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Evaluations of the fast neutron cross sections

of ⁵⁸Ni including

complete covariance information

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1. Abstract

A new evaluation of all important neutron cross sections of ⁵⁸Ni was performed in the neutron energy range 0.812 - 20 MeV, that is for the whole energy range above the resonance region. The evaluation combines the results of nuclear model calculations and the complete existing experimental data base in order to obtain the most accurate description of the cross sections possible within our present knowledge. The evaluation was performed in the following way: The cross sections from the EFF - 2 file (results of model calculations) and their estimated covariances are used as prior information which is successively improved by adding experimental data and by applying Bayes' theorem to obtain the posterior information. For this process the code GLUCS was used. For some cross sections, not covered in EFF - 2, priors were taken from ENDF/B-VI and JENDL -3. For two cross - section types, (n,p) and (n,2n), where we had already done such evaluations previously, we used those results directly. As the results we obtained evaluated cross sections and their covariances for a chosen set of 16 independent cross sections. A final coupled set of evaluated cross sections and covariances was obtained by a last GLUCS run including the experimental data for "redundant" cross sections that is all cross sections which can be expressed as sum or differences of the basic cross sections chosen for the evaluation. The results of our new evaluation agree with ENDF/B–VI and EFF – 2 within the uncertainties of these evaluations. Most of the uncertainties of our evaluated cross sections, however are considerably smaller than those of ENDF/B–VI and EFF -2.

2. General evaluation procedure

The general principle of our evaluation is essentially the same as used in (*Vonach 92*). For a better understanding of this report we will give a short description of this procedure; it is shown schematically in Fig. 1. First we choose a set of non-redundant cross sections which give a complete sufficiently detailed description of the interaction of fast neutrons with ⁵⁸Ni as the subject of the evaluation. As the starting point we use the EFF – 2 evaluation (*Uhl 91*) and its covariances (*Tagesen 91*) with some modifications which are going to be discussed later in section 3. This constitutes our prior knowledge of the neutron cross sections of ⁵⁸Ni. Each type of cross section is represented by a cross section vector T and its covariance matrix M. For some rare reactions, not contained in EFF – 2 we have used ENDF/B–VI and JENDL – 3 (see section 3). Then Bayes' theorem was used to add successively the experimental data for the various ⁵⁸Ni cross sections to the prior. This is done in the following way: If the data are described by a vector *R* with the covariance matrix *V*, application of Bayes' theorem matrix *M*'

$$T' = T + MG^{+}(GMG^{+} + V)^{-1}(R - R_{T})$$
(1)

$$M' = M - MG^{+} (GMG^{+} + V)^{-1} GM$$
 (2)

where R_T presents the prior value interpolated at the point where *R* is given, *G* is the sensitivity matrix of the new experimental data relative to the prior data with the matrix elements $g_{ij} = \delta R_i / \delta T_j$, and the up scripts (+) and (-1) mean transpose and inverse operation respectively. One of the most important conditions for obtaining these formulae is an absence of correlations between the data vectors *T* and *R*. This condition is fulfilled as *T* was derived from nuclear model calculations and *R* are results of measurements.

From this procedure (depicted at the left side of Figure 1) we get a set of improved cross sections with much reduced uncertainties compared to the prior EFF – 2 values. Cross sections for which no experimental data exist (e.g. $\sigma_{n,np}$, $\sigma_{n,n\alpha}$) remain unchanged at this step. This procedure however does not use the complete experimental data base. In addition to cross section measurements for our basic cross sections there exist always additional measurements on so-called redundant cross sections, which are sums or differences of our basic, linearly independent cross sections (see Fig. 1 and section 5.2). In order to also use this information in a final evaluation step (see right side of Figure 1) the results of our evaluations for the basic cross sections are used as a new improved

prior and the data for the redundant cross sections are added as data for the corresponding sums or differences of basic cross sections in a final evaluation step again using eq 1 and 2.

Thus the evaluations proceed in the following steps:

- 1) Establishment of the prior data for all cross sections of interest.
- 2) Establishment of the experimental data base.
- 3) Calculation of the improved cross sections T' and covariances M' for all important cross sections for which data are available.
- 4) Further improvement of the evaluation by adding the information from all redundant cross sections in a final evaluation step applied to the joint cross section vector for all reaction types.

This leads to a final result of the evaluation in form of a cross section vector T' containing a complete set of independent cross sections and one large covariance matrix M' which can be subdivided into covariance matrices for the individual cross sections and covariance matrices between different cross section types (interreaction covariance matrices).

Technically this procedure is performed by means of the code GLUCS (*Hetrick 80*) which implements Equ. (1) and (2) and provides output on T' and M' directly in ENDF/B format. As modified recently (*Tagesen 94*) it can also be used for the constrained least squares adjustment of step 4 of our evaluation procedure.

