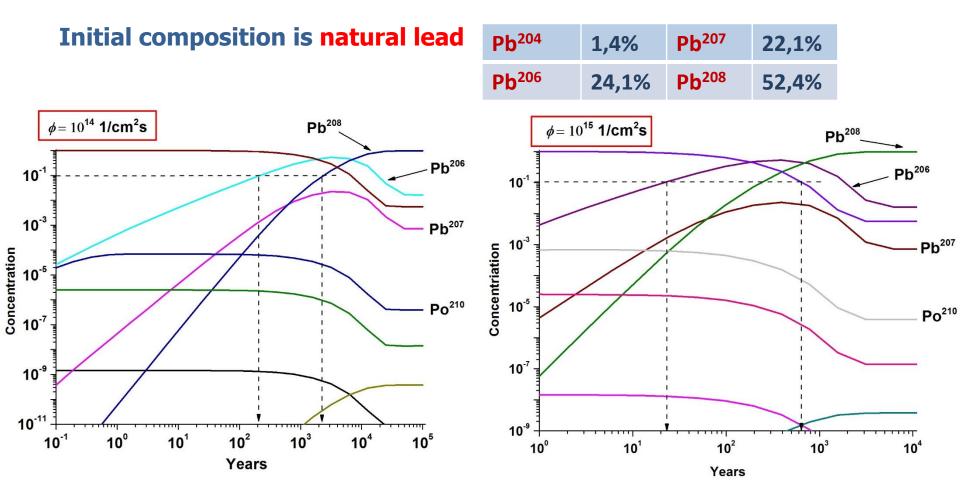


#### One group cross section (https://www-nds.iaea.org/exfor/endf.htm)



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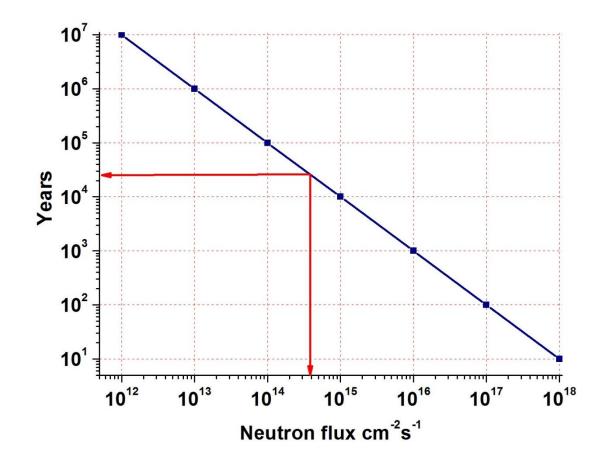
#### Number density change of nuclides under reactor neutron irradiation



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#### The time needed to reach the equilibrium state at different neutron fluxes

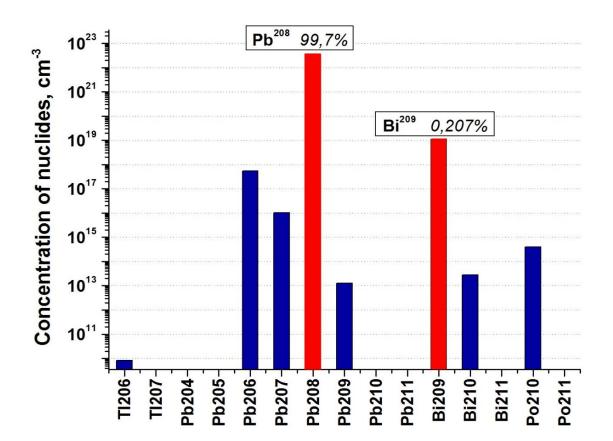


Problem is the time period of equilibrium state is too long

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#### Number density of nuclides at *equilibrium state.*



The problem is:

It is too difficult to enrich 15 nuclides for proper densities.

The *natural lead* composition is used for calculation because its isotope composition is closer to catalytic material composition

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#### How can catalytic material be used as reactor component?

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How can catalytic material be used as reactor component?

Main advantage of catalytic composition is:

- It is stable under long time neutron irradiation
- It can produce additional energy in reactor core

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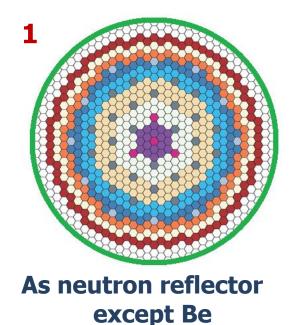


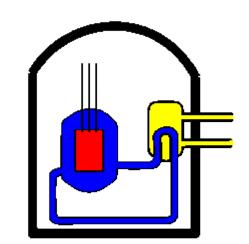
How can catalytic material be used as a reactor component?

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Main advantage of catalytic composition is:

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As liquid lead coolant in fast reactor

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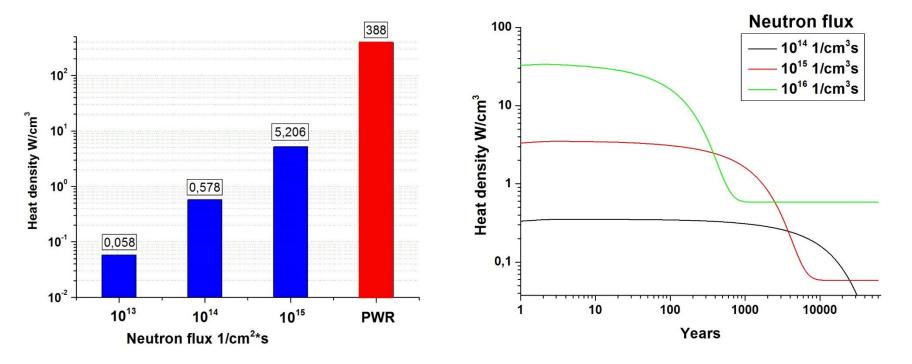


