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Supplement

Full report.

**IN DC**

**INTERNATIONAL NUCLEAR DATA COMMITTEE**

IAEA Technical Co-operation Interregional Project on Nuclear  
Data Techniques and Instrumentation (INT/1/018)

Report on a Training Course on  
Nuclear Data Evaluation and Processing Techniques

held at the

Nuclear Data Centre  
Instituto de Estudos Avançados  
Centro Técnico Aeroespacial  
BR-12.200 São José dos Campos, S.P., Brazil

from 15 November - 17 December 1982

by B. Strohmaier  
Institut für Radiumforschung und Kernphysik  
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## GENERAL REPORT

### 1. Task

The subject of this IAEA lecturer's mission was Data Evaluation and Processing Techniques, in particular the theoretical aspects and the practical use of nuclear reaction model computer codes. The use of such codes for the evaluation of nuclear data to be applied in nuclear reactor neutronics calculations is one of the recently started activities of the Nuclear Data Centre of the Instituto de Estudos Avançados of the Centro Técnico Aeroespacial, and therefore this course aimed at training the staff there in methods of nuclear data evaluation based on nuclear model calculations. The full report including lecture notes is available from the IAEA Nuclear Data Section as supplement to this report.

### 2. The Institute

The Instituto de Estudos Avançados (IEAv) is one of the institutes which belong to the Centro Técnico Aeroespacial (CTA) and comprises departments for nuclear energy, laser, theoretical physics and computing. The other four institutes belonging to the CTA are concerned with aeronautic technology, aircraft engine structure, space activities (missiles) and research and development concerning aviation. The Nuclear Data Centre involves collaboration of the groups for nuclear energy, theoretical physics and computer science, and also will cooperate with an experimental physics department to be founded in connection with the construction of an electron linear accelerator which is expected to become operative in 1986. The IEAv is located in new buildings outside the CTA campus several kilometres from the centre of São José dos Campos.

### 3. Participants

The course was mainly addressed to the members of the evaluation group which is part of the department for theoretical physics and consists of Dr. Helio Dias, Ricardo Afonso

do Rego, Tobias Frederico, Milton Pereira Isidro Filho and Jairo Fiorentino. The latter four persons are students at the University of São Paulo. This evaluation group participated in the theoretical and the practical part of the course; the theoretical lectures, moreover, were attended by up to five (mostly graduate) persons belonging to the reactor physics group of the nuclear energy division or other departments of the IEAv.

#### 4. Activities

The course was divided up into a theoretical and a practical part. Theory was presented in two lectures per day, 45 minutes each, starting at 8.15 and 9.15 a.m. The practical part consisted of more loosely organized "workshops" held on many days in the late morning and everyday in the afternoon. During these workshops all steps of the evaluation procedure were exercised by treating sample problems. The used computer codes ABACUS, IUPITOR and STAPRE had been installed at the CDC Cyber 170/750 at the IEAv already, more recent versions as well as small subsidiary programs for preparing input data and processing results I had brought with me. Advice was given with input preparation, output evaluation, comparison of the results to experimental data (partly brought with me in form of EXFOR listings) and parameter variation. A more detailed description of the problems treated in the workshops is given in the last part of the report. Besides that, the workshops also offered a possibility of discussing open questions in connection with the theoretical lectures. The contents of the lectures can be seen in the 2<sup>nd</sup> part of this report which consists of copies of the transparencies used. Such kind of lecture notes were also made during the course for all participants in order to give them the chance to go through the theory afterwards on their own. This was necessitated by the fact that often an immediate understanding of the lectures seems to have been hindered by their problems with the English language as well as by deficiencies in their basic

physics knowlegde.

Besides the time devoted to direct collaboration with the participants, much work was invested in lecture preparation, program modifications, debugging of sample runs and searching for particular experimental and evaluation papers in the library. In this context it may be worth stating that the library, despite its being equipped with nuclear theory textbooks rather completely, suffers from a grave lack of papers published before 1976.

### 5. Further needs

In order to support the beginning activities regarding model code-based evaluations, further experts' guidance is desirable. One of the aims of such support should be to enable the members of the evaluation group to work more independently which is not the case up to now, due partly to lack of experience, partly to the fact that they are mainly students and not yet used to perform independent research work. Maybe, advice can be given in written form in the frame of correspondence, maybe some other form of contact can be established. The director of the IEAv, Dr. Reginaldo, as well as the head of the nuclear energy department, Dr. Nair, asked me to come back for several months in late 1983 or beginning of 1984. Also, one thinks of sending 1-2 members of the evaluation group abroad for further training in the field of nuclear data evaluation.

A further mission of an expert from the ENEA Centro di Calcolo in Bologna is expected for middle 1983.

A complementary valuable source of obtaining information and advice is of course the participation in relevant training courses. In particular, the "Workshop on Nuclear Model Computer Codes" (Jan./Feb. 1984, Trieste) and the "Course on Methods of Nuclear Data Evaluation and Processing" (middle of 1984, Vienna) would probably be a suitable and helpful continuation of the presently described course for each of its participants.

Theoretical part: Contents of lectures

I. Introduction to the theory of elastic and inelastic scattering and nuclear reactions

- 1) Direct and compound reactions
- 2) Elastic scattering
- 3) Inelastic scattering
  - a) Coupled channels theory
  - b) DWBA
- 4) Nuclear reactions

II. Spherical optical model calculations

- 1) General description of the problem
- 2) Comparison with experimental data
- 3) General flow chart of spher. OM program

III. Coupled channels optical model calculations

- 1) Introduction
- 2) The interaction potential
- 3) The coupled equations
- 4) Scattering matrices and cross sections
- 5) Adiabatic approximation

IV. Statistical model for compound nucleus reactions and preequilibrium decay

- 1) Compound nucleus model
  - a) Theory
  - b) Subsidiary quantities
- 2) Preequilibrium exciton model

V. Survey of nuclear model computer codes

VI. ABACUS

- 1) Program operation
- 2) Input
- 3) Output

VII. IUPITOR

- 1) Program operation
- 2) Input
- 3) Output

VIII. STAPRE

- 1) Program operation
- 2) Input
- 3) Output

IX. Evaluation procedure

- 1) Retrieval of experimental data
- 2) First choice of model parameters
- 3) Input preparation
- 4) Output evaluation
- 5) Parameter variation
- 6) Consideration of special features
- 7) Accuracy



# I) INTRODUCTION TO THE THEORY OF ELASTIC AND INELASTIC SCATTERING AND NUCLEAR REACTIONS

## 1) Direct and compound reactions

processes that take place when two nuclei collide

calculate • types of reaction products

- their frequencies

- their energies

- their angular distributions

- their spin states

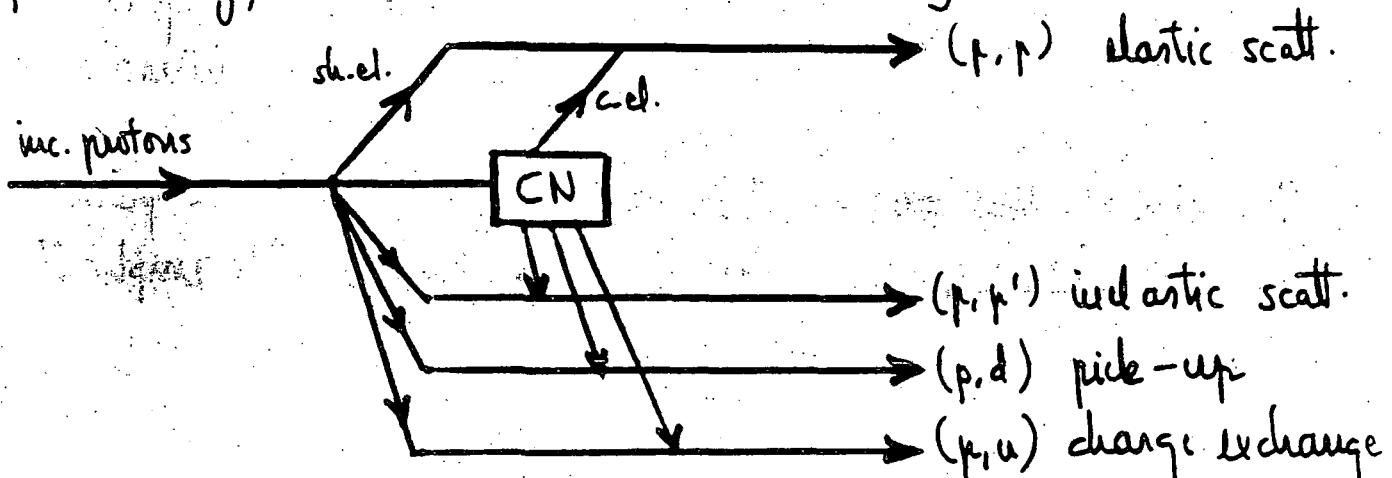
this information depends in many cases on structures of initial and final nuclei

→ comparison between  $\chi S^2$  expected from various models of nuclear structure and experimental data can teach us about nuclear structure

example: proton incident on nucleus

$E_p \ll E_a$  : interaction with Coulomb field of target nucleus only  
Coulomb barrier → elastic scatt. acc. Rutherford's law

higher energy : interaction with nuclear field :



direct reactions pass from initial to final state without any intermediate state (CN stage)

character of the reaction depends on the structure of the target nucleus  
 light target  $\rightarrow$  well spaced levels  $\rightarrow \chi S^2$  show resonance behaviour  
 heavier target  $\rightarrow$  levels closely spaced, overlapping  $\rightarrow$  resonance structure  
 is averaged out and  $\chi S^2$  vary more smoothly with energy

### compound nucleus reactions — direct interactions

both processes may simultaneously contribute to the reaction in particular channel; cannot be distinguished experimentally  
 $\Rightarrow$  calculated  $\chi S^2$  have to be combined before comparison to experimental data

electronic computers  $\Rightarrow$  gain in accuracy !!  
 $\qquad\qquad\qquad$  time !!

practical calculations require approximations that cannot be rigorously justified

e.g.: inelastic scattering: truncate infinite set of coupled equations  
 $\Rightarrow$  account for this by allowing the coupling potentials to be complex

these potentials are adjusted to fit the experimental data  
 $\Rightarrow$  serve to cover up the deficiencies of the approximations  
 $\Rightarrow$  no longer derivable from microscopic theory of the interaction

The aim of the present treatment is to provide a path from general principles to practical calculations, with emphasis on the physical ideas.

## 2) Elastic scattering

basic task of nuclear reaction theory is to find solution of Schrödinger equation of the system that satisfies boundary condition

many-body Schrödinger equation practically impossible to solve

$\Rightarrow$  describe interaction between incoming particle and target nucleus by one body potential  $V(r)$  ( $r \dots$  separation)

form is considered later on

spinless neutral particle, spherical local real potential

C.M. system

$$\nabla^2 \psi + \frac{2m}{\hbar^2} \{ E - V(r) \} \psi = 0$$

requirement: in asymptotic region: incoming plane wave + scattered spherical wave

spherical polar coordinates,  $z$  axis = direction of inc. beam:

$$\psi = e^{ikz} + \frac{e^{ikr}}{r} f(\theta) \quad \text{with } k = \frac{\sqrt{2mE}}{\hbar}$$

problem: calculate  $f(\theta)$  for given  $V(r)$

$$\Rightarrow \text{differential scattering XS} \quad \frac{d\sigma}{d\Omega} = |f(\theta)|^2$$

$$\text{expansion: } \psi = \sum L \frac{u_L(r)}{r} P_L(\cos \theta)$$

orbital angular momentum

$$\frac{d^2 u_L}{dr^2} + \left[ \frac{2m}{\hbar^2} \{ E - V(r) \} - \frac{L(L+1)}{r^2} \right] u_L = 0$$

$$\text{corner case of } L=0: \frac{d^2 u_0}{dr^2} + \frac{2m}{\hbar^2} \{ E - V(r) \} u_0 = 0$$

large distances:  $V(r)$  falls off more rapidly than  $r^{-1} \Rightarrow$  may be neglected beyond a certain radius  $R$

[not true for  $C_6$  potential  $\rightarrow$  not considered at present]

$$\text{general solution } u_0 = A \sin(kr + \delta) \equiv A \frac{e^{i\delta}}{2i} (e^{2id} e^{ibr} - e^{-ibr})$$

int. const.

since  $u = \pi \psi$ , this is  $\pi \{ \underbrace{\psi_{in}(L=0)}_{e^{ikr}(L=0)} + \psi_{out}(L=0) \}$

$L=0$  part of  $e^{ikr}$  is found from  $e^{ikr} = \sum_{L=0}^{\infty} (2L+1)i^L j_L(kr) P_L(\cos \theta)$

$$\text{as } e^{ikr}(L=0) = \frac{\sin kr}{kr} = \frac{1}{2ikr} (e^{ikr} - e^{-ikr})$$

$$\begin{aligned} \triangleright \psi_{out}(L=0) &= \frac{u_0}{\pi} - \psi_{in}(L=0) = \\ &= \underbrace{\frac{Ae^{-i\delta}}{2ir} (e^{2i\delta} e^{ikr} - e^{-ikr})}_{\psi} - \underbrace{\frac{1}{2ikr} (e^{ikr} - e^{-ikr})}_{\psi_{in}} \end{aligned}$$

from wholly outgoing  $\Rightarrow$  no terms in  $e^{-ikr}$

$$\triangleright \frac{Ae^{-i\delta}}{2i} = \frac{1}{2ik}$$

$$\psi_{out}(L=0) = \frac{1}{2ikr} (e^{2i\delta} - 1) e^{ikr} = \frac{1}{r} e^{ikr} f_0(\theta)$$

$$f_0(\theta) = \frac{1}{2ik} (e^{2i\delta} - 1)$$

for  $L \neq 0$  similar : in asymptotic region  $\left. \frac{V(r)}{L(L+1)} \right\} \rightarrow 0$

$$\Rightarrow \frac{d^2 u_L}{dr^2} + k^2 u_L = 0$$

general solution in  $L$  dependent form :

$$u_L \sim A \sin(kr - \frac{L\pi}{2} + \delta_L) \equiv \frac{Ae^{-i\delta_L}}{2i} (e^{2i\delta_L} e^{i(kr - \frac{L\pi}{2})} - e^{-i(kr - \frac{L\pi}{2})})$$

$-\frac{L\pi}{2}$  arbitrary, as  $\delta_L$  is a constant whose value is fixed

later on by the integration in the nuclear region;

$-\frac{L\pi}{2}$  is introduced so that  $\delta_L \rightarrow 0$  as  $V(r) \rightarrow 0$  for all  $L$

part of  $e^{ikr}$  corresponding to certain  $L$ :

$$\begin{aligned} 2i^L j_L(kr) &\leftarrow \frac{1}{ikr} (e^{ikr} - e^{iL\pi} e^{-ikr}) \\ &\leftarrow \frac{i^L}{ikr} (e^{i(kr - \frac{L\pi}{2})} - e^{-i(kr - \frac{L\pi}{2})}) \end{aligned}$$

$$\psi_{\text{out}}^L = \psi^L - \psi_{\text{in}}^L = \frac{A e^{-i\delta_L}}{2ik} \left( e^{2i\delta_L} e^{i(kr - \frac{L\pi}{2})} - e^{-i(kr - \frac{L\pi}{2})} \right) P_L(\cos \theta) - \\ - (2L+1) \frac{i^L}{2ikr} \left( e^{i(kr - \frac{L\pi}{2})} - e^{-i(kr - \frac{L\pi}{2})} \right) P_L(\cos \theta)$$

no terms in  $e^{-ikr} \Rightarrow \frac{A e^{-i\delta_L}}{2ik} = -(2L+1) \frac{i^L}{2ikr}$

L component of outgoing wave:  $\frac{(2L+1)i^L}{2ikr} P_L(\cos \theta)(e^{2i\delta_L} - 1) e^{i(kr - \frac{L\pi}{2})}$

Total scatt. amplitude:  $f(\theta) = \frac{1}{2ik} \sum_{L=0}^{\infty} (2L+1)(e^{2i\delta_L} - 1) P_L(\cos \theta)$

partial wave amplitude  $\frac{1}{2i}(e^{2i\delta_L} - 1)$

All the physical inform. is carried by the  $\delta_L$  from the potential  $V(r)$  to the XS:

Can be shown by consideration of the radial wave function  $u_0(r)$ :

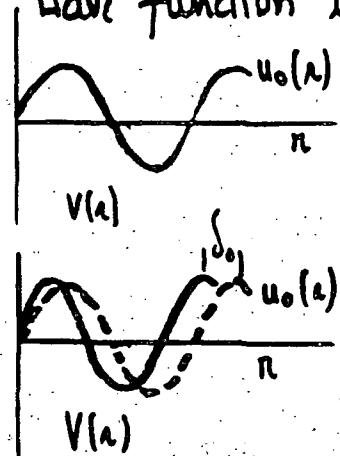
$$V(r)=0 \Rightarrow J_L \cdot 0 \Rightarrow \text{sinusoidal}$$

$$V(r) < 0 \text{ (attractive)} \Rightarrow \delta_L \neq 0$$

in the region of the potential: short wavelength

beyond the potential: same sinusoidal form as

for  $V(r)=0$ , but shifted in phase by  $\delta_0$



similar for other partial waves

observed scattering is determined only by the asymptotic forms of the wave functions  $\Rightarrow \delta_L$  carry all information from  $V(r)$  to the observed scattering

usual for convenience:  $e^{2i\delta_L} = S_L$  (scattering matrix element)

total elastic XS.:  $\sigma_E = \int |f(\theta)|^2 d\Omega = \frac{\pi}{k^2} \sum_L (2L+1) / (1 - S_L)^2$

### 3) Inelastic scattering

- simplest type of non-elastic interaction

XS may be calculated by perturbation theory expressions

↓  
not sufficiently accurate when there is strong coupling  
between elastic and inelastic channels

then: solve coupled equations for the wave functions in  
all the reaction channels

### Coupled channels theory

interaction of a neutral spinless particle with a nucleus that can be raised into a series of spinless excited states by the interaction

assumption: only elastic and inelastic scattering, no more complicated reactions

$$T = -\frac{\hbar^2}{2m} \nabla_{\vec{r}}^2 \quad \text{kinetic energy of incident particle}$$

relative motion

$H(\xi)$  nuclear Hamiltonian ( $\xi \dots$  all nuclear coordinates)

$V(\vec{r}, \xi)$  interaction between incident particle and target nucleus

Schrödinger equation for whole system:

$$\{T - V(\vec{r}, \xi) + H(\xi)\} \Psi(\vec{r}, \xi) = E \Psi(\vec{r}, \xi)$$

nuclear states defined by  $H(\xi) \chi_{\alpha}(\xi) = \varepsilon_{\alpha} \chi_{\alpha}(\xi)$

$\chi_{\alpha}$  complete, ON set  $\Rightarrow \Psi(\vec{r}, \xi) = \sum_{\alpha} \psi_{\alpha}(\vec{r}) \chi_{\alpha}(\xi)$

$$\{T - V(\vec{r}, \xi) + H(\xi)\} \sum_{\alpha} \psi_{\alpha}(\vec{r}) \chi_{\alpha}(\xi) = E \sum_{\alpha} \psi_{\alpha}(\vec{r}) \chi_{\alpha}(\xi)$$

$$\sum_{\alpha} \{T - V(\vec{r}, \xi) + \varepsilon_{\alpha}\} \psi_{\alpha}(\vec{r}) \chi_{\alpha}(\xi) = E \sum_{\alpha} \psi_{\alpha}(\vec{r}) \chi_{\alpha}(\xi)$$

multiply from the left with  $\chi_{\alpha}^*$ , integrate over  $d\xi$ , use orthonormality:

$$(T - E - \varepsilon_{\alpha}) \psi_{\alpha}(\vec{r}) = \underbrace{\sum_{\alpha'} \psi_{\alpha'}(\vec{r}) \int d\xi \chi_{\alpha'}^*(\xi) V(\vec{r}, \xi) \chi_{\alpha}(\xi)}_{V_{\alpha\alpha'}(\vec{r})} \quad (*)$$

remove angular coordinates by partial wave expansion:

$$\psi_\alpha(\vec{r}) = \sum_{LM} \frac{u_\alpha(r)}{r} Y_{LM}(\theta, \phi)$$

insert in eq. (\*), multiply from the left with  $Y_{L'M'}$ , integrate over  $d\Omega$ :

$$\int Y_{L'M'}(\theta, \phi) (T - E_\alpha) \sum_{LM} \frac{u_\alpha(r)}{r} Y_{LM}(\theta, \phi) =$$

$$= \boxed{\left( Y_{L'M'}(\theta, \phi) \right) \sum_{\alpha} \frac{u_\alpha(r)}{r} \int Y_{LM}(\theta, \phi) V_{\alpha\alpha'}(\vec{r}) d\Omega}$$

where  $E_\alpha = E - \epsilon_\alpha = \frac{\hbar^2 k_\alpha^2}{2m}$

$$=: \frac{\hbar^2}{2m} W_{\alpha\alpha'}(r)$$

$$\Rightarrow \left( \frac{d^2}{dr^2} - \frac{l(l+1)}{r^2} + k_\alpha^2 \right) u_\alpha(r) = \sum_{\alpha'} W_{\alpha\alpha'}(r) u_{\alpha'}(r)$$

$$\boxed{\left( \frac{d^2}{dr^2} - \frac{l(l+1)}{r^2} + k_\alpha^2 - W_{\alpha\alpha}(r) \right) u_\alpha(r) = \sum_{\alpha' \neq \alpha} W_{\alpha\alpha'}(r) u_{\alpha'}(r)} \quad (28)$$

→ set of coupled equations for the wave functions in the elastic and all the inelastic channels in the reaction being considered

in principle: if  $V(\vec{r}, \vec{s})$  and  $H(\vec{s})$  known → set can be solved for all  $u_\alpha$   
 → by application of appropriate boundary conditions elastic and inelastic  $\chi S^2$  can be calculated

in practice: number of equations that can be solved is limited;

approximation: truncate set of equations, allow for the effect of not explicitly considered channels by letting  $V(\vec{r}, \vec{s})$  be complex

formalism may be extended to spin dependent interactions

⇒ calculation of polarizations and asymmetries for particles with spin

## DWBA

(C theory) in principle exact calculation  
in many cases sufficient to use a scattering matrix element  
that is exact in the limit of weak coupling between elastic and  
inelastic channels  $\Rightarrow$  DWBA

incoming channel :  $\alpha$

outgoing channels :  $\alpha', \beta$

$S_{\alpha\alpha'}$  : amplitude of the outgoing wave in the channel  $\alpha'$  when a wave  
of unit amplitude is incident in channel  $\alpha$

asymptotic forms of the waves:

$$u_\alpha^\infty(r) \sim e^{-i(kr - \frac{L\pi}{2})} - S_{\alpha\alpha'} e^{i(kr - \frac{L\pi}{2})}$$

$$u_{\alpha'}^\infty(r) \sim -S_{\alpha\alpha'} e^{i(kr - \frac{L\pi}{2})}$$

$u_\alpha^\infty(r)$  satisfies the equation (1):

$$\left\{ \frac{d^2}{dr^2} - \frac{L(L+1)}{r^2} + k_\alpha^2 - W_{\alpha\alpha}^\infty(r) \right\} u_\alpha^\infty(r) = \sum_{\alpha' \neq \alpha} W_{\alpha\alpha'}^\infty(r) u_{\alpha'}^\infty(r) \quad (1)$$

consider reaction  $\alpha$  that occurs when particles are incident in channel

$$\left\{ \frac{d^2}{dr^2} - \frac{L(L+1)}{r^2} + k_\alpha^2 - W_{\alpha\alpha}^\beta(r) \right\} u_\alpha^\beta(r) = \sum_{\alpha' \neq \alpha} W_{\alpha\alpha'}^\beta(r) u_{\alpha'}^\beta(r) \quad (2)$$

From (1):

$$\left\{ \frac{d^2}{dr^2} - \frac{L(L+1)}{r^2} + k_\alpha^2 - W_{\alpha\alpha}^\infty(r) \right\} u_\alpha^\infty(r) - \sum_{\alpha' \neq \alpha, \beta} W_{\alpha\alpha'}^\infty(r) u_{\alpha'}^\infty(r) = W_{\alpha\beta}^\infty(r) u_\beta^\infty(r) \quad (1')$$

From (2):

$$\left\{ \frac{d^2}{dr^2} - \frac{L(L+1)}{r^2} + k_\alpha^2 - W_{\alpha\alpha}^\beta(r) \right\} u_\alpha^\beta(r) - \sum_{\alpha' \neq \alpha, \beta} W_{\alpha\alpha'}^\beta(r) u_{\alpha'}^\beta(r) = W_{\alpha\beta}^\beta(r) u_\beta^\beta(r) \quad (2')$$

Multiply (1') by  $u_\alpha^\beta(r)$  and (2') by  $u_\alpha^\infty(r)$  and subtract:

$$u_\alpha^\beta(r) \frac{d^2}{dr^2} u_\alpha^\infty(r) - u_\alpha^\infty(r) \frac{d^2}{dr^2} u_\alpha^\beta(r) - \left[ u_\alpha^\beta(r) \sum_{\alpha' \neq \alpha, \beta} W_{\alpha\alpha'}^\infty(r) u_{\alpha'}^\infty(r) - u_\alpha^\infty(r) \sum_{\alpha' \neq \alpha, \beta} W_{\alpha\alpha'}^\beta(r) u_{\alpha'}^\beta(r) \right]$$

$$= u_\alpha^\beta(r) W_{\alpha\beta}^\infty(r) u_\beta^\infty(r) - u_\alpha^\infty(r) W_{\alpha\beta}^\beta(r) u_\beta^\beta(r)$$

Transferred heat [ ] = 0

$$\nabla u_\alpha^\beta(r) \frac{d^2}{dr^2} u_\alpha^\beta(r) - u_\alpha^\beta(r) \frac{d^2}{dr^2} u_\alpha^\beta(r) = u_\alpha^\beta(r) W_{\alpha\beta}(r) u_\beta^\alpha(r) - u_\alpha^\beta(r) W_{\alpha\beta}(r) u_\alpha^\beta(r) \quad (3)$$

integrate from 0 to  $\infty$ :

$$\left[ u_\alpha^\beta(r) \frac{d}{dr} u_\alpha^\beta(r) \right]_0^\infty - \int_0^\infty \frac{d}{dr} u_\alpha^\beta(r) \frac{d}{dr} u_\alpha^\beta(r) dr - \left[ u_\alpha^\beta(r) \frac{d}{dr} u_\alpha^\beta(r) \right]_0^\infty + \int_0^\infty \frac{d}{dr} u_\alpha^\beta(r) \frac{d}{dr} u_\alpha^\beta(r) dr \\ = -S_{\beta\alpha} e^+ (-ik e^- - ik S_{\alpha\alpha} e^+) - (e^- - S_{\alpha\alpha} e^+) (ik) S_{\beta\alpha} e^+ \quad \xrightarrow{\text{left hand side of (3)}} \\ \text{using asymptotic forms} \\ = 2ik S_{\beta\alpha} e^+ e^- = 2ik S_{\beta\alpha}$$

right hand side of (3) :

1st term negligible due to  $u_\alpha^\beta(r) \ll u_\alpha^\alpha(r)$   $\leftarrow$  inelastic channels

weakly coupled to elastic channel

$$\Rightarrow 2ik S_{\beta\alpha} = - \int_0^\infty dr u_\alpha^\beta(r) W_{\alpha\beta}(r) u_\beta^\beta(r)$$

true for all channels  $\beta$ :  $\beta \rightarrow \alpha, \gamma \rightarrow \alpha'$

$$\Rightarrow S_{\alpha\alpha'}^{LM} = -\frac{1}{2ik} \int_0^\infty dr u_{\alpha'}^\alpha(r) W_{\alpha'\alpha}(r) u_\alpha^\alpha(r) \quad \text{DWBA expression for scatt. matrix element}$$

[superscript LM as radial fcts.  $u$  should in fact carry this superscript]

$$S_{\alpha\alpha'} = \sum_{LM} S_{\alpha\alpha'}^{LM}$$

$$\text{total inelastic XS: } \sigma_{\alpha\alpha'} = \frac{4\pi}{k^2} |S_{\alpha\alpha'}|^2$$

$$[S_{\alpha\alpha'} = -\frac{2m}{\pi^2} \cdot \frac{1}{2ik} \int d\vec{r} \psi_{\alpha'}(\vec{r}) V_{\alpha\alpha'}(\vec{r}) \psi_\alpha(\vec{r}) d\vec{r}]$$

## 4) Nuclear Reactions

if incident energy  $>$  corresponding thresholds  $\rightarrow$  many nuclear reactions can take place in addition to elastic and inelastic scatt. apart from inelastic scatt. the coupling to non-elastic channels is weak

Strong coupling

enough for perturbation theory to be sufficient  
by accurate  $\Rightarrow$  general perturbation theory  
approximation for reaction amplitudes

higher energies  $\rightarrow$  more than 2 particles

sequential emission  $\Rightarrow$  successive application of the formalism  
of 2 particle reactions

simultaneous emission  $\Rightarrow$  reaction mechanism?

for binary reaction:

if reaction time relative to transit time comparable — long

direct interaction

perturb. theory  
as above

pre-equilibrium decay

compound nucleus reaction

in compound nucleus reactions:

many degrees of freedom excited, XS complicated function of energy  
description of intermediate states not individual, but statistical  
(average values, correlation functions)  $\rightarrow$  statistical model

compound nucleus = system formed from projectile and target  
nucleus, in statistical equilibrium

states whose excitation is determining for energy dependence of XS  
resonances

isolated

overlapping

- isolated resonances: Breit-Wigner formula

$$\sigma_{ab} = \frac{\pi}{k_a^2} \frac{\Gamma_{ja} \Gamma_{jb}}{(E - E_{\mu})^2 + \frac{1}{4} \Gamma_{\mu}^2}$$

$\mu$ -resonance

$$\Gamma_{\mu} = \sum_j \Gamma_{j\mu}$$

$$\sigma_a^{\text{comp}} = \sum_b \sigma_{ab} = \frac{\pi}{k_a^2} \frac{\Gamma_{ja} \Gamma_{j\mu}}{(E - E_{\mu})^2 + \frac{1}{4} \Gamma_{\mu}^2}$$

partial widths

$$\Delta \sigma_{ab} = \sigma_a^{\text{comp}}(E) \cdot \frac{\Gamma_{jb}}{\Gamma_{\mu}}$$

• overlapping resonances:

contributions of many resonances interfere  $\rightarrow$  fluctuations

Baut-Wigner-formula cannot be used

$\triangleright$  above formula is taken over for average XS:

$$\langle \sigma_{ab} \rangle = \langle \sigma_a^{\text{comp}} \rangle \frac{\langle \Gamma_{\mu b} \rangle}{\langle \Gamma_{\mu} \rangle}$$

$$\sum_i \langle \Gamma_{\mu i} \rangle = \langle \Gamma_{\mu} \rangle$$

averages with respect to  $\mu$

independence of formation and decay

Bohr's hypothesis

experimental evidence for Bohr's hypothesis: Ghoshal experiment

$$\frac{\langle \sigma_{ab} \rangle}{\langle \sigma_{ac} \rangle} = \frac{\langle \sigma_{db} \rangle}{\langle \sigma_{dc} \rangle} \quad \text{for equal exc. en. of CN}$$

Now use:  $k_a^2 \langle \sigma_{ab} \rangle = k_b^2 \langle \sigma_{ba} \rangle$  reciprocity  $\&$  time reversal invarian

for same exc. en. of CN

$$\frac{k_a^2 \langle \sigma_a^{\text{comp}} \rangle \langle \Gamma_{\mu b} \rangle}{\langle \Gamma_{\mu} \rangle} = \frac{k_b^2 \langle \sigma_b^{\text{comp}} \rangle \langle \Gamma_{\mu a} \rangle}{\langle \Gamma_{\mu} \rangle}$$

$$\frac{\langle \Gamma_{\mu a} \rangle}{k_a^2 \langle \sigma_a^{\text{comp}} \rangle} = \frac{\langle \Gamma_{\mu b} \rangle}{k_b^2 \langle \sigma_b^{\text{comp}} \rangle} = f(E, J, \Pi) \quad \text{channel independent}$$

$$\langle \Gamma_{\mu a} \rangle = k_a^2 \langle \sigma_a^{\text{comp}} \rangle \cdot f(E, J, \Pi)$$

$$\langle \sigma_{ab} \rangle = \langle \sigma_a^{\text{comp}} \rangle \frac{k_b^2 \langle \sigma_b^{\text{comp}} \rangle}{\sum k_c^2 \langle \sigma_c^{\text{comp}} \rangle}$$

$$\text{definition: } T_a = \frac{k_a^2}{\pi} \sigma_a^{\text{comp}}$$

$$\triangleright \langle \sigma_{ab} \rangle = \frac{\pi}{k_a^2} T_a \frac{T_b}{\sum T_c} \quad (\ast)$$

factors that characterize formation and decay are determined by the same quantities

transmission coefficients

observable XS : ( $\ast$ ) summed over many channels  $\rightarrow$  Faust-Feshbach formula

## II) SPHERICAL OPTICAL MODEL (CALCULATIONS)

### 1) General description of the problem

$$\text{Schrödinger equation: } [-\frac{\hbar^2}{m} \nabla^2 + V] \Psi = E \Psi$$

$$\mu = \frac{m_i m_t}{m_i + m_t}$$

$$E = E_{lab} \cdot \frac{m_t}{m_i + m_t} \quad \text{C.M. energy}$$

$$\text{Optical potential: } V = V_{\text{coul}}(r) + V_{CR}(r) + i V_{CI}(r) + \{V_{SR}(r) + i V_{SI}(r)\} + (\vec{J}, \vec{L}) \cdot \vec{S}$$

central, real       $\vec{J} \cdot \vec{S} + \vec{L}$

inc. part.      rel. motion

other terms have also been considered, seem to play a minor part  
separation of the variables  $\Rightarrow$  radial equation:

$$\frac{d^2}{dr^2} - \frac{l(l+1)}{r^2} + \frac{k^2}{E} [E - (V_{\text{coul}}(r) + V_{CR}(r) + i V_{CI}(r)) - (V_{SR}(r) + i V_{SI}(r))] k^2 (j(j+1) - l(l+1) - s(s+1))/2] u_l^1(r) = 0$$

$u_l^1(r)$  ... radial wave function, must satisfy the following boundary condition

- must vanish at the origin
- asymptotic form of the solution should in principle be matched to a plane wave plus an outgoing wave

in the actual case: solution is matched to a linear combination of regular and outgoing Coulomb wave functions at radius  $r_m$  beyond which the nuclear potential is sufficiently small:

$$u_l^1(r) = F_l(\eta, kr_m) + C_l [G_l(\eta, kr_m) + i F_l(\eta, kr_m)]$$

$F$  ... regular } normalized Coulomb wave functions

$G$  ... irregular }

$$\eta = \mu \frac{z z' e^2}{\hbar k}$$

$Z$  ... incident } particle charge number

$Z'$  ... target }

$$C_l^d = -\frac{i}{2} [ \exp(2i\delta_l) - 1 ] = -\frac{i}{2} [\gamma_l^d - 1]$$

phase shift                    absorption coefficient

total reaction cross section:

$$\sigma_R = \frac{4\pi}{(2s+1)k} \sum_{l=0}^{\infty} \sum_{j=|l-s|}^{l+s} (2j+1) \{ \operatorname{Im} C_l^d - |C_l^d|^2 \}$$

angular distributions: scattering amplitudes are expressed in terms of Legendre coefficients; expansion coefficients are functions of  $C_l^d$