3. Establishment of the prior information for all cross sections of interest

For this evaluation we chose the following cross sections as our complete basic set of non-redundant cross sections, from which all other cross sections of interest can be derived as linear functions: σ_{tot} (MT1), $\sigma_{n,2n}$ (MT16), $\sigma_{n,n\alpha}$ (MT22), $\sigma_{n,np}$ (MT28), $\sigma_{n,n1}$ (MT51), $\sigma_{n,n2}$ (MT52), $\sigma_{n,n3}$ (MT53), $\sigma_{n,n4-8}$ (MT851), $\sigma_{n,ncont}$ (MT91), $\sigma_{n,\gamma}$ (MT102), $\sigma_{n,p}$ (MT103), $\sigma_{n,d}$ (MT104), $\sigma_{n,t}$ (MT105), $\sigma_{n,3He}$ (MT106), $\sigma_{n,\alpha}$ (MT107) and $\sigma_{n,p\alpha}$ (MT112).

Most of the choices are obvious, the only important point is the amount of detail used to describe inelastic neutron scattering to discrete levels. Our starting point EFF-2 contains cross sections for the excitation of 21 levels of ⁵⁸Ni; thus in principle excitation of all those levels could have been included separately in our evaluation. It is however intended to combine the file 3 and 33 data of this evaluation with the file 6 of ENDF/B-VI for the energy/angle distributions of the emitted particles. In this evaluation only cross sections for the excitation of the first 8 levels of ⁵⁸Ni are given separately, whereas inelastic scattering to all higher levels is included in the continuum cross section (MT91). Thus in order to be consistent with this choice, we decided to add the cross sections for all levels above No. 8 (that is MT59-71) to $\sigma_{n,ncont}$ (MT91) and to retain only MT51-58. In addition the excitation energies of levels 4-8 are so close together that it is reasonable to treat them together and only evaluate the sum of their cross sections. From these considerations we finally decided to describe inelastic scattering by 5 cross sections (n,n₁), (n,n₂), (n,n₃), (n,n₄₋₈) and (n,n_{cont}) as listed before.

We decided to use the EFF – 2 evaluation as far as possible as the basis for the prior vector and covariance matrix respectively (T,M) in this evaluation because it provides an already good description of the ⁵⁸Ni cross sections, has sufficiently detailed covariance information and is essentially uncorrelated with the experimental data to be added (see Table 1). In detail, however, some modifications had to be made. Therefore, in the following a brief description of the prior quantities actually used is given:

A) Cross section

1) For the cross sections σ_{tot} , $\sigma_{n,n1}$, $\sigma_{n,n2}$, $\sigma_{n,n3}$, $\sigma_{n,n4-8}$, $\sigma_{n,\gamma}$, $\sigma_{n,\alpha}$ and $\sigma_{n,np}$ the cross sections from EFF-2 were used as prior values without any change. The cross sections for $\sigma_{n,ncont}$, however, were taken from ENDF/B-VI as we used the same definition of the continuum border as in ENDF/B-VI in order to be compatible with the file 6 data of ENDF/B-VI.

- 2) For the cross sections (n,2n) and (n,p) we made use of recent accurate evaluations of our group (*Wagner 90* and *Badikov 96*) which already include all experimental data. Therefore step 1 of our evaluation (see Fig. 1) for these cross sections was replaced by the use of these existing accurate evaluations.
- 3) For the small cross sections $\sigma_{n,d}$ and $\sigma_{n,n\alpha}$ not given in EFF-2 cross sections from ENDF/B-VI were used as prior, for $\sigma_{n,t}$ and $\sigma_{n,3He}$ the only existing evaluation JENDL-3 was used.

B) Covariances

1. EFF-2 cross sections

Relative uncertainties as a function of neutron energy were taken from the EFF-2 covariance estimates (*Tagesen 91*) for $\sigma_{n,np}$, $\sigma_{n,d}$ and $\sigma_{n,\gamma}$. For inelastic neutron scattering to discrete levels EFF-2 only gives covariances to the sum of all discrete cross sections. Therefore uncertainties for $\sigma_{n,n1}$, $\sigma_{n,n2}$, $\sigma_{n,n3}$, $\sigma_{n,n4-8}$ and $\sigma_{n,ncont}$ were estimated from the differences of those cross sections between the evaluations EFF-2, ENDF/B-VI, JENDL-3 and BROND using the procedures developed in *Tagesen 91*. In the same way the uncertainty of $\sigma_{n,ncont}$ taken from ENDF/B-VI was derived. For the small cross sections $\sigma_{n,3He}$ and $\sigma_{n,p\alpha}$, for which no covariances are given in EFF-2, rather large uncertainties are assumed based on our experience on the reliability of calculations of such cross sections.

