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===== Virgin
PROGRAM VIRGIN Virgin
VERSION 76-1 (NOVEMBER 1976) Virgin
VERSION 84-1 (JUNE 1984) *DOUBLE PRECISION ENERGY Virgin
VERSION 86-1 (JANUARY 1986)*FORTRAN-77/H VERSION Virgin
VERSION 88-1 (JULY 1988) *OPTION...INTERNALLY DEFINE ALL I/O Virgin
FILE NAMES (SEE, SUBROUTINE FILEIO Virgin
FOR DETAILS). Virgin
*IMPROVED BASED ON USER COMMENTS. Virgin
VERSION 89-1 (JANUARY 1989)*PSYCHOANALYZED BY PROGRAM FREUD TO Virgin
INSURE PROGRAM WILL NOT DO ANYTHING Virgin
CRAZY. Virgin
*UPDATED TO USE NEW PROGRAM CONVERT Virgin
KEYWORDS. Virgin
*ADDED LIVERMORE CIVIC COMPILER Virgin
CONVENTIONS. Virgin
VERSION 92-1 (JANUARY 1992)*COMPLETE RE-WRITE Virgin
*OUTPUT IN PLOTTAB FORMAT Virgin
*UP TO 2000 THICKNESSES Virgin
*INCREASED INCORE PAGE SIZE TO 6000 Virgin
CROSS SECTION POINTS Virgin
*ADDED PHOTON CALCULATIONS Virgin
*ADDED BLACKBODY SPECTRUM Virgin
*ADDED MULTIPLE LAYERS Virgin
*ADDED SPATIALLY DEPENDENT DENSITY Virgin
*ADDED FORTRAN SAVE OPTION Virgin
*COMPLETELY CONSISTENT I/O ROUTINES - Virgin
TO MINIMIZE COMPUTER DEPENDENCE. Virgin
VERSION 92-2 (MAY 1992) *CORRECTED TO HANDLE MULTIGROUP CROSS Virgin
SECTIONS AS INPUT IN ENDF/B FORMAT. Virgin
VERSION 96-1 (JANUARY 1996) *COMPLETE RE-WRITE Virgin
*IMPROVED COMPUTER INDEPENDENCE Virgin
*ALL DOUBLE PRECISION Virgin
*ON SCREEN OUTPUT Virgin
*UNIFORM TREATMENT OF ENDF/B I/O Virgin
*IMPROVED OUTPUT PRECISION Virgin
*DEFINED SCRATCH FILE NAMES Virgin
VERSION 99-1 (MARCH 1999) *CORRECTED CHARACTER TO FLOATING Virgin
POINT READ FOR MORE DIGITS Virgin
*UPDATED TEST FOR ENDF/B FORMAT Virgin
VERSION BASED ON RECENT FORMAT CHANGE Virgin
*GENERAL IMPROVEMENTS BASED ON Virgin
USER FEEDBACK Virgin
VERS. 2000-1 (FEBRUARY 2000)*GENERAL IMPROVEMENTS BASED ON Virgin
USER FEEDBACK Virgin
VERS. 2002-1 (MAY 2002) *OPTIONAL INPUT PARAMETERS Virgin
VERS. 2004-1 (MARCH 2004) *ADDED INCLUDE FOR COMMON Virgin
*UP TO 2000 THICKNESSES Virgin
*INCREASED INCORE PAGE SIZE TO 12,000 Virgin
OWNED, MAINTAINED AND DISTRIBUTED BY Virgin
----- Virgin
THE NUCLEAR DATA SECTION Virgin
INTERNATIONAL ATOMIC ENERGY AGENCY Virgin
P.O. BOX 100 Virgin
A-1400, VIENNA, AUSTRIA Virgin
EUROPE Virgin
ORIGINALLY WRITTEN BY Virgin
----- Virgin
DERMOTT E. CULLEN Virgin
UNIVERSITY OF CALIFORNIA Virgin
LAWRENCE LIVERMORE NATIONAL LABORATORY Virgin
L-159 Virgin
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THIS PR