### Potential terms in radial Schrödinger equation:

1) Coulomb pot.: Term ( $\lambda$ ) usually taken to correspond to a constant charge density within the nucleus extending to a distance  $a_c = R_c m_t^{1/3}$

$$V_{\text{coul}}(\lambda) = \begin{cases} (ZZ'e^2/2r_c)(3-\lambda^2/a_c^2) & \text{for } \lambda \leq a_c \\ ZZ'e^2/\lambda & \text{for } \lambda \geq a_c \end{cases}$$

other forms suggested; in practice little effect on the final results

2) Central real nuclear potential:  $V_{\text{cpl}}(\lambda)$ , usually Saxon-Woods

$$V_{\text{cpl}}(\lambda) = V_0 \left[ 1 + \exp(\lambda - \lambda_R)/\alpha_R \right]^{-1}$$

$$V < 0 \quad \lambda_R = R_R m_t^{1/3}$$

for attractive potential

### 3) Central imaginary nuclear potential : $V_{CI}(r)$

- Volume absorption : Woods - Saxon

$$V_{CI}(r) = W_v \left[ 1 + \exp((r - R_I)/a_I) \right]^{-1}$$

- Surface absorption :

- Gaussian absorption :  $V_{CI}(r) = W_s \exp\left[-((r - R_I)/b)^2\right]$

- Derivative absorption :  $V_{CI}(r) = \alpha_I W_s \left[ -\frac{d}{dr} \left( 1 + \exp((r - R_I)/a_I) \right) \right]$

$W_s, W_v < 0$  for an absorptive potential

$$R_I = R_I m_t^{1/3}$$

both forms of surface absorption have also been combined with a volume absorption

### 4) Spin orbit potential : usually assigned a Thomas factor :

$$V_{SO}(r) = V_{SO} \left( \frac{2}{\pi r} \right) \left( -\frac{d}{dr} \left[ 1 + \exp((r - R_I)/a_I) \right]^{-1} \right)$$

$$V_{SI}(r) = W_{SO} \left( \frac{2}{\pi r} \right) \left( -\frac{d}{dr} \left[ 1 + \exp((r - R_I)/a_I) \right]^{-1} \right)$$

#### Parameters of the model

$R_C$  .... Coulomb radius parameter

$R_R$  .... real potential radius parameter

$R_I$  .... imag. -" -" -" -"

$a_R$  .... real potential surface parameter

$a_I$  .... imag. -" -" -" -"

$b$  .... Gaussian absorption width

$V$  .... real potential depth

$W_v$  .... volume } absorption potential depth

$W_s$  .... surface }

$V_{SO}$  .... real } spin-orbit potential depth

$W_{SO}$  .... imag. }

} geometrical parameters

} dynamic parameters

several of these parameters are usually related to each other

## 2) Comparison with experimental data

Comparison of the fits to the experimental data obtained with various sets of DM parameters may be given quantitatively by

$$\chi^2_{\sigma} = \sum_{i=1}^N \left[ (\sigma(\theta_i) - \sigma^*(\theta_i)) / \Delta \sigma^*(\theta_i) \right]^2$$

$\sigma^*(\theta_i)$  ... experimental differential XS at  $\theta_i$

$\Delta \sigma^*(\theta_i)$  ... experimental error

similar for polarization:  $\chi^2_p$

total  $\chi^2$ :  $\chi^2 = \chi^2_{\sigma} + \chi^2_p$

[spin 1:  $\chi^2 = \chi^2_{\sigma} + \sum \chi^2_p$ ]

$\chi^2$  criterion can be modified to take into account experimental uncertainties in the overall normalization of the data

→ divide data by renormalization factor  $\lambda$  which is chosen so as to minimize  $\chi^2$ ; permissible range  $\Delta \lambda^*$  should be specified as an experimental uncertainty about a given value  $\lambda^*$ :

$$\chi^2(\lambda) = \sum \left[ \lambda \sigma(\theta_i) - \sigma^*(\theta_i) \right] / \Delta \sigma^*(\theta_i)]^2 + [\lambda - \lambda^*] / \Delta \lambda^* ]^2$$

$$\chi^2_{\sigma} = \min_{\lambda} \chi^2(\lambda)$$

two further sources of errors in the experimental  $\theta_i$  can also be included in the  $\chi^2$  criterion:

- detector width

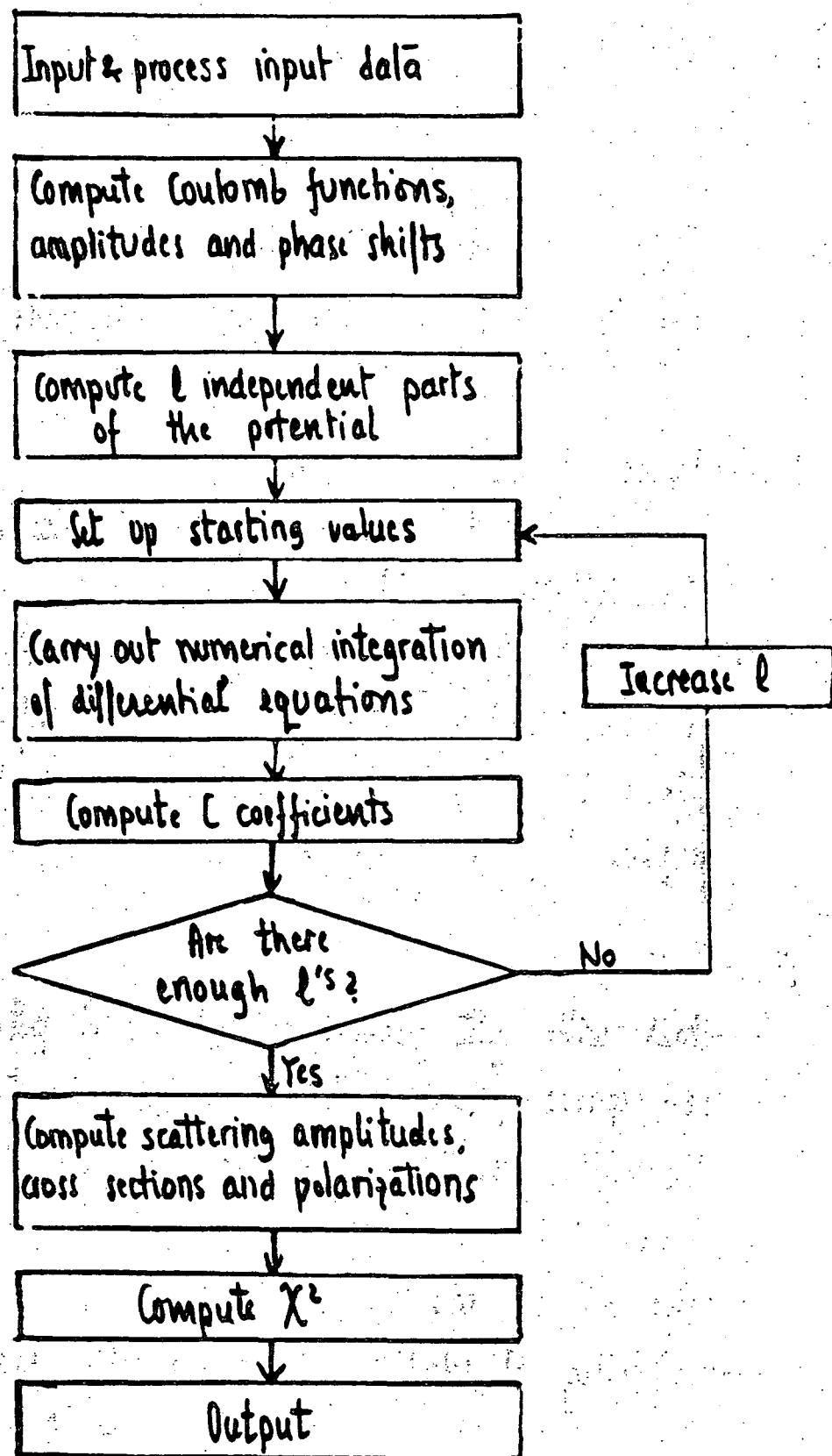
- exp. uncertainty in the measured  $\theta_i$

## Types of exp. data that may be used for comparison

- total cross section  $\sigma_t$  as fct. of inc. energy
- total elastic cross section  $\sigma_E$  — " —
- reaction cross section  $\sigma_R$  — " —
- differential elastic cross section  $\frac{d\sigma}{d\omega}$  as fct. of angle at various inc. energies
- polarizations  $P(\theta)$  as fct. of angle at various inc. energies
- strength functions  $S_1$  (mostly  $S_0$  and  $S_1$ ); ref to 1 eV

### 3) General flow chart of the program for a single run calculation

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### III) COUPLED CHANNELS OPTICAL MODEL CALCULATIONS

#### 1) Introduction

inelastic scattering: involved interactions sometimes much stronger than in transmutation reactions

→ DWBA poor approximation

improvement - higher order BA  $\rightarrow$  involved task  
- CCC

Advantages of CCC:

- interaction is treated exactly within the channels considered ("to infinite order")
- certain low-lying states of collective nature (higher phonon state in vibrational nuclei; higher members of rotational bands of deformed nuclei) cannot be excited in single step process  $\rightarrow$  would require higher order BA

Formulation:

- start with quite general optical model potential (non-spherical)
- re-express potentials in some approximate ways, the way depending on the nature of the target  $\Rightarrow$  derive coupling terms between different channels
- solve set of coupled equations
- matching of solutions to asymptotic wave functions  
 $\Rightarrow$  S matrix elements
- compute XS from S matrix elements

[If target nucleus well deformed and energy of incident particle sufficiently high  $\rightarrow$  adiabatic approximation.]

## 2) The interaction potential

(CC required only if (direct or indirect) couplings between excited and ground state channels are strong, i.e. when the low lying states of the target nucleus have a strong collective nature)

$$V(r, \theta, \phi) = -(V + iW) \frac{1}{1 + \exp[(r - R)/\bar{a}]} \quad \text{real & vol. imag. : SW}$$

$$- 4iW_D \frac{\exp[(r - \bar{R})/\bar{a}]}{\{1 + \exp[(r - \bar{R})/\bar{a}]\}^2} \quad \text{surface imag. : de.SW}$$

$$- V_{SO}(\vec{S}, \vec{l}) \hat{z}_n \text{ or } \frac{1}{\{1 + \exp[(r - R)/\bar{a}]\}^2} \quad \text{spin-orbit : Thomas}$$

$$+ V_{\text{coul}} \quad \text{Coulomb}$$

if  $R$  and  $\bar{R}$  independent of angle: spherical OM

if  $R$  and  $\bar{R}$  dependent on angle: deformed OM



according to collective nature of target nucleus:

$\Delta$  spherically symmetric, but susceptible to vibrations around spherical shape:  $R = R_0(1 + \sum_{\lambda p} \alpha_{\lambda p} Y_{\lambda p}(\theta, \phi))$

$$\bar{R} = \bar{R}_0(1 + \sum_{\lambda p} \alpha_{\lambda p} Y_{\lambda p}(\theta, \phi))$$

$\Delta$  axially symmetric deformed nucleus:

$$R = R_0(1 + \sum_{\lambda} \beta_{\lambda} Y_{2\lambda}(0'))$$

$$\bar{R} = \bar{R}_0(1 + \sum_{\lambda} \beta_{\lambda} Y_{2\lambda}(0'))$$

$R_0 = k_0 A^{1/3}$
$\bar{R}_0 = \bar{k}_0 A^{4/3}$

$0'$  refers to body fixed system

impractical to solve scattering problem subject to the above potential with their expressions for radii  $\Rightarrow$  plausible approximations:

## Vibrational nucleus :

$$f(\lambda) = \left\{ 1 + \exp \left[ (\lambda - R)/a \right] \right\}^{-1} = \left\{ 1 + \exp \left[ (\lambda - R_0 (1 + \sum_{\lambda_p} \alpha_{\lambda_p} Y_{\lambda_p}(\theta, \phi))) / a \right] \right\}^{-1}$$

$$g(\lambda) = \exp \left[ (\lambda - \bar{R}) / \bar{a} \right] \cdot \left\{ 1 + \exp \left[ (\lambda - \bar{R}) / \bar{a} \right] \right\}^{-2} =$$

$$= \left\{ 1 + \exp \left[ (\lambda - \bar{R}_0 (1 + \sum_{\lambda_p} \alpha_{\lambda_p} Y_{\lambda_p}(\theta, \phi))) / \bar{a} \right] \right\}^{-2} \cdot \exp \left[ (\lambda - \bar{R}_0 (1 + \sum_{\lambda_p} \alpha_{\lambda_p} Y_{\lambda_p})) / \bar{a} \right]$$

Notation:  $\Sigma = \sum_{\lambda_p} \alpha_{\lambda_p} Y_{\lambda_p}$

$$e = \exp \left[ (\lambda - R_0) / a \right]$$

$$\bar{e} = \exp \left[ (\lambda - \bar{R}_0) / \bar{a} \right]$$

$\triangleright f(\lambda) = \left\{ 1 + \exp \left[ \frac{\lambda - R_0}{a} - \frac{R_0}{a} \Sigma \right] \right\}^{-1} = \left\{ 1 + e \cdot \exp \left[ -\frac{R_0}{a} \Sigma \right] \right\}^{-1} = F(\Sigma)$

expand around  $\Sigma = 0$

$$F(\Sigma) = \left\{ 1 + e \cdot \exp \left[ -\frac{R_0}{a} \Sigma \right] \right\}^{-1}$$

$$\frac{dF(\Sigma)}{d\Sigma} = e \frac{R_0}{a} \exp \left[ -\frac{R_0}{a} \Sigma \right] \cdot \left\{ 1 + e \exp \left[ -\frac{R_0}{a} \Sigma \right] \right\}^{-2}$$

$$\left. \frac{dF(\Sigma)}{d\Sigma} \right|_{\Sigma=0} = e \frac{R_0}{a} (1+e)^{-2}$$

$$\begin{aligned} \frac{d^2F(\Sigma)}{d\Sigma^2} &= -e \frac{R_0^2}{a^2} \exp \left[ -\frac{R_0}{a} \Sigma \right] \cdot \left\{ (1+e)^{-2} + 2e^2 \frac{R_0^2}{a^2} \exp \left[ -\frac{R_0}{a} \Sigma \right] \right\}^{-3} = \\ &= e \frac{R_0^2}{a^2} \exp \left[ -\frac{R_0}{a} \Sigma \right] \cdot \left[ -\left\{ (1+e)^{-2} + 2e^2 \exp \left[ -\frac{R_0}{a} \Sigma \right] \right\}^{-3} \right] \end{aligned}$$

$$\begin{aligned} \left. \frac{d^2F(\Sigma)}{d\Sigma^2} \right|_{\Sigma=0} &= e \frac{R_0^2}{a^2} \left[ -(1+e)^{-2} + 2e(1+e)^{-3} \right] = e \frac{R_0^2}{a^2} (1+e)^{-3} (-1-e+2e) = \\ &= e \frac{R_0^2}{a^2} (e-1)(1+e)^{-3} \end{aligned}$$

$$F(\Sigma) = F(0) + \left. \frac{dF}{d\Sigma} \right|_{\Sigma=0} \cdot \Sigma + \frac{1}{2} \left. \frac{d^2F}{d\Sigma^2} \right|_{\Sigma=0} \cdot \Sigma^2 =$$

$$= (1+e)^{-1} + e \frac{R_0}{a} (1+e)^{-2} \Sigma + \frac{1}{2} e \frac{R_0^2}{a^2} (e-1)(1+e)^{-3} \Sigma^2$$

analogous for  $g(r)$ , with expansions for  $f(\lambda)$  and  $g(\lambda)$  in potentials, leads to:

$$\begin{aligned}
 V(\lambda, \theta, \phi) = & \frac{(V+iW)(1+e)^{-1} - 4iW_D \bar{e}(1+e)^{-2} - V_{SO} (\bar{\sigma} \cdot \bar{l}) (\bar{\lambda}_\mu^2 / \alpha r) e(1+e)^{-2}}{1} \\
 & + \left\{ (V+iW) \frac{R_0}{a} e(1+e)^{-2} - 4iW_D \frac{R_0}{a} \bar{e}(1-\bar{e})(1+\bar{e})^{-3} \right\} \sum_{\lambda\mu} \alpha_{\lambda\mu} Y_{\lambda\mu} + \\
 & + \left\{ (V+iW) \frac{R_0^2}{a^2} e(1-e)(1+e)^{-3} - 4iW_D \frac{R_0^2}{2a^2} \bar{e}(1-4\bar{e}+\bar{e}^2)(1+\bar{e})^{-4} \right\} \left( \sum_{\lambda\mu} \alpha_{\lambda\mu} Y_{\lambda\mu} \right)^2 + \\
 & + V_{coul}
 \end{aligned}$$

Use following relation:

$$\left( \sum_{\lambda\mu} \alpha_{\lambda\mu} Y_{\lambda\mu} \right)^2 = \sum_{\lambda\lambda''} \frac{1_{2\lambda'+1} \sqrt{2\lambda''+1}}{\sqrt{4\pi} \sqrt{2\lambda+1}} (\lambda'' \otimes \lambda'') | \lambda \rangle \sum_{\mu} Y_{\lambda\mu} \underbrace{(\alpha_{\lambda'} \otimes \alpha_{\lambda''})}_{\text{vector addition}} | \lambda \mu \rangle$$

$$\text{vector addition } (\alpha_{\lambda'} \otimes \alpha_{\lambda''})_{\lambda\mu} = \sum_{\mu'\mu''} (\lambda'' \otimes \lambda')_{\mu'\mu''} | \lambda\mu \rangle \alpha_{\lambda'\mu'} \alpha_{\lambda''\mu''}$$

Specify Coulomb interaction:

$$\begin{aligned}
 V_{coul} &= ZZ' \epsilon^2 \int \rho(r', \theta', \phi') |\vec{r} - \vec{r}'|^{-1} dr' = \\
 &= 4\pi Z Z' \epsilon^2 \sum_{\lambda\mu} \int \rho(r', \theta', \phi') (2\lambda+1) n_r^{\lambda} n_s^{-\lambda} Y_{\lambda\mu}(\theta', \phi') Y_{\lambda\mu}^*(\theta, \phi) n'' dr' d\theta' d\phi'
 \end{aligned}$$

using expansion of  $|\vec{r} - \vec{r}'|^{-1}$  in spher. harmonics

$$\text{where } n_r^{\lambda} n_s^{-\lambda} = n^{\lambda} (n')^{-(\lambda+1)} \theta(n'-n) + n'^{\lambda} n^{-\lambda} \theta(n-n')$$

charge distribution in the target is assumed to be constant within the cb radius  $R_c(\theta', \phi')$  and zero outside:

$$\rho(r', \theta', \phi') = \frac{3}{4\pi R_c^3} \theta(R_c(\theta', \phi') - r')$$

$$\text{const. radius vibration: } R_c(\theta, \phi) = R_c(1 + \sum_{\lambda\mu} \alpha_{\lambda\mu} Y_{\lambda\mu})$$

$$\Rightarrow \rho(r', \theta', \phi') = \underbrace{\frac{3}{4\pi R_c^3} \theta(R_c(1 + \sum_{\lambda\mu} \alpha_{\lambda\mu} Y_{\lambda\mu}(\theta, \phi')) - r')}_{\text{use this expression in the above integral}}$$

use this expression in the above integral

$$\begin{aligned}
 V_{coul} &= \frac{Z Z' \epsilon^2}{R_c^3} \sum_{\lambda\mu} \frac{Y_{\lambda\mu}(\theta, \phi)}{2\lambda+1} \int Y_{\lambda\mu}^*(\theta, \phi') \theta(R_c(1 + \sum_{\lambda\mu} \alpha_{\lambda\mu} Y_{\lambda\mu}(\theta, \phi')) - r') \left[ n^{\lambda} (n')^{-(\lambda+1)} \theta(n'-n) + n'^{\lambda} n^{-\lambda} \theta(n-n') \right] \\
 &\quad \cdot n'' dr' d\theta' d\phi' =
 \end{aligned}$$

$$\begin{aligned}
 &= \frac{3Z^2' \epsilon^2}{R_c^3} \sum_{\lambda\mu} \frac{Y_{2\mu}(\theta, \phi)}{2\lambda+1} \int_0^\pi d\theta' \sin\theta' \int_0^{2\pi} d\phi' \int dr' n'' Y_{2\mu}^*(\theta', \phi') R_c(\theta', \phi') \\
 &\quad \cdot [n^2(x')^{-(\lambda+1)} \Theta(x'-n) + n'^2 n^{-(\lambda+1)} \Theta(n-x')] = \\
 &= \frac{3Z^2' \epsilon^2}{R_c^3} \sum_{\lambda\mu} \frac{Y_{2\mu}(\theta, \phi)}{2\lambda+1} \int_0^\pi d\theta' \sin\theta' \int_0^{2\pi} d\phi' Y_{2\mu}^*(\theta', \phi') \left\{ \Theta(R_c(\theta', \phi') - n) \int dr' n^2(x')^{-(\lambda+1)} + \right. \\
 &\quad \left. + \Theta(R_c(\theta', \phi') - n) \int dr'(x')^{\lambda+2} n^{-(\lambda+1)} + \Theta(n - R_c(\theta', \phi')) \int dr'(r')^{\lambda+2} n^{-(\lambda+1)} \right\} = \\
 &= \frac{3Z^2' \epsilon^2}{R_c^3} \sum_{\lambda\mu} \frac{Y_{2\mu}(\theta, \phi)}{2\lambda+1} \int d\Omega' Y_{2\mu}^*(\Omega') \left\{ \Theta(R_c - n) \frac{n^\lambda}{2-\lambda} [R_c(\Omega')^{-\lambda+2} - n^{-\lambda+2}] + \underline{\underline{II}} + \underline{\underline{III}} \right\}.
 \end{aligned}$$

neglecting angle dependence of  $\theta$  fct.

$$\begin{aligned}
 &= \frac{3Z^2' \epsilon^2}{R_c^3} \sum_{\lambda\mu} \frac{Y_{2\mu}(\theta, \phi)}{2\lambda+1} \int d\Omega' Y_{2\mu}^*(\Omega') \left\{ \frac{\Theta(R_c - n)}{2-\lambda} \left[ n^\lambda R_c^{-\lambda+2} \left( (1 + \sum_{\lambda' \neq \lambda} \alpha_{2\mu} Y_{2\mu}(\Omega'))^{-\lambda+2} - n^{-\lambda+2} \right) \right] + \right. \\
 &\quad \left. + \underline{\underline{II}} + \underline{\underline{III}} \right\}
 \end{aligned}$$

leads to:

$$\begin{aligned}
 V_{\text{coupl}} &= \frac{3Z^2' \epsilon^2}{2R_c} \left[ 3 - \frac{n^2}{R_c^2} \right] \Theta(R_c - n) + \frac{3Z^2' \epsilon^2}{n} \Theta(n - R_c) + \\
 &+ \sum_{\lambda\mu} \frac{3Z^2' \epsilon^2}{2\lambda+1} \left[ n^\lambda R_c^{-(\lambda+1)} \Theta(R_c - n) + R_c^\lambda n^{-(\lambda+1)} \Theta(n - R_c) \right] (\alpha_{2\mu} Y_{2\mu}) + \\
 &+ \sum_{\lambda\mu} \frac{3Z^2' \epsilon^2}{2\lambda+1} \left[ (-\lambda) n^\lambda R_c^{-\lambda+1} \Theta(R_c - n) + (\lambda+2) R_c^\lambda n^{-\lambda+1} \Theta(n - R_c) \right] \\
 &+ \frac{1}{2\lambda''} \sum_{\lambda''} \frac{(2\lambda+1)(2\lambda''+1)}{4\pi(2\lambda+1)} (\lambda'' \alpha_{2\mu} Y_{2\mu}) \sum_{\mu} (\alpha_{2\mu} \Theta \alpha_{2\mu}) Y_{2\mu}
 \end{aligned}$$

$$V(\alpha, \theta, \phi) = \underbrace{V_{\text{diag}}}_{\text{vibrational}} + \underbrace{V_{\text{coupl}}}_{\text{vibrational}}$$

No  $Y_{2\mu}$  linear or quadratic in  $Y_{2\mu}$

$$\begin{aligned}
 \Delta V_{\text{diag}} &= -(V+iW)(1+\epsilon)^{-1} - 4iWg \bar{e}(1+\bar{e})^{-2} - U_{SO} \frac{d\pi}{dr} (\bar{\sigma} \bar{L}) \epsilon (1+\epsilon)^{-2} + \\
 &+ \frac{3Z^2' \epsilon^2}{2R_c} \left( 3 - \frac{n^2}{R_c^2} \right) \Theta(R_c - n) + \frac{3Z^2' \epsilon^2}{n} \Theta(n - R_c)
 \end{aligned}$$

$$V_{\text{coupl}}^{(v)} = \sum_{\lambda\mu} V_{\text{cp};\lambda}^{(1)(v)} (\alpha_{2\mu} Y_{2\mu}) + \sum_{\lambda\lambda'\lambda''} V_{\text{cp};\lambda}^{(3)(v)} \left( \frac{(2\lambda+1)(2\lambda'+1)}{4\pi(2\lambda+1)} \right) (\alpha_{2\lambda} \alpha_{2\lambda'} \alpha_{2\lambda''}) Y_{2\mu}$$

with:

$$V_{cp;2}^{(1)(*)}(n) = - \left\{ (V+iW) \frac{R_0}{a} e(1-e)^{-2} - 4iW_0 \frac{\bar{R}_0}{a} \bar{e}(1-\bar{e})(1+\bar{e})^{-3} \right\} + \\ + \frac{322'\epsilon^2}{2\lambda+1} \left\{ n^2 R_c^{-\lambda-1} \theta(R_c-n) + R_c^2 n^{-\lambda-1} \theta(n-R_c) \right\}$$

$$V_{cp;2}^{(2)(*)}(n) = (V+iW) \frac{R_0^2}{2a^2} e(1-e)(1+e)^{-3} - 4iW_0 \frac{\bar{R}_0^2}{2\bar{a}^2} \bar{e}(1-4\bar{e}+\bar{e}^2)(1+\bar{e})^{-4} + \\ + \frac{322'\epsilon^2}{2\lambda+1} \left\{ (1-\lambda)n^2 R_c^{-\lambda-1} \theta(R_c-n) + (\lambda+2)R_c^2 n^{-\lambda-1} \theta(n-R_c) \right\}$$

$V_{\text{diag}}$  ... diagonal with respect to ang. mom.  $j$  of the projectile and angular spin  $I$  of the target nucleus  
= usual optical model potential

$V_{\text{coupl}}^{(*)}$  ... coupling potential between channels with different  $j$  and  $I$

## Rotational nuclei

Use  $\left\{ \begin{array}{l} R = R_0(1 + \sum \beta_2 Y_{20}(\theta')) \\ \bar{R} = \bar{R}_0(1 + \sum \beta_2 Y_{20}(\theta')) \end{array} \right\}$  in expression for potential, expand potential in powers of  $\sum \beta_2 Y_{20}(\theta')$ , leads to exactly the same expressions as for vibrational nucleus except that  $\alpha_{20}$  and  $Y_{1p}(\theta, \phi)$  are replaced by  $\beta_2$  and  $Y_{20}(\theta')$ .

Replace  $Y_{20}(\theta')$  by  $\sum_p J_{p0}^2(\theta_i) Y_{2p}(\theta, \phi)$   
in body fixed system       $\underbrace{\text{station matrix}}_{\text{in space fixed system}}$       Euler angles

diagonal elements of coupling pot: linear term has vanishing  
- " - " - for vibrational nucleus, nonvanishing for  
rotational nucleus

expanding potential in powers of  $\sum \beta_\lambda Y_{\lambda 0}(\theta')$  and retaining a few of its leading terms may be a poor approximation when  $\beta_\lambda$  is large ( $\sim 0.3$ ) as is the case in many actual deformed nuclei.

$\Rightarrow$  expansion of potential not in powers of  $\sum \beta_\lambda Y_{\lambda 0}(\theta')$  but in terms of Legendre polynomials

for nuclear part:

$$V(r) = -(V+iW) \left[ 1 + \exp\left(\frac{r-R_0(1+\sum \beta_\lambda Y_{\lambda 0}(\theta'))}{a}\right) \right]^{-1} - 4iW_0 \exp\left[\frac{r-\bar{R}_0(1+\sum \beta_\lambda Y_{\lambda 0}(\theta'))}{a}\right] \left\{ 1 + \exp\left[\frac{r-\bar{R}_0(1+\sum \beta_\lambda Y_{\lambda 0}(\theta'))}{a}\right] \right\}$$

$$= \sum_{\lambda'} f_{\lambda'}(r) P_{\lambda'}(\cos \theta') = \sum_{\lambda'} f_{\lambda'}(r) \sqrt{\frac{4\pi}{2\lambda'+1}} Y_{\lambda' 0}(\theta') \quad (\Phi)$$

$$f_{\lambda'}(r) = 4\pi \int Y_{\lambda' 0}(\theta') V(\bar{a}) d\cos \theta' =$$

$$= -4\pi (V+iW) \int d\cos \theta' Y_{\lambda' 0}(\theta') \left[ 1 + \exp\left(\frac{r-R_0(1+\sum \beta_\lambda Y_{\lambda 0}(\theta'))}{a}\right) \right]^{-1} -$$

$$- 4iW_0 \int d\cos \theta' Y_{\lambda' 0}(\theta') \exp\left(\frac{r-\bar{R}_0(1+\sum \beta_\lambda Y_{\lambda 0}(\theta'))}{a}\right) \left[ 1 + \exp\left(\frac{r-\bar{R}_0(1+\sum \beta_\lambda Y_{\lambda 0}(\theta'))}{a}\right) \right]$$

with  $\lambda' = 0$  this is diagonal part of nuclear part; add other terms (SO, CB)

$$V_{\text{diag}} = \sqrt{4\pi} \left\{ \frac{-(V+iW)}{1 + \exp[(r-R_0(1+\sum \beta_\lambda Y_{\lambda 0}(\theta')))/a]} + \frac{-4iW_0 \exp[(r-\bar{R}_0(1+\sum \beta_\lambda Y_{\lambda 0}(\theta')))/\bar{a}]}{\{1 + \exp[(r-\bar{R}_0(1+\sum \beta_\lambda Y_{\lambda 0}(\theta')))/\bar{a}]\}^2} \right\} d\cos \theta'$$

$$- V_{SO} \frac{\hat{\tau}_{\perp}^2}{ar} (\vec{\sigma}, \vec{l}) e(l+e)^2 + \frac{ze'^2}{2R_c} (3 - \frac{z^2}{R_c^2}) \Theta(R_c - r) + \frac{ze'^2}{a} \Theta(a - R_c)$$

Now  $Y_{\lambda 0}(\theta') = \sum_i D_{\mu 0}^{\lambda}(\theta_i) Y_{\lambda \mu}(\theta, \phi)$  in  $(\Phi)$ :

$$V(r) = \sum_{\lambda'} f_{\lambda'}(r) \sum_{\mu} D_{\mu 0}^{\lambda'}(\theta_i) Y_{\lambda' \mu}(\theta, \phi)$$

With  $\lambda' \neq 0$ : coupling part of nuclear potential

$$V_{\text{coupl}} = \sum_{\lambda' \neq 0} v_{cp}^{(\lambda)(\mu)}(r) D_{\mu 0}^{\lambda} Y_{\lambda' \mu}(\theta, \phi)$$

(rotational)

$$v_{cp}^{(\lambda)(\mu)} \propto f_{\lambda'}(r)$$

in particular:

$$V_{cp}^{(2)(r)}(n) = 4\pi \left\{ \frac{-(V+iW)}{1+\exp[(r-R_0(1+\sum_x \beta_x Y_{x0}(\theta')))/a]} + \frac{-4iW_0 \exp[r-\bar{R}_0(1+\sum_x \beta_x Y_{x0}(\theta'))]/a}{\{1+\exp[r-\bar{R}_0(1+\sum_x \beta_x Y_{x0}(\theta'))]/a\}^2} \right. \\ \left. * Y_{20}(\theta') \cos \theta' \right\}$$

(l) part in coupling potential: power series expansion is sufficiently good approximation  $\rightarrow$  as for vibrational nucleus except that  $\alpha_{2\mu} Y_{2\mu}$  must be replaced by  $\beta_\lambda D_{\mu} Y_{2\mu}$

### 3) The coupled equations

$I_n, \pi_n, \omega_n \dots$  spin, parity and energy of  $n^{\text{th}}$  target state,  $n=1, \dots N$ .  
coupled strongly (directly or indirectly)  
to ground state by  $V_{\text{coupl}}$

incident particle:  $E, \dots$  C.M. energy

energy of particle which leaves target in its  $n^{\text{th}}$  state:  $E_n = E_i - \omega_n$

counder channel corresponding to  $n^{\text{th}}$  state of target,  
particle spin  $\vec{s}$ , tot. ang. mom.:  $\vec{l}_n$ , total ang. mom.  $\vec{j}_n = \vec{s} + \vec{l}_n$ ,

ang. mom. and parity of whole system:

$$\vec{J} = \vec{I}_n + \vec{j}_n \quad \vec{\Pi} = \pi_n (-)^{l_n} \quad (\textcircled{S})$$

with the interaction described by the coupling potentials, none  
of  $I_n, j_n, I_n, \pi_n$  or  $(-)^{l_n}$  is a good quantum number, but  
 $J$  and  $\Pi$  are good

$\Rightarrow$  partial waves whose  $I_n$  and  $j_n$  satisfy  $(\textcircled{S})$  [or given  $J\Pi$ ]  
are coupled together through coupling potential to form a set of  
coupled differential equations

number of  $(l_n, j_n)$  coupled to a given  $J\pi : n_c^{(n)}$

maximum possible number :  $N_c^{(n)}$

for given $I_n$ :	$N_c^{(n)} = I_n + 1$	$s=0$ and $I_n$ is an integer
	$= I_n + \frac{1}{2}$	$s=0$ $I_n$ half odd integer
	$= 2I_n + 1$	$s = \frac{1}{2}$ all $I_n$
	$= 3I_n + 2$	$s=1$ $I_n$ integer
	$= 3I_n + \frac{3}{2}$	$s=1$ $I_n$ half odd integer

total number of coupled partial waves for given  $J\pi : n_c = \sum_{n_s}^{N_s} n_c^{(n)}$   
 max. " "  $N_c = \sum_{n_s}^{N_s} N_c^{(n)}$

terminology :

"partial wave channel" ... particular  $(l_n, j_n)$

" $n^{\text{th}}$  state channel" ...  $n_c^{(n)}$  values  $(l_n, j_n)$

in calculations :  $J = J_{\min} (0 \text{ or } \frac{1}{2}) \dots J_{\max} = J_i + j_{\max}$  for each  $\pi$

max.  $j_s$  of the partial wave that gives non-negligible contribution  
to (elastic) scattering

Hamiltonian:

$$\mathcal{H} = T + \mathcal{H}_t + V(z, \theta, \phi) = T + \mathcal{H}_t + V_{\text{diag}} + V_{\text{coupl}}$$

| internal motion of the target  
kinetic energy of inc. particle

$$\text{Schrödinger eq.: } \mathcal{H} \Psi = E \Psi$$

energy of inc. particle

total wave function:  $\Psi = \tilde{r}^{-1} \sum_{J \in L_{\text{tot}}} R_{J \in L_{\text{tot}}}(\alpha) (Y_{L \in L_{\text{tot}}} \otimes \Phi_{I \in I})_{JM}$   
 radial part of relative motion

$$= \tilde{r}^{-1} \sum_{J \in L_{\text{tot}}} R_{J \in L_{\text{tot}}}(\alpha) \sum_{m_I M_I} (j_u I_m m_I M_I | JM) Y_{L \in L_{\text{tot}}, m_I} \Phi_{I \in I, M_I}$$

where  $Y_{L \in L_{\text{tot}}, m_I} = \sum_{m_S m_S} (l_S m_S m_S l_S m_S) i^L Y_{L, m_S} \chi_{S, m_S}$   
 spin of projectile  
 angular part of rel. motion

target states  $\mathcal{H}_t \Phi_{I \in I, M_I} = \omega_n \Phi_{I \in I, M_I}$  wave fn. of target in its  $n^{\text{th}}$  state

- insert expressions for  $\mathcal{H}$  and  $\Psi$  into Schrödinger equation
- multiply by  $(Y_{L \in L_{\text{tot}}} \otimes \Phi_{I \in I})_{JM}^*$  from the left
- integrate over all coordinates except  $r$
- divide by  $E_n$

$$\boxed{D \left( \frac{d^2}{dp_n^2} - \frac{l(l+1)}{p_n^2} - \frac{1}{E_n} V_{\text{diag}} + 1 \right) R_{J \in L_{\text{tot}}, j \in j}(\alpha) =}$$

$$- E_n^{-1} \sum_{m_I M_I} \langle (Y_{L \in L_{\text{tot}}} \otimes \Phi_{I \in I})_{JM} | V_{\text{coupl}} | (Y_{L \in L_{\text{tot}}} \otimes \Phi_{I \in I})_{JM} \rangle R_{J \in L_{\text{tot}}, j \in j(n)}$$

$$p_n = k_n e$$

$k_n$  ... wave number

set of  $n_c$  coupled equations,

quite general, holds irrespective of the nature of the projectile or the target  
 assumptions about nuclear structure only affect coupling matrix elements

evaluation of these is most crucial  
 part of the calculations!