- 2. For σ_{tot} , where good experimental data are available for the whole energy range of the evaluation uncertainties for the prior were set to 10% about an order of magnitude larger than the experimental uncertainties in order to obtain a so-called uninformative prior which does not influence the evaluation result.
- 3. For $\sigma_{n,p}$ and $\sigma_{n,2n}$ the covariance matrices given in (*Badikov 96*) and (*Wagner 90*) were used.
- 4. For the cross sections ($\sigma_{n,d}$ and $\sigma_{n,n\alpha}$) taken from ENDF/B-VI also the corresponding covariance matrices from ENDF/B-VI were used. For $\sigma_{n,t}$ taken from JENDL-3 approximate covariance data were estimated based on our experience about the reliability of the calculations of such cross sections as in the cases $\sigma_{n,3He}$ and $\sigma_{n,p\alpha}$ discussed before.

In EFF - 2 the energy range of the evaluations has been divided into intervals of 0.5 MeV and 1 MeV for the representation of the covariance matrices within which cross sections are fully correlated. In the lower energy range of our evaluation these intervals appeared to be too large for a detailed description of the excitation function.

Therefore a finer energy grid (33 intervals) was adopted for this evaluation. Energy bins of 0.2 MeV were chosen in the energy range up to 3.0 MeV, 0.5 MeV in the energy range 3.0 - 6.0 MeV and 14.0 - 15.0 MeV and 1.0 MeV for the rest of the energy range (see e.g. Table 13). This structure of the covariance matrices was used for all cross sections.

For EFF – 2 a triangular decrease of correlation with increasing distance in energy was assumed for all cross sections in order to describe the (positive) correlations between the cross section uncertainties at different neutron energies E_1 and E_2 (see discussion on page 6 in *Pavlik 91*). To prevent high rigidity of shape of the excitation functions at low energies a variable FWHM of the triangular decrease was calculated as

FWHM = $(E_1 + E_2)/10. + 2.e+5$ (eV)

which results in FWHM ranging from $\approx 400 \text{ keV}$ at 1 MeV up to $\approx 4 \text{ MeV}$ at 20 MeV incident neutron energy for generating the off – diagonal elements of the covariances of our priors. Correlation coefficients between cross section uncertainties at the energies E_1 and E_2 were calculated according to the relation

$$\operatorname{cov}(\sigma_{1}\sigma_{2}) = \sqrt{Var(\sigma_{1}) \cdot Var(\sigma_{2})} \cdot \frac{(FWHM - ABS(E_{1} - E_{2}))}{FWHM}$$
(3).

in case of ABS $(E_1 - E_2) \le FWHM$ and zero otherwise

4. Establishment of the experimental data base including construction of covariance matrices for all data sets

We used the experimental data compiled in EXFOR (*Lemmel 86*, *McLane 88*) and supplemented them by very recent ones which were mostly obtained directly from the authors. In addition to measurements on 58 Ni we also used measurements on natural nickel for such cross sections for which the difference between 58 Ni and nat Ni is known to be small as is the case for σ_{tot} , σ_{non} and σ_{el} above 4 MeV; also such cross section measurements on nat Ni were used, which could be converted to 58 Ni cross section by means of information for the remaining isotopes ($\sigma_{\alpha-prod}$). Additionally, in order to widen our data base also some more complex cross sections like the γ – production cross section for the first 2⁺ level were included in our data base, if good measurements have existed and accurate conversion procedures to basic cross sections, e.g. σ_{inel} , could be developed. Differential elastic and inelastic scattering cross sections measured over a sufficient angular range were used to derive the total elastic and inelastic scattering cross sections by means of fits with Legendre polynomials in those cases where the integrations had not been performed by the authors.

All data sets were critically reviewed, obviously wrong data were rejected. The accepted data were renormalized if necessary with regard to the standard cross sections or decay data used. In some cases renormalizations were also applied if comparisons of a data set with other data consistently have indicated the need for such renormalizations.

For the construction of the covariance matrices of the experimental data sets it is necessary to have detailed information on all uncertainty components of the measurements and the correlation of each component within the data set. As this information is not given for most of the experiments various approximations had to be used.

We assumed that the covariance matrix of total uncertainties can be split into two matrices of partial uncertainties:

1) a diagonal covariance matrix of partial uncertainties describing short – energy – range (SER) correlation properties such as statistical uncertainties due to a finite number of counts per channel;

2) a constant covariance matrix of partial uncertainties connected with properties which induce large - energy - range (LER) correlations, such as systematic uncertainties due to any normalization of the cross sections in order to get absolute values, to the determination of the number of nuclei in a sample, to geometrical sizes and distances and to sample self – absorption properties for the non – resonance energy

region. This means we assume complete correlation over all energy groups for these long – range uncertainty components.