EVALUATED DATA

RELATED COMPUTER CODES

OUTPUT FORMAT

TALLY GROUPS

PREPRO 2004

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(1) CONSTANT...ENERGY INDEPENDENT (INPUT 0)
(2) 1/E (INPUT 1)
(3) BLACKBODY - PHOTON SPECTRUM
(4) BLACKBODY - ENERGY SPECTRUM (E TIMES THE PHOTON SPECTRUM)
(5) TRANSMITTED SPECTRUM FROM PREVIOUS CASE

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NOTE, INCIDENT SPECTRA IS NORMALIZED TO UNITY OVER THEIR ENTIRE ENERGY RANGE - NOT OVER THE ENERGY RANGE OF THE GROUPS. IF THE ENERGY RANGE OF THE GROUPS IS LESS THAN THAT OF THE SPECTRUM ONLY THAT PORTION OF THE SPECTRUM WILL BE USED AND THIS WILL NOT BE RE-NORMALIZED TO UNITY.

IN THE OTHER THREE CASES THE TWO REQUESTED CROSS SECTIONS ARE TREATED AS TWO CONSTITUENTS OF A MIXTURE OF TWO MATERIALS AND THE TWO CROSS SECTIONS ARE USED BOTH TO DEFINE A TOTAL CROSS SECTION FOR ATTENUATION AND A REACTION CROSS SECTION TO DEFINE REACTIONS. IN THESE CASES THE MIXTURE WILL VARY CONTINUOUSLY, E.G., IN CASE 4) HALF WAY THROUGH THE LAYER THE COMPOSITION WILL BE 1/2 THE MATERIAL DEFINED BY THE TOTAL AND 1/2 THE MATERIAL BASED ON THE REACTION. IN THESE CASES RATHER THAN THINKING OF THE TWO CROSS SECTIONS AS A TOTAL AND REACTION CROSS SECTION, IT IS BETTER TO THINK OF THEM AS THE TOTAL CROSS SECTIONS FOR

MULTIPLE LAYERS

IN THE CASE OF MULTIPLE LAYERS, ONE LAYER AFTER ANOTHER, THE TRANSMITTED ENERGY DEPENDENT SPECTRUM IS USED AS THE INCIDENT SPECTRUM FOR THE NEXT LAYER. THERE IS NO LIMIT TO THE NUMBER OF LAYERS WHICH MAY BE USED - EACH LAYER IS TREATED AS A COMPLETELY INDEPENDENT PROBLEM WITH A DEFINED INCIDENT SOURCE, AND AS SUCH THE CYCLE OF TRANSMISSION THROUGH EACH LAYER AND USING THE TRANSMITTED SPECTRUM AS THE INCIDENT SPECTRUM FOR THE NEXT LAYER MAY BE REPEATED ANY NUMBER OF TIMES.

RESULT OUTPUT UNITS

THICKNESS AND DENSITY

GRAMS/(CM*CM) ARE RELATED TO ATOMS/BARN THROUGH THE RELATIONSHIP

$$\text{GRAMS} / (\text{CM} * \text{CM}) = (\text{ATOMS} / \text{BARN}) * (\text{GRAMS} / \text{MOLE}) * (\text{MOLE} / \text{ATOM})$$

OR...

$$\text{GRAMS}/(\text{CM}^2) = (\text{ATOMS}/\text{BARN}) * (\text{ATOMIC WEIGHT}) / 0.602$$

CROSS SECTIONS AT A SPACE POINT AND OPTICAL THICKNESS

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1) C = UNIFORM DENSITY
2) C**2*(X/T) = LINEAR VARIATION FROM 0 TO C
3) C*(2-2***(X/T)) = LINEAR VARIATION FROM C TO 0
4) C**3*(X/T)**2 = SQUARE VARIATION FROM 0 TO C
5) C*(3-3***(X/T)**2)/2 = SQUARE VARIATION FROM C TO 0
6) C**4*(X/T)**3 = CUBIC VARIATION FROM 0 TO C

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IN ORDER TO CALCULATE REACTIONS AT A POINT THE MICROSCOPIC
REACTION CROSS SECTION NEED MERELY BE SCALED BY THESE DENSITIES.