#### Heat density results

**Total heat generated by decays** 

**E**<sub>i</sub> is the emitted energy by a decay of nuclide *i* 

$$H(t) = \sum_{i} E_{i} \lambda_{i} N_{i}(t) + \sum_{i} E_{i}' \phi \sigma_{i} N_{i}(t)$$



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### Sensitivity analysis of nuclear data

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#### Sensitivity analysis of nuclear data

$$S^{i} = \frac{dN_{i}(T)}{N_{i}(T)} / \frac{d\sigma}{\sigma} = \frac{\sigma}{N_{i}(T)} \cdot \frac{dN_{i}(T)}{d\sigma}$$
$$\frac{dN_{i}(T)}{d\sigma} = \int_{0}^{T} \left( N^{*} \frac{dM}{d\lambda} N \right) dt$$

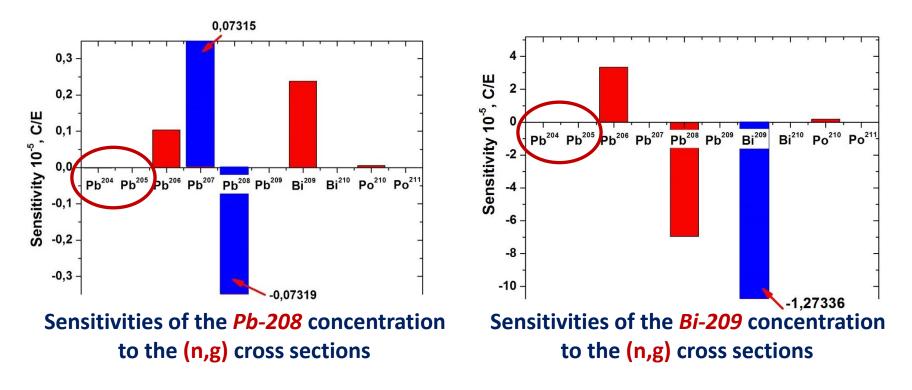
**M** is burnup matrix  $N^*$  is adjoint number density vector **T** is the time after irradiation  $\sigma$  capture cross section (n,g)

Derivative term can be derived using *General Perturbation Theory.* The calculation method was developed by Prof. Go Chiba in JAEA. (Sensitivity Analysis of Fission Product Concentrations for LWR Burned Fuel)

Note: The position dependence of concentrations N(r) and the energy dependence of cross sections  $\sigma(E)$  are ignored here.

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## **Sensitivity analysis** of nuclear data can show which nuclear data is important to results.

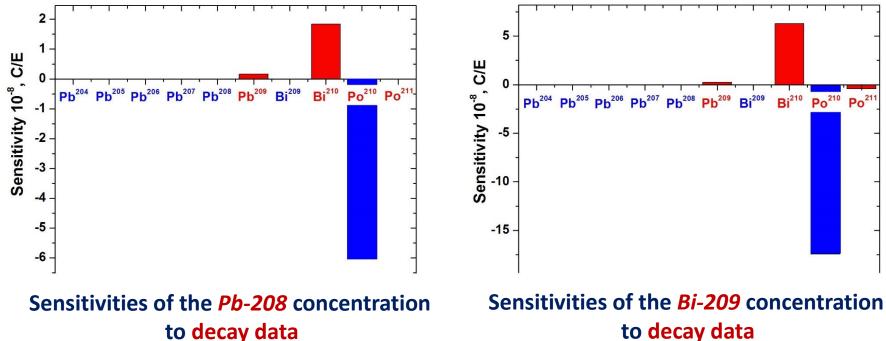


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#### Sensitivity analysis of nuclear data

#### Also we can see which *decay data* is important to concentration changes of nuclides

$$S^{i} = \frac{dN_{i}(T)}{N_{i}(T)} / \frac{d\lambda}{\lambda} = \frac{\lambda}{N_{i}(T)} \cdot \int_{0}^{T} \left( N^{*} \frac{dM}{d\lambda} N \right) dt$$



to decay data



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#### Sensitivity analysis of nuclear data

Such sensitivity analysis of nuclear data is important in reactor physics, to define most important data for FPC.

The reactivity of nuclear fuels decreases through burnup since fissile nuclides contained in fuels transform into fission products.

By taking this fact into account, it becomes possible to manage criticality safety issues in nuclear facilities more rationally and more economically.

Journal of NUCLEAR SCIENCE and TECHNOLOGY, Vol. 47, No. 7, p. 652-660 (2010)

#### ARTICLE

#### Sensitivity Analysis of Fission Product Concentrations for Light Water Reactor Burned Fuel

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The accurate prediction of fission product concentrations (FPCs) is necessary for application of the burnup credit to nuclear facilities. In order to specify important nuclear data for the accurate prediction of FPC, we extensively evaluate the sensitivities of FPC to nuclear data with the depletion perturbation theory. The target fission products are twelve important ones for the burnup credit, Mo-95, Tc-99, Rh-103, NH 110, N

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#### Conclusion

Following results were obtained:

- The nuclide density of catalytic material in equilibrium state
- Heat density of catalytic material at several neutron flux level
- Sensitivity analysis of nuclides concentrations to CS and decay data

In the future decay heat from FPC of Molten Salt Reactor will be calculated using BurnUP equation.

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