The magnitudes of the described two components were chosen according to the uncertainty information given by the authors, or in case of missing information they were estimated by the authors according to their experience about typical uncertainties at the time of the respective experiments.

Only for the total cross sections it was necessary to use a third partial uncertainty matrix, describing so-called medium-energy range correlations (MER). For this covariance matrix the correlations between the uncertainties for different energy groups are described by a linear model of correlation propagation with a certain energy E_c (typical 2 MeV within which the correlation decreases linearly from 100% to zero.

A summary on the data base prepared in this way is given in Tables 2 - 12. For each data set, accepted for the evaluation, the tables give the energy range of the experiment, the number of data points, the short and long-range uncertainties assigned to the respective data set and in some cases information about special treatment of the data prior to the use in the evaluation. The numerical values of the cross sections and the covariances cannot be given in this report, they are however available on request at our institute.

While most of the cross-section values could be directly put into the evaluation some pre-treatment was necessary for a part of the cross-section types and some special data sets. In detail the following procedures were used .

1. Total cross sections: A number of total cross section measurements have been performed with high-resolution using white neutron sources resulting in a very large number of data points (see Table 2). These data sets have been pre-averaged into bins corresponding to the group structure of the evaluation and only these averaged values were used as evaluation input. Thus also our evaluated total cross sections are in principle group cross sections (averages over the 0.2 – 1.0 MeV intervals chosen for the evaluations). This fact is important for the lower energy range up to about 4 MeV, where the total cross sections exhibit considerable fluctuations (which have to be re-introduced in a final step following this evaluation). Above 4 MeV the fluctuations are small and the general energy dependence is rather weak, therefore above 4 MeV these group cross sections can also be considered as point cross sections at the respective group centers. Total cross section data for natural nickel have been included for neutron energies above 4 MeV, as in this energy region the cross section difference between ⁵⁸Ni and ^{nat}Ni is expected to be smaller than the

uncertainty of the measurements. In addition it is intended to use these cross section of ^{nat}Ni for the following evaluation of ⁶⁰Ni; thus small errors will be cancelled if these two evaluations are combined to describe ^{nat}Ni.

- 2. Inelastic scattering cross sections for excitation of the first level (E = 1.45 MeV): As noted in Table 3 a number of data sets reporting only differential cross sections were integrated over angle using the code GPOLFIT (*Pavlik 90*).
- 3. Inelastic cross sections for excitation of higher levels (Table 4): In addition to the direct neutron scattering measurements, also the γ -production measurements of Traiforos et al. (*Traiforos 79*) were used. These data which are not available in numerical form were read from the graphs in the original paper and inelastic neutron scattering cross sections for the various levels were derived by adding the γ -production cross sections for all γ -transitions deexciting the particular level and subtracting (if necessary) γ -transitions feeding the level from higher levels.
- 4. Total inelastic cross sections (see Table 8) were derived from the measurements of the γ-production cross sections for the2⁺ → g.s. transition (see Figure 2) using an energy-dependent correction factor for the small fraction of direct γ-transitions from higher levels to the ground-state. An uncertainty of 5% was assumed for this correction factor for neutron energies above 3 MeV. Below this energy there are no direct ground state transitions and the correction factor is exactly unity.
- 5. Elastic cross sections for ^{nat}Ni were included for $E_n > 4$ MeV for the reasons discussed before.
- 6. Cross sections for total α -production in ^{nat}Ni were converted into isotopic cross sections by means of the relation

$$\sigma_{_{58}Ni} = \frac{\sigma_{_{nat}Ni}}{f_{58} \cdot \left[1 + \frac{f_{60}}{f_{58}} \frac{\sigma_{60}}{\sigma_{58}}\right]},$$

where $f_{58} = 0.681$ and $f_{60} = 0.262$ are the isotopic abundances of ⁵⁸Ni and ⁶⁰Ni. Values for the ratio σ_{60}/σ_{58} were taken from a recent experiment of Haight et al. (*Haight 98*), were both cross sections have been measured under identical conditions. As the factor $(f_{58}/f_{60}) \cdot (\sigma_{60}/\sigma_{58})$ remains below 0.25 for all energies, the uncertainty in this correction factor can be neglected compared to the uncertainties of $\sigma_{nat_{Ni}}$ (see Table 11).

7. The results of *Pavlik 91* at $E_n = 14$ MeV in Tables 8, 9 and 10 are taken from the evaluation of Pavlik et al. (*Pavlik 91*) which give the weighted average of all cross section measurements at 14 MeV. Details about the original data can be found in (*Pavlik 91*).