- 1) $C \cdot X$
- 2) $C \cdot X \cdot (X/T)$
- 3) $C \cdot X \cdot (2 - (X/T))$
- 4) $C \cdot X \cdot (X/T)^2$
- 5) $C \cdot X \cdot (3 - (X/T)^2)/2$
- 6) $C \cdot X \cdot (X/T)^3$
- 7) $C \cdot X \cdot (4 - (X/T)^3))/3$

THE VARIATION OF THE DENSITY THROUGH THE LAYER MAY BE DEFINED BY SETTING $X = 0$ OR $X = T$ TO FIND,

1) C	C
2) 0	2*C
3) 2*C	0
4) 0	3*C
5) 3*C/2	0
6) 0	4*C
7) 4*C/3	0

NOTE - FOR THE SAME OPTICAL PATH LENGTHS THROUGH THE LAYER THE TRANSMISSION WILL BE EXACTLY THE SAME. HOWEVER, VARYING THE DENSITY WILL ALLOW YOU TO MODIFY THE REACTION RATES AT SPECIFIC DEPTHS INTO THE LAYER.

STARTING FROM TOTAL CROSS SECTIONS, REACTION CROSS SECTIONS AND A SOURCE SPECTRUM ALL OF WHICH ARE GIVEN IN TABULAR FORM WITH LINEAR INTERPOLATION BETWEEN TABULATED POINTS ALL REQUIRED INTEGRALS CAN BE DEFINED BY ANALYTICAL EXPRESSIONS INVOLVING NOTHING MORE COMPLICATED THAN EXPONENTIALS. THE INTEGRALS THAT MUST BE EVALUATED ARE OF THE FORM...

$$\int_{E_K}^{E_{K+1}} S(E) \exp(-XCT(E) \cdot Z) dE$$
$$(\text{INTEGRAL EK TO EK+1}) (S(E)*XCR(E)*\text{EXP}(-XCT(E)*Z)*DE)$$

EK TO EK+1 = LONGEST ENERGY INTERVAL OVER WHICH S(E), XCT(E) AND
XCR(E) ARE ALL LINEARLY INTERPOLABLE.

S(E), XCR(E) AND XCT(E) ARE ALL ASSUMED TO BE GIVEN IN TABULAR FORM WITH LINEAR INTERPOLATION USED BETWEEN TABULATED POINTS. IN OTHER WORDS BETWEEN TABULATED POINTS EACH OF THESE THREE IS DEFINED BY A FUNCTION OF THE FORM...

$$F(E) = ((E - E_K) * FK + 1 + (E_{K+1} - E) * FK) / (E_{K+1} - E_K)$$

EACH OF THESE THREE CAN BE CONVERTED TO NORMAL FORM BY THE
CHANGE OF VARIABLES....

$$X = (E - 0.5 * (EK+1 + EK)) / (EK+1 - EK)$$

IN WHICH CASE X WILL VARY FROM -1 (AT EK) TO +1 (AT EK+1) AND EACH FUNCTION REDUCES TO THE NORMAL FORM...

$$F(X) = 0.5 * (FK * (1 - X) + FK+1 * (1 + X))$$
$$= 0.5 * (FK+1 + FK) + 0.5 * (FK+1 - FK) * X$$

BY DEFINING THE AVERAGE VALUE AND 1/2 THE CHANGE ACROSS THE
INTERVAL.

$$AVF = 0.5 * (FK + 1 + FK)$$

$$DF = 0.5 * (FK+1 - FK)$$

$$DE = 0.5 * (EK+1 - EK)$$

EACH OF THE THREE FUNCTIONS REDUCES TO THE SIMPLE FORM...

$$F(X) = AVF + DF * X$$

AND THE TWO REQUIRED INTEGRALS REDUCE TO...