General form of coupling term:

$$V_{\text{coupl}} = \sum_{t,\lambda} v_{\lambda}^{(t)}(\omega) (Q_{\lambda}^{(t)} \cdot Y_{\lambda})$$

$t$ ... character of term with given rank

$\lambda$ ... tensorial rank

$Q_{\lambda}^{(t)}$ ... operates only on the coordinate of the target nucleus

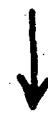
$$\langle (2j_I \otimes \Phi_I)_{JM} | V_{\text{coupl}} | (2j'_{I'} \otimes \Phi_{I'})_{JM} \rangle =$$

$$= \langle l_I I | V_{\text{coupl}} | l'_I I' \rangle =$$

$$= \sum_{t,\lambda} v_{\lambda}^{(t)}(\omega) \langle I \| Q_{\lambda}^{(t)} \| I' \rangle A(l_I, l'_I I', \lambda J_S)$$

reduced matrix element | geom factor (A matrix)  
contains all the dynamics | from combination of  $Y$  in  $V_{\text{coupl}}$   
involved in the problem | with  $Y$  in wave functions;

| separated by  $(J)$  symbols



defined by:

$$\langle IM_I | Q_{\lambda p}^{(t)} | I'M'_I \rangle = \langle I \| Q_{\lambda}^{(t)} \| I' \rangle \frac{1}{\sqrt{2I+1}} (I' \lambda M'_I \mu | IM_I)$$

Q Matrix

B matrix

Explicit form of reduced matrix elements for various cases

### A. Vibrational nucleus (even mass)

Comparing  $V_{\text{coupl}} = \sum_{t,\lambda} v_{\lambda}^{(t)}(\omega) (Q_{\lambda}^{(t)} \cdot Y_{\lambda})$

and  $V_{\text{coupl}}^{(v)} = \sum_{2p} v_{cp,2}^{(1)}(\omega) \alpha_{2p} Y_{2p} +$

$$+ \sum_{2\lambda_1, 2\lambda_2} v_{cp,2}^{(2)(+)}(\omega) \frac{(2\lambda_1+1)(2\lambda_2+1)}{4\pi(2\lambda+1)} (\lambda_1 \lambda_2 00/\lambda 0) \sum_J (\alpha_{\lambda_1} \otimes \alpha_{\lambda_2})_{2p} Y_{2p}$$

leads to  $Q_{\lambda\mu}^{(1)} = \alpha_{\lambda\mu}$

$$Q_{\lambda\mu}^{(2)} = \sum_{\lambda_1, \lambda_2} \frac{(2\lambda_1+1)(2\lambda_2+1)}{4\pi(2\lambda+1)} (\alpha_{\lambda_1} \otimes \alpha_{\lambda_2})_{\lambda\mu} \quad \left. \right\} (o)$$

express operator  $\alpha_{\lambda\mu}$  as sum of creation and annihilation operator:

$$\alpha_{\lambda\mu} = \beta_\lambda \sqrt{2\lambda+1} (b_{\lambda\mu} + (-)^{\lambda} b_{\lambda-\mu}^*)$$

$|0\rangle$  no-phonon (ground) state

(a) one phonon state  $|1; IM\rangle = b_{IM}^* |0\rangle$

(b) two phonon state  $|2; IM\rangle = (1 + \delta_{\lambda_1, \lambda_2})^{-\frac{1}{2}} (b_{\lambda_1}^* \otimes b_{\lambda_2}^*)_{IM} |0\rangle$

multipolarities  
of the 2 phonons

(c) three quad. phonon state  $|3; IM\rangle = \sum_{I'} N_I^{(I')} ((b_2^* \otimes b_2^*)_{I'} \otimes b_2^*)_{IM} |0\rangle$

fractional percentage coefficients

(= amplitudes of the different states with intermediate spin  $I'$ )

Using (o) for the operators and (w) for the wave functions, one gets the following matrix elements  $\langle I || Q_{\lambda}^{(t)} || I' \rangle$

(i) Operators linear in  $\alpha$

(a') Ground state  $\leftrightarrow$  one phonon state (arbitrary  $\lambda$ ):

$$\langle 0; 0 || Q_{\lambda}^{(1)} || 1; I \rangle = \sum_{\lambda} (-)^{\lambda} \beta_{\lambda}$$

spin  
phonon number

(b') One quad. phonon state  $\leftrightarrow$  two quad. phonon state:

$$\langle 1; 2 || Q_{\lambda}^{(2)} || 2; I \rangle = \beta_{\lambda} [2(2I+1)/5]^{\frac{1}{2}}$$

(c') Two quadrupole plus non state  $\leftrightarrow$  three quadrupole phonon state:

$$\langle 2; I \parallel Q_2^{(1)} \parallel 3; I' \rangle = \frac{\beta_2}{\sqrt{10}} \sum_{I''} N_I^{(I'')} \left( 2 S_{II''} (-)^{I+I'} \sqrt{2I'+1} + \right. \\ \left. + 4 \sqrt{(2I+1)(2I+4)(2I''+1)} W(222I'; I''I) \right)$$

(d') One octupole phonon state  $\leftrightarrow$  quad. oct. two phonon state:

$$\langle 1; 3 \parallel Q_3^{(1)} \parallel 2 \otimes 3; I \rangle = \beta_2 [(2I+1)/5]^{\frac{1}{2}}$$

multipolarities, not phonon numbers

(e') One quadrupole phonon state  $\leftrightarrow$  quad. oct. two phonon state:

$$\langle 1; 2 \parallel Q_3^{(1)} \parallel 2 \otimes 3; I \rangle = \beta_3 (-)^I [(2I+1)/7]^{\frac{1}{2}}$$

(ii) Operators quadratic in  $\alpha_\lambda$

(a'') Ground state  $\leftrightarrow$  two quadrupole phonon state:

$$\langle 0; 0 \parallel Q_\lambda^{(2)} (\lambda_1=\lambda_2=2) \parallel 2; I \rangle = \beta_2^2 \delta_{I\lambda} (2200 | I0) / \sqrt{20}$$

(b'') One quadrupole phonon state  $\leftrightarrow$  three quadrupole phonon state:

$$\langle 1; 2 \parallel Q_\lambda^{(2)} (\lambda_1=\lambda_2=2) \parallel 3; I \rangle = \beta_2^2 (2200 | 20) \sum_{I''} N_I^{(I'')} * \\ * (2 S_{I''\lambda} \sqrt{\frac{2I+1}{2\lambda+1}} + 4 \sqrt{(2I+1)(2I''+1)} W(222I; I''\lambda)) / \sqrt{4\pi}$$

(c'') Ground state  $\leftrightarrow$  quadrupole octupole two phonon state:

$$\langle 0; 0 \parallel Q_2^{(2)} (\lambda_1=2, \lambda_2=3) \parallel (2 \otimes 3); I \rangle = \beta_2 \beta_3 S_{\lambda I} (2300 | I0) (-)^{I+1} / \sqrt{40}$$

(d'') One quadrupole phonon state  $\leftrightarrow$  one octupole phonon state:

$$\langle 1; 2 \parallel Q_\lambda^{(2)} (\lambda_1=2, \lambda_2=3) \parallel 1; 3 \rangle = \beta_2 \beta_3 (2300 | \lambda 0) / \sqrt{40}$$

Hermiticity:  $\langle I \parallel Q_\lambda^{(t)} \parallel I' \rangle = (-)^{I-I'+\lambda} \langle I' \parallel Q_\lambda^{(t)} \parallel I \rangle$

$\triangleright$  Bra matrix not hermitian

A matrix  $\text{---} \parallel \text{---}$  (same property as Bra matrix above)

$\triangleright$  coupling matrix hermitian, as it should be

When  $\lambda_1 = \lambda_2$  in (o) : coupling term contributes nonvanishing diagonal elements:

$$(a'') \text{ Ground state: } \langle 0; 0 || Q_\lambda^{(2)} (\lambda_1 = \lambda_2 = 2) || 0; 0 \rangle = \beta_2^2 \delta_{\lambda 0} / \sqrt{4\pi}$$

$$(b'') \text{ One quad. ph. st.: } \langle 1; 2 || Q_\lambda^{(2)} (\lambda_1 = \lambda_2 = 2) || 1; 2 \rangle = \beta_2^2 (2200 | \lambda 0) (2 + 5 \delta_{\lambda 0}) / \sqrt{4\pi}$$

$$(c'') \text{ Two quads. ph. st.: } \langle 2; I || Q_\lambda^{(2)} (\lambda_1 = \lambda_2 = 2) || 2; I' \rangle = \beta_2^2 \frac{1}{\sqrt{4\pi}} (2200 | \lambda 0) + \\ * \left\{ \sqrt{5(2I+1)} \delta_{\lambda 0} \delta_{II'} + 4 \sqrt{(2I+1)(2I'+1)(2\lambda+1)} W(2I|2I'; 2\lambda) \right\}$$

### B. Rotational nucleus

consider only the excitation of the states of the ground state rotational band (same internal structure as ground state, but additional rotation)

$$V_{\text{coupl}} = \sum_{t, \lambda} v_{\lambda}^{(t)} (a) (Q_\lambda^{(t)}) \gamma_\lambda$$

$$V_{\text{coupl}}^{(n)} = \sum_{\lambda \neq 0} v_{cp}^{(n)} (a) \langle \gamma_\lambda^{(n)} (0, \phi) \rangle$$

$$\circ \langle l_j I | V_{\text{coupl}} | l'_j I' \rangle_{JM} = \sum_{\lambda} v_{cp}^{(\lambda)} (a) B_\lambda (I J') A(l_j I, l'_j I'; \lambda) \delta_{JM}$$

$$\text{where } B_\lambda (I, I') = \sqrt{2I+1} \langle I' \lambda K 0 | I K \rangle$$

projection of spin on body fixed axis

for the excitation of rotational states of bands or vibrational states ( $\beta$  and/or  $\gamma$  vibrations):  $B_\lambda (I J')$  were involved

## 4) Scattering matrices and cross sections

Solve coupled equations for radial wave function  $R_{\text{sym}}(r)$  }  $\rightarrow S$  matrix  
match at  $R_\infty$  to asymptotic solution

assumption: projectile and target initially both in polarized state  
(unpolarized state included as special case)

amplitudes:  $a_{M_1}^{(i)}, b_{M_1}^{(i)}$

$i, i' \dots$  specify different spin mouthes when more than one mouth is needed for the description of the pol. state amplitudes of different mouthes do not interfere, amplitudes of one mouth do interfere.

### A. Shape Scattering XS's and Polarizations

asymptotic form of wave fn.:

$$\Psi_{\text{asym}} = \frac{1}{(k_n \sqrt{\nu_n})} \sum_{(i,i') M_1 M_2} a_{M_1}^{(i)} b_{M_2}^{(i')} \sum_{J, JM} (\ell_S m_S | j m_S) (j J, m_S M_1) JM * \\ * \sum_{n' l'} [\sqrt{2l+1} \exp(i\zeta_l^{(n)}) \delta_{n1} \delta_{l1} \delta_{j1} F_1^{(n)} + \sqrt{2l'+1} \left(\frac{k_n}{k_n}\right)^{\frac{1}{2}} \exp(i\zeta_{l'}^{(n)}) * \\ * (G_{j,n} e^{i\zeta_{l'}^{(n)}} (G_{l'}^{(n)} + i F_{l'}^{(n)})) (Y_{l,j} \otimes \Phi_{In}) JM$$

"scattering coefficients"

inv. ref. Ch fits. for arb. ang. mom.  $l'$  and every  $E_n$

at  $r = R_m$

$$\eta_n = \frac{m^2 \varepsilon^2 \varepsilon'}{t^2 k_n} \quad m \dots \text{reduced mass}$$

$\zeta_l^{(n)} \dots$  Ch place stuff

for uncharged projectile:  $q_u = 0$

$$\sigma_l^{(n)} = 0$$

$$\text{replace } F_l^{(n)}, G_l^{(n)} \rightarrow k_n R_m j_l^{(n)}, k_n R_m n_l^{(n)}$$

spher. Born Neumann

incident wave  $\Psi_{\text{inc}}$ : (a distorted plane wave plus

(a scattered wave - - - - -)

$$\begin{aligned} \Psi_{\text{inc}} = & \frac{1}{\sqrt{n}} \left\{ \exp \left[ i(k_{\text{in}} - \eta_n \ln(2k_{\text{in}})) \right] \left\{ 1 - \frac{\eta_n^2}{ik_{\text{in}}(n-1)} \right\} + \right. \\ & + f_c(\theta) \frac{1}{n} \exp \left[ i(k_{\text{in}} - \eta_n \ln(2k_{\text{in}})) \right] \left\} e^{i\omega t} \right. \\ & \left. + \sum_{(i')m_s M_1}^{(ii)} a_{m_s}^{(i')} b_{M_1}^{(i')} \chi_{sm_s} \Phi_{I_1 M_1} \right. \end{aligned}$$

add second terms of inc. and asympt. wave, noting the asymptotic behavior of the  $a$ ,  $b$  pts.:  $A_1^{(n)} \xrightarrow[n \rightarrow \infty]{} \cos \Sigma_1^{(n)}$

$$F_1^{(n)} \xrightarrow[n \rightarrow \infty]{} \sin \Sigma_1^{(n)}$$

$$\Sigma_1^{(n)} = k_{\text{in}} n - \eta_n \ln(2k_{\text{in}}) - \frac{l\pi}{2} + \delta_1^{(n)}$$

$$\begin{aligned} \Delta \Psi_{\text{scat}} = & \sum_n \frac{\exp[i(k_{\text{in}} - \eta_n \ln(2k_{\text{in}}))]}{n \sqrt{n}} \sum_{(i')m_s M_1}^{(ii)} a_{m_s}^{(i')} b_{M_1}^{(i')} * \\ & \left\{ f_c(\theta) \delta_m \chi_{sm_s} \Phi_{I_1 M_1} + \sum_{l, j, j'} \frac{4\pi}{k_n} \sqrt{2l'+1} \exp(2i\sigma_l^{(n)}) C_{lj; n l' j'} * \right. \\ & \left. = (ls 0 m_s | jm_s) (j I_1 m_s M_1 | JM) (2j_{ij'} \otimes \Phi_{I_1}) JM \right. \end{aligned}$$

shape scattering differential  $\chi_S$  which leaves the target in its  $n$ th state

$$\boxed{\delta_n^{(s)}(\theta, \phi) = \sum_{(i')m_s M_1} \left| \sum_{m_s M_1}^{(ii)} a_{m_s}^{(i')} b_{M_1}^{(i')} \left\{ f_c(\theta) \delta_{nn} \delta_{m_s m_s} \delta_{M_1 M_1} + \sum_{l, j, j'} \frac{4\pi}{k_n} \sqrt{2l'+1} \right. \right. \right.}$$

summation over final states

$$\begin{aligned} & \left. \left. \left. * \exp(2i\sigma_l^{(n)}) C_{lj; n l' j'} (ls 0 m_s | jm_s) (j I_1 m_s M_1 | JM) (l' s m_s' m_s' | j' m_j') * \right. \right. \right. \\ & \left. \left. \left. = (j' I_1 m_j' M_1 | JM) Y_{l' m_j'}(\theta, \phi) \right\} \right|^2 \right. \end{aligned}$$

depends in general on azimuthal angle  $\phi$

introduce the amplitude:

$$X_{m_s M_s, m'_s M'_s}(\theta, \phi) = f_c(\theta) \delta_{m_l} \delta_{m_s m'_s} \delta_{M_s M'_s} + \\ + \sum_{l, l', j, m_l, m'_s, M_s} \frac{\sqrt{4\pi}}{k_n} \sqrt{2l'+1} \exp(2i\delta_l^{(n)}) C_{l, l'; m_l, m'_s}^j (l s 0 m_s | j m_s) (j I, m_s M_s | JM) \\ * (l' s m'_s m'_s | j' m'_s) (j' I, m'_s M'_s | JM) Y_{l', m'_s}(\theta, \phi)$$

$$\triangleright G_n^{(s)}(\theta, \phi) = \sum_{(i, i') m_s M_s} \left| \sum_{m_s M_s} X_{m_s M_s, m'_s M'_s}(\theta, \phi) a_{m_s}^{(i)} b_{M_s}^{(i')} \right|^2$$

Vector polarization also given as bilinear function of  $X$

### B. Total and Reaction Cross Sections

$$G_{abs} + \sum_{n \neq 1} G_n^{(s)} = -\frac{1}{v_i} [\vec{\phi} \vec{j} d\vec{l}]$$

prob. flux density

Gabs ... compound nucleus XS

$\sum_{n \neq 1} G_n^{(s)}$  ... direct inelastic XS

$$G_{abs} + \sum_{n \neq 1} G_n^{(s)} = \frac{n}{2im} \left[ \left( \frac{\partial \phi_i}{\partial r} - \phi_i \frac{\partial \phi_i}{\partial r} \right), r^2 dI d\Omega \right]$$

| dI ... integration and summation over intern. coord.

| dΩ ... --||-- over angular variables of rel. motion

$G_{sh.el.}$  ... total shape elastic XS

$$G_t = G_{abs} + G_{sh.el.} + \sum_{n \neq 1} \sigma_n^{(s)} = G_{abs} + \sum_n G_n^{(s)} \dots \text{total cross section}$$

if incident particle is charged :  $G_{sh.el.} \rightarrow \infty$

$$\triangleright G_t \rightarrow \infty$$

$\Rightarrow$  consideration of  $\sigma_{sh.el.}$  and  $G_t$  has meaning only for neutral projectile

simplification of the expressions for  $G_t$  and  $G_{abs}$  by introducing

$$Z_{m_s M_s, m'_s M'_s; l'} = \sum_{l, l', j, m_l, m'_s, M_s} (l s 0 m_s | j m_s) (j I, m_s M_s | JM) *$$

$$= C_{l, l'; m_l, m'_s}^j (l' s 0 m'_s | j' m'_s) (j' I, m'_s M'_s | JM)$$

amplitude, intimately related to  $X$

$$\Delta \sigma_t = \frac{4\pi}{k_i^2} \sum_{l'} (2l'+1) \left\{ \text{Im} \sum_{(ii') m_s M_s; M'_s} a_{m_s}^{(i)} a_{m'_s}^{(i')} b_{M_s}^{(i)} b_{M'_s}^{(i')} Z_{m_s M_s; m'_s M'_s; l'} \right\} \xrightarrow{\text{opt. theorem}}$$

$$\begin{aligned} G_{\text{abs}} + \sum_{n \neq 1} G_n^{(s)} &= G_t - \int \sigma_s^{(n)}(\theta, \phi) d\Omega = \\ &= G_t - \frac{4\pi}{k_i^2} (2l'+1) \sum_{ii'j'j} \left| \sum_{m_s M_s} a_{m_s}^{(i)} b_{M_s}^{(i')} \sum_j (l_s 0 m_s | j m_s) (j I_s m_s M_s | j M) C_{I_s j; i' j'} \right|^2 \end{aligned}$$

↓ precluding section

### C. Compound Contribution to the Differential Scattering $\chi S^5$

when energy of incident particle is low  $\rightarrow$  add contribution of compound process to scattering  $\chi S$  to  $n^{\text{th}}$  state

Hansen-Feshbach formalism



$\chi S$  as function of probabilities  $T_l^{(n)}$  for various channels  $n$  and orb. ang. mom.  $l$

$T_l^{(n)}$  computed from scattering coefficients  $C_l^{(n)}$

spin orbit interaction  $\Rightarrow C_{lj}^{(n)} \Rightarrow T_{lj}^{(n)}$

CCOM :  $C_{l_1; n'l'_1} \triangleright$  modify HF cross section:

$C_{l_1; n'l'_1} \dots$  amplitude of outgoing wave in channel  $n'l'_1$  when there is an incoming wave in the channel  $l_1 l'_1$  with amplitude  $1 \exp(i\sigma_{l_1}^{(n)})$

define probabilities in ground state channels

which scattering coefficients:

$C_{nl_1; n'l'_1} \dots$  amplitude of outgoing wave in channel  $n'l'_1$  when there is an incoming wave in channel  $nl_1$  with amplitude  $1 \exp(i\sigma_{l_1}^{(n)})$

$$((S|_{\partial K} Y_{\lambda}) \{ \sum_k + 1 \})_{\partial K} = \bar{R}$$

Def.: generalized S-matrix element  $S_{n'l'j'}^{(3)}$

$$S_{n'l'j'}^{(3)} = \delta_{nn'} \delta_{ll'} \delta_{jj'} + 2i \sqrt{\frac{2l'+1}{2l+1}} \frac{k_e}{k_e} C_{nlj;n'l'j'}$$

$$T_{nlj}^{(3)} = 1 - \sum_{n'l'j'} S_{nlj;n'l'j'}^{(3)} S_{nlj;n'l'j'}^{(3)*} \text{ generalized transm. coeff.}$$

Compound contribution to scattering xs leaving target in its  $n^{\text{th}}$  state:

$$G_n^{(c)}(\theta) = \frac{1}{k_e^2} \sum_{ii'm_m M_m} (a_m^{(i)})^2 (b_m^{(i)})^2 \sum_j \left[ 1 / \sum_{nlj} T_{nlj}^{(3)} \right] *$$

$$* \sum_{l's m_s M_s} (2l+1) (l s 0 m_s | j m_s)^2 (j I_s m_s M_s | JM)^2 *$$

$$- \frac{1}{4 l' j' (m)} * (l' s m_s m'_s | j' m'_s)^2 (j' I_m m'_m M_m | JM)^2 T_{nlj} T_{nlj'} | Y_{l'm'_s} |^2$$

independent on  $\phi$

$T_{nlj}$  real

### 3. Adiabatic approximation (Acc)

requirements

- target well deformed  $\rightarrow$  exc. spectrum is closely that of an ideal rotational band
- inc. energy  $\gg$  exc. energy of these rotational states
- interested only in excitation of ground state rotational band

Coupling to all states of ground band is included automatically  
 $\Rightarrow$  quite accurate results with less complicated and faster calculations than with non-adiabatic coupled channels calc. (NACC)

same potential as with NACC

$$R = R_0 (1 + \sum_\lambda \beta_\lambda Y_{\lambda 0}(\theta'))$$

$$\bar{R} = \bar{R}_0 (1 + \sum_\lambda \beta_\lambda Y_{\lambda 0}(\theta'))$$

$$\Psi_{\text{coupl}}^{(n)} = \sum_{\lambda \neq 0} v_{cp}^{(\alpha)(\lambda)} (\lambda) \underbrace{\Upsilon'_{\lambda 0}}_{(\lambda \neq 0)} \quad \begin{array}{l} \text{don't transform to space fixed system} \\ \text{with respect to body fixed system} \end{array}$$

Denote by  $\bar{m}_j$  the projection on the nuclear symmetry axis of the angular momentum  $j$  of a partial wave of the projectile

$$\triangleright \Psi = \frac{1}{\sqrt{2}} \sum_{ij\bar{m}_j} R_{ij\bar{m}_j} (\lambda) \underbrace{2Y_{ij\bar{m}_j}}_{\tilde{\Upsilon}_{\text{LW}, X_{\text{SW}}}}$$

### Coupled equation:

$$\left( \frac{d^2}{dp^2} - \frac{1(l+1)^2}{p^2} - E^{-1} V_{\text{diag}} + 1 \right) R_{ij\bar{m}_j} = \\ = E^{-1} \sum_{i'j'} \langle 2Y_{i'j'\bar{m}_j} | \sum_{\lambda} v_{cp}^{(\alpha)(\lambda)} (\lambda) \Upsilon'_{\lambda 0} | 2Y_{i'j'\bar{m}_j} \rangle R_{i'j'\bar{m}_j}$$

where  $p = k\lambda$

reason why the body fixed system was preferred is that otherwise there would be coupling between different  $\bar{m}_j$  in addition to coupling of different  $j$ .

### Coupling matrix:

$$\langle 2Y_{i'j'\bar{m}_j} | \sum_{\lambda} v_{cp}^{(\alpha)(\lambda)} \Upsilon'_{\lambda 0} | 2Y_{i'j'\bar{m}_j} \rangle = \\ = \sum_{\lambda} v_{cp}^{(\alpha)(\lambda)} * \text{coupling geom. factor}$$

$\triangleright$  B matrix is replaced by c matrix which is unity

Asymptotic form of the wave function:

$$\Psi_{\text{asym}} = \frac{14\pi}{\alpha \hbar \Gamma \nu_1} \sum_{(ii') m_s M_1} a_{m_s}^{(i)} b_{M_1}^{(i')} \sum_l (l s 0 m_s | j m_j) D_{m_s \bar{m}_j} (\theta_i) \sum_{\text{space body}} \sqrt{2l'+1} \exp(i\phi_{ij}^{(i)}) \\ = \left[ \delta_{ii'} \delta_{jj'} F_{ij}^{(i)} + \underbrace{C_{ij;ij} \bar{m}_j}_{\text{body}} (G_{ij}^{(i)} + i F_{ij}^{(i)}) \right] 2Y_{ij\bar{m}_j} \Phi_{i'm_s}$$

Important difference between ACC and NACC : in ACC no coupling

of  $I_a$  and  $j \leftarrow$  ACC supposes that target nucleus is inert during the scattering process and thus carries no angular momentum dynamically

rotation fact. for transformation between space and body fixed system  
scattered wave :

$$\begin{aligned} \Phi_{\text{scatt}} &= \frac{1}{n\sqrt{v_n}} \exp(ik_n z - i\eta_n \ln 2 b_n n) \sum_{(i'') m_s M_n}^{(i)} a_m^{\prime\prime} b_{M_n}^{\prime\prime} * \\ &\quad * \left[ f_c(\theta) \chi_{sm_s} + \frac{4\pi}{k_n} \sum_{l_1 l_2 j_1 \bar{m}_j m_j} \sqrt{2l'+1} \exp(2i\sigma_{l_1}^{\prime\prime}) C_{l_1 j_1 l_2 j_2} (\text{Ls } 0 m_s | j m_s) * \right. \\ &\quad \left. * J_{m_s \bar{m}_j}(\theta_i) \left[ 2 \tilde{y}_{l_1 j_1}^{\bar{m}_j} \right] \right] \Phi_{I_a M_n} = \\ &= \frac{1}{n\sqrt{v_n}} \exp(ik_n z - i\eta_n \ln 2 b_n n) \sum_{(i'') m_s M_n}^{(i)} a_m^{\prime\prime} b_{M_n}^{\prime\prime} * \\ &\quad * \left[ f_c(\theta) \chi_{sm_s} + \frac{4\pi}{k_n} \sum_{l_1 l_2 j_1 \bar{m}_j m_j} \sqrt{2l'+1} \exp(2i\sigma_{l_1}^{\prime\prime}) C_{l_1 j_1 l_2 j_2} (\text{Ls } 0 m_s | j m_s) * \right. \\ &\quad \left. * \langle l' \circ m'_s | j' m'_j \rangle, J_{m_s \bar{m}_j}(\theta_i), J_{m'_s \bar{m}'_j} Y_{j' m'_j} \chi_{sm'_s}; \right] \Phi_{I_a M_n} \end{aligned}$$

expand right hand side (except  $\frac{1}{n\sqrt{v_n}} \exp(\dots)$ ) in terms of eigenfunctions  $\Phi_{I_a M_n}$  of the target  $\Rightarrow$  expansion coefficients give scattering amplitudes to leave the target in that particular state

note that  $\Phi_{I_a M_n} = [2I_a + 1]/8\pi^{\frac{1}{2}} D_{M_n K}^{I_a}(\theta_i)$   
spacetime

K... projection of  $I_a$  to the nuclear symmetry axis

$$[\quad] \Phi_{I_a M_n} = \sum_{n m_s} \alpha_{n m_s M_n m'_s} \Phi_{I_a M_n}$$

$$\alpha_{n m_s M_n m'_s} = \langle \Phi_{I_a M_n} | [\quad] | \Phi_{I_a M_n} \rangle$$

leads to :

$$\begin{aligned} \Phi_{\text{scatt}}^{(\text{Acc})} &= \frac{1}{\pi \sqrt{\nu_0}} \exp(i k_0 z - i \eta_0 \ln(2 \pi k_0)) \sum_{n(iii) m_s M_s m'_s}^{(i)} a_{m_s}^{(i)} b_{M_s}^{(i')} \alpha_{n m_s M_s m'_s} \Phi_{I n M_n}^{(\text{Acc})} = \\ &= \frac{1}{\pi \sqrt{\nu_0}} \exp(i k_0 z - i \eta_0 \ln(2 \pi k_0)) \sum_{n(iii) m_s M_s m'_s}^{(i)} a_{m_s}^{(i)} b_{M_s}^{(i')} X_{m_s M_s; m'_s M_n} \chi_{sm'_s} \Phi_{I n M_n}^{(\text{Acc})} \end{aligned}$$

with  $X_{m_s M_s; m'_s M_n}^{(\text{Acc})}(\theta, \phi) = f_c(\theta) \delta_{m_s} \delta_{m'_s} \delta_{M_s M_n} +$   
 $+ \sum_{l_1 l'_1 j' \bar{m}_j w_j w'_j}^{\frac{14\pi}{k_0} \sqrt{2l_1+1}} \exp(2i\sigma_{l'_1}^{(i)}) C_{l_1 j' l'_1 j'} (l_1's 0 m_s | j' w_s) *$   
 $* \sum_{JM_J} \left[ (-)^{\bar{m}_j - m'_s} \sqrt{\frac{2l_1+1}{2J+1}} (I_1 J K 0 | I_n K) (I_1 J M_s M_j | I_n M_n) (j j' \bar{m}_j - \bar{m}_j) \right. *$   
 $\left. * (j j' | w_s - w_j | JM_J) (l_1's m'_s m'_s | j' w_j) Y_{l'_1 w_j}(\theta, \phi) \right]$

$X_{m_s M_s; m'_s M_n}^{(\text{Acc})}$  plays exactly the same role as  $X_{w_s M_s; w'_s M_n}$  in NACC

Expressions for XS<sup>s</sup> and polarizations derived for NACC can be used for ACC by replacing  $X_{m_s M_s; m'_s M_n}(\theta, \phi) \rightarrow X_{m_s M_s; m'_s M_n}^{(\text{Acc})}$

$$\begin{aligned} Z_{m_s M_s; m'_s M_n; l''} &\rightarrow Z_{m_s M_s; m'_s M_n; l''}^{(\text{Acc})} = \sum_{l_1 j' \bar{m}_j w_j w'_j} (l_1's 0 m_s | j' w_s) C_{l_1 j' l''} * \\ &= (l_1's m'_s m'_s | j' w_j) \sum_{JM_J} \left[ (-)^{\bar{m}_j - m'_s} (I_1 J K 0 | I_n K) * \right. \\ &\quad \left. * (I_1 J M_s M_j | I_n M_n) (j j' \bar{m}_j - \bar{m}_j | J 0) (j j' m_s - m'_s | JM_J) \right] \end{aligned}$$

Saving of computational time and core storage with ACC :

- Symmetry relations of X and Z under  $\bar{m}_j \rightarrow -\bar{m}_j$   
 $\Rightarrow$  coupled equations need to be solved for  $\bar{m}_j > 0$  only
- number of coupled channels for given  $\bar{m}_j$  (ACC) is smaller than for given  $J$  (NACC)
- number of systems of coupled equations to be solved is smaller with ACC than with NACC
- sizes of coupled equations to be solved (ACC) are unchanged if incident energy is fixed, irrespective of how high we go up in the excited states

## IV) THE STATISTICAL MODEL FOR COMPOUND NUCLEUS REACTIONS AND PREEQUILIBRIUM DECAY

### 1) Compound nucleus model

#### A. Theory

In theoretical treatment of nuclear reactions :  $\chi S^*$  expressed in terms of  $S$  matrix:

$$\sigma_{ab} = \frac{\pi}{k_a^2} |\delta_{ab} - S_{ab}|^2$$

general properties of  $S$  : unitarity  $S S^\dagger = S^\dagger S = I$  (flux conservation)  
symmetry  $S^\dagger = S$  (time reversal inv.)