- 8. Finally it has to be mentioned, that the experimental database for ⁵⁸Ni(n,2n) and ⁵⁸Ni(n,p) reactions is not given here, as good recent evaluations of these reactions are available (*Wagner 90* and *Badikov 96*), which have been used by us in order to avoid unnecessary duplication of work as discussed in Section 3. The experimental data summarized in Tables 2-12. In addition to the data listed in Tables 2-12 one cross section value ($244 \pm 11 \text{ mb}$) for $\sigma_{n,n \text{ cont}}$ (MT91) at $E_n = 14.1 \text{ MeV}$ derived from the secondary neutron production cross section at 14.1 MeV of ^{nat}Ni integrated over the secondary neutron energy range 5-11 MeV (*Pavlik 93*) was also used in the evaluation. The conversion of this cross section integral into values for $\sigma_{n,n \text{ cont}}$ for both ⁵⁸Ni and ⁶⁰Ni was done by comparing the measured cross section integral to that calculated with ENDF/B-VI and scaling the ENDF/B-VI cross sections for $\sigma_{n,n \text{ cont}}$ with the ratio of these two integrals. The uncertainty of the experimental cross section integral was also assigned to the values of $\sigma_{n,n \text{ cont}}$ derived in this way.
- 9. There is consistency both within the database and between the priors and the data as can be seen from Fig. 3 22 discussed in section 6.

5. Cross section evaluation

5.1. Evaluation of the cross sections for individual reactions

In the first evaluation step the experimental data for the basic cross sections were combined with the respective priors by means of the code GLUCS according to the general procedure described in Section two (see Fig. 1). This was done for the cross sections σ_{tot} , $\sigma_{n,n1}$, $\sigma_{n,n2}$, $\sigma_{n,n3}$, $\sigma_{n,n4-8}$, $\sigma_{n,\alpha}$, $\sigma_{n,d}$ and $\sigma_{n,t}$. For the cross sections $\sigma_{n,2n}$ and $\sigma_{n,p}$ this work has already been done in the evaluation (*Wagner 90*) and (*Badikov 94*) used as priors, thus these priors could be used directly as input for the second evaluation step. For the cross sections $\sigma_{n,n \text{ cont}}$, $\sigma_{n,3He}$, $\sigma_{n,np}$, $\sigma_{n,n\alpha}$ and $\sigma_{n,p\alpha}$ there are no experimental data; accordingly no improvement of the priors was possible in the first evaluation step.

5.2. Consistent joint evaluation of all cross sections

The cross sections σ_{inel} , σ_{non} , σ_{el} , $\sigma_{57Co-prod}$ and $\sigma_{\alpha-prod}$ summarized in Table 8-12 are "redundant" cross sections that is they are sums or differences of the basic cross sections chosen for our evaluation (see Table 1). They are connected to the basic cross sections by means of the relations

$$\sigma_{inel} = \sigma_{n,n_1} + \sigma_{n,n_2} + \sigma_{n,n_3} + \sigma_{n,n_{4-8}} + \sigma_{n,n_{cont}}$$

$$\tag{4}$$

$$\sigma_{non} = \sigma_{inel} + \sigma_{n,2n} + \sigma_{n,p} + \sigma_{n,np} + \sigma_{n,\alpha} + \sigma_{n,n\alpha} + \sigma_{n,d} + \sigma_{n,t} + \sigma_{n,p\alpha} + \sigma_{n,\gamma}$$
(5)

$$\sigma_{el} = \sigma_{tot} - \sigma_{non} \tag{6}$$

$$\sigma_{s_{7}Co-prod} = \sigma_{n,np} + \sigma_{n,d} \tag{7}$$

$$\sigma_{\alpha-prod} = \sigma_{n,\alpha} + \sigma_{n,n\alpha} \tag{8}$$

As the final step of the evaluation (see right side of Figure 1), an improved evaluation using the information contained in both our basic and redundant cross sections, was obtained in the following way: The redundant cross sections were added as "data" of sums or differences of basic cross sections, according to Equation 4 - 8, by using again the code GLUCS, based on Equation 1 and 2 (see Section 2). The posterior data derived in this way not only strictly fulfill the consistency relations (Equation 4 - 8) but are also considerably improved in quality as many of the redundant cross sections (e.g. σ_{non} or σ_{inel}) are known rather accurately and this accuracy is in part transferred to the basic cross sections by means of the applied constrained least squares fit. Technically the

accepted redundant cross sections (see Tables 8 - 12) of all types were added as one large data vector to the prior consisting of the coupled set of all basic cross sections in one GLUCS run.

Because of the conditions (4 - 8) and the consideration of all basic cross sections as one coupled set, the resulting correlation matrix now includes parts, which describe correlations between different energy intervals of different cross sections. In most cases these correlations are small (< 10%), in some cases however, e.g. between different partial inelastic cross sections, they are important and have to be taken into account.