FLUX

— — — —

$$DE \cdot \exp(-AVXCT \cdot Z) \cdot \left(\int_{-1}^{+1} ((AVS + DS \cdot X) \cdot \exp(-DXCT \cdot Z \cdot X)) \cdot DX \right)$$

REACTION

$$\text{DE*EXP}(-\text{AVXCT*Z}) * (\text{INTEGRAL } -1 \text{ TO } +1) \\ ((\text{AVS*AVXCR} + (\text{AVS*DXCR} + \text{AVXCR*DS}) * \text{X} + \text{DS*DXCR*X*X}) * \text{EXP}(-\text{DXCT*Z*X}) * \text{DX})$$

WHERE

AVXCT	=	AVERAGE VALUE OF THE TOTAL CROSS SECTION
AVXCR	=	AVERAGE VALUE OF THE REACTION CROSS SECTION
AVS	=	AVERAGE VALUE OF THE SOURCE
DXCT	=	1/2 THE CHANGE IN THE TOTAL CROSS SECTION
DXCR	=	1/2 THE CHANGE IN THE REACTION CROSS SECTION
DS	=	1/2 THE CHANGE IN THE SOURCE
DE	=	1/2 THE CHANGE IN THE ENERGY

NOTE THAT IN THIS FORM THE ENERGY ONLY APPEARS IN FRONT OF THE INTEGRALS AND THE INTEGRALS ARE EXPRESSED ONLY IN TERMS OF THE TABULATED VALUES OF $S(E)$, $XCT(E)$ AND $XCR(E)$. IN PARTICULAR NO DERIVATIVES ARE USED, SO THAT THERE ARE NO NUMERICAL INSTABILITY PROBLEMS IN THE VICINITY OF DISCONTINUITIES IN $S(E)$, $XCT(E)$ OR $XCR(E)$. INDEED, SINCE $(E_{K+1} - E_K)$ APPEARS IN FRONT OF THE INTEGRAL POINTS OF DISCONTINUITY AUTOMATICALLY MAKE ZERO CONTRIBUTION TO THE INTEGRALS.

THE REQUIRED INTEGRALS CAN BE EXPRESSED IN TERMS OF THE THREE
INTEGRALS IN NORMAL FORM....

$$F(A,N) = (\text{INTEGRAL } -1 \text{ TO } 1) (X^N \cdot \text{EXP}(-A \cdot X) \cdot DX), \quad N=0,1 \text{ AND } 2.$$

THESE THREE INTEGRALS CAN BE EVALUATED TO FIND...

N=0

$$F(A,0) = (\text{EXP}(A) - \text{EXP}(-A)) / A$$

[illegible]

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                (SORTED AT END OF RUN AND OUTPUT SEPARATELY)
SCR2          13  TALLY GROUP ENERGY BOUNDARIES (BINARY)
SCR3          14  SOURCE SPECTRUM (BINARY)
SCR4          15  TOTAL CROSS SECTION (BINARY)
SCR5          16  REACTION CROSS SECTION (BINARY)

OPTIONAL STANDARD FILE NAMES (SEE SUBROUTINE FILIO1 AND FILEIO2)
-----
UNIT  FILE NAME  FORMAT
-----
   2  VIRGIN.INP  BCD
   3  VIRGIN.LST  BCD
  10  ENDFB.IN   BCD
11-15 (SCRATCH)  BINARY
   16  PLOTTAB.CUR PLOTTAB OUTPUT FORMAT DATA

INPUT LINES
-----
ANY NUMBER OF CASES MAY BE RUN ONE AFTER THE OTHER. AFTER THE
FIRST CASE HAS BEEN RUN THE FOLLOWING CASES MAY USE THE SAME
THICKNESSES, GROUP STRUCTURE AND SPECTRUM AS THE PRECEDING CASE.
IN ADDITION THE TRANSMITTED SPECTRUM FROM ONE CASE MAY BE USED
AS THE INCIDENT SPECTRUM IN THE NEXT CASE, TO ALLOW MULTIPLE
LAYERS OF DIFFERENT MATERIALS.

LINE  COLS.  FORMAT  DESCRIPTION
----  ----  -
   1   1-60  ENDF/B INPUT DATA FILENAME
                (STANDARD OPTION = ENDFB.IN)

LEAVE THE DEFINITION OF THE FILENAMES BLANK - THE PROGRAM WILL
THEN USE STANDARD FILENAMES.