Theory of nuclear reactions aims at calculation of  $S$  matrix by solving Schrödinger equation for A particle system  
from general reaction theories (particularly R matrix theory):

$$S_{ab} = S_{ab}^0 - i \sum_\mu \underbrace{\frac{g_{\mu a} g_{\mu b}}{E - E_\mu + \frac{i}{2}\Gamma_\mu}}$$

resonance pole term

$S_{ab}^0$  slowly varying function of energy, compared to 2<sup>nd</sup> term  
for energy interval  $\Delta E$  around  $E_0$ :

$$S_{ab} = \bar{S}_{ab} + S_{ab}^{fl} \quad \bar{S}_{ab} = \frac{1}{\Delta E} \int_{E_0 - \frac{\Delta E}{2}}^{E_0 + \frac{\Delta E}{2}} dE S_{ab}$$

$$\bar{S}_{ab}^{fl} = 0$$

averaging of unitary relation leads to relation between  $\bar{S}_{ab}$  and  $S_{ab}^{fl}$

$$\sum_c S_{ac} S_{bc}^* = \sum_c \bar{S}_{ac} \bar{S}_{bc}^* + \sum_c \overline{S_{ac}^{fl} S_{bc}^{fl}*} = \delta_{ab}$$

averaging of cross section :

$$\bar{\sigma}_{ab} = \frac{1}{\Delta E} \int_{E_0 - \frac{\Delta E}{2}}^{E_0 + \frac{\Delta E}{2}} dE \sigma_{ab}(E) = \frac{\pi}{k_a^2} |\delta_{ab} - \bar{S}_{ab}|^2 + \frac{\pi}{k_a^2} |\bar{S}_{ab}^{fl}|^2 = \sigma_{ab}^{dir} + \langle \sigma_{ab}^{fl} \rangle$$

interpretation:  $\sigma_{ab}^{dir}$  :  $\bar{S}_{ab}$  describes direct reactions

$\sigma_{ab}^{fl}$  :  $S_{ab}^{fl}$  describes compound nucleus reactions

assumption:  $\bar{S}_{ab}$  known from direct reaction model  
 aim of the statistical theory of cross sections: calculation of  
 $\langle S_{ab}^H \rangle$  (and correlation fcts.) from  $\bar{S}_{ab}$

Cases:

A) No direct reactions in non-elastic channels:  $\bar{S}_{ab} = \delta_{ab} \bar{S}_{aa}$

$\bar{S}_{aa}$  from single channel optical model

transmission coefficient:  $\frac{\pi}{k_a^2} T_a = \sum_b \langle S_{ab}^H \rangle = \frac{\pi}{k_a^2} (1 - |\bar{S}_{aa}|^2)$

$$T_a = 1 - |\bar{S}_{aa}|^2 \text{ with } 0 \leq T_a \leq 1$$

▲ Isolated resonances  $\frac{\langle \Gamma_p \rangle}{D} \ll 1$

then  $\langle \Gamma_p \rangle \dots \text{average width} \} \text{ of res.}$   
 $D \dots \text{spacing}$

$$S_{ab}^0 = S_{ab} e^{2i\varphi_a} \quad \varphi_a - \text{phase shift for potential scattering}$$

$g_{\mu a} = e^{i\varphi_a} \Gamma_{\mu a}^\frac{1}{2}$  in resonance pole term

$$\triangleright S_{ab} = S_{ab} e^{2i\varphi_a} - i e^{i(\varphi_a + \varphi_b)} \sum_\mu \frac{\Gamma_{\mu a}^\frac{1}{2} \Gamma_{\mu b}^\frac{1}{2}}{E - E_\mu + i \Gamma_\mu} \quad \Gamma_\mu = \sum_c \Gamma_{\mu c}$$

$$\bar{S}_{ab} = S_{ab} e^{2i\varphi_a} - e^{i(\varphi_a + \varphi_b)} \underbrace{\frac{1}{D} \langle \Gamma_{\mu a}^\frac{1}{2} \Gamma_{\mu b}^\frac{1}{2} \rangle}_\mu = S_{ab} e^{2i\varphi_a} \left( 1 - \frac{1}{D} \langle \Gamma_{\mu a} \rangle \right)$$

$\langle \Gamma_{\mu a} \rangle_\mu$  since  $\bar{S}_{ab}$  assumed to be diagonal

$$T_a = 1 - |\bar{S}_{aa}|^2 = \underbrace{\frac{2\pi}{D} \langle \Gamma_{\mu a} \rangle}_{\ll 1} + \underbrace{\frac{\pi^2}{D^2} \langle \Gamma_{\mu a} \rangle^2}_{\text{negligible if } \langle \Gamma \rangle / D \ll 1}$$

$$\text{Calculate } S_{ab}^{fl} = S_{ab} - \bar{S}_{ab}$$

$$\triangleright |S_{ab}^{fl}|^2$$

$$\triangleright \overline{|S_{ab}^{fl}|^2} \text{ average over } \Delta E$$

leads to

$$\langle \sigma_{ab}^{(II)} \rangle = \frac{1}{\Delta E} \int_{E_0 - \frac{\Delta E}{2}}^{E_0 + \frac{\Delta E}{2}} dE \left\{ \frac{\pi}{k_a^2} \sum_b \frac{\Gamma_{ja} \Gamma_{jb}}{(E - E_j)^2 + \frac{1}{4} \Gamma_j^2} + \text{resonance interference term} \right\} = \\ = \frac{\pi}{k_a^2} \left\{ \frac{2\pi}{D} \underbrace{\left\langle \frac{\Gamma_{ja} \Gamma_{jb}}{\Gamma_j} \right\rangle}_{\mu} + O\left(\frac{\langle \Gamma_j \rangle^2}{D^2}\right) \right\}$$

average over  $\Delta E \hat{=} \text{ensemble average over resonance parameter}$

$$\frac{\pi}{k_a^2} T_a = \sum_b \langle \sigma_{ab}^{(II)} \rangle = \frac{\pi}{k_a^2} \frac{2\pi}{D} \langle \Gamma_{ja} \rangle$$

$$\triangleright T_a = \frac{2\pi}{D} \langle \Gamma_{ja} \rangle \ll 1 \quad \text{for isolated resonances}$$

"weak absorption"

$$\sum_a T_a = \frac{2\pi}{D} \langle \Gamma_j \rangle \text{ due to } \sum_a \Gamma_{ja} = \Gamma_j$$

Rewrite  $\langle \frac{\Gamma_{ja} \Gamma_{jb}}{\Gamma_j} \rangle_\mu$  in order to express  $X_S^*$  by means of  $T_a$ :

$$\left\langle \frac{\Gamma_{ja} \Gamma_{jb}}{\Gamma_j} \right\rangle = \frac{\langle \Gamma_{ja} \rangle \langle \Gamma_{jb} \rangle}{\langle \Gamma_j \rangle} W_{ab}$$

$$W_{ab} = \left\langle \frac{\Gamma_{ja} \Gamma_{jb}}{\Gamma_j} \right\rangle \frac{\langle \Gamma_j \rangle}{\langle \Gamma_{ja} \rangle \langle \Gamma_{jb} \rangle} \quad \text{"width fluctuation correction factor"}$$

$W_{ab}$  can be calculated if statistical properties of  $\Gamma_{ja}$  are known  
closed form expression for  $W_{ab}$  if the following conditions are satisfied:

$$(i) \langle \Gamma_{ja} \cdot \Gamma_{jb} \rangle = \langle \Gamma_{ja} \rangle \langle \Gamma_{jb} \rangle \quad \text{for } a \neq b$$

(ii)  $\Gamma_{ja}$  follows  $\chi^2$  distribution with  $\nu_a$  degrees of freedom

$$\triangleright \boxed{W_{ab} = \left(1 + \frac{2}{\nu_a} \delta_{ab}\right) \int_0^\infty dt \prod_c \left(1 + \frac{2t}{\nu_c} \frac{\langle \Gamma_{jc} \rangle}{\langle \Gamma_j \rangle}\right)^{-\left(\frac{1}{2}\nu_c + \delta_{ac} + \delta_{bc}\right)}}$$

for isolated resonances :  $\nu_c = 1 \dots$  Poiss. Thomas distribution

## Properties of $W_{ab}$ :

$W_{aa} > 1$  ("elastic enhancement")

$W_{ab} < 1$  for  $a \neq b$  (in general);

$\xrightarrow{N \gg 1} 3 \}$  where  $N$  is the #  
 $\xrightarrow{N \gg 1} 1 \}$  of open channels

$$\Delta \langle S_{ab}^{fl} \rangle = \frac{\pi}{k_a^2} \frac{T_a T_b}{\sum_c T_c} W_{ab}$$

$$W_{ab} = \left( 1 + \frac{2}{\nu_a} \delta_{ab} \right) \int_0^\infty dt \prod_c \left( 1 + \frac{2t}{\nu_c} \frac{T_c}{\sum_c T_c} \right)^{-\left( \frac{\nu_c}{2} + \delta_{ac} + \delta_{bc} \right)}$$

width fluctuation corrected Hauser-Feshbach formula

$\Delta \langle S_{ab}^{fl} \rangle$  completely expressed in terms of  $T_c = 1 - |\bar{S}_{cc}|^2$

▲ Overlapping resonances:  $\frac{\langle \Gamma_p \rangle}{D} > 1$

[for neutrons incident on medium heavy nuclei: already at a few tens of keV]

$T_c \lesssim 1$  "strong absorption"

$|\bar{S}_{ab}^{fl}|^2$  cannot be described sufficiently simply to express it in terms of transmission coefficients

This is due to the fact that the condition  $SST = I$  causes complicated correlations between resonance parameters  $\{E_\mu, g_{\mu c}, \Gamma_\mu\}$  for different  $\mu$ .  $\Rightarrow$  exact calculation of average resonance interference terms impossible

but "computer experiments" (Moldauer 1975) as evidence for validity of WF corrected HF formula also for overlapping resonances:

$$\langle S_{ab}^{fl} \rangle = \frac{\pi}{k_a^2} \frac{T_a T_b}{\sum_c T_c} \left( 1 + \frac{2}{\nu_a} \delta_{ab} \right) \int_0^\infty dt \prod_c \left( 1 + \frac{2t}{\nu_c} \frac{T_c}{\sum_c T_c} \right)^{-\left( \frac{\nu_c}{2} + \delta_{ac} + \delta_{bc} \right)}$$

WF corrected  
HF formula

$$T_c = 1 - |\bar{S}_{cc}|^2$$

$$\nu_c = 1 + \sqrt{T_c}$$

1.1 Cr. factor  $\xrightarrow{N \gg 1} \rightarrow$  for  $a = b$  ("elastic enhancement")

## B) Direct reactions in non-elastic channels: $\bar{S}_{ab} \neq 0$ for $a \neq b$

Direct reactions between channels  $a$  and  $b$  lead to correlations between  $\Gamma_{pa}, \Gamma_{pb}$  > enhancement in channels which are coupled to the incident channel via direct reaction

$\bar{S}_{ab}$  from coupled channels optical model

$$\text{transmission coefficients : } \frac{\pi}{k_a^2} T_a = \sum_b \langle S_{ab}^{fl} \rangle = \frac{\pi}{k_a^2} \sum_b |\bar{S}_{ab}^{fl}|^2 = \frac{\pi}{k_a^2} \left( 1 - \sum_b |\bar{S}_{ab}^{fl}|^2 \right)$$

↑ unitarity

$$\Rightarrow T_a = 1 - \sum_b |\bar{S}_{ab}^{fl}|^2$$

Generalization of transmission coefficients: transmission matrix  $T_{ab}$

$$T_{ab} = \delta_{ab} - \sum_c \bar{S}_{ac} \bar{S}_{bc}^* = \sum_c \bar{S}_{ac}^{fl} \bar{S}_{bc}^{fl*}$$

$$T_{aa} = T_a$$

In order to calculate  $\langle S_{ab}^{fl} \rangle$  in the case where  $\bar{S}_{ab}$  is non-diagonal, diagonalize transmission matrix:

$$(UPU^*)_{ab} = p_a \delta_{ab} \text{ Engelhardt Wiedenmüller Transf.}$$

$$\text{unitary : } UU^* = U^*U = I$$

Properties of transformed scattering matrix  $S' = USU^*$ :

$$\text{i) } \bar{S}_{ab}^{fl} = \delta_{ab} \bar{S}_{aa}^{fl}$$

ii) same statistical properties as scattering matrix of a problem with no direct reactions in non-elastic channels

► Procedure for calculating  $\langle S_{ab}^{fl} \rangle$ :

1) determination of  $U$  by diagonalizing  $T$

2) calculate  $X S'$  from  $S'^{fl}$ :

$$\langle S_{ab}^{fl} \rangle = \frac{\pi}{k_a^2} \sum_{cdef} U_{ca}^* U_{db}^* U_{ea} U_{fb} \bar{S}_{cd}^{fl} \bar{S}_{ef}^{fl*}$$

3) Calculation of  $S_{cd}^{(H)} S_{cd}^{(H)*}$  by means of WF connected HF formulae

$$\triangleright \langle \sigma_{ob}^{(H)} \rangle = \sum_c |U_{ca}|^2 |U_{cb}|^2 \langle \sigma_{cc}^{(H)} \rangle +$$

$$+ \sum_{d \neq c} [U_{ca}^* U_{db}^* (U_{ca} U_{db} + U_{da} U_{db}) + (\frac{2}{\nu_e} - 1)^{\frac{1}{2}} (\frac{2}{\nu_d} - 1)^{\frac{1}{2}} U_{ca}^* U_{cb}^* U_{da} U_{db}] \langle \sigma_{cd}^{(H)} \rangle$$

$$\text{with } \langle \sigma_{cd}^{(H)} \rangle = \frac{\pi}{k_e^2} \frac{T_c' T_d'}{\sum_e T_e'} (1 + \frac{2}{\nu_e} \delta_{cd}) \int_0^\infty dt \prod_e \left( 1 + \frac{2t}{\nu_e} \frac{T_e'}{\sum_e T_e'} \right)^{-\left(\frac{\nu_e}{2} + \delta_{ec} + \delta_{ed}\right)}$$

$$T_c' = 1 - |S_{cc}^{(H)}|^2 \quad \nu_e' = 1 + \sqrt{T_e'}$$

computer experiments (Moldauer 1975)

### B. Subsidicary quantities

#### 1) Particle transmission coefficients

$$T_l = 1 - |S_{cl}|^2$$

$$\text{if spin-orbit term: } T_{LJ} ; \quad T_L = \sum_l w_{lj} T_{Lj}$$

$$\text{weight, for } s = \frac{1}{2} : \frac{1+l}{2l+1}$$

$T_l$  are needed for all incoming and outgoing channels in relevant energy range and for reasonable range of partial waves

- ↓    ↓ also charged particles
- centrifugal barrier  $\propto l(l+1)$
- weight in stat. model calc.  $\underbrace{(2l+1) T_l}_{\text{cntr. to } \sigma_{abs}}$

2)  $\gamma$  ray transmission coefficients:

$$T_{XL}(\varepsilon_\gamma) = 2\pi \varepsilon_\gamma^{2L+1} f_{\gamma XL}(\varepsilon_\gamma)$$

type (M, E) multipolarity  $\gamma$  ray strength function

- Haensel model: st. fcts. energy independent, values are calculated in a single particle picture
- Brink - Axel model: st. fcts. related to  $\gamma$  ray absorption XS

for E1:

$$f_{\gamma E1}(\varepsilon_\gamma) = \frac{1}{(2\pi\hbar c)} \cdot g^2 \frac{1}{\varepsilon_\gamma} \underbrace{\langle \sigma_\gamma E1(\varepsilon_\gamma) \rangle}_{\text{average photo-absorption XS}} \quad \text{"Brink hypothesis"}$$

statistical weight of comp. nucleus avg. move. J

for energy dependence of photo abs. XS Lorentz form is adopted:

$$\langle \sigma_\gamma E1(\varepsilon_\gamma) \rangle = \frac{1}{2} g^2 \sigma_R \frac{(\Gamma_R \varepsilon_\gamma)^2}{(\varepsilon_\gamma^2 - E_R^2)^2 + \Gamma_R^2 \varepsilon_\gamma^2}$$

where  $E_R$  ... resonance energy

$\Gamma_R$  ... -- width

$\sigma_R$  ... peak cross section

for deformed nuclei: splitting of the E1 giant resonance  
 $\Rightarrow$  superposition of Lorentz curves

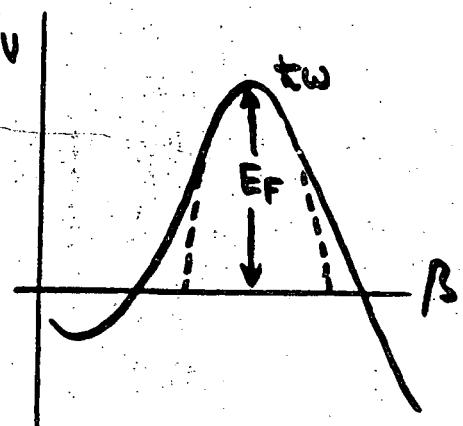
other multipolarities:

in principle same procedure, in practice information  
 of giant resonances missing

normalization of  $T_{\chi_1}$  such that exp. values of  $\frac{\langle \Gamma_y \rangle}{\langle \Gamma_y \rangle_{\text{av}}}$  are reproduced  
 where  $\langle \Gamma_y \rangle$  ... average radiation width } of s-wave neutron  
 D ... -" - resonance spacing }

if exp. data are lacking  $\Rightarrow$  use of systematics of str. fcts., normalization by fitting to exp. low energy neutron capture XS of neighbouring nuclei

### 3) fission transmission coefficients



fission barrier, assumed to be one-dimensional  
 transmission coefficients for fission are  
 related to transition states at saddle point  
 deformation

#### a) single humped barrier

approximation: parabolic shape, height  $E_F$ , curvature  $t_w$

$$P(E) = \left\{ 1 + \exp \left[ \frac{2\pi}{t_w} (E_F - E) \right] \right\}^{-1} \quad \text{"penetrability"}$$

Hill Wheeler formula

fission transmission coefficient for CN states with  $(E, J, \pi)$  is the sum of contributions of all transition states with quantum numbers  $(J, \pi)$

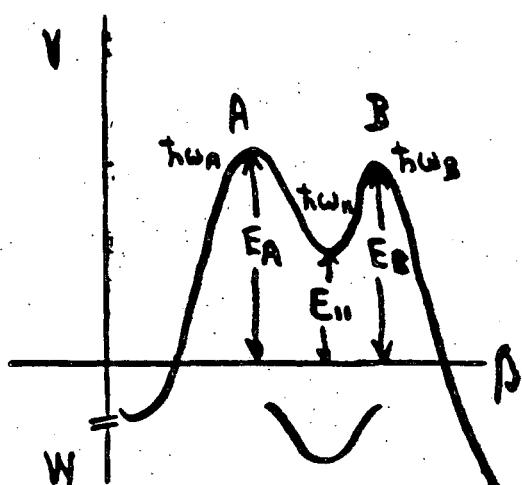
$$T_f(E, J, \pi) = \int_0^\infty dE' \rho_f(E', J, \pi) \left\{ 1 + \exp \left[ \frac{2\pi}{t_w} (E' - E) \right] \right\}^{-1} \quad (88)$$

where  $\rho_f(E', J, \pi)$  ... density of transition states

barrier shape is assumed to be the same for all transition states

$E'$  ... exc. energy referred to lowest transition state

## b) double bumped barrier



description by model of Back et al.

usually : three smoothly joined parabolae

"inner barrier" A :  $E_A, t_{wA}$

"outer barrier" B :  $E_B, t_{wB}$

"secondary minimum" :  $E_{11}, t_{w11}$

definition of fission transmission coefficients has to allow for the following consequences of the secondary minimum in the potential energy surface :

### i) damping in the 2<sup>nd</sup> well :

excitation of CN states by interaction of the fission motion with internal degrees of freedom : "damping" of the fission mode accounted for by adding to real deformation potential a negative imaginary part of parabolic shape, located at position of 2<sup>nd</sup> well [solution of Schrödinger eqn.  $\Rightarrow$  • directly transmitted flux  $T_f^{AB}(E)$

= penetrability through combined barrier

• absorbed flux  $\sigma^{AB}(E)$

$T_f^{AB}$  describes "direct" fission contr.,  $\sigma^{AB}$  provides "indirect" fission  
will show vibrational resonances at the positions of quasitonic levels in the 2<sup>nd</sup> minimum

relative magnitude of direct and indirect fission depends on strength of the absorptive potential : partial  $\leftrightarrow$  complete damping

no direct fission contr.

### ii) intermediate class II structure :

coupling of CN states in 1<sup>st</sup> and 2<sup>nd</sup> well enhances indirect fission contribution near a state in 2<sup>nd</sup> well ("class II state")

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iii. the limit of complete damping and smeared out class II structures (realized at higher incident energies):

$$T_f(E, J, \Pi) = \frac{T_f^A(E, J, \Pi) T_f^B(E, J, \Pi)}{T_f^A(E, J, \Pi) + T_f^B(E, J, \Pi)}$$

in this limit terms act independently;

$T_f^A, T_f^B$  calculated according to (88) (p. 47)

#### 4) level density

= number of excited levels per unit energy

Δ phenomenological models for spherical nuclei:

##### Fermi gas model

independent particles, no residual interactions, equidistant spacing of the single particle states near the Fermi surface, saddle point approximation (concerns integration for Laplace transformation of grand canonical partition function)

- conventional shifted Fermi gas model (Gilbert & Cameron):

consideration of odd-even effects by means of a pairing energy shift  $\Delta_{\text{pair}}$ ; i.e.: exc. energy is measured from a fictive ground state which is assumed to coincide with the actual ground state for odd nuclei and to be shifted upwards by the conventional pairing energies for odd mass and even nuclei

$\Rightarrow$  fictive ground state is determined by experimental mass differences, 1 free parameter ("a")

conv. shifted Fermi gas formula provides reasonable description of level density only for a rather small range of a few MeV around the excitation energy when a-parameter is adjusted, e.g. at neutron binding energy  $\Rightarrow$  underestimation below, overestimation above

- composed four-parameter formula (Gilbert & Cameron):
   
conv. shifted Fermi gas formula at higher exc. energies only  
 at low exc. energies constant temperature formula  $C \exp\left(\frac{U}{T}\right)$   
 both parts smoothly joined

- back shifted Fermi gas model:

ground state position as adjustable parameter  $\Delta = \Delta_{\text{pair}} - \Delta_{BS}$   
 spin dependent level density:

$$\rho(U, t) = \frac{1}{24\sqrt{\pi}} \frac{2t+1}{5^3 a^{44}} \frac{\exp[2(a(U-\Delta))^{\frac{1}{2}} - t(t+1)/25^2]}{(U-\Delta+t)^{5/2}}$$

where  $a$  ... "a-parameter"

$t$  ... thermodynamic temperature:  $U-\Delta = at^2 - t$

$\sigma^2$  ... spin cut-off parameter, describes spin distribution

$$\sigma^2 = \frac{I_{\text{app}} \cdot t}{t^2} = \eta \frac{I_{\text{rigid}} \cdot t}{t^2} \quad \text{with } \eta = \frac{I_{\text{app}}}{I_{\text{rigid}}}$$

fitting procedure:

$$N_0 = \int_0^{U_0} \rho(U) dU = F(a, \Delta, A, U_0)$$

number of levels up to  $U_0$ , summed over all spins

$$\frac{2}{J_{l=0}} = \left\{ \begin{array}{l} \rho(S_n + \frac{1}{2}\Delta E, It + \frac{1}{2}) + \rho(S_n + \frac{1}{2}\Delta E, It - \frac{1}{2}) \\ \rho(S_n + \frac{1}{2}\Delta E, \frac{1}{2}) \end{array} \right\} = G(a, \Delta, A, S_n + \frac{1}{2}\Delta E, It) \quad \text{for } \begin{cases} It \neq 0 \\ It = 0 \end{cases}$$

$D_{l=0}$  ... spacing of  $l=0$  resonances of one parity, averaged over  $[S_n, S_n + \Delta E]$

for both parities: factor 2

$F(\dots)$  and  $G(\dots)$  each represent a curve in the  $(a, \Delta)$  plane;  
 only  $(a, \Delta)$  corresponding to their crossing point reproduce  
 $N_0$  and  $D_{l=0}$  simultaneously

- Δ... large negative for odd nuclei
- slightly -"-" for odd mass nuclei
- moderately positive for even nuclei

$$\Delta_{BS} = \Delta_{pair} - \Delta \quad \left. \begin{array}{l} \\ \end{array} \right\} \text{show shell effects}$$

a-parameters

### — BCS model for microscopic calc. of level density

In order to account for effect of shell structure and pairing  
on the energy dependence of the level density  
not for "routine calculations" of XS's

### — semi-empirical level density formulae : Kataria & Ramamurthy

Jensen

Ignatyuk

parametrization of shell effects in terms of shell correction to  
nuclear ground state mass

also account for pairing

This type of parametrization is extremely useful for applications

△ for deformed nuclei : enhancement of level density by  
rotational degree of freedom

△ density of transition states in the continuum is calculated  
in the same way as level densities at equilibrium de-  
formation ; excitation energy refers to the lowest trans-  
ition state

## 2) Pre-equilibrium model (exciton)

starting from simple configuration the composite system is assumed to equilibrate through a series of two-body collisions and to emit particles from all intermediate states

$$\text{exciton number : } n = p + h$$

particles holes (no distinction between protons & neutron

$$\text{state density } \omega(p, h, E) = \frac{2(2E - A_{p,h})^{p+h-1}}{p! h! (p+h-1)!}$$

$$A_{p,h} = \frac{p^2 + h^2 + p - 3h}{4}$$

Tsallis principle correction

e.g. single particle state density

residual interactions : assumed to be energy conserving and two-body in nature  $\Rightarrow$  transitions  $\Delta p = \Delta h = 0, \pm 1$

rates for these transitions :

$$\lambda_+ (p, h, E) = \frac{2\pi}{h} M^2 \omega(p+1, h+1, E)$$

$$\lambda_0 (p, h, E) = \frac{2\pi}{h} M^2 \omega(p, h, E)$$

$$\lambda_- (p, h, E) = \frac{2\pi}{h} M^2 \omega(p-1, h-1, E)$$

where  $M$  ... average matrix element:

$$M^2 = k A^{-3} E^{-1} (\text{MeV}^2)$$

or, more exactly:

$$M^2(n, E) = \frac{k'}{A^3 e} \left(\frac{e}{7 \text{MeV}}\right)^{\frac{1}{2}} \left(\frac{e}{2 \text{MeV}}\right)^{\frac{1}{2}} \quad e < 2 \text{ MeV}$$

$$M^2(n, E) = \frac{k'}{A^3 e} \left(\frac{e}{7 \text{MeV}}\right)^{\frac{1}{2}}$$

$$2 \leq e < 7 \text{ MeV}$$

$$M^2(n, E) = \frac{k'}{A^3 e}$$

$$7 \leq e \leq 15 \text{ MeV}$$

$$M^2(n, E) = \frac{k'}{A^3 e} \left(\frac{15 \text{ MeV}}{e}\right)^{\frac{1}{2}}$$

$$15 \text{ MeV} < e$$

$$e = \frac{E}{n}$$

Average rate of emission of particle of type  $\nu$  with energy  $\varepsilon_\nu$ :

$$\lambda_\nu^e(n, \varepsilon_\nu) d\varepsilon_\nu = \lambda_\nu^e(p, h, E, \varepsilon_\nu) d\varepsilon_\nu = \\ = \frac{2s_\nu + 1}{\pi^2 \hbar^3} \mu_\nu \varepsilon_\nu \sigma_\nu(\varepsilon_\nu) R_\nu(p) \frac{w(p-p_\nu, h, E-\varepsilon_\nu)}{w(p, h, E)} d\varepsilon_\nu$$

from "detailed balance" (quasi equilibrium)  $\Rightarrow$  justification ??

$p_\nu$  ... nucleon # }  
 $s_\nu$  ... spin }  
 $\mu_\nu$  ... reduced mass } of particle  $\nu$   
 $B_\nu$  ... binding energy }

$\sigma_\nu(\varepsilon_\nu)$  ... inverse reaction XS (replaced by OM abs. XS)

$R_\nu(p)$  ... factor which takes account of distinguishability of partons from neutrons:

If  $p_\nu$  nucleons are imagined to be chosen at random from among the  $p$  excited particles available,  $R_\nu(p)$  is intended to give the probability that they have the right combination of protons and neutrons to make a particle of type  $\nu$ :

$$R_\nu(p) = \left(\frac{\bar{z}}{A}\right)^{q_\nu} \left(1 - \frac{\bar{z}}{A}\right)^{p_\nu - q_\nu} \binom{p_\nu}{q_\nu}$$

$\bar{z}$  ... charge # of composite system

$q_\nu$  ... parton # of particle  $\nu$

### Nucleon induced reactions:

a) nucleon emission:  $R_\nu(p) = \frac{n+1}{n}$

+ ... if projectile & yechile of same type  
 - ... " " diff. - " -

b)  $\alpha$  particle emission:  $R_\nu(p) = \frac{q K_{n-1}^\alpha}{q K_n^\alpha + (1-q) K_n^\nu}$

$q$  ...  $\alpha$  cluster formation probability

$K_{n-1}^\alpha, K_n^\alpha, K_n^\nu$  ... tabulated constants

$p_\nu = 1 \leftarrow \alpha$  cluster considered as 1 nucleon!

### A) Master equation approach

$P(p, h, t)$  ... occupation probability = probability that the system will be found in a state with  $p$  particles and  $h$  holes at time  $t$   
 differential equation describing the approach of the nucleus towards statistical equilibrium: master equation:

$$\frac{dP(p, h, t)}{dt} = P(p-1, h-1, t) \lambda_+ (p-1, h-1, E) + P(p+1, h+1, t) \lambda_- (p+1, h+1, E) - P(p, h, t) [\lambda_+(p, h, E) + \lambda_-(p, h, E) + \sum_{\nu} \int_{\varepsilon_{\nu}^{\text{max}}} d\varepsilon_{\nu} \lambda_{\nu}^c (p, h, E, \varepsilon_{\nu})]$$

one such equation for each allowed class of  $p$ - $h$ -configurations  
 at time  $t=0$ : initial particle and hole number :  $P(p, h, 0) = \underbrace{\delta_{pp_0} \delta_{hh_0}}$

initial cond. for numer. integration

spectra emitted up to equilibrium time  $T$ :

$$\frac{d}{d\varepsilon_{\nu}} \sigma_{\nu} (\varepsilon_{\nu}, T) d\varepsilon_{\nu} = \sigma_{\text{abs}} \cdot \sum_p \lambda_{\nu}(p, h, \varepsilon_{\nu}) d\varepsilon_{\nu} \int_0^T P(p, h, t) dt$$

PE component of the energy spectrum of particles of type  $\sim$

$\sigma_{\text{abs}}$  ... comp. nucleus formation  $\times S$

$T$  ... time when all states in the system are equally populated

### B) Random walk approach

occupation probabilities are not considered as functions of time but as functions of the # of internal transitions that have already taken place

$b^{(k)}(n) \equiv b^{(k)}(p, h)$  ... population probability of the states of a  $p$ - $h$ -config.  
 nation resulting from  $k$  internal transitions

$$b^{(k+1)}(n) = b^{(k)}(n+2) \frac{\lambda_{-}(n+2)}{\lambda(n+2)} + b^{(k)}(n) \frac{\lambda_{+}(n)}{\lambda(n)} + b^{(k)}(n-2) \frac{\lambda_{+}(n-2)}{\lambda(n-2)}$$

with  $\lambda(n) = \lambda_-(n) + \lambda_0(n) + \lambda_+(n) + \lambda^c(n)$  where  $\lambda^c(n) = \sum_{\nu} \int_{\varepsilon_{\nu}^{\text{max}}} d\varepsilon_{\nu} \lambda_{\nu}^c (n, \varepsilon_{\nu})$

initial population probability :  $b^{(0)}(n) = \delta_{nn_0}$ , i.e.:  $b^{(0)}(p,h) = \delta_{pp_0} \delta_{hh_0}$   
 successive application of the above equation describes quilibrium process  
 with increasing  $k$  the ratio  $\frac{b^{(k-1)}(n)}{b^{(k)}(n)}$  becomes independent of  $n$  and  $k$   
 $\Rightarrow$  upper limit  $K$  for the number of internal transitions to be considered for PE decay ( $\hat{=}$  quilibrium time  $T$ ) from following condition:

$$\left| \frac{b^{(k-1)}(n)}{b^{(k)}(n)} - Q^{(k)} \right| < 0.01 * Q^{(k)} \quad \text{for all } n \text{ and } k \geq K$$

where  $Q^{(k)} = \frac{\sum_n b^{(k-1)}(n)}{\sum_n b^{(k)}(n)}$

PE spectrum (part. type,  $\gamma$ ):

$$\frac{d\sigma_v^{\text{PE}}}{d\varepsilon_v} d\varepsilon_v = \sigma_{\text{abs}} \sum_{k=0}^K \sum_n \frac{b^{(k)}(n)}{\lambda(n)} \frac{\lambda_v^e(n, \varepsilon_v)}{\lambda(n)} d\varepsilon_v$$

Fraction  $q^{\text{PE}}$  of the initial population which survives PE:

$$q^{\text{PE}} = 1 - \sum_{k=0}^K \sum_n b^{(k)}(n) \frac{\lambda^e(n)}{\lambda(n)}$$

Closed form expressions for PE emission spectra result from "random walk equations" by neglecting the rates  $\lambda_+(u)$  and  $\lambda_0(u)$ :

$$\frac{d\sigma_v^{\text{PE}}}{d\varepsilon_v} d\varepsilon_v = \sigma_{\text{abs}} \sum_{n=n_0}^{\infty} D_n \frac{\lambda_v^e(n, \varepsilon_v)}{\lambda_+(n) + \lambda^e(n)}$$

$$\overline{n} = \sqrt{2gE}$$

most probable acc. #

$$D_n = \prod_{n'=n_0+2}^n \frac{\lambda_+(n')}{\lambda_+(n') + \lambda^e(n')} \quad D_{n_0} = 1$$

"depletion factors"

## V) SURVEY OF NUCLEAR MODEL COMPUTER CODES

### 1) Optical model (and equilibrium compound nucleus model)

(Ref.)	Features regarding optical model	Features regarding equilibrium CN model
<b>CERBERO</b> F. Fabbri et al., Rept. RT/FI(74) 36 (1974) Rept. RT/FI(77) 6 (1977)	spherical opt. pot., local, non-local and local equivalent of non-local pot.	binary reactions, emission of n, p, d, g. WFC for continuous channels. Improvement of Gilbert-Cauchois level density at low exc. en.
<b>COMNUC / CASCADE</b> (C. Dunford, Rept. AI-AEC-12931 (1970))	spherical opt. pot.	XS <sup>s</sup> for (n,g), (n,n'), (n,gn), (n,2n), (ng), (u,n'). Gamma-ray cascades. Single humped fission barrier.
<b>CRAPONE</b> F. Fabbri et al., Rept. RT-FI(77) 3 (1977)	spherical opt. pot., local, non-local and local equivalent of non-local pot. Automatic search on total, differential elastic and abs. XS, s- and p-wave str. fcts. and scattering radius	
<b>DWUCK-4</b> P.D. Kunz, unpubl.	DWBA method. Transfer reactions and inelastic scatt., optionally deformed opt. pot. for inelastic scatt.	
<b>ELIESE-3</b> S. Igarashi, Rept. JAERI 1224 (1972)	spherical opt. pot., local and non-local pot. Automatic search on diff. el. XS <sup>s</sup> and polarizations (spins $\frac{1}{2}$ and 1).	binary reactions. All types of XS <sup>s</sup> involving absorption and emission of n, p, d, a.
<b>ERINNI</b> F. Fabbri et al., Rept. RT/FI(77) 4 (1977)	spherical opt. pot., local, non-local and local equivalent of non-local pot.	binary and ternary reactions: (x,a), (x,ab), (x,abc) where x can be n, p or d and b can be n, p, d or g, c can be n or g

IUPITOR-1 T.Tanura, Rept. ORNL-4152(1962)	deformed opt. pot., coupled channels calc. Variety of different coupling schemes for vibr. and rot. nuclei is provided for.	
PELINSKA C.A. Engelhardt et al., Rept. PEL-202 (1974)	spherical opt. pot. Automatic search on total, diff. elastic and reaction XS <sup>s</sup> and polarizations (eqiv $\frac{1}{2}$ ).	reactions of type (ab) and (a,bg) differential and integrated XS <sup>s</sup> for up to 33 levels of each residual nucleus. Decay & angular correlations.
GENDA F.Purey, unpubl.	spherical opt. pot. Automatic search on total, diff. elastic and abs. XS <sup>s</sup> for different nuclei simultaneously.	
ECIS J.Raynal IAEA-SMR-9/8(1972)	deformed opt. pot. coupled channels calcs.	
SCAT2 O.Berillon Rept.CEA-N-227	spherical opt. pot., local pot. and local equivalent of non-local pot.	
ABAREX (new version of ABACUS) T.A. Moldauer, unpubl.	spherical opt. pot. (local)	elastic & inelastic scatt., capture, fission. WFC

## 2) Pre-equilibrium and equilibrium CN model codes

Code Ref.	Features of the models	Decay modes	Calcd. quantities
ALICE - 80 M. Blaum, Rept. COO-3494-29 (1975), Rept. UR-NSRL-181 (1981)	(geometry dependent) hybrid model, multi-step Wüskopf-Swing with approx. treatment of aug. mom. Single humped fission barriers.	n, p, d, $\alpha$ , f Residual nuclei may be out of a grid, 11 mass units wide and 9 charge numbers deep.	Particle spectra, activation & production XS, fission XS.
AMALTHEE D. Bersillon et al., Rept. NEANDCE 191 "L" (1977)	Exciton model, time integrated master eqn. gives PE and equil. con- tribution. Approx. treat- ment of 2 <sup>nd</sup> chance PE. No aug. mom. effects.	n, p, d, t, $^3\text{He}$ , $\alpha$ , $\gamma$ Binary and ternary reactions. Inversi. XS all input.	Particle spectra
GNASH P.G. Young et al., Rept. LA-6947 (1977)	Exciton model plus semi-empirical direct reaction contribution. Multi-step Hauser- Feshbach, no WFC, $\gamma$ ray cascades, single humped fission barriers. Accepts dir. reaction input	n, p, d, t, $^3\text{He}$ , $\alpha$ , $\gamma$ , f Several reaction paths in 1 run, involving up to 10 decaying nuclei.	Particle spectra, $\gamma$ ray spectra, activation & production XS, isomeric state XS fission XS.
HAUSER - 5 F.M. Mann, Rept. HEDL-TME 78-83 (1978)	Exciton model plus semi empirical direct reaction contribution. Multi-step Hauser-Feshbach. Double humped fission barriers, compl. damping. Accepts dir. reaction input.	6 reaction pairs (in- cluding $\gamma$ and f). Binary and ternary reactions.	Particle spectra, double diff. XS for particles, activation XS, fission XS.