6. Results of the evaluation

The main result of this evaluation is a complete but non-redundant set of cross sections (σ_{tot} , $\sigma_{n,n1}$, $\sigma_{n,n2}$, $\sigma_{n,n3}$, $\sigma_{n,n4-8}$, $\sigma_{n,n}$ cont, $\sigma_{n,p}$, $\sigma_{n,d}$, $\sigma_{n,\alpha}$, $\sigma_{n,n\alpha}$, $\sigma_{n,3He}$, $\sigma_{n,2n}$, $\sigma_{n,np}$, $\sigma_{n,p\alpha}$ and $\sigma_{n,\gamma}$) and their covariances in the fast neutron energy range 0.812 – 20 MeV. In addition to this, cross sections and covariances for σ_{el} , σ_{non} and σ_{inel} were obtained by expressing these cross sections as linear functions of the basic cross sections (see Equations 4 - 8). In Table 13 the final results of this evaluation, i.e., the cross sections and their uncertainties, are listed. There is, however, some difference in the meaning of the listed cross section values between σ_{tot} and σ_{el} on the one hand and all the other cross sections on the other hand. Due to the special evaluation procedure used for σ_{tot} (see Section 4) the evaluated cross sections are group cross sections averaged over the bins of our 33 group bin structure. As σ_{el} was derived essentially as difference between σ_{tot} and all other cross sections, the listed σ_{el} values are group - averaged cross sections, too. All other cross sections, however, are point cross sections, as their priors are the point cross sections from EFF - 2. Also the added data are approximately point cross sections. This difference however is only important in the energy range below 4 MeV. For higher energies both σ_{tot} and σ_{el} are smooth functions of energy and the listed values can also be considered as point cross sections at the appropriate energy bin centers. Therefore in Table 13 σ_{tot} and σ_{el} are given as group cross sections in the energy range below 4 MeV, above this energy all cross sections are given as point cross sections. In the energy region below 4 MeV, the known fine structure of the total (and elastic) cross sections will have to be superimposed on our evaluated group cross sections for an accurate description of σ_{tot} in file three of our evaluated data file, while retaining our course group structure in the description of the covariances in file 33.

These results are also presented in Figures 3 - 22 and compared to the EFF-2 and ENDF/B-VI evaluations and to the experimental data base. Two figures are given for each cross section. The first one compares our new result to the prior (EFF 2) and to the experimental data; the second one compares our new evaluation only to ENDF/B-VI. (For those cases where ENDF/B-VI had to be used as prior, as no EFF evaluation exists, of course only one figure is given.) For each evaluation both the evaluated cross sections and "error bands" calculated from the respective covariance reactions are shown.

In these figures the progress, achieved in this evaluation, is immediately obvious. Our main conclusions are rather similar to those obtained in our previous evaluations for ⁵⁶Fe and ⁵²Cr (*Vonach 92, Pronyaev 95*):

- 1. Except for the total cross sections in the fluctuation region below 4 MeV, the results of this evaluation remain within the uncertainty limits of EFF 2 for all reaction types and energies. Thus our new evaluation, which is more accurate, confirms the validity of the estimations, concerning the uncertainties for the EFF 2 cross sections which were derived from the dispersion of recent evaluations (*Tagesen 91*).
- 2. The largest improvement with respect to EFF-2 in the evaluated cross sections was obtained for σ_{tot} and σ_{el} in the energy region below 3 MeV. At these low energies, the theoretical description of the cross section, by means of the optical model, becomes rather poor, so that rather large uncertainties are to be assigned to any calculated cross sections (*Tagesen 91*) and experimental data are more accurate.
- 3. Our new evaluation is also in excellent agreement with ENDF/B–VI for all important cross sections except for $\sigma_{n,\alpha}$ where our evaluated cross sections are considerably smaller than the ENDF/B–VI values in the energy range 6 12 MeV. This discrepancy is due to the fact that the only data set existing at the time of the ENDF/B–VI evaluation was in error as found out by several later experiments and is thus clarified. For many important cross sections the agreement between our new evaluations and the ENDF/B–VI is even considerably better than to be expected according to the rather large uncertainties assigned to ENDF/B–VI and it appears that on average the uncertainties in ENDF/B–VI have been estimated too cautiously as already observed in (*Vonach 92*) and (*Pronyaev 95*) for ⁵⁶Fe and ⁵²Cr.
- 4. The most important improvement of our new evaluation compared to both EFF-2 and ENDF/B–VI is certainly the considerable reduction of the cross section uncertainties in all energy ranges where accurate measurements exist. For the most important cross section σ_{tot} the uncertainties could be reduced by more than a factor of five compared to both EFF-2 and ENDF/B–VI over the whole energy range. A similar improvement compared to EFF-2 could be obtained for σ_{el} and $\sigma_{n,\alpha}$. Considerable improvements could also be obtained for most cross sections important for neutron transport (σ_{inel} , σ_{non} , $\sigma_{n,n1}$, $\sigma_{n,n}$ cont, $\sigma_{n,2n}$ and $\sigma_{n,p}$). Due to the large number of cross section measurements around $E_n = 14$ MeV our new evaluation gives especially low uncertainties in this energy region, which is especially important for fusion neutronics.