2-3   1-72   18A4   TWO LINE TITLE DESCRIBING PROBLEM
   4   1- 6   I6     ZA (1000*Z+A) OF TARGET FOR TOTAL
       7-11   I5     MT OF TOTAL
12-22  E11.4  DENSITY FOR TOTAL
23-28   I6     ZA (1000*Z+A) OF TARGET FOR REACTION
29-33   I5     MT OF REACTION
                = 0 - NO REACTION CALCULATION (ONLY FLUX).
                = GREATER THAN 0 - CALCULATE REACTIONS.
34-44  E11.4  DENSITY FOR REACTION
45-50   I6     NUMBER OF TARGET THICKNESSES
                = GREATER THAN 0 = READ FROM INPUT
                (1 TO 2000 ALLOWED)
                = 0 = SAME AS LAST CASE
51-55   I5     NUMBER OF TALLY GROUPS
                (REMEMBER NUMBER OF GROUP BOUNDARIES
                IS ONE MORE THAN THE NUMBER OF GROUPS)
                UP TO 2000 GROUPS ARE ALLOWED
                BUILT-IN GROUP STRUCTURES.
                = GREATER THAN 0 = READ FROM INPUT
                = 0 SAME AS LAST CASE
                = -1 TART 175 GROUPS
                = -2 ORNL 50 GROUPS
                = -3 ORNL 126 GROUPS
                = -4 ORNL 171 GROUPS
                = -5 SAND-II 620 GROUPS..UP TO 18 MEV.
                = -6 SAND-II 640 GROUPS..UP TO 20 MEV.
                = -7 WIMS 69 GROUPS
                = -8 GAM-I 68 GROUPS
                = -9 GAM-II 99 GROUPS
                =-10 MUFT 54 GROUPS
                =-11 ABBN 28 GROUPS
56-60   I5     NUMBER OF POINTS IN SOURCE SPECTRUM
                (MUST BE AT LEAST TWO POINTS)
                = GREATER THAN 1 = READ FROM INPUT
                = 0 = SAME AS LAST CASE
                = -1 = CONSTANT (ENERGY INDEPENDENT)
                = -2 = 1/E
                = -3 = BLACKBODY - PHOTON SPECTRUM

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			= -4 = BLACKBODY - ENERGY SPECTRUM	Virgin
			= -5 = TRANSMITTED SPECTRUM FROM LAST CASE	Virgin
			NOTE, ALL SPECTRA, EXCEPT THE TRANSMITTED	Virgin
			SPECTRUM FROM THE LAST CASE, WILL BE	Virgin
			NORMALIZED SUCH THAT ITS INTEGRAL OVER	Virgin
			ENERGY WILL BE UNITY.	Virgin
61-64	1X,3I1		SPATIALLY DEPENDENT OUTOUT	Virgin
			= 0 = NO	Virgin
			= 1 = YES	Virgin
			FOR THE 3 QUANTITIES	Virgin
			COLUMN 67 FLUX	Virgin
			68 REACTIONS	Virgin
			69 AVERAGE CROSS SECTION	Virgin
65-65	I1		ENERGY DEPENDENT OUTOUT	Virgin
			= 0 = NONE	Virgin
			= 1 = INCIDENT SPECTRUM	Virgin
			= 2 = TRANSMITTED SPECTRUM	Virgin
			= 3 = INCIDENT REACTIONS	Virgin
			= 4 = TRANSMITTED REACTIONS	Virgin
			= 5 = TOTAL CROSS SECTION	Virgin
			= 6 = REACTION CROSS SECTION	Virgin
5	1-11	E11.4	BLACKBODY TEMPERATURE IN EV	Virgin
	12-22	E11.4	FLUX NORMALIZATION	Virgin
	23-33	E11.4	REACTION NORMALIZATION	Virgin
			CALCULATIONS WILL BE BASED ON THE SPECTRUM	Virgin
			AND CROSS SECTIONS AS READ. AT OUTPUT THE	Virgin
			RESULTS WILL BE MULTIPLIED BY THESE	Virgin
			NORMALIZATION FACTORS.	Virgin
34-44	I11		DENSITY PROFILE	Virgin
			= 0 - UNIFORM - BASED ON TOTAL DENSITY	Virgin
			= 1 - UNIFORM - TOTAL + REACTION DENSITY	Virgin
			= 2 - TOTAL + LINEAR REACTION	Virgin
			= 3 - LINEAR (TOTAL + REACTION)	Virgin
			= 4 - TOTAL + SQUARE REACTION	Virgin
			= 5 - SQUARE (TOTAL + REACTION)	Virgin
			= 6 - TOTAL + CUBIC REACTION	Virgin
			= 7 - CUBIC (TOTAL + REACTION)	Virgin
6-N	1-66	6E11.4	TARGET THICKNESSES IN CM	Virgin
			IF SAME AS LAST CASE THIS SECTION IS NOT	Virgin
			INCLUDED IN THE INPUT.	Virgin
VARY	1-66	6E11.4	TALLY GROUP ENERGY BOUNDARIES	Virgin
			(NUMBER OF BOUNDARIES IS ONE MORE THAN	Virgin
			THE NUMBER OF TALLY GROUPS)	Virgin
			IF THE STANDARD OPTION (-11 TO 0) IS	Virgin
			SELECTED THIS SECTION IS NOT INCLUDED	Virgin
			IN THE INPUT	Virgin
VARY	1-66	6E11.4	SOURCE SPECTRUM IN ENERGY (EV)-SOURCE PAIRS	Virgin
			(MUST BE AT LEAST TWO POINTS)	Virgin
			IF STANDARD OPTION (-5 TO 0) IS SELECTED THIS	Virgin
			SECTION IS NOT INCLUDED IN THE INPUT	Virgin