PREANG J.M. Akkumans et al., Rept. ECN 60 (1979)	Exciton model, generalized for ang. distrs. (Mantzouranis), time integrated master eqns. give PE and equil. contr. No ang. mom. effects.	n, p, d, t, $^3\text{He}$ , $\alpha$ Binary reactions only. Inverse XS's are input.	Particle spectra, double diff. XS's for particles.
PRECO-D C. Kalbach, unpubl.	Exciton model plus semi-empirical direct reaction, MSC and MSD contr. Weisskopf - Ewing. Single humped fission barrier. Phenomen. ang. distr. No ang. mom. effects.	n, p, $\alpha$ , f + 1 arbitrary particle. Binary reactions only. Inverse XS's are input.	Particle spectra, double diff. XS's for particles, fission XS.
STAPRE M. Uhl et al., Rept. IRK 76/01 + addenda	Exciton model for 1 <sup>st</sup> chance particle, multi-step Hauser Feshbach, $\gamma$ ray cascades. Double humped fission barrier, partial or compl. damping.	n, p, d, $\alpha$ , $\gamma$ , f Up to 6 emitted part., but one reaction path only. Transm. coeffs. are input.	Particle spectra, $\gamma$ -ray spectra, activation XS's, isomeric state XS's, fission XS.
TNG1 C.Y. Fu, Rept. ORNL/TM-7042	Exciton model for 1 <sup>st</sup> chance particle, considers ang. mom. Multi-step Hauser Feshbach, $\gamma$ ray cascades. Accepts dir. reaction input.	n, p, $\alpha$ , $\gamma$ Up to 3 emitted particles	Particle spectra, $\gamma$ ray spectra, double diff. XS's for particles. Act. XS's, isomeric state XS's
PENELOPE G. Rigo et al., Rept. NEAND C(E) 222	Exciton model for 1 <sup>st</sup> chance particle, considers ang. mom. and pairing in p-h-state densities. Multi-step Hauser Feshbach.	.	.

## VI) ABACUS

### 1) Program operation

#### a) Possible problems

#### CLASS 1

calculates scattering by an optical potential  
potential well is generated and the Schrödinger equation solved by  
partial waves

- Results:
- absorption coefficient  $\gamma_{ij} = e^{2i\delta_{ij}}$  ( $\delta_{ij}$ ... phase shift)
  - transmission — " —  $T_{ij} = 1 - 1/\gamma_{ij}$
  - partial reaction XS  $\sigma_{ij}$

\* for each  $l_{ij}$  up to an  $l_{max}$  ( $\leftarrow$  given as input or determined by an internal criterion)

• reaction cross section  $\sigma_{\text{reac}}$

- total — " —  $\sigma_{\text{total}}$
  - shape elastic — " —  $\sigma_{\text{shape}}$
  - angular distributions  $\frac{d\sigma}{d\omega}$
  - polarization  $P(\theta)$
  - for charged particles  $\frac{d\sigma}{d\omega}$  Rutherford
- } if desired; results in C.M. and lab. system

Incident particle may have spin 0 or  $\frac{1}{2}$

#### Including

- internal solution by numerical integration of radial Schrödinger equation
- external --- (beyond well cutoff) constructed from Bessel functions (neutral incident particle) or Coulomb functions (charged inc. part.)
- determination of 1 integration constant from  $\lim_{r \rightarrow 0} u(r) \rightarrow 0$
- " - of scattering matrix (absorption coefficient) from matching of logarithmic derivative at well cutoff

## CLASS 2

computes a bound state radial wave function for a specific  $l$  and  $j$   
 same problem as Class 1 except — only real parts of pot. considered  
 — energy is such that particle is bound

Results: radial wave function

internal and external logarithmic derivative

number of nodes inside well

energy eigenstate of particular  $l$  and  $j$ , if desired (by means of search)

### Procedure:

- either : — numerical integration of radial Schrödinger equation to well cutoff or even further, if desired
- search for energy eigenstates
- or : — construction of — " — (exponentially decreasing) form modified Hankel functions beyond well cutoff
- inward integration (numerical)

## CLASS 3

Solution of Class 1 problem to obtain transmission coefficients plus  
 Hauser-Feshbach calculation of compound elastic and inelastic  
 scattering cross sections

- Results:
- partial inelastic scattering  $\chi S^5$  for each excited level (compound) } without WFC
  - compound elastic  $\chi S$
  - total elastic  $\chi S$
  - $\frac{d\sigma_{inel}}{dw}$  shape, compound
  - $\frac{d\sigma_{inel}}{dw}$  compound

### Proceding:

solution of scattering by opt. pot. as Class 1  
then Hauser-Feshbach calculation:

$$\langle \sigma_{ab} \rangle = \frac{\pi}{k_a^2} \sum_j g_a \frac{\sum_i T_a^{ij} \sum_i T_b^{ij}}{\sum_{i''j''} T_c^{i''j''}}$$

$$\bar{I}, \bar{s}, \bar{I}_{\text{tot}} \rightarrow \bar{j}$$

j coupling scheme : 1.  $\bar{j} = \bar{l} + \bar{s}$       } (in ABACUS)  
2.  $\bar{j} = \bar{j} + \bar{I}_{\text{tot}}$

whereas in the channel spin coupling scheme : 1.  $\bar{I}_{\text{ch}} = \bar{s} + \bar{I}_{\text{tot}}$   
(in STAPRE)      2.  $\bar{j} = \bar{I}_{\text{ch}} + \bar{l}$

### CLASS 4

calculation of radial integrals

#### Results:

$$\int U_0 u_{(1)} U_1 u_{(2)} \dots U_n u_{(n)} n^{-n+2} r^n dr$$

where  $u_{(i)}$  ... partial radial wave functions of specified  $l, j$  and energy  
 $U_i$  ... operators, that may be unity

- pot. well components  $V_{re}, V_{im}, V_{so}, V_{coul}$
- diff. operators  $\frac{d}{dr}$  or  $\frac{d}{dr} \cdot \frac{1}{r}$

m ... input parameter

#### Proceding:

- calculation of radial wave fct. in (separate) Class 1 and 2 runs
- calculation of radial integrals by numerical integration

### b) Available well forces

Real:

- for nuclear part:
  - Saxon Woods
  - modified saxon Woods (squared off toward the interior square well)
  - special force, given by special subroutine or point by point
- for Coulomb part:
  - Ch pot. resulting from uniform charge distribution inside the well,  $\frac{1}{n}$  outside the well
  - special force, given by special subroutine or point by point

Imaginary:

- same force as real nuclear potential
- Saxon Woods (with parameters different from real potential)
- surface Gaussian
- derivative of the real well force
- derivative of Saxon-Woods (with parameters different from real pt)
- linear combination of volume force (as real potential) and surface force
- special force given by special subroutine or point by point

Spin-orbit: real and/or imaginary

- Thomas force
- special force given by special subroutine or point by point

### c) Comparison with experimental data

- Calc. for one set of parameters
- Parameter scan : variation of up to 5 parameters in the run
- Search : exp. data given as input, procedure seeking minimum  $\chi^2$  by a modified method of steepest descent (calculations at several values of one input parameter)

### d) Modified VARIUS (Vienna)

#### "ABACUSTL"

averaging over transmission coefficients with same  $l$  but different  $j$

$$\text{for } s = \frac{1}{2} : T_L(\varepsilon) = \frac{1}{2L+1} [ L T_{L,j=L-\frac{1}{2}}(\varepsilon) + (L+1) T_{L,j=L+\frac{1}{2}}(\varepsilon) ]$$

[necessary if transmission coeffs. are used as input for STAPRE, because it uses channel spin coupling scheme]

#### "ABACUST"

use of typ formula to account for fluctuation of level widths

$$\frac{1}{N(U,J,\Pi)} T_{j_0 l_0}(\varepsilon_0) T_{j_1 l_1}(\varepsilon_1) \text{ in Hauser-Feshbach formula}$$

with  $N(U,J,\Pi) = \sum_{i,j,l_i} T_{j_i l_i}(\varepsilon_i)$  is replaced by

$$\frac{1}{N_t(U,J,\Pi)} V_{j_0 l_0}(\varepsilon_0) V_{j_1 l_1}(\varepsilon_1) \{ 1 + \delta_{j_0} \delta_{j_1} \delta_{l_0 l_1} (W_{l_0 j_0} - 1) \} \quad (1)$$

$V_{j_l}$  ... modified transmission coefficient

$W_{l_j}$  ... elastic enhancement

$$\langle \sigma_{ab}^{tot} \rangle = \bar{\sigma}_a \bar{\sigma}_b \quad \text{for } a \neq b \quad (2)$$

$$T_a = \sum_b \langle \sigma_{ab}^{tot} \rangle = \sum_{b \neq a} \bar{\sigma}_a \bar{\sigma}_b + \langle \sigma_{aa}^{tot} \rangle \quad (3)$$

neglecting  $\frac{1}{k_a^2}$

$$\text{Elastic enhancement } \langle \sigma_{aa}^{tot} \rangle = \bar{\sigma}_a^2 W_a \quad (4)$$

Ansatz,  $\bar{f}_a = V_a X^{-\frac{1}{2}}$  where  $X = \sum_c V_c$

Using this ansatz in eq. (3):  $T_a = \sum_b \langle \sigma_{ab}^N \rangle = \bar{f}_a^2 W_a + \bar{f}_a \sum_{b \neq a} \bar{f}_b$

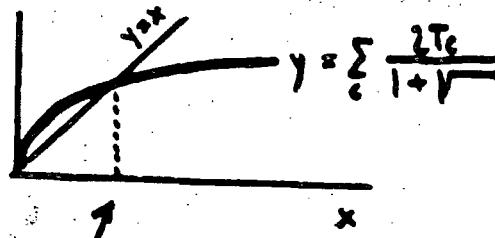
$$\begin{aligned} T_a &= \frac{V_a^2}{X} W_a + \frac{V_a}{X^{\frac{1}{2}}} \sum_{b \neq a} \frac{V_b}{X^{\frac{1}{2}}} \\ &= \frac{V_a^2}{X} W_a + \frac{V_a}{X^{\frac{1}{2}}} \left( \sum_b \frac{V_b}{X^{\frac{1}{2}}} - \frac{V_a}{X^{\frac{1}{2}}} \right) \\ &= \frac{V_a^2}{X} W_a + \frac{V_a}{X} (X - V_a) \end{aligned}$$

$$\underbrace{\frac{V_a^2}{X} (W_a - 1) + V_a}_{= T_a} = T_a$$

quadratic equation for  $V_a$ , can be solved for known  $T_a$  and  $W_a$

$$V_a = \frac{2T_a}{1 + \sqrt{1 + \frac{W_a - 1}{X} T_a}}$$

Determination of  $X$ : since  $X = \sum_c V_c \Rightarrow X = \sum_c \frac{2T_c}{1 + \sqrt{1 + (W_c - 1) X^{-1} T_c}}$



find solution numerically

Electric enhancement factor must be given.

Empirical relation for it:

$$W_a = 1 + \frac{2}{1 + \sqrt{T_a}} \rightarrow \begin{cases} 3 & T_a \ll 1 \text{ weak absorption} \\ 2 & T_a \rightarrow 1 \text{ strong } \text{--} \end{cases}$$

Approximation (used in ABACUST):

$$\frac{V_a}{\sum_c V_c} \approx \frac{T_a}{\sum_c T_c} \quad \text{need not calculate } X$$

$$\Rightarrow V_a = \frac{T_a}{1 + \frac{T_a}{\sum_c T_c} (W_a - 1)}$$

above relation  $W_a = 1 + \frac{2}{1 + \sqrt{T_a}}$  results also from this approximation

This approximation does not measure the normalization exactly.

## e) list of routines

Main ABACUS

Sr. AUTO automatic sequencing (searches and scan)

Sr. CALC for cont. state calcs. and control of bound state calcs.

Sr. EDIT edit of radial wave ft.

Sr. ETA phase shifts and radial wave ft. normalization

Sr. BESL spherical Bessel fits.

Sr. COUL Coulomb wave functions

Sr. COULA — " — special subroutine

Sr. PSUBL legendre polynomials and derivatives

Sr. FWDINT integration of Schrödinger equation in well

Sr. WELLS generation of potential wells

Sr. WREAD

Sr. WELR

Sr. WELI

Sr. WELS

Sr. WELC

} dummy to be replaced by special sr. generating { real  
spin-orbit } well  
Coulomb

Sr. BOUND calc. of bound state radial wave function

Sr. HNK1 (modified) Hankel functions

Sr. HFESH Hauser-Feshbach compound elastic and inelastic with aug. distr.

Sr. FWXINT integration beyond well cutoff

Sr. BKWINT — " — (inward) beyond well cutoff

Sr. NUIN1 integrand development (for integration)

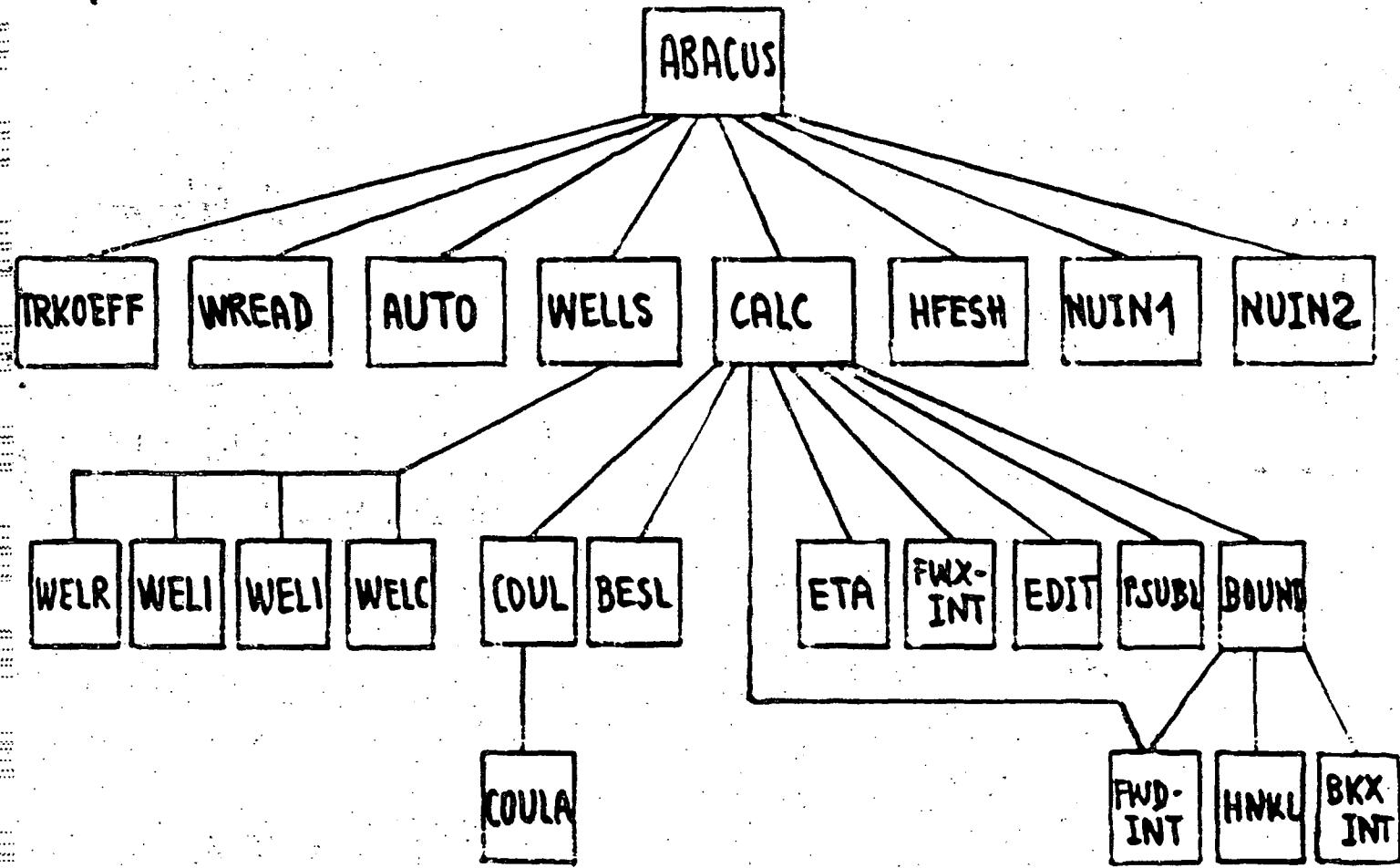
Sr. NUIN2 numerical integration

Ft. CLEB Clebsch-Gordan coefficients

Ft. RACAH Racah coeffs.

[ Sr. TRKOEFF averaging of transmission coefficients ] It is over

## f) Flow chart



## 2) Input

Control # 1 ... start of new problem

2 ... Call Trkoef if Abacustl, class 1, KT2≥1, else EXIT

Title

KLASS Class of problem to be calculated

KT1 (Class 3, 4)

Control # for whether or not the well parameters are retained unchanged for all levels (Class 3) or for all radial wave fcts. (Class 4)

KT2 (Class 3, Class 1 if AbacussII)

Control # for print/punch of Te

NOE (Class 3) : # of energy levels including ground state,  $\leq 25$

NOW (Class 4) : # of wave functions in integrand,  $\leq 6$

MM (Class 4) : power of r appearing in integrand of radial integral

KRE  
KIM  
KSO  
KCL

} (all classes)

control # for forms of various parts of pot. well

KPTS1 (all classes) : # of mesh points at which there is a potential acting  
(other than  $\frac{1}{r}$  C6 pot.); determines integration interval

      |      |      |      |      | KPTS1-1 intervals

r=0

$r = C_1$   
cutoff

$\leq 500$

KPTS2 (optional, Class 1, 2, 3) : # of mesh points at which a wave function will be calculated. For Class 1 and 3, KPTS2 > KPTS1 unnecessary

(optional, Class 4) : # of mesh points over which integration is to be performed

Control # for angles at which aug. distr. will be calc'd.

KP1 (Class 1, 3) : Output printing control (xs<sup>3</sup>, aug. distr<sup>3</sup>, pot<sup>3</sup>)

KP2 (Class 1, 2, 4) : — + — (wave fcts.)

KP3 (operative only with search or scan)

control # concerning input of exp. data and X<sup>c</sup> calc

KP4 (operative only with search or scan)

control # for suppressing print in dependence on X<sup>c</sup> value

KAUTO (all classes) : search and scan control

(operative only with search or scan)

KK1 dimension of parameter space searched or scanned

NOV (operative only with search or scan)

# of values of specified parameters at which calc. are made to compute a single  $\chi^2$

NOA (Class 1, 3)

number of angles calcd. (equally spaced with respect to angle or cosine) or given as input

Ignored if exp. data are supplied; thus define angle  $\leq 150^\circ$

KPS (operative only if KP2  $\neq 0$ ): wave fn. print control

KPC (all classes): well and wall parameters print control

KP7 Control number for special search ('SCHIFFER')

AIN (optional): mass of incident particle

RC (-" - ): radius of charge distribution

KP8 depending on value of KP7: punch control for aux. disk. or control for calc. of scaling factors for special search

ZZP charge product

AND mass of target nucleus

VRE

VIM

VIVOL

VSR

VSI

} well depths (MeV); may. ignored for Class 2

KTRLW input control for additional well parameters

VRE1

VRE2

VIM1

VIM2

} val & mag. well depth energy dependence

VX1

VX2

VX3

} additional parameters for special well subroutines

(KRE, KIM, KSO, KCL = 8)

C1 well cutoff (fm)

required for  $KRE = \phi, 1, 8, 9$ ; for  $KRE = 2 - 7$  C1 is set internally

$\left. \begin{matrix} R_1 \\ A_1 \\ R_2 \\ A_2 \end{matrix} \right\}$  val and imag. pot. geometrical parameters

C2 volume fraction of imag. pot.;  $0 \leq C2 \leq 1$

How to input combined volume & surface imag. potential:

1.  $\underline{\text{VIM}} \neq 0, C2 \neq \phi$

total imag. pot. depth

vol. part =  $C2 * \text{total imag. pot.}$  (obtained from VIM considering energy dependence)

surf. part = tot. imag. pot - vol. part

2.  $\underline{\text{VIM}} \neq 0, \underline{\text{VIVOL}} \neq 0, C2 = \phi$  (ignored if  $\neq \phi$ )

$\rightarrow$  surf.  $\rightarrow$  vol.

VIS = preliminary surf. term (obtained from VIM considering v. dep.)

VIV =  $- - - \text{vol. term} ( - " - \text{VIVOL} - " - )$

$$C2 = \frac{VIV}{VIV + VIS}$$

surface = pul. surface \*  $(1 - C2)$  } program internal renormalization

volume = pul. volume \*  $C2$

$\Rightarrow$  in order to use values  $\text{VIM}_{\text{actual}}, \text{VIVOL}_{\text{actual}}$ , one has to multiply them and the parameters for the energy dependence by  $\frac{(\text{VIVOL} + \text{VIM})_{\text{actual}}}{\text{VIM}_{\text{actual}}}$  in order to obtain these values after the internal renormalization

(0) wave function cutoff (fm)

necessary only if  $\text{KPTS}2 \neq \text{KPTS}1$

For class 4, CO is the upper limit of integration

$$CO < C1 : \frac{CO}{KPTS2-1} = \frac{C1}{KPTS1-1} [\pm 1] \text{ same mesh interval}$$

CO > C1 : " " not necessary  $\Rightarrow$  mesh interval beyond C1 may be different from that between n=0 and C1

### KTRLR Input control for radii

(actual radii  $\propto r_0$  in  $r = r_0 A^{1/3}$ )

Input by point potential wells (for KRE, KIM, KSO, KCL = 9)

In each potential : set of KPTS1 cards

E energy of inc. particle (Class 1,3) or binding energy (Class 2) (MeV)

LC lab./CM control

EJJ } l specification of partial wave to be printed/punched (Class 1,3)

ELL } or bound state to be computed (Class 2)

LMAX (Class 1,3) Max. orb. ang. mom.

internal criterion checks sufficiency of number of l's

KOP (Class 3) ang. distr. control (operative only if KP1  $\neq 0$ )

EJQ } (Class 3) { spin } of ground state of the target nucleus  
PIQ } { parity }

Energy level cards (Class 3,4)

Class 3 : NOE - 1 cards, one for each of the excited levels

Class 4 : NOW cards, one for each bound state

Angles (or cosines) list (Class 3)

for ang. distr. for excited levels

## Further comments on the input parameters

### Integration parameters

accuracy of numerical integration is determined by

- # of mesh points (KPTS1)
- cutoff (C1)
- reduced mass  $\mu$  (calcd. from AIN, ANO)
- energy (E)

Integration in terms of variable  $x = Kr$

$$\text{let } E' = |E_{cm} - V|$$

$$\Rightarrow \Delta x = 0.22 \sqrt{\mu E'} \frac{C1}{KPTS1-4}$$

values must be chosen so that  $\Delta x \ll 1$  radian

### Search and scan control

Types of search and scan procedures :

- a) single parameter search : one parameter varied to obtain a match between one of the calculated quantities and a given comparison value for that quantity ( $KAUTO = 1$ )
- b) parameters space scan : 1-5 parameters varied and calcs. performed for each set of parameters ( $KAUTO = 2$ )
- c) minimum  $\chi^2$  search : 1-5 parameters varied to obtain min.  $\chi^2$  with respect to comparison values given as input ( $KAUTO = 3$  or  $4$ )

additional input necessary

## Comparison with experimental values

Calculation of  $\chi^2$ :

$$\chi^2 = \sum_{i=1}^{NOV} \left( \sum_j w_i (\sigma_j^{calc} - \sigma_j^{exp})^2 + \frac{1}{N} \sum_j w_j (d\sigma_j^{calc} - d\sigma_j^{exp})^2 \right)$$

↑  
not aug. distr.

↑  
aug. distr.

$w_i, w_j$  ... weights, determined by the code ( $KAUTO = 3$ )  
or given as input ( $KAUTO = 4$ )

sum is taken over the NOV values of one of the parameters

additional input necessary

## Changes between problems

If new problem is identical in all respects to previous one but for changes in a few parameters, following procedure may be used:

- parameters which are relevant to class and well types can be changed
- control card entries and levels (class 3) and wave fcts. (class 1)  
may not be changed

\* by "change cards" (change control #, control # for parameter changed, new value)

### 3) Output

Computers success depends on values of output control parameters

Minimum output comprises well parameters and results

With explanatory

Useful:

- check of well parameters
- when performing a search, review variation of  $\chi^2$  and of parameters during the course of the search ("local minimum")?
- when comparing data "externally" (plot or by hand)

1. be aware of the meaning of  $\sigma_{\text{reac}}$ :

in ABACUS:  $\sigma_{\text{reac}}$  is the total compound nucleus reaction XS  
so it comprises comp. el. scattering also.

Other nomenclature:  $G_{\text{abs}} = \sigma_{\text{comp. el.}} + \sigma_{\text{reac}}$

total comp. nucleus  
reaction XS

XS for non-elastic  
comp. nucleus reactions

2. use the following relations for potential scattering radius and strength fcts.:

$$S_1 = \frac{1}{2\pi} \sqrt{\frac{E_0}{E}} \frac{1}{T_1} \frac{(l+1) T_{1,j} = l+1/2 + \frac{1}{2} T_{2,j} = l-1/2}{2l+1}$$

Str. fcts.

$$P_0 = 1$$

$$P_1 = \frac{(ka)^n}{1 + (ka)^n}$$

} penetration factors

$$E_0 = 1 \text{ eV}$$

n ... radius of  
nat. pot.

$$R' = \sqrt{\frac{G_{\text{sh. el.}}(E_0)}{4\pi}}$$

potential scattering radius

## VII) IUPITOR

### i) Program description

#### a) Types of problems

Solution of scattering problem by means of CCC

- spin of projectile 0,  $\frac{1}{2}$ , 1 ( $0, \frac{1}{2}$  for ACC)
- target nucleus of some collectivity of either even or odd A
  - vibrational (spherical)
  - rotational (deformed)
- for deformed target nucleus: NACC or ACC
- " " : excitation of states belonging to higher (vibrational) bands can be considered (NACC only)
- inclusion of Cb excitation
- force factor either real (RFF) or complex (CFF)
- up to six states can be coupled at one time
- up to 30 partial waves can be coupled at one time  
(up to 25 " - , if projectile energy becomes negative in some excited channels)
- $l_{\max} = 69$
- computation of diff. XS<sup>s</sup> for up to 100 angles for any number of states (up to 35 angles if polarized beam or target); computation of total and reaction XS and s- and p-wave str. pct (only diff. d. and total XS for ACC)
- if projectile is a neutron, its energy in some excited channels can be negative
- automatic plot of theoretical and experimental diff. XS<sup>s</sup> and polarizations

## b) Modified version

### KARLSRUHE

Δ Automatic search routine for fitting experimental data:

$$\chi^2 \text{ minimizing routine in order to minimize the sum}$$

$$S = \sum_{i,n} \left( \frac{\sigma_{\text{exp}}^{(n)}(\theta_i) - \sigma_{\text{calc}}^{(n)}(\theta_i)}{0.1 * \sigma_{\text{exp}}^{(n)}(\theta_i)} \right)^2 + \sum_{i,m} \left( \frac{P_{\text{exp}}^{(m)}(\theta_i) - P_{\text{calc}}^{(m)}(\theta_i)}{0.1} \right)^2$$

overall error of 10%.

$n$  } number of exp. { cross sections } in set  
 $m$  } polarizations }

additional input required

Δ Improvement of rotational model treatment

- nucl. pot.: inclusion of terms with  $\lambda=8$  (Legendre expansion)
- Ch. pert.: — II — — II — up to 2<sup>nd</sup> order (Taylor — II —)

VIENNA (on the basis of KARLSRUHE version)

Δ Integration of differential XS' with respect to angle

$$\sigma_n^{(s)} = \int \sigma_n^{(s)}(\theta, \phi) d\cos \theta d\phi =$$

$$= \frac{4\pi}{k_n^2} \sum_{m_1 M_1} \sum_{m_2 M_2} \sum_{l_1 l_2} \sum_{j_1 j_2} \sum_{l_1' l_2'} \sum_{j_1' j_2'} |a_{m_1 l_1} b_{m_2 l_2}|^2 C_{l_1 j_1; m_1 j_1}^* C_{l_1' j_1'; m_1' j_1'} (l_1 s_0 m_1 | j_1 m_1) (j_1 I_1 m_1 M_1 | j_1')$$

$$* a_{m_2' l_2'} b_{m_1' l_1}^* C_{l_2 j_2; m_2 j_2}^* (l_2 s_0 m_2' | j_2 m_2) (j_2 I_2 m_2' M_2' | j_2')$$

### $\Delta$ Extraction of transmission coefficients :

$$\begin{aligned} T_{11j}^3 &= 1 - \sum_{n'l'j'} |S_{n'l'j'; 1l_j}|^2 = \\ &= 1 - \sum_{n'l'j'} \frac{2l'+1}{2l+1} \frac{k_i^2}{k_n^2} |f_{an} f_{al} f_{jj'} + 2i C_{l,j; n'l'j'}|^2 \end{aligned}$$

$$T_{11} = \sum_{j=|I-j|}^{I+1} g^3 T_{11j}^3 / \left( \sum_j g_j \right) \quad \text{where} \quad g_j = \frac{2j+1}{(2I+1)(2s+1)}$$

$$\triangleright T_1 = \frac{2s+1}{2j+1} \sum_j g^3 T_{11j}^3$$

$$\text{for } s = \frac{1}{2} : \quad T_1 = \frac{1}{2j+1} ( (T_{11j} = l-j_2 + (l+1) T_{11j} = l+1/2) )$$

### c) list of routines

Serial #

- 1 Main IUPITOR reads input cards and outputs them immediately
- 2 { Sr. CCCTRL control of coupled channels calc., fixes basic quantities and calls subroutines  
Sr. NLJJJK set up nly of the partial waves coupled together for given JT
- 3 { Sr. FLGLCH } (b.fcts.) for { pos. } energy projectiles at matching radius  
Sr. FLGLNG }
- 4 Sr. POTENT compute potentials that appear in the coupled equation
- 5 { Sr. COUPLE solves coupled equations (after geometrical part has been prepared by AMATRIX and BMATRIX)  
Sr. RANGE exponent shift for reals (Karlsruhe)  
Sr. BMATRIX < || || >  
Sr. AMATRIX AMATRIX = AMATRIX \* BMATRIX } coupling matrix element

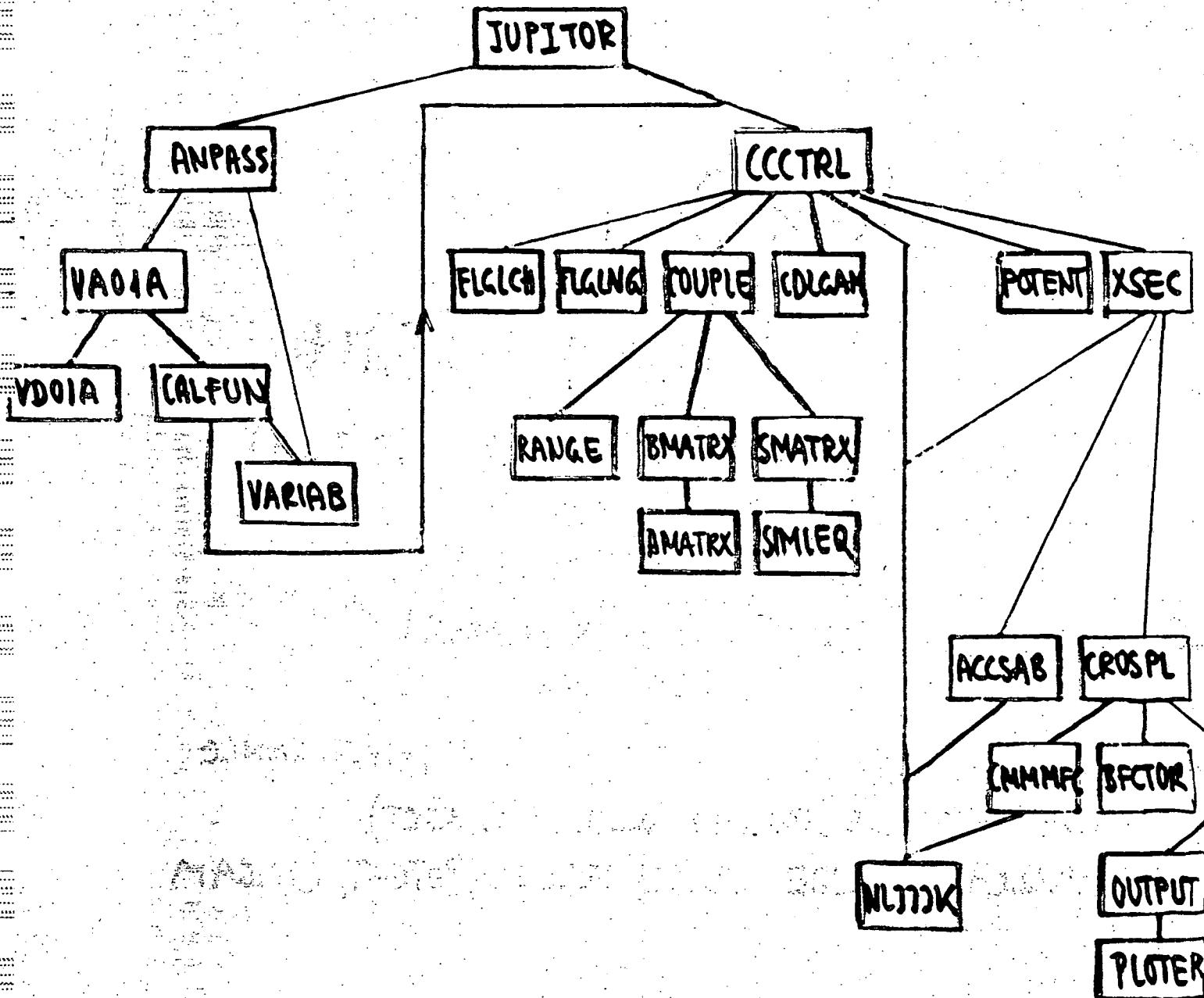
- 6 { Sr. SMATRIX constructs matching equations (using solution obtained with COUPLE)
- 7 { Sr. SIMLEQ solves matching equations  $\Rightarrow$  C matrix elements  
7 { Sr. XSEC partial summations of C matrix elements (NACC)  
7 { Sr. ACCSAB " " (Acc)
- Fr. CROSPL rest of summations of C matrix elements to obtain cross sections (with help of CMMMF<sub>C</sub>, BFCTOR)
- 8 { Fr. CMMMF<sub>C</sub> } take part in summations for computing XS<sup>S</sup>  
8 { Fr. BFCTOR }
- 9 { Sr. OUTPUT outputs the obtained results  
9 { Sr. PLOTER automatic plot of exp. and calcd. XS<sup>S</sup> and polarizations
- Sr. RACT Racah      } coefficients  
 Sr. CLEB Clebsch Gordon      }  

Sr. DOTEST check of whether indeed set of range (Karlsruhe)

Sr. ANPASS  
 Sr. VARIAR  
 Sr. CALFUN  
 Fct. CBRT  
 Fct. CDLGAM  
 Sr. VA01A  
 Sr. VDC1A  
 Fct. W3JS Wigner 3J symbols  
 Sr. TRANS transmission coefficients (Vienna)

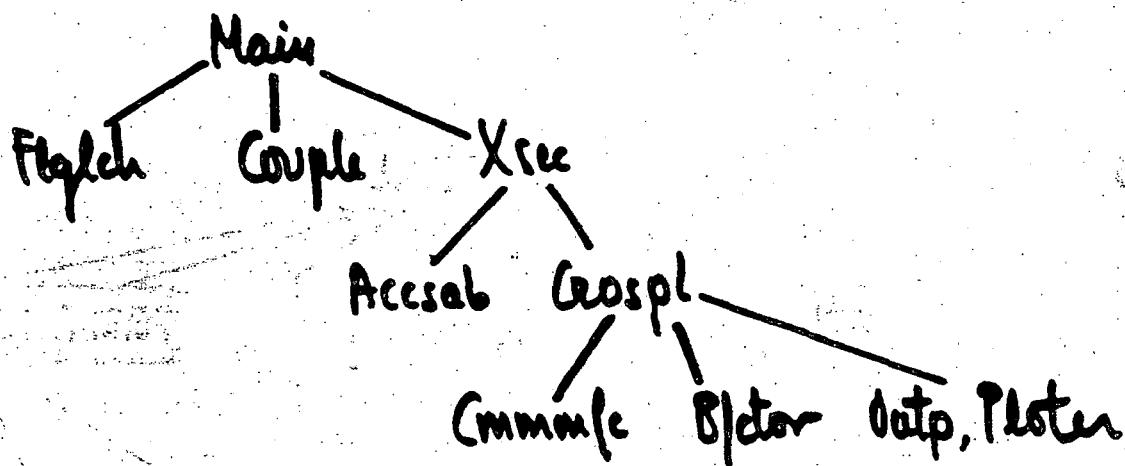
} Karlsruhe search procedure

d) Flow chart



Note : CBRT, CLEB, JTEST, RACT, W3JS are not contained in the flow chart. They are called by many of the above routines.