Reduction of uncertainties could not only be obtained for those cross sections where accurate data were available, but also for a number of cross sections, where no direct measurements exist as $\sigma_{n,n\alpha}$, $\sigma_{n,np}$ and $\sigma_{n,n}$ cont through the use of redundant cross sections as described in Section 5.2 (for example accurate $\sigma_{n,np}$ values could be derived from $\sigma_{n,p}$ and $\sigma_{n,p-prod}$ cross sections). Only for some reactions with very small cross sections and no data at all, e.g. $\sigma_{n,\gamma}$, $\sigma_{n,3He}$, $\sigma_{n,p\alpha}$, $\sigma_{n,n2}$ and $\sigma_{n,n3}$ at high energies it was not possible to obtain any improvement by our new evaluation. Most of these cross sections - with exception of $\sigma_{n,\gamma}$ in the lower energy range - will however not be very important for applications and the present high cross sections in the lower MeV range, however, are of some importance for neutron transport calculations and are probably the point where new measurements are most urgently needed.

One question may be the rather small uncertainties, resulting from our evaluation because of possible correlations between our prior data and the added data sets. However, this objection is not valid, because the statistical weight of the priors becomes negligible, if the added data are much more accurate than the prior data, and this is exactly the situation which exists in those parts of our evaluation, where the uncertainties are very low.

Of course, as is the case with any evaluation of experimental data, the uncertainties of our results could be too small because of unrealistically low uncertainty estimates, given for the data or because of neglecting correlations between different data sets. As it has been discussed in the previous chapters, we accounted for such effects by increasing the uncertainty components, estimated by the authors in all cases, which seemed to be doubtful. The correlations between different data sets were checked and generally seemed to be small. Finally our uncertainty estimates are confirmed by the fact that in all evaluations of individual cross sections and in the final joint evaluation χ^2 values of about unity were obtained. According to our judgement, which is also based on our previous experience with evaluations of experimental data (*Pavlik 88, Wagner 90, Pavlik 91, Vonach 92*), the final uncertainties of the present evaluation are realistic effective standard deviations at the 1σ confidence level.

All correlation matrices for the uncertainties of the different reactions are positive definite. There are strong positive correlations between cross sections for neighboring energies, which decrease strongly with the energy difference between the considered points (see Fig. 23 - 38).

For most applications concerning neutron transport and activation in fusion devices, the accuracy of the present evaluation will probably be sufficient. The weakest point is to our judgement the capture cross sections in the lower MeV range where data are almost completely missing and thus very large uncertainties have to be assigned to the calculated cross sections. A new accurate measurement of $\sigma_{n,\gamma}$ in the MeV range therefore seems to us the most urgent neutron data requirement for ⁵⁸Ni.

<u>Disclaimer</u>: This work has been carried out within Association EURATOM-ÖAW. The content of the publication is the sole responsibility of the authors and does not necessarily represent the views of the European Commission or its services.

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Reaction	Cross Section	Covariance Matrix
σ_{tot}	EFF-2	uninformative
$\sigma_{n,n1}$	EFF-2	new estimate
$\sigma_{n,n2}$	EFF-2	new estimate
$\sigma_{n,n3}$	EFF-2	new estimate
$\sigma_{n,n4-8}$	EFF-2	new estimate
$\sigma_{n,ncont}$	ENDF/B-VI	new estimate
$\sigma_{n,2n}$	Wagner 90	Wagner 90
$\sigma_{n,\gamma}$	EFF-2	EFF-2
$\sigma_{n,p}$	Badikov 96	Badikov 96
$\sigma_{n,d}$	ENDF/B-VI	ENDF/B-VI
$\sigma_{n,t}$	JENDL/3	new estimate
$\sigma_{n,3He}$	EFF-2	new estimate
$\sigma_{n,\alpha}$	EFF-2	EFF-2
$\sigma_{n,np}$	EFF-2	EFF-2
$\sigma_{n,n\alpha}$	ENDF/B-VI	ENDF/B-VI
$\sigma_{n,p\alpha}$	EFF-2	new estimate