ANY NUMBER OF CASES MAY BE RUN ONE AFTER ANOTHER.

EXAMPLE INPUT NO. 1

CALCULATE THE UNCOLLIDED FLUX AND CAPTURE (MT=102) THROUGH
30 CM OF IRON (DENSITY 7.87 G/CC). TALLY THE RESULTS USING
THE TART 175 GROUP STRUCTURE. THE SOURCE WILL BE CONSTANT
FROM 1 KEV TO 20 MEV. USE THE STANDARD ENDF/B INPUT DATA
FILENAME.

ENDFB.IN

IRON 0 TO 30 CM THICK.

CONSTANT SOURCE FROM 1 KEV TO 20 MEV.

26000	1	7.87000+	0	26000	102	7.87000+	0	2	0	2	1100
0.00000+	0	1.00000+	0	1.00000+	0	0	0.00000+	00			
0.00000+00		3.00000+01									
1.00000E+03		1.00000E+00		2.00000E+07		1.00000E+00					

EXAMPLE INPUT NO. 2

CALCULATE THE UNCOLLIDED PHOTON FLUX THROUGH A MIXTURE OF SILICON AND IRON FOR 100 MEV PHOTONS INCIDENT. THE TRANSMISSION WILL BE CALCULATED FOR 21 THICKNESSES VARYING BETWEEN 0 AND 1 CM. THERE WILL BE ONLY 1 TALLY GROUP SPANNING A VERY NARROW ENERGY RANGE NEAR 100 MEV, AND THE SOURCE SPECTRUM WILL BE CONSTANT OVER THE SAME ENERGY RANGE. USE THE STANDARD ENDF/B INPUT DATA FILENAME BY LEAVING THE FIRST INPUT LINE BLANK.

(THIS IS A BLANK LINE TO USE THE STANDARD INPUT FILENAME)

100 MEV PHOTONS

SILICON + 5 % IRON

14000	521	2.30000+	0	26000	521	1.15000-	1	21	1	2	1000	Virgin
0.00000+	0	1.00000+	0	1.00000+	0			1	0.00000+00			Virgin
0.00000+00		5.00000-01		1.00000+00		1.50000+00		2.00000+00		2.50000+00		Virgin
3.00000+00		3.50000+00		4.00000+00		4.50000+00		5.00000+00		5.50000+00		Virgin
6.00000+00		6.50000+00		7.00000+00		7.50000+00		8.00000+00		8.50000+00		Virgin
9.00000+00		9.50000+00		1.00000+01								Virgin
9.99000+	7	1.00100+	8									Virgin
9.99000+	7	1.00000+	4	1.00100+	8	1.00000+	4					Virgin

===== Virgin