### e) Symmetrization



SUBXS TREE CROSPL - (CHMMFC, BFCCTOR, OUTPUT)

OUTPUT INCLUDE OUTPUT, PLOTTER

XSEC TREE XSEC - (ACCSAB, CROSPL)

COUP TREE COUPLE - (BMATRIX, SMATRIX)

SMATRIX INCLUDE SMATRIX, SIMLEQ

BMATRIX INCLUDE BMATRIX, AMATRIX, RACT, RANGE

IUP TREE IUPITOR - (FLGLCH, COUP, XSEC)

FLGLCH INCLUDE FLGLCH, FLGLNG, POTENT, CDLGAM

### f) Remarks on the numerical calculations

Dependence of various XS's on parameters and scheme of coupling

- set of states between the strong coupling is considered
- type of coupling

Notation : if imag. terms in  $v_{cp;2}^{(1)(v)}$ ,  $v_{cp;2}^{(2)(v)}$ ,  $v_{cp}^{(2)(v)}$  are

neglected : RFF (real form factor), otherwise CFF

takes only about half the comp. time

## Standard set of OM parameters (used for this investigation)

Nucleons < 30 MeV : F. G. Ferri, Phys. Rev. 131 (1963) 745

$$R_0 = \bar{R}_0 = R_C = 1.25 \text{ fm}$$

$$a = 0.65 \text{ fm}$$

$$\bar{a} = 0.47 \text{ fm } (A < 150)$$

$$\bar{a} = 0.76 \text{ fm } (A > 150)$$

$$V_{SO} = 7.5 \text{ MeV}$$

$$W = 0$$

$$V \quad \} \text{ varied, starting point: } \{ (52.2 - 0.3 E) \text{ MeV}$$

$$W_0 \quad \} \text{ varied, starting point: } \{ 11.5 \text{ MeV } (\leftarrow \text{without coupling})$$

## Studies of dependence on parameters and coupling scheme

(i) comparison vibrational - rotational, same A and  $Z$  ( $^{156}\text{Gd}$ , in reality def.)

CFF

$$0^+ - 2^+ - 4$$

in matrix el.:  $0^+ - 2^+ 1 \text{ qu.ph.}$

$$2^+ - 4^+ - \dots \} \text{ same } \beta_2$$

$$0^+ - 4^+ 2 \text{ qu.ph.}$$

CFF, ACC

$\lambda' = 2$  highest order of def. in expansion of radius

$$\beta_2 = .32$$

"ideal vibrator"

$$\beta_2 = .2$$

$$\frac{d\sigma}{d\Omega}$$



— not.  
--- vibe.

- structure of XS is much more pronounced in vibrational case than in deformed case
- use of different  $\beta_2$  in vibrational case leaves structure unchanged, but changes magnitude (not shown in figure)

(ii) vibrational nucleus : dependence of elastic scattering on coupling of higher states :

coupled calculation with  $W_0 = 7.5 \text{ MeV}$  almost coincides with uncoupled calculation with  $W_0 = 9.5 \text{ MeV}$

$\Rightarrow$  about 20% of the absorptive potential stored in the (pure) elastic case is accounted for by the coupling to the  $2^+$  state (when  $\beta_2 = .2$ )

$\Rightarrow$  fitting procedure vib. nuclei :

- global potential as starting point

- adjust  $V, W_0$  (or.  $V_{S0}$ ) to fit exp. diff. d.  $\chi S^2$

- $0^+ - 2^+$  coupling with reduced  $W_0$  (20%), adjust  $\beta_2$  to fit data

- couple to two phonon states :

- increase the above  $\beta_2$  by  $\sim 10\%$  when coupling to 2 ph. st. reduces  $\chi S$  of 1 ph. st.

- adjust  $\beta_2$  values for coupling between 1 ph. st. - 2 ph. st.

by fit to  $\chi S$  curve

$$\frac{B(E2; 0 \leftrightarrow 2)}{B(E2; 2 \leftrightarrow 1)} = \left( \frac{\beta_{02}}{\beta_{21}} \right)^2$$

'red. electric transition probability'

ratio is measure of how badly the simple harmonic nature of the vibration is violated  
 $\rightarrow$  important from the nuclear structure point of view

(iii) rotational nuc. : dependence of elastic scattering on coupling of higher states :

## NACC, Legendre expansion of potential

diag. part contains  $v_{cp}^{(\lambda=0)(r)}$  (r) which is a fct. of  $\sum \beta_{\lambda} Y_{\lambda}^0$

diag. pot. not the same if  $\beta_2 = 0$  or  $\neq 0$

$\rightarrow$  elastic scattering XS is fct. of  $\beta_2$  even if there is no coupling to higher state

$\Rightarrow$  adjustment of  $W_D$  does not compensate for coupling

$\Rightarrow$  no step by step parameter adjustment procedure

This does not matter for ACC, since one has to solve coupled equation, irrespective of how many states are considered

(iv) a) vibrational red.: dependence of 1 ph. st. XS on  $W_D$  and coupling scheme:

$0^+ - 2^+ - 3^- - 3^-$

$1\text{qu.ph.}$       |      \  
      1 oct.ph.      1 qu.ph., 1 oct.ph.

consider XS of 1<sup>st</sup> 3<sup>-</sup> state:

- RFF - CFF affects position of maxima and minima  
 $\rightarrow$  CFF preferable

- setting off 2<sup>nd</sup> 3<sup>-</sup> state  $\Rightarrow$  1<sup>st</sup> 3<sup>-</sup> increased

- assuming  $0^+ - 3^-$  coupling  $\Rightarrow$  — || —

although 2<sup>+</sup> and 1<sup>st</sup> 3<sup>-</sup> coupled only indirectly through separate coupling to ground state

but:  $0^+ - 2^+$  coupling accounts for ~20% of the absorption

$\Rightarrow$  leaving out 2<sup>+</sup> st. similar to change in  $W_D$ , and can in fact be compensated by it

- b) vibrational nucl.: comparison of  $0_0^+ - 2_1^+ - 0_2^+ - 2_3^+ - 4_2^+$  coupling to separate coupling  $0_0^+ - 2_1^+ - 0_2^+$  and  $0_0^+ - 2_3^+ - 4_2^+$   
 $\Rightarrow$  two ph. st.  $X5^3 \sim 10\%$  larger with separate coupling  
 $\Rightarrow$  separate calc. can cause  $\sim 5\%$  error in  $\beta_2$  values  
 $\Rightarrow \beta_2$  values depend on coupling scheme

this ambiguity could be removed if a sufficiently large number of states could be coupled and it is assumed that the same  $W_D$  can be used in all the channels large numbers of states impossible with presently available computers  $\rightarrow$  effect of neglected coupling to the possible higher excited states is taken into account phenomenologically by using large values of  $W_D$  in the higher excited coupled states than are used in the lower coupled states: "fudging"

- (v) rotational nucl.: dependence of various  $X5^3$  on coupl. scheme RFF, NACC-ACC, some parameters

large difference (in magnitude) in exc. states of ground band  
 If requirements of ACC ("ideal rotational band" = low excitation energies of exc. states, relatively high exc. energy)  
 are fulfilled, ACC results are more accurate than those of NACC,  
 if in NACC not all states are coupled, because in ACC coupling  
 of all members of grd. st. band is accounted for automatically

(vi) rotational nucle.: comparison power series expansion - Legendre exp.  
 ACC... drastic differences between the two calculations, although  
 somewhat better if one goes to higher order in power  
 series expansion and  $\lambda=4$  in Legendre expansion

NACC... even worse

$\Rightarrow$  power series expansion should not be used for well de-  
 formed nuclei

(vii) rotational nucleus, ACC, comp. protons-neutrons

- in neutrons:
  - oscillations in elastic XS
  - $2^+$  XS much larger

(viii) magnitude of  $V_{S0}$ :

if it turns out that one can put  $V_{S0}=0$  without  
 losing much accuracy of the result  $\Rightarrow$  assume spin=0,  
 at least for parameter search  $\Rightarrow$  saving of comp. time  
 Not to be used for polarizations, of course

## 2) Input

KTRL(N), N=1,...,28 control numbers, specify different uses of the  
 program

$$\text{KTRL}(1)=\begin{cases} 0 & \text{target core A} \\ 1 & \text{-" - odd A} \end{cases}$$

$\text{KTRL}(2)>0$  range of vals is limited to  $\exp(\text{KTRL}(2))$  in COUPLE  
 (Karlsruhe)

$$\text{KTRL}(3)=\begin{cases} 0 & \text{only diff. XS} \\ 1 & \text{diff. XS}^s, \text{total reaction XS}^s, s \& p \text{ wave str. fcts.} \\ 2 & \text{total, reaction XS}^s, s \& p \text{ wave str. fcts.} \end{cases} \text{are computed}$$

$KTRL(4) = 1$  vibr. nuc. : contribution of coupling terms quadratic  
in  $\alpha$  to diagonal potential are considered

$KTRL(5) = 1$  parameter search is performed, with additional data  
(Karlsruhe)

$KTRL(6) = \begin{cases} 1 & \text{direct (a exc.)} \\ 2 & \text{direct and multiple (b exc.)} \end{cases}$  } added for rotational nuc.,  
Legendre expansion ( $KTRL(11) =$

$KTRL(7) = 1$  ACC

$KTRL(8) = \begin{cases} 1 & \text{both projectile and target initially polarized} \\ 2 & \text{only projectile} \\ 3 & \text{only target nucleus} \end{cases} \quad - \quad " -$

$KTRL(9) = \begin{cases} 1 & \text{range of } JJ \text{ and } K \text{ are restricted by} \\ 2 & \frac{1}{J \text{ or } \bar{m}_j} \quad \frac{1}{\pi} \end{cases} \quad \left\{ \begin{array}{l} KEXCOM(5,6,7) \\ KEXCOM(5,1) \end{array} \right.$

usually :  $JJ = 1, \dots, JJ_{MAX}$

where : • for vibr. nuc. & rot. nuc. with NACC ( $KTRL(7)=0$ )

$$JJ = J+1 \quad \text{if } J \text{ integer}$$

$$JJ = J+\frac{1}{2} \quad \text{if } J \text{ half odd integer}$$

$$JJ_{MAX} \text{ smallest integer } \geq l_{max} + J_1 + s + 1$$

- rot. nuc. with ACC ( $KTRL(7)=1$ ):

$$JJ = \bar{m}_j + 1 \quad \text{if } \bar{m}_j \text{ integer}$$

$$JJ = \bar{m}_j + \frac{1}{2} \quad \text{if } \bar{m}_j \text{ half odd integer}$$

$$JJ_{MAX} \text{ smallest integer } \geq l_{max} + s + 1$$

whereas :  $JJ = KEXCOM(5), \dots, KEXCOM(6)$

$K = KEXCOM(7)$  only considered parity } if  $KTRL(9)=1$

$JJ = KEXCOM(5), \dots, KEXCOM(6) \} \text{ if } KTRL(9)=2$   
no restriction of parity }

KTRL(10) unassigned

KTRL(11)=1 legendre expansion of potential (act. nucl.)

KTRL(12)=1 CFF

KTRL(13)=1 b exc. is added

KTRL(14) to (16) unassigned

KTRL(17)=1 theoretical den. diff XS's are divided by Rutherford XS

KTRL(18) ≠ 0 Suyibrecht - Friedeldey potential (Sienna)

KTRL(19)=1 ( $\bar{\sigma}, \bar{I}$ ) interaction is added (act. nucl., RFF only)

KTRL(20) to (24) unassigned

KTRL(25) ≠ 0 computation of transmission coefficients (Sienna)

KTRL(26) unassigned

KTRL(27)=1 segmentation option of original IUPITOR, splitting calc. in two runs. With KTRL(27)=1 it is assumed that C matrices were computed in previous run

KTRL(28) unassigned

KEXCOM(N), N=1,...,14 control parameters:

KEXCOM(1) unassigned

KEXCOM(2) number of mesh points (within matching radius) if no b exc.

{ default: IFIX [max( $r_0 A^{1/3} + 10a$ )]/DX }  
 of real, vol. im., surf. im.; so }  
 : mesh size  
 matching radius }  
 (KTRL(13)=0)

KEXCOM(3) unassigned

KEXCOM(4) ≠ 0 number of redefinition of number of meshpoints if b exc. is considered (KTRL(13)≠0)

Previous number of meshpoints increased by KEXCOM(4);

This corresponds to increase of matching radius with respect to "coupling radius" up to which nucl. pot. is const.

KEXCOM(5) lower } limit for JJ summation if KTRL(9) ≠ 0

KEXCOM(6) upper }

KEXCOM(7) solely considered parity if KTRL(9) = 1

KEXCOM(8) to (11) unassigned

KEXCOM(12) spin of two qu. ph. state to which the even core is excited, if target is odd A with nucleus (ground state spin  $\frac{1}{2}$ ) (INTYPE = 5)

KEXCOM(13) number of three phonon states to be included in the calc. if the target is even A vibrational nucleus (only 0 or 1 allowed presently)

KEXCOM(14) number of partial waves ( $l_{\max} + 1$ )

KTLOUT(N), N=1, ... 28

KTLOUT(2n-1)=1 small } output from routine with "serial number" n  
 KTLOUT(2n)=1 extended } (see "list of routines")

EXTCOM(N), N=1, ..., 10 "extra common"

presently unused, useful if program is modified such that communication of a quantity from a routine to another is needed, and this quantity is to be given as input data

IICPLE number of coupled states in the target (if ACC is used (KTRL7) = 1)  
 IICPLE has to be = 1)

INTYPE, INTMAX control numbers specifying type of coupling

Cases :

INTYPE=2 even vibr. nucl., no quadrupole multi-phonon states considered

INTYPE=2, INTMAX=1: 1) SCOM (spherical) if IICPLE=1  
2)  $0^+$ - $I^{\pi}$  coupling if IICPLE $\neq 1$   
one ph. st. with natural parity ( $0^+, 1^-, 2^+$ , ...)

$\beta_2 \rightarrow VCOUPL(1)$

INTYPE=2, INTMAX=2:  $0^+ - 2^+ - 3^-$  coupling

1 qua.ph.      1 oct.ph.

$\beta_2 \rightarrow VCOUPL(1)$

$\beta_3 \rightarrow VCOUPL(2)$

[sums to be in error]

} only terms linear in  $\alpha$  cons.

INTYPE=2, INTMAX=5: 1)  $0^+ - 2^+ - 3^-$  coupling if IICPLE=3

also terms quadratic in  $\alpha$  are included

$\beta_2 \rightarrow VCOUPL(1)$  } used in lin. terms  $\langle 0;0||1\ 1\rangle$

$\beta_3 \rightarrow \dots (2)$

$\beta_2 \rightarrow \dots (3)$  } used in quadri. terms  $\langle 1;2||1\ 1;3\rangle$

$\beta_3 \rightarrow \dots (4)$

2)  $0^+ - 2^+ - 3^- - I^-$

quadrup. octup. 2 ph. st. ( $1^-, 2^-, \dots, 5^-$ )

$\beta_2 \rightarrow VCOUPL(1)$  } used in lin. terms  $\langle 0;0||1\ 1;2\rangle$

$\beta_3 \rightarrow \dots (2)$

$\beta_2 \rightarrow \dots (3)$  } used in bin. terms  $\langle 1;\lambda||1\ 1;I\rangle$

$\beta_3 \rightarrow \dots (4)$  } used in quadri. terms  $\langle 1;\lambda||1\ 1;\lambda_2\rangle$

90

INTYPE=3 even vibrational nucleus, quad. multi-photon states considered

1)  $0_0^+ - 2_1^+ - I_2^+$  ( $I_2^+ = 0_2^+, 2_2^+ \text{ or } 4_2^+$ ) with IIICPLE=3

2)  $0_0^+ - 2_1^+ - I_2^+ - I_2'^+$  ( $I_2^+, I_2'^+$  any combination)

{  $0_2^+, 2_2^+, 4_2^+$

} with IIICPLE=4

or  $0_0^+ - 2_1^+ - I_2^+ - I_3^+*$ ) ( $I_2^+ = 0_2^+, 2_2^+ \text{ or } 4_2^+$ ,

$I_3 = 0, 2, 3, 4, 6$ )

3)  $0_0^+ - 2_1^+ - 0_2^+ - 2_2^+ - 4_2^+$

or  $0_0^+ - 2_1^+ - I_2^+ - I_2'^+ - I_3^+*$ ) ( $I_2, I_2', I_3$  same as above) } with IIICPLE=5

4)  $0_0^+ - 2_1^+ - 0_2^+ - 2_2^+ - 4_2^+ - I_3^+*$ )

with IIICPLE=6

Corresponding  $\beta$ 's :

Notation :  $\beta_{02}$  grad. st. - 1 qu. ph. st.

$\beta_{2I}$  1 qu. ph. st. - 2 qu. ph. st.

$\beta'_{0I}$  grad. st. - 2 qu. ph. st.

$\beta''_{0I}$  grad. st. - 1 ph. st., but appears in matrix element grad. st. - 2 qu. ph. st., so it describes one ph. admixture in 2 qu. ph. st.

Input:  $\beta_{02} \rightarrow \text{VCOUP}(1)$

$\beta_{24} \rightarrow \text{VCOUP}(6)$

$\beta_{20} \rightarrow (2)$

$\beta'_{04} \rightarrow (7)$

$\beta'_{00} \rightarrow (3)$

$\beta''_{00} \rightarrow (8)$

$\beta_{22} \rightarrow (4)$

$\beta''_{02} \rightarrow (9)$

$\beta'_{02} \rightarrow (5)$

$\beta''_{04} \rightarrow (10)$

\* requires KEXCOM(13)=1

and a 2<sup>nd</sup> card with coupling potentials:

$\beta_2 \rightarrow \text{VCOUP}(11)$  quad. in linear term  $\langle 2; I || 113; I' \rangle$

$\beta_2 \rightarrow \text{VCOUP}(12)$  - n - quads. term  $\langle 1; 2 || 113; I \rangle$

INTYPE = 4 deformed nuclei (make KTRL(1)=1 ... Legendre exp.)

INTYPE = 4, INTMAX = 1 (NACC or ACC)

only one term of Legendre expansion of pot. ( $\lambda=2$ ) considered

$\beta_2 \rightarrow \text{VCOUP}(1)$   
ev.  $\beta_4 \rightarrow \text{VCOUP}(2)$  } belong to Legendre exp. of radii !

INTYPE = 4, INTMAX = 2 (NACC or ACC)

Legendre expansion up to  $\lambda=4$

$\beta_2 \rightarrow \text{VCOUP}(1)$

$\beta_4 \rightarrow \text{VCOUP}(2)$

INTYPE = 4, INTMAX = 3 (NACC)

odd A target, spin-spin interaction considered (KTRL(19)=1,  
do not make KTRL(12)=1 (CFF))

$V_{ss} \rightarrow \text{VCOUP}(3)$

INTYPE = 4, INTMAX = 4 (NACC, ACC; Karlsruhe)

Legendre expansion up to  $\lambda=8$

for Cb pot. same treatment as for nuclear part (unlike

INTMAX = 1,2, where there is power series exp. for Cb pot.)

KTRL(6)=1 in Cb pot. only terms linear in  $\beta_2$  (direct Cb ex.)

KTRL(6)=2 — " — also quadri. terms (direct & multiple Cb ex.)

INTYPE = 5 odd A vibrational nucleus

INTYPE = 5, INTMAX = 1

core excitation is restricted to one phonon (quadri. or octupole)

target ground state spin  $I_z \leq 9/2$

$\beta_2 \rightarrow \text{VCOUP}(1)$  for coupling grd.st.-1<sup>st</sup> exc.st. } concern same

$\beta_2 \rightarrow (2)$  — " — grd.st.-2<sup>nd</sup> exc.st. } core exc.

INTYPE = 5, INTMAX = 2

core excitation up to two phonon states (quadrupole)

requires target grad. n. spin  $I_1 = 1/2$

only one target state may have a 2 ph. core, together with 3 states with 0 and 1 ph. cores:

$$\frac{1}{2} - \underbrace{\frac{3}{2}}_{1} - \underbrace{\frac{5}{2}}_{1} - I \quad \text{with } IICPLE = 4$$

0 ph.    1 qu.ph.    2 qu.ph.:  $I = 1/2, \dots, 9/2$

$$\beta_2 \rightarrow VCOUPL(1)$$

$$\beta_{2I_1} \rightarrow (2)$$

$$\beta'_{0I_1} \rightarrow (3)$$

$\tau^*$ )  $\rightarrow$  (4) } if 1<sup>st</sup> and 2<sup>nd</sup>  $\frac{3}{2}$  states are considered to

$a(\frac{3}{2})^{**} \rightarrow$  (7) } be a mixture of 1 and 2 ph. states:

$$\psi_1 = a|1\rangle \pm c\sqrt{1-a^2}|2\rangle + \dots$$

$$\psi_2 = -a|2\rangle \pm c\sqrt{1-a^2}|1\rangle + \dots$$

$$\text{sign}(\frac{3}{2}) \rightarrow (8)$$

$$a(\frac{5}{2})^{**} \rightarrow (9)$$

$$\text{sign}(\frac{5}{2}) \rightarrow (10)$$

\*)  $|c| \leq 1$  accounts for the case that  $|1\rangle$  and  $|2\rangle$  do not represent  $\psi_1$  and  $\psi_2$

\*\*)  $\sqrt{\frac{1}{2}} \leq a \leq 1$

INTYPE=6 even A rotational nucleus, excitation of vibrational bands are to be considered requires additional cards with states of the considered bands ( $\leq 7$ ). (see KEXCOM(21) - (27))

$\beta_2 \rightarrow$  VCOUPL(1) fd. band

$\eta_6 \rightarrow$  (3) } strengths of the excitation of the  $\leq$  six  
 $\eta_6 \rightarrow$  : ex. bands  
 $\eta_6 \rightarrow$  (8) }

## In Appendix A of Jupiter manual

ISTRTW 2\* projectile spin

NANGLR number of angles for which diff. xs' and polarizations are comput.

IXICAL number of states for which diff. XS's are computed

NACC:  $\{ \text{JIXCAL} = \text{JICPLE}$  usually

NAME: JAMES CALICPLE If inc. energy < inc. en. of an exc. state

ACC : IIXCAL > IICPLE = 1 usually

**IIXPLT** number of states for which th. & exp. diff.  $\chi S^2$  are to be machine plotted

IIXPLT ≤ IIXCAL

IIPCAL} same for polarizations

IIPPLT  $\leq$  2

KANGRD control number for angles 0 cm

=1 angles given as input

= 0 initial angle and moment given as input,  
 $\theta_{CM}$  quiet distant

[ KEXCOM(N), N=21,...27 additional bands, if vibrational states  
 of deformed even nucleus are to be  
 considered (INTYPE=6) ]

(IIREAD(N), KPRJTR(N), QVALUE(N)), N=1,...Nc

spin ( $\frac{1}{2}$ , if A odd), parity, energy of  $n^{\text{th}}$  target state  
 Nc ... IICPLE or IIIXCAL, resp.

$N_{\text{ACC}}$        $A_{\text{CC}}$

certain rules for the order of appearance of  
 these states (cf. IUPITOR manual)

ELAB laboratory system energy of the projectile in MeV

PMAS mass of the projectile in amu or pmu depending on AMUPMU

TMAS mass of the target

CHARGE charge product

XMES1 meshsize  $h_1$ } used in differential equation integration  
 XMES2 meshsize  $h$

In integration:  $h_1, 2h_1, 4h_1, \dots, h, 2h, 3h, \dots$  are used

$$\Rightarrow h_1 = \frac{h}{2^k} \quad (k \text{ integer})$$

AMUPMU control number for mass unit

=0 atomic	}	- "
=1 parton	}	- "

ANGLER(N) CM angles in degree

N=1,...NANGLR, if KANGRD=0

N=1,2 (min 0, increment), if KANGRD=1

S6MEXP(N,I), POLEXP(N,I) exp. XS<sup>3</sup> and polarizations for plot (Tamura)

angle | angle |      or March (Karlsruhe)

state, I=1,...IIIXPLT≤6      state, I=1,...IIPPLT≤2

Angles and amplitudes of polarized states (only if KTRL(8) ≠ 0)

VSX depth of real pot.

WSX — " — vol. imag. pot.

WSF — " — surf. — " —

VSO — " — spin orbit pot.

WC(N), N=1,...6 "fudge" factors for the strength of vol. and/or surf. imaginary potential (no fudging = 1.0)

DFN, RZERO diffusion, radius of real pot.

DFNW, RZEROW — " — vol. imag.

DFNS, RZEROS — " — surf. — " — } all diffuse -  
  necks ≠ 0 !

DFNSP, RZEROSP — " — spin orbit pot.

RZEROC radius parameter of C6 pot. (>0 also for necks !)

RONE

RONEW

RONES

}  $r_1^s$  in Engelhardt-Friedländer pot. (Vienna)  
 $(R = r_0 A^{1/3} + r_1)$

VCOPL(N), N=1,...10 quantities related to coupling, see INTYPE, INTMAX

KREADA control number for continuation of input

=1 new problem

=2 next input starts with incident energy

=3 — " — potential diffus

Number of exp. points = NANGLR \* (IIIXPLT + IIIPPLT)

N number of variable parameters

MA max. number of complete sets of calc. ( $MA \geq N+4$ ) } (Karlruhe  
search)

IP point control number

ES step size parameter

### 3) Output

Notation :

SGTOTL ...  $\sigma_t$ , total cross section

$$\text{REACCR} \dots \sigma_t - \sigma_{\text{sh. el.}} = \sum_{n \neq 1} \sigma_n^{(s)} + \sigma_{\text{abs}}$$

"reaction cross section" in the sense that it gives the cross section for all processes apart from shape el. scatt., different from both meanings of " $\sigma_{\text{rec}}$ " mentioned on p. 74

STRGFS, STRGFP ...  $S_0, S_1$ , strength functions for  $\ell=0$  and 1

$$\text{in fact, } S_\ell = \lim_{E \rightarrow 0^{\pm}} \frac{1}{\pi} \frac{T_\ell}{P_\ell}$$

therefore, even if  $S_1$  refers to  $E_0 = 1 \text{ eV}$  due to the factor  $\sqrt{\frac{E}{E_0}}$  (cf. p. 74),  $S_1$  may differ when calculated at different energies  $E$ , if constancy is not yet reached

[ $S_0, S_1$  in JUPITOR output up to 1 eV]

## VIII.) STAPRE

### 1) Program operation

#### a) Possible programs

— calculation of energy averaged cross sections of particle induced nuclear reactions in the frame of the statistical model

- activation cross sections
- population cross sections of isomeric states
- production XS<sup>3</sup> for  $\gamma$ -rays from low excited levels
- energy spectra for all emitted particles
- $\gamma$ -ray production spectra

— up to 6 emitted particles and  $\gamma$ -rays (sequential evaporation)

— angular momentum and parity conservation

— width fluctuation correction

— pre-equilibrium decay (1st step)

### b) Formalism

#### Notation

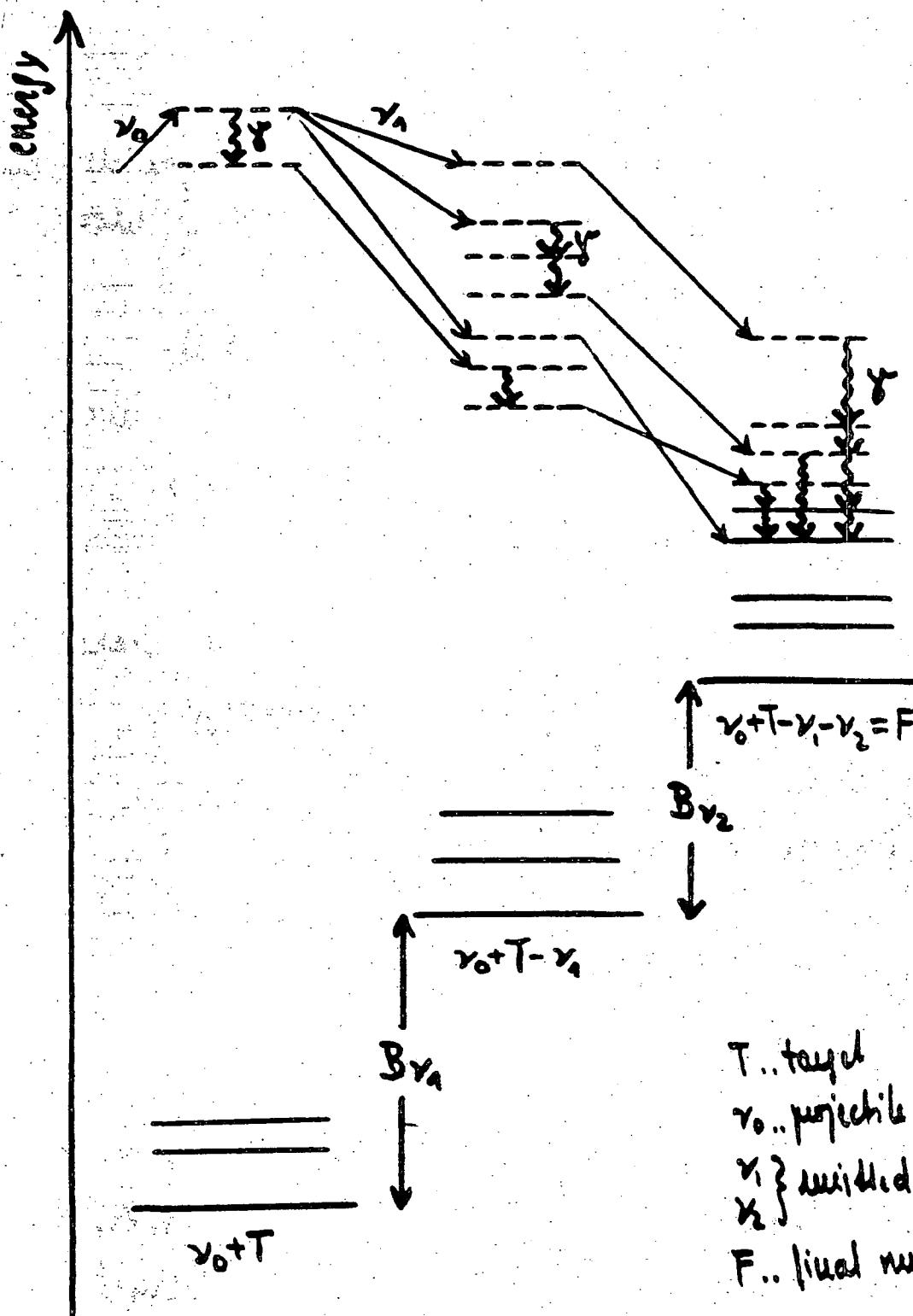
$i^{\text{th}}$  compound nucleus ( $CN$ ) = nucleus resulting from emission of  $i-1$  particles of a specified sequence  $v_1, v_2, v_3 \dots$

1<sup>st</sup> CN: composite system of projectile + target

2<sup>nd</sup> CN: after emission of one particle  $v_1 \dots$

WB<sub>i</sub>(E, J, π)ΔE ... primary population of states with sec. energy in interval ΔE around E, ang. mom. J, parity π of  $i^{\text{th}}$  CN

$$T(\nu_0, \nu_1, \nu_2, \gamma) F$$



$T$  .. target

$\nu_0$  .. projectile

$\nu_1 \} \nu_2$  .. emitted particles

$F$  .. final nucleus

$\overline{W}_{i,j,\pi}^{\text{pre}}(E, J, \pi) \Delta E$  ... population of states  $E, J, \pi$  of  $i^{\text{th}}$  CN after  $\gamma$ -ray cascade

$\frac{\partial \sigma_{\nu}^{\text{pre}}}{\partial \epsilon_{\nu}} d\epsilon_{\nu}$  ... pre-equilibrium contribution to emission spectrum of 1<sup>st</sup> particle (cf. p. 55)

$g^{\text{pre}}$  ... fraction of the initial population which survives pre-equilibrium

$\left. \begin{aligned} \frac{\partial \sigma_{\nu}^{\text{HF}}}{\partial E'}(E, J, \pi') \Delta E' \\ \frac{\partial \sigma_{\gamma}^{\text{HF}}}{\partial E'}(E, J, \pi') \Delta E' \end{aligned} \right\}$  Hauser Feshbach contribution to 1<sup>st</sup> emission step for  $\left\{ \begin{array}{l} \text{part.} \\ \gamma \text{ rays} \end{array} \right\}$

$$\frac{\partial \sigma_{\nu}^{\text{HF}}}{\partial E'}(E, J, \pi') \Delta E' = \frac{\pi}{k^2} \sum_{j\pi} g_j \frac{\sum_{s_0, s_1} T_{\nu, s_0, s_1, l_0} \sum_{l_1} T_{\nu, l_0, l_1}}{N_i(E, J, \pi)} W_{\nu, s_0, s_1, l_0, l_1} \rho_{\nu}(E, J, \pi') \Delta E'$$

$$\frac{\partial \sigma_{\gamma}^{\text{HF}}}{\partial E'}(E, J, \pi') \Delta E' = \frac{\pi}{k^2} \sum_{j\pi} g_j \frac{\sum_{s_0, s_1} T_{\gamma, s_0, s_1, l_0} \sum_{l_1} T_{\gamma, l_0, l_1}}{N_i(E, J, \pi)} \rho_{\gamma}(E, J, \pi') \Delta E'$$

↑  
limit of infinite number of open channels,  
non-elastic process  $\Rightarrow W \rightarrow 1$

$N_i(E, J, \pi)$  ... Hauser Feshbach denominator of  $i^{\text{th}}$  CN

$$\begin{aligned} N_i(E, J, \pi) = & \sum_{\nu} \sum_{J', \pi'} \sum_{s_1} \int_{E-B_V}^E d\epsilon_{\nu} T_{\nu, s_1}(E_{\nu}) \rho_{\nu}(E-B_V-\epsilon_{\nu}, J', \pi') + \\ & + \sum_{\gamma} \sum_{J', \pi'} \int_{E}^{\infty} d\epsilon_{\gamma} T_{\gamma, s_1}(E_{\gamma}) \rho_{\gamma}(E-\epsilon_{\gamma}, J', \pi') + \\ & + \int_{0}^{\infty} dE' \rho_f(E', J, \pi) \left\{ 1 + \exp \left[ \frac{2\pi}{\hbar \omega} (E' - E) \right] \right\}^{-1} \end{aligned}$$

$\rho_{\nu}(E, J, \pi')$   
 $\rho_{\gamma}(E, J, \pi')$  } — " — a CN resulting from { part. } emission

$\rho_f(E, J, \pi)$  ... transition state density

$W_{\nu, s_0, s_1, l_0, l_1}^{w\pi}$  ... width fluctuation correction factor

## Combination of HF & PE model

$$WB_1(E, J, \pi) \Delta E = q_{\text{PE}} \frac{\partial \sigma_{\nu}^{\text{HF}}}{\partial E}(E, J, \pi) \Delta E \quad \text{for 1st chance \gamma ray em.}$$

$$WB_2(E, J, \pi) \Delta E = \left\{ q_{\text{PE}} \frac{\partial \sigma_{\nu}^{\text{HF}}}{\partial E}(E, J, \pi) + \frac{\partial \sigma_{\nu}^{\text{PE}}}{\partial E} \frac{\frac{\partial \sigma_{\nu}^{\text{HF}}}{\partial E}(E, J, \pi)}{\sum_{J' \pi'} \frac{\partial \sigma_{\nu}^{\text{HF}}}{\partial E}(E, J', \pi')} \right\} \Delta E$$

↑  
for 1<sup>st</sup> chance particle em.

↑  
since PE model  $J$  independent : for each  $J$ , PE contribution is weighted with relative share of this  $J$  in equilibrium  $\rightarrow ??$

## Later chance particle emission

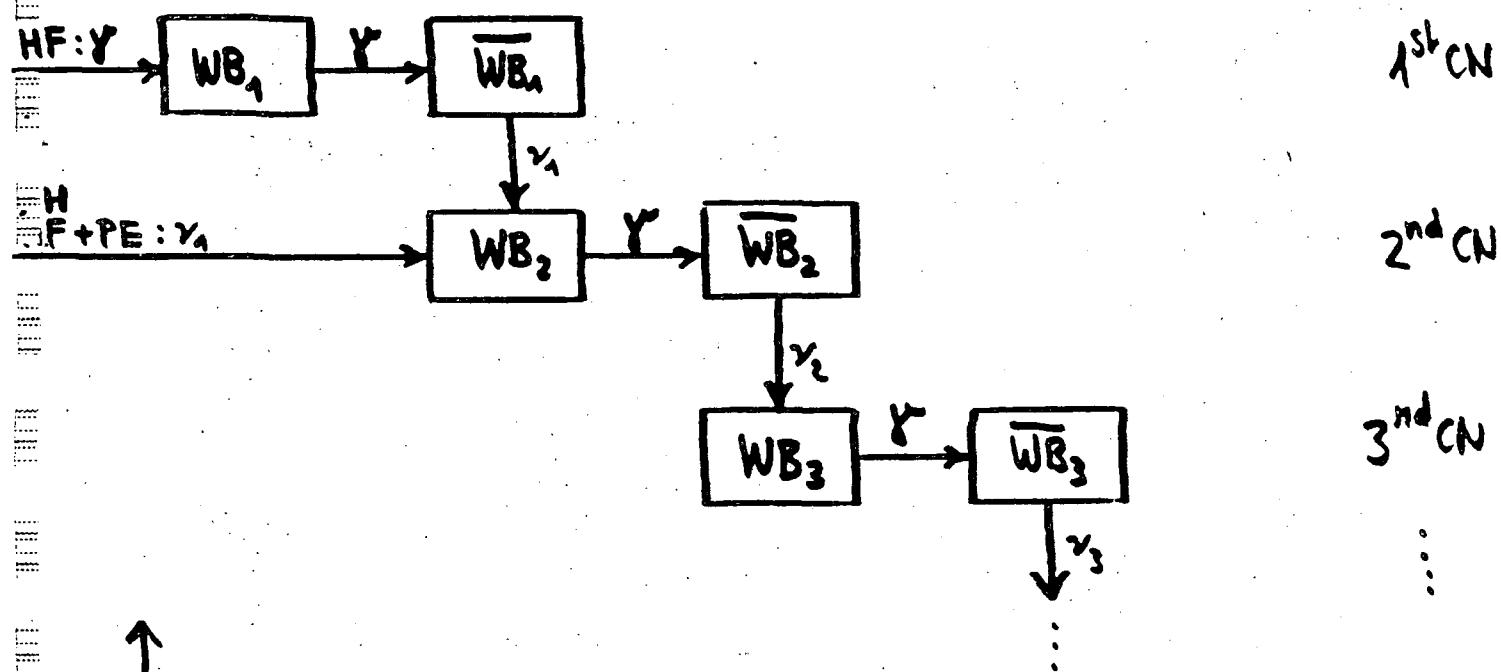
Evaporation of  $i^{\text{th}}$  particle from  $i^{\text{th}}$  CN with population  $WB_i(E, J, \pi) \Delta E$  leads to population  $WB_{i+1}(E', J', \pi') \Delta E'$  of  $(i+1)^{\text{th}}$  CN:

$$WB_{i+1}(E', J', \pi') \Delta E' = \sum_{J'' \pi''} \int_{E'+\delta \nu_i}^{E_{\max}} dE \overline{WB}_i(E, J, \pi) \frac{\Gamma_{\nu_i}(E, J, \pi; E', J', \pi')}{\Gamma_i(E, J, \pi)} \frac{f_{\nu_i}(E', J', \pi') \Delta E'}{f_i(E, J, \pi) \Delta E'}$$

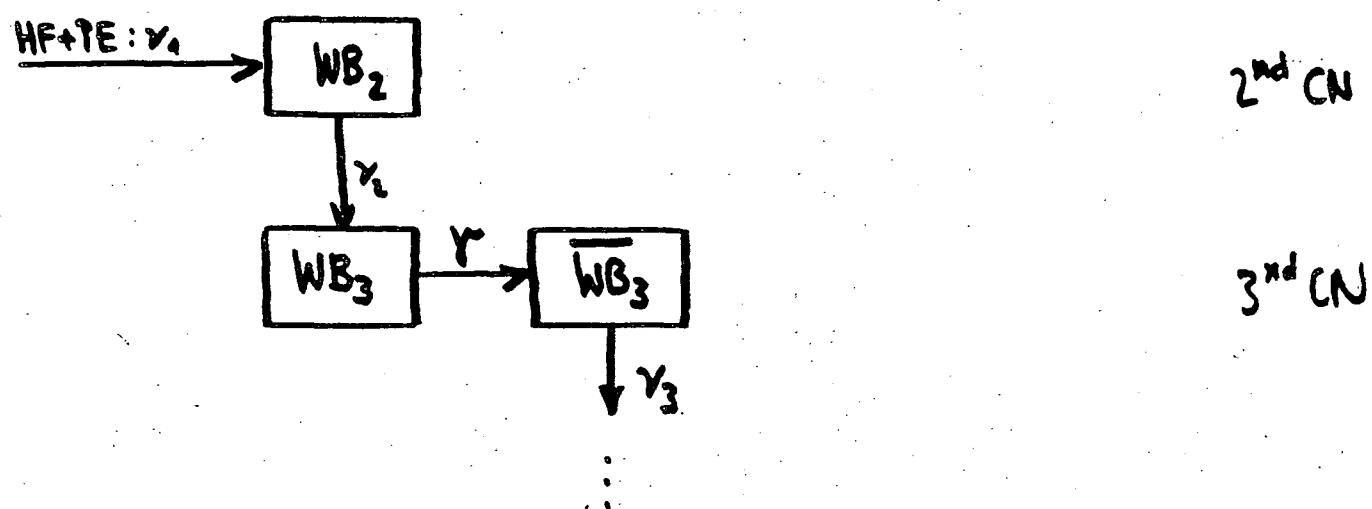
$$\text{where } \frac{\Gamma_{\nu_i}(E, J, \pi; E', J', \pi')}{\Gamma_i(E, J, \pi)} = \frac{1}{N_i(E, J, \pi)} \sum_{l, s, i} T_{\nu_i l i}(E - E' - \delta \nu_i)$$

$\Gamma_i(E, J, \pi) \dots$  total width of state  $E, J, \pi$  of  $i^{\text{th}}$  CN

Schematic representation :



above : consideration of  $\gamma$  decay starts in the first CN  
 below : " "  $3^{\text{rd}}$  CN



## Fission cross sections

1<sup>st</sup> chance fission :

$$q^{\text{fus}} \frac{\pi}{k} \sum_{\gamma\eta} g_{\gamma} \sum_{f_{\gamma\eta}} \sum_c \frac{1}{D^{2n}} \int_{E - \frac{D^{2n}}{2}}^{E + \frac{D^{2n}}{2}} dE \frac{T_{\gamma\eta\eta} T_{fc}}{N(E, \gamma, \eta)}, \quad W_{\gamma\eta\eta, fc}$$

average with respect to intermediate  
class II structures

higher chance fission (cont. of i<sup>th</sup> CN) :

$$\sum_{\gamma\eta} \int_{E_{\min}}^{E_{\max}} dE \bar{W}_B(E, \gamma, \eta) R_{fi}(E, \gamma, \eta)$$

where  $R_{fi}$  ... fission probability of i<sup>th</sup> CN  
 = sum of transm. coeff: for direct & indirect  
 fission, divided by  $N(E, \gamma, \eta)$

## c) list of routines

Main STAPRE control & stat. model calc., loop for emission steps

Sr. READ input

Sr. GAMMA1 calc. of gamma transmission coefficients

Sr. TRANS preparation of particle transm. --" (from flux supplied as input)

Sr. TLINT1 interpolation of particle transmission coefficients

Sr. INTER interpolation polynomial

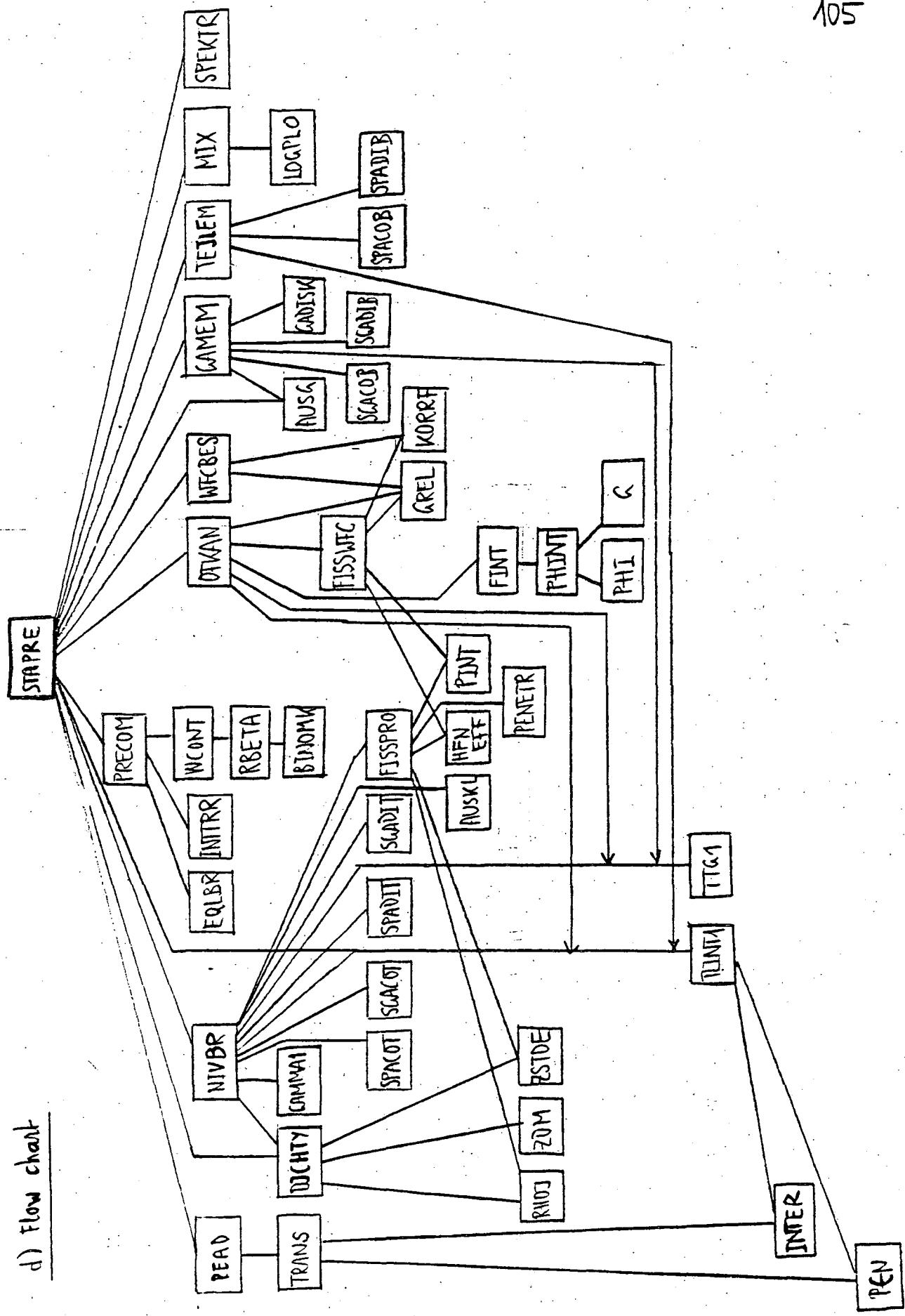
Td. PEN fission factors

- Sr. NIUBR calc. of total level width
- Sr. DICHTY level density as fct. of exc. en. and angular momentum
- Fd. RH0J — " — dependence on ang. mom.
- Fd. ZDM density of states with given magnetic quantum number
- Sr. ZSTDE state density (Fermi gas and/or const. temperature formula)
- Sr. SPACOT contribution of particle emission to continuum states to total width
- Sr. SGACOT — " —  $\gamma$  ray " "
- Sr. SPADIT — " — particle emission to discrete states to total width
- K. SGADIT — " —  $\gamma$  ray " "
- Sr. TTG1 interpolation of  $\gamma$  ray transmission coefficients
- Sr. FISSPRO fission probability and fission contribution to total width
- Sr. AUSKL edit of 2 dim. array
- Fd. HFNEFF HF denominator and fission prob. (average over class II structures)
- Fd. PINT interpolation of probabilities
- Sr. PENETR probabilities through fission barrier
- Sr. PRECOM calc. of PE contribution
- Sr. EQLSR equilibrium of population of excited states
- Sr. INTTRR internal transition ratio
- Sr. WCONT continuum emission ratio
- Fct. RBETA factor  $R_r$  (cf. p. 53)
- Fct. BINOMK binomial coefficients
- Sr. OFKAN preparation of WFC factor
- Sr. FISSWFC fission contribution to HF denominator and 1<sup>st</sup> chance fission XS
- Sr. WFCBES population resulting from 1<sup>st</sup> chance part. or  $\gamma$  ray emission (HF)
- W. GREL limits of vib. ang. momentum in WFC factor
- W. KORRF numerical integration of WFC

- fct. FINT part of integrand of WFC factor  
 fd. PHINT averaging over class II structure  
 fct. PHI integrand for averaging over class II structure  
 fct. G part of --- , ---  
 fr. AUSG edit of 3 dim. arrays  
 fr. GAMEM calc. of population by  $\gamma$  ray emission  
 fr. SGACOB population of continuum states by  $\gamma$  ray emission  
 fr. SGADIB — v — discrete " "  
 fr. GADISK  $\gamma$  rays between discrete levels  
 fr. TEILEM calc. of population by particle emission  
 fr. SPACOB population of continuum states by particle emission  
 fr. SPADIB — " — discrete " "  
 fr. MIX combination of HF & PE contribution  
 fr. LOGPLO logarithmic plot of HF & PE spectrum  
 fr. SPEKTR summing of contributions of all emission steps to  
 part. and  $\gamma$  ray prod. sp.

STAPRE

d) Flow chart



## 2) Input

TITLE, in 1st col.: \*

NLAUF(I), I=1,7 control # for the reaction

NLAUF(1) ... code number of projectile

NLAUF(I), I>2 ... code # for particle emitted from (I-1)<sup>th</sup> CN

(codes: 1... neutron

2... proton

3... e

4... deuteron

99... non-standard part. (only for NLAUF(1))

N ... number of CN,  $1 \leq N \leq 6$

NGACOM number of that CN from which the consideration of  $\gamma$ -rays starts,  $\leq N$

NPAR types of particles whose emission is considered in the HF calculation

1. neutrinos

2. neutrons, protons

3... -"-, -"-, e

4... -"-, -"-, e, deuterons

LLMAX maximum multipolarity of  $\gamma$ -rays

1... E1, M1

2... E1, M1, E2, M2

3... E1, M1, E2, M2, E3, M3

$NPAR \geq NLAUF(I)$

except for  $NLAUF(1)=99$

DU ... binary (full) or unary grid

NFISS control number for calc. of fusion XS

0... no fusion

1... explicit consideration of fusion channels

2... all continuum fusion channels are treated as 1 channel

NPHI control # for averaging of WF corrected 1st chance fission  
xs over intermediate class II structure

- Φ .... by means of use of "effective fission transm. coefficients"
- >Φ ... by means of integration

NNWFC control # for WFC

Φ ... on

1 ... off

GRE limit of HF denominator above which WFC is put = 1  
default : 5Φ.

NNFREI number of degrees of freedom of level width distr.  
default : 1

DDEL desired relative accuracy for integration of WFC  
default : .Φ1

NNINT max. # of meshpoints for calc. of integral in WFC  
must be a power of 2  
default : 64  
if  $> 64 \Rightarrow \text{NNINT} = 64$  internally

(PARC(I,1), PARC(I,2)), I=1,N characteristics of CN

PARC(I,1) ... chem. symbol } of I<sup>th</sup> CN

PARC(I,2) ... charge number }

ATAR max # of target

STAR spin } of target

KPTAR parity (+1 or -1) }

Q binding energy of projectile to target (required only  
if NLMUF(1) = 99)

AEFSCH mass # } of projectile; required only if NLAUF(1)=11  
 SGESCH spin }

EEJNL incident energy in lab. system

will be adjusted according to energy grid

KDE control number for variation of inc. energy

KRZ2MM total number of inc. energies for which calc. are to be performed

FM constant ( $\text{MeV}^3$ ) determining the internal transition matrix element for PE model

= 0 ... no PE considered

NPI initial particle number, default : 2

NHI initial hole number. - " - : 1

IPAU1 control # for consideration of Pauli principle in internal trans. rates

0 .. off

1 .... on

KTESTP control # for single particle state density  $g$  and energy shift  $D\Delta$  used in p-h-state density formula

0 or 1 ....  $g = \frac{6}{\pi^2} \frac{A}{g}$ ,  $D\Delta = 0$

2 or 3 ....  $g = \frac{6}{\pi^2} \frac{A}{g}$ ,  $D\Delta = \sqrt{\frac{12}{A}} * \left\{ \begin{array}{ll} 0 & \text{odd} \\ 1 & \text{odd mass} \\ 2 & \text{even} \end{array} \right\}$  nuclei

4 or 5 ....  $g = \frac{6}{\pi^2} \frac{A}{g}$ ,  $D\Delta = \Delta$

6 or 7 ....  $g = \frac{6}{\pi^2} \frac{A}{g}$ ,  $D\Delta = 0$

8 or 9 ....  $g = \frac{6}{\pi^2} \frac{A}{g}$ ,  $D\Delta = \Delta$

↑

odd values: extended protocol

MILANO control # for calc. of emission rates (in PE step) for nuclear induced reactions

$\Phi$  ... general expressions are used      } c.p. 53  
 I ... expressions of Milano group are used }

PHIMIL & cluster formulation probability in Milano expression for  
 & part. emission rate

KTEST1 output control # for printing bad densities, contributions of  
 particle and photon contr. to HF denominator, fission  
 prob. and total decay widths

$\Phi$  ... off

I ... on

KTEST2 output control # for printing WB and  $\overline{WB}$

$\Phi$  ... off

I ... on

KTEST3 output control # for printing particle and, if calcd.,  $\gamma$  ray  
 spectra from decay of each CN

$\Phi$  ... off

I ... on

KTESTW control numbers for WFC protocol

$\Phi$  .. short

I ... extended

KGAPR output control numbers for printing production  $\times 10^3$  of  $\gamma$  rays  
 between discrete levels

$\Phi \approx 1$  ... none

$\geq 2$  .... for levels 2, ..., J where  $J = \min(\#\text{of disc. levels}, KGAPR)$

((PARR(I,K), K=1,NPAR), I=1,N) separation energies (HWH)

PARR(I,K) .. sep. energy of particle with wave # K from  $I^{th}$  CN

LMAX max. ord. ang. mom }  
Transmission coeffs. } for inc. channel, required only if NLAUF(1)=99

NTRAN ctrl. # for transm. coeffs.

1....one set of - " — for all CN

N....each CN has its own set of transm. coeffs.

LO(K), K=1,NPAR number of partial waves for all particles } NTRAN sets  
Transmission coeffs. for all particles }

(DC(L), L=1,13), ISYMC level density parameters for 1<sup>st</sup> CN

DC(1) .. "a- parameter"

DC(2) ..  $\eta = I_{eff} / I_{rigid}$

DC(3) ..  $\Delta$

DC(4) .. shell correction

DC(5)-DC(12) .. parameters regarding const. temperature formula

DC(13) ...  $I_1 / I_{rigid}$  for rot. nuclei

ISYMC ... control # for ang. mom. dependence of level density

$\phi$  ... spherical nuclei

1-5.. deformed -" - with various symmetry properties

-1 ... usual Fermi gas formula (q. p. 4.)

NDISK .. number of discrete levels of 1<sup>st</sup> CN

ED(J), SD(J), KPD(J), J=1,NDISK levels of 1<sup>st</sup> CN

ED(J) .. uc. m.

SD(J) ... spin

KPD(J) .. parity (+1 or -1)

required only if

NCALOM = 1

Following data are required for each CN ( $I=1, \dots, N$ ):

UB neutron separation energy (MeV)

S1 } spins of s wave neutron resonances

S2 } parity

GR average total radiation width (meV) at neutron binding energy

NF number of subsequent cards for specifying  $\gamma$  ray str. fcts.  
for the present,  $NF \leq 1$  ( $\leftarrow E1$  only)

$NF = \emptyset$  ... Weisskopf model for all multipolarities

PG( $J$ ),  $J = 1, \dots, 6$  normalization factors for  $\gamma$  ray str. fcts.

PG(1) ... normalization factor for  $f_{\gamma E1}(\varepsilon_\gamma)$

default: by fitting total radiation width to GR

PG(2) ...  $f_{\gamma M1}(\varepsilon_\gamma = UB) / f_{\gamma E1}(\varepsilon_\gamma = UB)$

PG(3) ...  $f_{\gamma E2}(\varepsilon_\gamma = UB) / f_{\gamma E1}(\varepsilon_\gamma = UB)$

PG(6) ...  $f_{\gamma M3}(\varepsilon_\gamma = UB) / f_{\gamma E1}(\varepsilon_\gamma = UB)$

for  $J = 2, \dots, 6$ : default: ratios of Weisskopf units

ERR(L), GRR(L), SRR(L), L=1,3 parameters of giant resonances if  
photo absorption cross section

ERR(L) ... position (MeV)

GRR(L) ... width (MeV) } for  $L^{\text{th}}$  giant resonance

SRR(L) ... peak XS (mb)

for  $ERR(L) = \emptyset$ , with  $L \geq 2$ :  $L^{\text{th}}$  giant res. not considered

for  $ERR(1) = \emptyset$ : one E1 giant res. with global parameters (Brink-Axel)

ES1 lower limit  
 ES2 upper limit  
 FRS reduction factor applied for  $\varepsilon_y < ES1$  } describing step in E1 str. fd.  
 fraction of Weisskopf contribution to  $f_{\gamma E1}^{\text{photo abs.}}$ :  

$$\underline{f_{\gamma E1}} = QSP + \underline{f_{\gamma E1}^{\text{photo abs.}}} (\varepsilon_y = US)$$

this energy independent fraction is added to energy dep. one

(VZD(L,M), M=1,L), L=1, NDISKC ... gray branching ratios

VZD(L,M) ... branching ratio for  $\gamma$  transition from the L<sup>th</sup> to the M<sup>th</sup> level of the I<sup>th</sup> CN.

where NDISKC ... number of discrete levels of I<sup>th</sup> CN (in order of ascending energy)

VZD(L,M) need not be normalized

VZD(L,M)=0, M=1,...L : L<sup>th</sup> level static or inelastic

(DR(L), L=1,13), ISYM ... level density parameters for residual nuclei after particle emission from I<sup>th</sup> CN (NPAR cards for each CN)

DR(L), ISYM have the same meaning as DC(L), ISYMC for 1<sup>st</sup> CN

NAN1, NAME ... number of levels ( $1 \leq NAN1 \leq 50$ ), symbol } of residual nuclei  
 EDR(J), SDR(J), KPDR(J), J=1,...,NAN1 ... discrete levels } after part. emission  
 EDR(J) ... excitation energy } from I<sup>th</sup> CN  
 SDR(J) ... spin } (NPAR sets required)  
 KPDR(J) ... parity (+1 or -1)

BARR(L), L=1,...12 fission barrier parameters

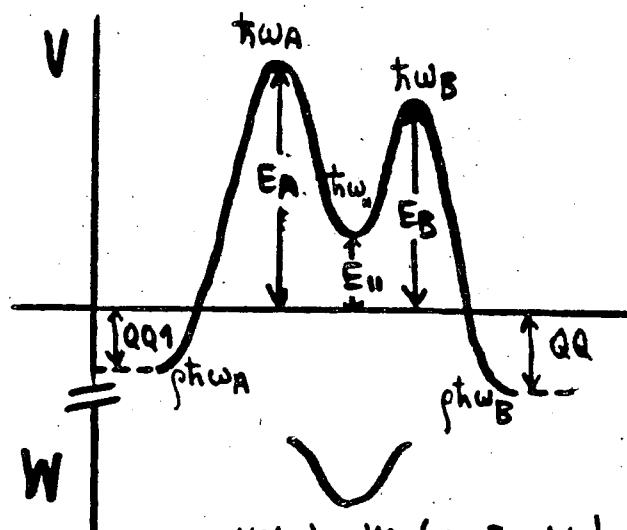
BARR(1) ... EA	}	in MeV
BARR(2) ... $\tau_{WA}$		
BARR(3) ... EB		
BARR(4) ... $\tau_{WB}$		
BARR(5) ... $E_{11}$		
BARR(6) ... $\tau_{\omega_{11}}$		

BARR(7) ... $W_0$	}	in MeV
BARR(8) ... $W_1$		
BARR(9) ... $Q_1$		
BARR(10) ... $Q_2$		

BARR(11) ...  $\rho$ , default:  $\rho = 2$ .  
 BARR(12) ... unassigned



$$W(E) = W_0 (E - E_{11} - W_1)$$

From the quantity BARR(L) a ctrl. # NBARR is derived:

NBARR = 1 if BARR(L) = 0, for  $L \geq 3$  single humped barrier  
 = 2 " " for  $L \geq 5$  double humped barrier,  
 complete damping  
 = 3 if BARR(5) > 0 and BARR(6) > 0, double humped barrier,  
 partial damping

NSTEP number of meshpoints for integration for averaging over intermediate class II structure; default value from interval crit.,  
 NSTEP < INDE & INDE

(DR(L), L=1..13), ISYM(NB) level density of continuum transition states

DR(L), ISYM have meaning as above

NFISSD(NB), (DFISS(L,NB), L=1,4) direct transition states

NFISS(NB).. number of bandheads ( $\leq 10$ )

DFISS(1,NB).. rotational constant (keV)

DFISS(2,NB).. decoupling parameters

DFISS(3,NB).. unassigned

DFISS(4,NB).. energy determining continuum edge  
of transition states

EB(L,NB), KB(L,NB), PB(L,NB), L=1, NFISSD(NB) heads of rot.bands

EB(L,NB)... exc. en. (MeV)

KB(L,NB)... K quantum # } of L<sup>th</sup> band head

PB(L,NB)... parity (+1 or -1)

for  
NB=1, NBARR

\*)

\*) NBARR = 1 for the only barrier

= 2 for barrier A and barrier B

= 3 for barrier A, barrier B and combined barrier AB

$NFISS \neq 0$   
only

### 3) Output

#### a) General part:

Sequence of compound nuclei, for each of them level density parameters and discrete levels of the nuclei resulting from emission of the various particle types are printed, if emission is energetically possible.

#### b) For each incident energy:

- protocol of PE calc.
- -- of WFC
- then for the sequence of compound nuclei the most important results are printed, optionally extended to include
  - level density
  - contr<sup>s</sup> to HF denominator
  - population before and after  $\gamma$ -ray cascades
  - spectra from each CN
- particle &  $\gamma$  ray production spectra summed over emission steps

#### c) Final part

table of excitation functions

## IX) EVALUATION PROCEDURE

Motivation for nuclear model calc.:

a) To supplement experimental cross sections to supply cross section data for applications in science and technology ("applied science aspect")

- to fill gaps in excitation functions ("interpolation")

Many excitation functions of threshold reaction of importance for reactor neutron dosimetry are based on calculations in some energy regions

- to extend excitation functions to higher energy regions where scarce or no data exist ("extrapolation")

The development of d+li neutron sources for fusion materials irradiation test facilities requires the knowledge of neutron XS<sup>s</sup> for energies up to 40–50 MeV. These requirements have to be met by calculations which reproduce data at lower energies. Similar for biomedical applications.

- to produce XS<sup>s</sup> of interest for which no experimental data at all exist, e.g. for unstable target nuclei ("prediction") such XS<sup>s</sup> are of interest for astrophysical applications and also for energy related technology as e.g. for the assessment of the buildup of fission products and actinides.

- 1) to analyze experimental data in order to check the applicability of the models, eventually refine them, and learn about reaction mechanisms and nuclear structure ("pure science aspect")

## 1) Retrieval of experimental data

### Types of exp. data:

- a) cross sections for the reaction(s) of interest, if available
- b) all experimental data which may serve for determination or adjustment of the model parameters entering to the calcs.:
  - total, total elastic, diff. elastic, diff. inelastic  $\times S^5$  } for choice of opt.
  - strength functions } model parameters
  - resonance densities } for determination of level density parameter
  - discrete levels } and possibly determine level density parameters of nuclei with no resonance data
  - cross sections for competing reactions : to confirm whole parameter set and possibly determine level density parameters of nuclei with no resonance data
  - cross sections for reactions induced by particles } to check transm.  
which in the reactions of interest are the outgoing } coeffs. for these  
particles or compete with these } particles
  - particle production spectra : to check PE model parameters
  - photon production spectra, radiation width, } for determination of  
parameters (  $\gamma$  abs. XS,  $\gamma$  ray strength fcts. ) }  $\gamma$  ray transm. coeffs

activation data - emission data

production xs of specified nucleus by various reaction paths, e.g. ( $n, pn$ ), ( $n, np$ ), ( $n, d$ )

production xs of specified particle by various reaction paths, e.g. ( $n, \alpha$ ), ( $n, n\alpha$ ), ( $\nu, p\alpha$ )

### Sources of exp. data:

- EXFOR
- CINDA
- Pertinent papers in journals
- Proceedings of pertinent conferences & symposia
- Compilations (e.g. BNL-325 (1979), vol. 1, INDC compilations, IAEA, Vienna)
- "Table of Isotopes"
- Underlying data bases of previous evaluations
- Individual laboratory reports

## 2) First choice of model parameters

### A) References

#### a) spherical optical model

##### - global potentials :

neutrons: F.G. Perey, B. Buck, Nucl. Phys. 32 (1962) 353

D. Wilmore, P.E. Hodgson, Nucl. Phys. 55 (1964) 673

F.D. Becchetti, G.W. Greenlees, Phys. Rev. 182 (1969) 1190

C.A. Engelbrecht, H. Fiedeldey, Ann. Phys. 42 (1967) 642

B. Holmqvist, T. Wiedling, J. Nucl. Energy 27 (1973) 543

L. Rosen et al., Ann. Phys. 34 (1965) 96

protons: G.S. Mani, M. A. Mulkanoff, I. Ion, Rept. C.E.A. 2379 (1963)

F.G. Teray, Phys. Rev. 131 (1962) 745

C. A. Johnson, Phys. Rev. Lett. 39 (1977) 1604

$\alpha$  particles: J.R. Huizinga, G. Igo, Rept. ANL-6373 (1961) and

Nucl. Phys. 29 (1962) 462

I. McFadden, G.R. Satchler, Nucl. Phys. 84 (1966) 177

O.F. Lemos, Decay Rept. Series A, № 136 (1972)

T.S. Tark, H.D. Jones, D.E. Bainum, Phys. Rev. C4 (1971) 788

- potentials determined by other authors for specified nucleus or  
for limited mass region:

neutrons: S. Igarashi, Proc. Conf. Nuclear Cross Sections and Technology,  
Washington (1975), vol. 1, p. 320

J.P. Bilaracque, Ch. Legrange, J. Salvy, IAEA Consultants Meeting  
Trieste (1975), IAEA - 190, vol. 1, p. 251

Ch. Legrange, Proc. 3<sup>rd</sup> Nat. Soviet Conf. Neutron Physics,  
Kiev (1975), CONF - 75061154, ATOMIZDAT (1976)

E.D. Akkun, P.G. Young, Rept. LA - 8626-Ms (ENDF-304) and  
Proc. Int. Symp. Neutron XS<sup>s</sup> 10 - 50 MeV,

Brookhaven (1980), p. 731

E.D. Akkun, P.G. Young, W.K. Matthes, Proc. Int. Symp. Neutron XS<sup>s</sup>  
10 - 50 MeV, Brookhaven (1980), p. 751

- J. Rapaport, V. Kulkaoui, R. W. Finlay, Nucl. Phys. A330 (1979) 15  
 J. Rapaport et al., Phys. Repts. 87 (1982) 25

A. Prince, Proc. Int. Conf. Nucl. Data for Science and Technology,  
 Antwerp (1982), in press

- opt. pot. obtained by means of search on appropriate data,  
 starting from a potential of one of the groups mentioned above

## 2) Deformed optical model

- pot. determined by other authors for specified nucleus or limited mass region:  
 — authors : J. T. Delaroche et al. } see above  
 Cu, hydrogen }  
 J. G. Madland, T.G. Young, Proc. Int. Conf. Nuclear Physics &  
 Nucl. Data, Harwell (1978), p. 349
- opt. pot. obtained by means of search on appropriate data,  
 starting from spher. opt. pot. or deformed opt. pot. determined by other authors  
 (see "step by step fitting procedure for vibr. nuclei," p. 82)
- deformation parameters : from electromagnetic transitions, and  
 analyses of inelastic scatt., also of other particles, on same nucleus  
 Nuclear Data Sheets, Academic Press, N.Y. and London  
 and Recent References therein  
 P.H. Stelson et al., Nucl. Phys. C8 (1965) 97

Y Yamamoto, Proc. Int. Conf. Nucl. Cross Sections for Technology.

Knoxville (1979), NBS Spec. Publ., p. 146

M. Hyukatake et al., J. Phys. Soc. Japan 38 (1975) 606

c) Pre-equilibrium & compound nucleus model:

— level density parameters

W. Dilg, W. Schantl, H. Vorach, M. Uhl, Nucl. Phys. A 217 (1973) 219

A. Gilbul, A. G. W. Cameron, Can. J. Phys. 43 (1965) 1446

J. L. Cook et al., Austral. J. Phys. 20 (1967) 477

— separation energies

A. H. Wapstra, N. B. Gove, Nucl. Data Tables 9 (1971) N° 4-5

N. B. Gove, A. H. Wapstra, Nucl. Data Tables 11 (1972) N° 2-3

A. H. Wapstra, K. Bos, Atomic Data & Nucl. Data Tables 19 (1977), N° 3, p. 215

V. E. Viola et al., Atomic Data & Nucl. Data Tables 13 (1974) N° 1

— discrete levels & branching ratios

Nucl. Data Sheets, Acad. Press, N.Y., London

P. M. Sudi, C. van der Leun, Nucl. Phys. A 105 (1967) 1

A 115 (1968) 697

A 214 (1973) 1

Table of Isotopes, Seiden & Shirley (eds.), J. Wiley, N.Y., 1978

F. Ajzenberg-Selove, Nucl. Phys. A 281 (1977) 1

- radiation widths

BNL-325, vol.1

S. M. Jakkarova et al., INDC(CCP)-2712 (1972)

M.S. Moore, Proc. Int. Conf. Neutron Phys. and Nucl. Data,  
Harwell (1978), p. 313

H. Weigmann, G. Rohr, Proc. Symp. Neutron Phys. with Thermal  
and Resonance Energy Neutrons, Petten (1973), p. 194

- resonance spacings

G. Rohr, Proc. Specialists Meeting on Neutron Data of Structural Materials for  
Fast Reactors, Gul (1977) p. 614

F.H. Fröhner, Proc. Int. Conf. Neutron Phys. and Nuclear Data,  
Harwell (1978) p. 268

- fission parameters

J. E. Lynn, Harwell Rept. AERE-R7468 (1974) 324

J. E. Lynn, Proc. Consultants Meeting, Trieste (1975), IAEA-190, vol. I, p.

B) Recommendations and Remarks:

a) spherical optical model (ABACUS)

- KCL  $\left\{ \begin{matrix} 0 \\ 1 \end{matrix} \right\}$  same form for Ch pot. (uniform charge dist. within  $R_c$ )
- if inf. pot. comprises volume part only, it must be input as VIM (not VIVOL)
- " " & surface part: see p. 70 for ways of specifying

- "parameter scan" comprises not only possibility of varying potential depths and geometrical parameters, but also target nucleus, projectile and incident energy (see manual)
- JUMP=2 at end of input deck is condition for transm. coeffs. to be written to file 7 ("ABACUSTL")
- Haase-Tschalbach words of ABACUS (Class 3) must not be used for incident energies higher than highest considered level, or, more generally speaking: for incident energies for which decay modes other than elastic & inel. scatt. to discrete levels have to be considered (inel. scatt. to continuum states, emission of competing particles)

### 2) Informed optical words (JUPITER)

- KTRL(4)=1 consideration of contribution of coupling terms }  
quad. in  $\alpha$  to diag. pot. (vibrational nuclei) } NO
- KTRL(9)= $\begin{cases} 1 \\ 2 \end{cases}$  restrictions of range of  $\gamma$  ( $\bar{m}_j$ , resp.) and } test runs  
TII loops } only
- KTRL(11)=1 Legendre expansion of pot. (rotational nuclei) YES
- KTRL(12)=1 CFF  $\begin{cases} \text{YES} & \text{if you search on potential of your own} \\ \text{NO} & \text{if you use pot. which was determined with RFF} \end{cases}$
- KTRL(25)=1 creation of transm. coeffs. (Viciua), not compatible with KTRL(7)=1 (Acc)

program calculates non-vanishing cross sections even for states whose population is not allowed from energy conservation, if they are coupled ("virtual coupling")

e.g.

inc.en. - - - - -  
grd.st. - - - - -

$\text{IIICPL} = 4$  virtual coupling  
(negative energy channels)

$\text{IIXCAL} > 1$  physically not meaningful

### c) In-equilibrium and compound nucleus model (STAPRE)

- consideration of  $\gamma$  competition is necessary

- near thresholds, e.g.:  $E_{in} \gtrsim 0$  ... NGACOM = 1  
 $E_{in} \gtrsim E_{thr}^{(n, 2n)}$  ... NWACOM = 2

- for calc. of gray production spectrum ... NWACOM = 1
- for calc. of population XS of isomeric } ... NGACOM  $\leq K$   
state in  $K^{\text{th}}$  compound nucle. }

- determination of quantity FM:

$$\lambda_+ (u=3, E \approx 21 \text{ MeV}) \approx 5 \times 10^{-21} \text{ s}^{-1}$$

found by extensive data analysis by

G. M. Praga-Marcattau et al., Phys. Rev. C6 (1972) 1398

E Gadioli, E. Gadioli-Srba, Acta Phys. Slovaca 25 (1975) 126

$$\text{since } \lambda_+ (u=3, E) = \frac{2\pi}{\hbar} (M)^2 \frac{g [g(E - \Delta_{ph}) - C_{3,2}]^2}{4}$$

where  $|M|^2 = FM * A^{-3} * E^{-1}$

$C_{3,2} = 6.5$

$g$  and  $\Delta ph$  determined by KTESTP

} see STAPRE manual

▷  $FM = 0.5 * 10^{22} * \frac{6.58 * 10^{-22} * A^3 * 21/4}{2\pi g [g(E - \Delta ph) - 6.5]^2}$

slight variation may be necessary to fit exp. data

- importance of level scheme for isomeric state cross sections:

- completeness of level scheme: compare high resolution ( $n, n' \gamma$ ) data with charged particle measurements; corresponding  $\gamma$  transitions found?
- spin & parity assignment: what multipole types? ( $E1, M1, E2$ )  
spin differences and parities compatible with  $\left\{ (-)^L \text{ cl. } \right\}_2$ ?  
 $\left\{ (-)^{L+1} \text{ aug. } \right\}_2$ .

if decay to several levels observed: spin assignment consistent?

- importance of spin cutoff parameter for calc. of isomeric state  $\overbrace{XS^5}$

sensitivity to  $I_{eff}/I_{nijd}$

- in PE model:  $\Delta ph = \Delta ph_{pair} = \frac{12}{\sqrt{A}} * \begin{cases} 0 & \text{odd-odd} \\ 1 & \text{odd mass} \\ 2 & \text{even-even} \end{cases} \}$  nuclei, since it

represents at least a simple account for pairing

- for combined Fermi gas and constant temperature level density:

$$\rho(U, J, \Pi) = \frac{1}{2} \rho(U, J) = \frac{1}{2\sqrt{\pi}} \frac{1}{\sigma^3(U)} \omega(U) (2J+1) \exp\left[\left(J+\frac{1}{2}\right)^2/2\sigma^2(U)\right]$$

level density assumed to be parity independent

$\omega(U)$  ... state density

$\sigma(U)$  ... spin cutoff parameter

e.g. 3 regions:

$$0 \leq U < U_1^t \quad \omega(U) = C_1 \exp\left(\frac{U}{T_1}\right)$$

$$\sigma(U) = \sigma_1$$

$$U_1^t \leq U < U_2^t \quad \omega(U) = C_2 \exp\left(\frac{U}{T_2}\right)$$

$$\sigma(U) = \sigma_2$$

$$U_2^t \leq U \quad \omega(U) = \frac{\sqrt{\pi}}{12} \frac{\exp(2\sqrt{a}(U-\Delta))}{a^{1/4} (U-\Delta)^{5/4}}$$

$$\sigma^2(U) = \frac{1}{4\pi} I_4 \sqrt{\frac{U-\Delta}{a}}$$

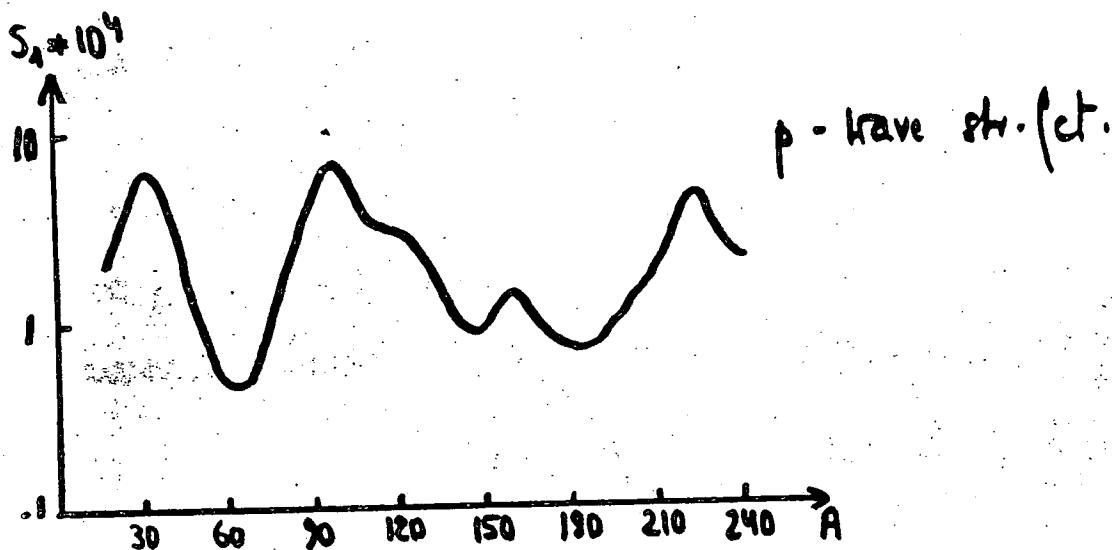
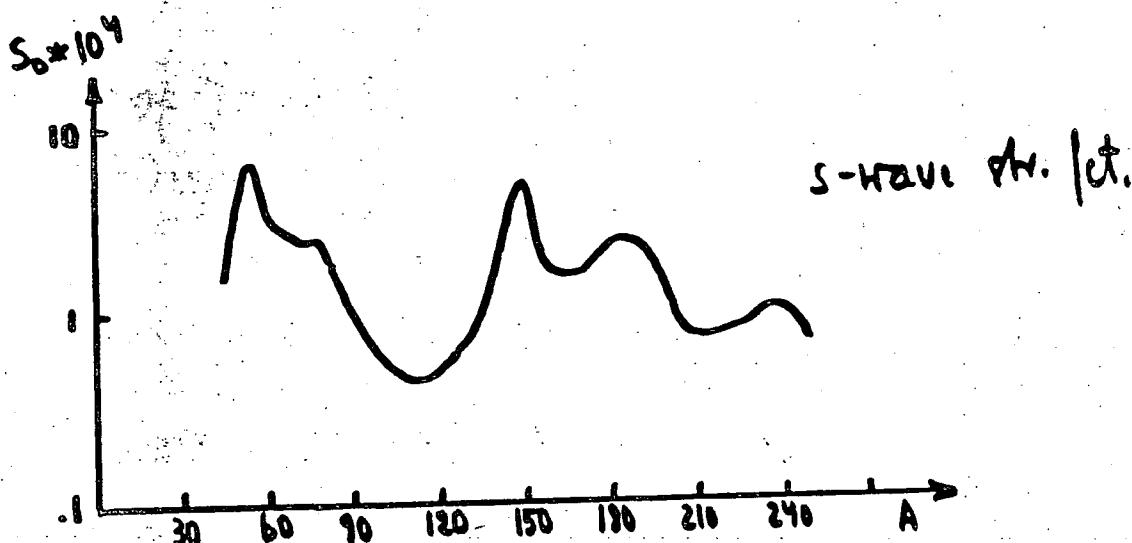
at transition energies  $U_1^t, U_2^t$ : smooth joining of different forms;  
 if  $\sigma$  are different  $\Rightarrow \omega$  and  $\rho$  cannot be joined smoothly at the same time; usually one joins  $\rho(U, J)$  (by appropriate choice of  $C_i$  or  $U_i^t$ )

parameter variation requires adjustment of parameters in other regions  
 in of transition energies

- choice of energy points for generation of  $T_i$ :

in mass regions where str. fcts. have extrema as fct. of  $A$

$\Rightarrow$  for given  $A$  strong dependence on energy, even for low energies



- $T_1$  must be generated
  - to very low energies to avoid extrapolation which relies on constancy of str. fits.
  - with small increments to avoid uncertainties in interpolation

### 3) Input preparation

manual - automatic



using auxiliary programs which construct input for nuclear model codes from simple input (+ appropriate compiled information)

automatic input construction desirable for

- spherical OM if radial dependence (well form) or energy dependence cannot be handled by SCOM code (ABACUS)
- statistical model, if several reactions involving the same nuclei shall be calculated with a consistent parameter set.

Automatic input construction requires libraries containing transmission coefficients, separation energies (or nuclear masses) and nuclear data as level information, level density parameters,  $\gamma$  decay data, PE model parameters.

Advantage of automatic input preparation :

- ▲ parameters of certain nucleus need not be given repeatedly for each occurrence of this nucleus in different reactions, but only once (to the library)
- ▲ choice and variations of parameters consistent for all considered reactions
- ▲ error probability reduced
- ▲ parameters adjusted to exp. data in previous work can easily be utilized for further evaluations in this mass region

## 4) Output evaluation

### - Check of input parameters

- well depths
- level density parameters
- geometr. parameters
- deformation - " "
- inc. energy
- discrete levels
- PE model parameters
- $\gamma$  decay - " -

### - Comparison of results to exp. data

- total XS, total elastic, abs. XS
- diff. el., diff. inel. XS
- activation cross sections (for single reaction paths)
- isomeric state production XS<sup>s</sup> ( — " — )

### - Comparison of quantities deduced from results to exp. data

- strength functions, see p. 74
- potential scatt. radius, - " -  $E_0 = 1 \text{ eV}$ , consider:  $1 \text{ fm} = 10^{-13} \text{ cm}$   
 $\sqrt{M_f} = 10^{-12} \text{ cm}$

- particle production spectra (summed over various reaction paths)  
transformation to lab. system may be necessary

$\Sigma_{\text{rel}}$  ... "channel energy" = energy of rel. motion, C.M. ( STAPRE! )

$\Sigma_{\text{part}}$  ... particle energy, C.M. = channel energy  $\times \frac{M_{RN}}{M_{CN}}$

RN ... residual } nucleus  
CN ... compound }

$\Sigma_{\text{part}}$  ... particle energy, lab.

$$\begin{aligned} \Sigma_{\text{part}}^{\text{lab}} &= \Sigma_{\text{part}}^{\text{C.M.}} + E_{\text{in}} \frac{M_{\text{part}} * M_{\text{RN}}}{M_{\text{RN}}^2} = \frac{M_{\text{RN}}}{M_{\text{CN}}} * \Sigma_{\text{part}}^{\text{C.M.}} + \text{terms (2nd order)} \\ &\approx \frac{M_{\text{RN}}}{M_{\text{CN}}} * \Sigma_{\text{part}}^{\text{C.M.}} \end{aligned}$$

$$\frac{\partial G}{\partial \Sigma_{\text{part}}^{\text{C.M.}}} = \frac{\partial G}{\partial \Sigma_{\text{part}}^{\text{lab}}} * \frac{\partial \Sigma_{\text{part}}^{\text{lab}}}{\partial \Sigma_{\text{part}}^{\text{C.M.}}}$$

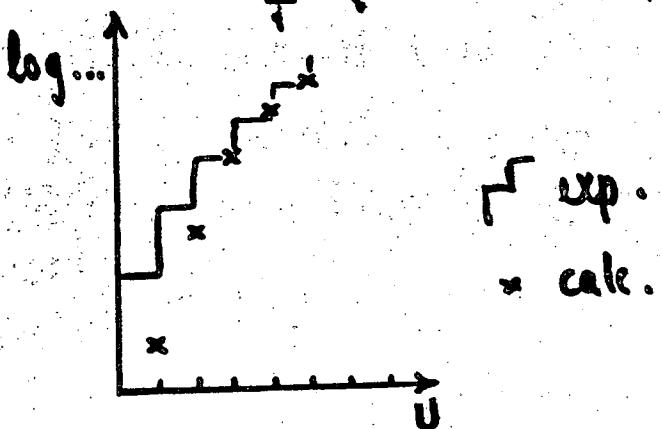
$$\Delta \frac{\partial G}{\partial \Sigma_{\text{part}}^{\text{lab}}} \approx \frac{M_{\text{CN}}}{M_{\text{RN}}} * \frac{\partial G}{\partial \Sigma_{\text{part}}^{\text{C.M.}}}$$

problem of later chance emission : for given particle energy energies of compound and residual nucleus not uniquely determined  
 $\Rightarrow$  no exact kinematical treatment possible  
 for nucleons transformation negligible, for  $\alpha$ 's necessary

- $\gamma$  ray production spectra (summed over various reaction paths)
- residual nucleus part. XS (                  "                  )
- "cumulative level densities"

$$\text{Comparison of } \sum_j \int p(U_j) dU \approx \sum_j \sum_i^K p(U_{i,j}) * dU \quad U_i \dots \text{middle of } i^{\text{th}} \text{ bin}$$

with experimental  $\sum_i^K N_i$        $K=1, 2, \dots$        $N_i \dots \# \text{ of exp. levels}$   
 in  $i^{\text{th}}$  bin



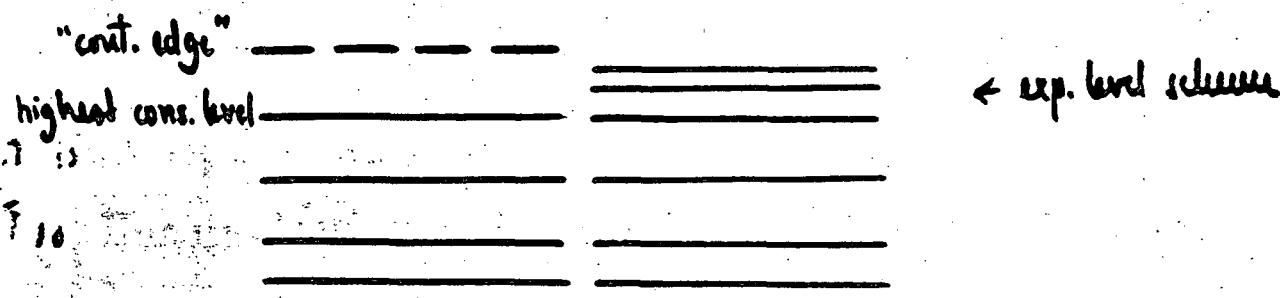
- cross sections for which compound nucleus model and direct contributions have to be combined :
  - o inelastic scattering (also to isomeric states)
  - o charged particle emission from heavy nuclei
- if no consideration of direct contributions possible  $\Rightarrow$  deficiencies of fit should be qualitatively compatible with missing direct interaction contribution (underestimation rather than overestimation, underestimation at the high energy end rather than at low energies...)

### 5) Parameters Variation (STAPRE)

- increase of level density (by means of increase in " $a$ " or decrease in  $\Delta$  in case of back shifted Fermi gas) of residual nucleus after emission of specified particle or of transition states at fission barriers enhances emission of this particle or fission and reduces branching ratios for other decay modes
- decrease of FM increases pre-equilibrium fraction and makes 1<sup>st</sup> chance particle emission spectrum harder; in general (but not necessarily) this reduces later chance particle emission  
 e.g.: reaction path ( $u, 2u$ ): reduction of FM in general increases ( $u, u'$ ) at the cost of ( $u, 2u$ )  
 reaction path ( $u, pn$ ): reduction of FM in general increases ( $n, p$ ) at the cost of ( $u, pn$ )  
 exception: if a certain decay mode competes more favourably in equilibrium stage (e.g.  $\Delta_{ph} = 0$ ,  $\Delta < 0$ )  $\Rightarrow$  reduction of

FM may cause decrease in activation XS of res. nucleus of this decay mode, since reduction of equ. position  $q_2^{P''}$  (cf. p. 50, 100) is more effective than making the spectrum harder.

- increase in  $\bar{T}_{\gamma}$  of certain CN increases activation cross section of this CN; effect is appreciable only if essential fraction of this activation XS comes from population of states where  $\gamma$  competition is effective. Important for isomeric state XS<sup>5</sup>.
- branching ratios of discrete levels influence  $\gamma$  ray production spectrum and isomeric XS ratio (if corresponding decays belong to cascades which populate different states (ground or isomeric). If branching ratios uncertain  $\Rightarrow$  try out other values in order to check effect.
- spin and parity assignment of discrete levels : in the case of uncertain spin parity assignment try alternative  $J^{\pi}$  in order to check influence on results, especially in case of isomeric state cross section calc.
- variation of number of discrete levels : since the lower limit of the lowest "continuum bin" ( $\leftarrow$  bins level density formula is applied) is smallest integer multiple of DU large than exc. energy of highest considered discrete level (relative to zero-point of energy grid), there may be a region without levels, in contradiction to exp. level scheme :



This deficiency may be overcome by adding or leaving out discrete levels; optimization never for all states simultaneously

e.g.: for  $S_0 G_1$ :

in  $S^1 F_0 (n, \alpha n) S^0 G_1$ : cont. edge is smallest integer multiple of  
 $S_\alpha (S^1 F_0) + S_n (S^1 G_1) + E_{\text{last level}}$

in  $S^0 G_1 (n, n') S^0 G_1$ : cont. edge is smallest integer multiple of  
 $S_n (S^1 G_1) + E_{\text{last level}}$

$\Rightarrow$  different positions of cont. edges if  $S_\alpha (S^1 F_0) \neq k * D_U$   
 $(k \text{ integer})$

## 6) Consideration of special features

Problems related to the use of transm. coeffs. created under consideration of direct inelastic scattering

### A) Coexistence of direct contributions and PE

If during the OM fitting procedure to exp. diff. inel.  $\chi^2$ 's no PE is considered, the PE decay populating the states that had been coupled in the OM fit should not be considered in the statist. model calc., either, because the direct contribution then fully accounts for the population of these states. Considering direct

reaction contr. and PE would be a double counting; the same is true with respect to the reduction of  $\sigma_{abs}$ :

$\sigma_{abs}$  in CC0M reduced with respect to SC0M to account for direct t,

$\sigma_{abs} \rightarrow \sigma_{abs} \cdot g^{PE}$  in Haussi Fockback part (q. p. 55, 100) to account for PE

$\Rightarrow$  effects all statist. model cross sections

since direct reactions and PE are considered to describe different reaction mechanisms, both should be considered during the CM fitting procedure. This would require the calc. of angular distributions in PE  $\Rightarrow$  in STAPRE at present

[ (par) approx.: assumption of isotropy  $\frac{\partial^2 \sigma^{PN}}{\partial \Omega \partial \varepsilon} \approx \frac{1}{4\pi} \frac{\partial \sigma^{PN}}{\partial \varepsilon}$  ]

### 3) Use of coupled channels transm. coeffs. for outgoing channels

here for statist. model usually the term  $T_1$  are used for formation and decay, the  $T_1$  of projectile relative to ground state of target are used also for the system of this particle relative to excited states in outgoing channels (also for the states not considered explicitly in CCC, and for the coupled states ( $T_{1g}^3$  instead of  $T_{1g}^2$ , cf. p. 35, 77)). Therefore the effects of absorption of flux to the coupled channels which is related to the collective nature of ground st. and coupled states are considered also when no such effects occur, in particular also for other nuclei if NTRAN = 1. It would be preferable not to use CCT<sub>1</sub> for outgoing channels. This is at present not possible in STAPRE.

## Isospin correction for p induced reactions

Isospin of target  $T_t$

in p induced reactions : 2 isospins of CN can be formed  $T_c = T_t - \frac{1}{2}$   
 $T_s = T_t + \frac{1}{2}$

isospin mixing : population can be transferred between  $T_c$  and  $T_s$  states

(e.g. without isospin corresponds to consideration of  $T_c$  states only)

Formulation : S. Primes et al., Phys. Rev. C5 (1972) 85

- isospin mixing consists in transfer of fraction  $\mu$  of the population of  $T_s$  states to  $T_c$  states ( $\mu$ : mixing parameter)
- for considered energy the density of  $T_s$  states of residual nuclei negligible

in particular for (p,n) reaction:

$$\sigma_{pn}(\mu) = \left( \frac{2T_0}{2T_0+1} + \mu \frac{1}{2T_0+1} \right) \sigma_{abs} \frac{\Gamma_n}{\Gamma_n + \Gamma_d + \Gamma_p + \left( \frac{2T_0}{2T_0+1} + \mu \frac{1}{2T_0+1} \right)}$$

where  $\Gamma_n, \Gamma_p, \Gamma_d$  are the widths obtained without cons. of isospin ( $\mu=1$ )

$$\triangleright \frac{\Gamma_p}{\Gamma_n} = \frac{\sigma_{pp}(\mu=1)}{\sigma_{pn}(\mu=1)} \quad \frac{T_c}{\Gamma_n} = \frac{\sigma_{abs} - \sigma_{pn}(\mu=1) - \sigma_{pp}(\mu=1)}{\sigma_{pn}(\mu=1)}$$

$$\text{Define } f(\mu) = \frac{2T_0}{2T_0+1} + \mu \frac{1}{2T_0+1}$$

$$\triangleright \sigma_{pn}(\mu) = f(\mu) \sigma_{abs} \frac{1 + \frac{\sigma_{abs} - \sigma_{pn}(\mu=1) - \sigma_{pp}(\mu=1)}{\sigma_{pn}(\mu=1)} + f(\mu) \frac{\sigma_{pp}(\mu=1)}{\sigma_{pn}(\mu=1)}}{\sigma_{pn}(\mu=1)}$$

$$\boxed{\sigma_{pn}(\mu) = f(\mu) = \sigma_{pn}(\mu=1) \frac{1 - \frac{\sigma_{pp}(\mu=1)}{\sigma_{abs}} (1 - f(\mu))}{1 - \frac{\sigma_{pp}(\mu=1)}{\sigma_{abs}} (1 - f(\mu))}}$$

## Comission of OM results due to non-consideration of capture

Usually, in OM codes no competing reactions like Rn-e. + neutr. scatt. are considered (cf. p. 123). Capture competes with these decay modes even at low- $E_\gamma$  energies:

$$\sigma_{\text{obs}} = \sigma_{\text{capt}} + \sigma_{\text{c.e.l.}} \text{ instead of } \sigma_{\text{obs}} = \sigma_{\text{c.e.l.}} !$$

Calculate  $\sigma_{\text{capt}}$  from statist. model and correct  $\sigma_{\text{c.e.l.}}$  for non-consideration of capture in the OM:

$$\boxed{\sigma_{\text{c.e.l.}} = \sigma_{\text{c.e.l.}}|_{\text{OM}} * \frac{\sigma_{\text{obs}} - \sigma_{\text{capt}}}{\sigma_{\text{obs}}}}$$

Necessary to satisfy ENDF/B consistency checks.

## 7) Accuracy

- A) Rough estimate of uncertainties of calculated cross sections from comparison to exp. data
  - if exp.  $\chi^2$ 's are reproduced reasonably  $\Rightarrow$  uncertainties of calc'd.  $\chi^2$ 's comparable to experimental uncertainties
  - if exp.  $\chi^2$ 's are reproduced badly  $\Rightarrow$  uncertainties of calc'd.  $\chi^2$ 's difficult to estimate, even if one doubts the experiment
  - if no exp.  $\chi^2$ 's for considered reaction exist  $\Rightarrow$  estimated uncertainty depends on how well the chosen parameter set is confirmed by reproduction of cross sections of competing  $\chi^2$ 's, level data, resonance data,  $\chi^2$ 's of "inverse reactions" ... (cf. p. 117)

B) Estimate of uncertainties of calculated cross sections from uncertainties of the parameters

Cross section values are assumed to be functions of  $n$  parameters  $p_1, \dots, p_n$  which are known with uncertainties  $\Delta p_1, \dots, \Delta p_n$ .

$\Rightarrow$  uncertainty of cross section :

$$\Delta \sigma_{\text{calc}}(E_i) = \left[ \left( \frac{\partial \sigma_{\text{calc}}(E_i)}{\partial p_1} \Delta p_1 \right)^2 + \left( \frac{\partial \sigma_{\text{calc}}(E_i)}{\partial p_2} \Delta p_2 \right)^2 + \dots + \left( \frac{\partial \sigma_{\text{calc}}(E_i)}{\partial p_n} \Delta p_n \right)^2 \right]$$

whereby the quantities  $\frac{\partial \sigma_{\text{calc}}(E_i)}{\partial p_k} \Delta p_k$  will in general be derived from the changes in cross sections if all parameters except  $p_k$  are kept fixed and only the parameter  $p_k$  in question is changed by the estimated amount  $\Delta p_k$  from its most probable value.

Uncertainties of the calculated cross section values for different energies are correlated to a high degree due to the fact that most parameter changes result in an increase or decrease of the whole excitation function.

From the above formula rather large  $\Delta \sigma_{\text{calc}}$  result, if one uses for  $\Delta p_m$  the uncertainties of the parameters without considering that there is the additional constraint of reproducing exp. cross sections.

If at least in a small energy region (usually 14-15 MeV) very accurate experimental data exist, from the condition that the changes in the calc'd. xs at this energy due to variations of the parameters shall be at most equal to  $\Delta \sigma$ .

smaller values for the  $\Delta_{pm}$  can be determined, from which smaller uncertainties of the whole calcd. excitation function result.

Description of correlations by means of covariance matrices,  
see:

F. Perey, Proc. Int. Conf. Nuclear Data for Reactors and Other  
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Practical part: Description of the problems treated in the workshops

1) Optical model calculations for  $^{48}\text{Ti+n}$

Spherical optical model calculations by means of the code ABACUS were performed using the potentials by

J. Rapaport, Phys. Repts. 87 (1982) 25 and

E.D. Arthur, P.G. Young, Rept. LA-8626-MS.

As both these potentials differ from what is provided for in ABACUS with respect to energy or radial dependence, an existing computer program for ABACUS input construction was modified so as to handle these potentials. The resulting s-wave strength function, total cross section and differential elastic cross section at 2.9 MeV were compared to experimental data by the following authors:

<u>Quantity</u>	<u>Energy</u>	<u>Reference</u>
$S_0$	2.7 - 300 keV	Allen et al., Exfor 30359.017
$S_0, R'$	17.6 - 270 keV	BNL-325
$\sigma_{\text{total}}$	.389 Mev	Bowman et al., Exfor 11600.012
$\sigma_{\text{total}}$	14.2 MeV	Djumin et al., Exfor 40149.004
$\frac{\partial \sigma_{\text{el}}}{\partial \Omega}$	2.9 MeV	Pasechnik et al., Exfor 40045.002

The sensitivity of the results to variations in the depths of real and imaginary potential was studied by means of the parameter scan option of ABACUS. As both potentials were found to reproduce the experimental data reasonably although they had been determined for slightly heavier nuclei and, in the case of the Rapaport potential, for energies above 7 MeV only, they were also used to prepare neutron transmission coefficients for the statistical model calculations.

2) Calculation of transmission coefficients for  $^{48}\text{Sc+p}$  and  $^{45}\text{Ca+a}$ .

For the  $^{48}\text{Ti+n}$  statistical model calculations, charged particle transmission coefficients were generated using the code ABACUS. For each particle type, two different potentials were used, namely

for protons:

G.S. Mani et al., Rept. C.E.A.-2379 (1963)

F.G. Perey, Phys. Rev. 131 (1962) 745

for  $\alpha$ -particles:

J.R. Huizenga et al., Rept. ANL-6373 (1961)

O.F. Lemos, Orsay Rept., Series A, No. 136 (1972)

Also for these calculations, some programming work regarding input construction was necessary.

### 3) Statistical model calculations for $^{48}\text{Ti} + \text{n}$

Input data for the code STAPRE were prepared for the reactions  $(n,2n)$ ,  $(n,p)$ ,  $(n,\alpha)$ ,  $(n,np)$ ,  $(n,na)$  on  $^{48}\text{Ti}$ . During the input preparation the use of various compilations of parameters necessary for STAPRE calculations was demonstrated and the models into which these parameters enter were repeated. The above reactions were chosen in order to be able to study the effect of parameter variations on all competing decay modes of the intermediate nuclei  $^{49}\text{Ti}$ ,  $^{48}\text{Ti}$  simultaneously and to compare the calculations with the following experimental data:

Quantity	Energy	Reference
$(n,\alpha)XS$	14.1 MeV	Yu Wen Yu et al., Exfor 11583.003
$(n,p)XS$	14.5 MeV	E.B. Paul et al., Exfor 11274.026
- " -	12.7-17 MeV	F. Gabbard et al., Exfor 11494.006
- " -	14.5 MeV	M. Hillman, Exfor 11610.004
- " -	14.7 MeV	D. Crumpton, Exfor 20931.005
- " -	5.8-14.1 MeV	M.T. Swinhoe et al., Exfor 20986.005
- " -	14.8 MeV	R. Prasad et al., Exfor 30336.011
- " -	14.7 MeV	V.K. Tikku et al., Exfor 30394.003
$(n,np)XS$	14.7 MeV	S. Qaim et al., CINDA Suppl. 78
$\alpha$ production spectrum	15 MeV	S. Grimes et al., Nucl. Sci. Eng. 62 (1977) 187
p production spectrum		

The calculations were performed with the various sets of transmission coefficients described in 1) and 2). During the level density parameter variations which were necessary for improving the agreement of the calculations with the  $(n,\alpha)$  and  $(n,p)$  cross sections, a method for checking the compatibility of the varied

parameters with experimental level information was practiced. The 2nd chance charged particle emission cross sections could not be calculated during the course time, and therefore the comparison of the production spectra could not be performed but advice was given for this kind of investigation.

4) Optical model calculations for  $^{238}\text{U}+\text{n}$

Coupled channels optical model calculations were performed with the code IUPITOR, using potentials determined by:

V.A. Konshin, Proc. Winter Course Nucl. Theory for Applications, Trieste, 1980, IAEA-SMR-68/I(1981) 139

A. Prince, International Nucl. Model Codes Comparison Study, NEANDC 128 "U"

The results were compared to the experimental total and elastic cross sections given in "Compilation of Actinide Neutron Nuclear Data", NEANDC(OR) 153/L and the experimental strength functions mentioned in J.P. Delaroche et al., Proc. Consultants Meeting on Nucl. Theory for Neutron Nuclear Data Evaluation, Trieste, 1975, IAEA-190 (1976) 251. Special investigation was devoted to the dependence of the strength functions on the number of states coupled virtually to the ground state. As the reproduction of the available experimental data by the calculations with the Konshin potential was satisfactory, neutron transmission coefficients were created with this potential and processed for use in the code STAPRE.

5) Statistical model calculations for  $^{238}\text{U}+\text{n}$

As time was not sufficient for the statistical model part of the  $^{238}\text{U}$  sample evaluation, recommendations regarding options and parameter values for the STAPRE input to be prepared were left to the participants in written form, together with a graphic representation of experimental excitation functions for  $(\text{n},\gamma)$  and  $(\text{n},\text{f})$  on  $^{238}\text{U}$  and their reproduction by STAPRE calculations performed by M. Uhl at the IRK (unpublished).