Table 1:Choice of Priors for the ⁵⁸Ni evaluation

Table 2	2: Expe	rimental	database	for the	total	cross	sections
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Part one: Total cross section measurements for ⁵⁸Ni EXFOR No. of No. of aver-Energy range Reference SER [%] MER [%] LER [%] ENTRY datapoints aged points [MeV] 2 2 10037 Boschung 71 5.05 - 5.551 2.6 1 12752 Butz 82 13 1 0.9 1 66 1.0 - 4.25 13523 Smith 91 71 19 1 0.9 1 1.05 - 20.040614 Fedorov 80 1 34 12 0.91 - 3.251 5.0 60949 Thibault 67 1 2.7 1 total 1 40813 Dukarevich 67 14.0 1 total 1 1 Larson 98 1 1 11561 20 0.91 - 8.5 0.5 Part two: Total cross section measurements for ^{nat}Ni 10047 1 Foster 71 145 1 0.2 15 4.0 - 14.910225 Green 71 a 53 7 4.0 - 8.551 0.4 1 10225 Green 71 b 72 7 1 1 4.0 - 8.670.6 10342 Perey 73 a 469 20 4.0 - 20.01 0.4 1 10342 Perey 73 b 449 20 1.5 0.1 1.5 4.0 - 20.010416 Schwartz 74 698 1 0.2 1 16 4.0 - 15.1310593 Guenther 76 35/20 3 4.0 - 5.01 1.7 1 10823 Smith 81 5 1 4.0 - 4.231 total 11056 Coon 52 1 1 14.12 1 total Goodman 52 11057 1 14.0 1 1 total 11108 Peterson 60 2 2 1 1 17.5 - 18.40.2 11155 Bratenahl 58 5 5 7.0 - 14.480.7 1 1 12882 Larson 81 317 20 4.0 - 20.01 0.2 1 20012 Cierjacks 68 1137 20 1.5 0.2 1.5 4.0 - 20.020480 Cabe 73 1 1 54 5 2.5 4.0 - 6.1921122 McCallum 60 13 8 12.37 - 20.01 0.6 1 30037 Mazari 55 7 6 13.0 - 16.21.5 0.9 1.5 30141 Angeli 71 1 1 14.7 1 total 31468 Polycroniades 94 3 2 1 1.4 1 4.04 - 6.7140559 Tutubalin 77 1 1 14.7 1 total 68023 Tsukada 66 1 1 4.7 1.5 total

EXFOR ENTRY	Reference	Corr. appl.	No. of datapoints	Energy range [MeV]	SER [%]	LER [%]
10037	Boschung 71		2	5.05 - 5.58	5	5
12930	Guss 85		4	7.9 – 13.94	5 - 10	5
40531	Korzh 77		3	2.0 - 3.0	5	10
11276	Rodgers 67	Integration of diff. c.s.	1	2.33	10 total	
12997	Pedroni 88	Integration of diff. c.s.	1	16.93	5 total	
12752	Budtz 82		36	2.13 - 3.93	8	5
13523	Smith 91	Integration of diff. c.s.	12	4.5 - 10.0	1 – 13	5
40065	Pasechnik 80	Integration of diff. c.s.	1	2.9	15 total	

Table 3: Experimental database for the inelastic scattering cross sections with excitation of
the first level (MT51)

Table 4: Experimental database for the inelastic scattering cross sections for excitation of58Ni levels (second and higher)

EXFOR ENTRY	Reference	Type of cross section	Method	No. of datapoints	Energy range [MeV]	SER [%]	LER [%]
12752	Budtz 82	(n,n ₂)	n-TOF	13	3.3 - 4.0	13	15
		(n,n ₃)		8	3.55 - 4.0	11	15
13523	Smith 91	(n,n ₂)	n-TOF	4	5.0 - 8.0	15	15
		(n,n ₃)		4	5.0 - 8.0	15	15
		(n,n ₄₋₈)		3	6.0 - 8.0	15	15
10852	Traiforos 79	(n,n ₂)	n-TOF	7	2.6 - 3.4	10	10
		(n,n ₃)		11	2.9 - 4.0	10	10
		(n,n ₄₋₈)		10	3.0 - 4.0	10	10
10037	Boschung 71	(n,n ₂)	n-TOF	2	5.05 - 5.58	10	10

	-	• • • •				
EXFOR ENTRY	Reference	Type of experiment	No. of datapoints	Energy range [MeV]	SER [%]	LER [%]
31446	Tang 95	α -det.	1	5.1	11 total	
31446	Tang 97	α-det.	2	6.0 - 7.0	10 - 20	7
31481	Majeddin 97	activation	1	14.7	7 total	
41239	Ketlerov 96	α-det.	29	3.55 - 6.83	6 – 8	5
	Sanami 98	α-det.	6	4.51 - 6.22	7	7
	Fessler 98 a	activation	5	9.5 - 12.3	4.5 - 5.2	7
	Fessler 98 b	activation	6	13.0 - 19.4	5.0 - 6.4	7

Table 5: Experimental database for the (n, α) cross sections (MT107)

 Table 6:
 Experimental database for the (n,d) cross sections (MT104)

EXFOR ENTRY	Reference	Type of experiment	No. of datapoints	Energy range [MeV]	SER [%] LER [%]
10827	Grimes 79	d-detection	1	14.8	43 total
12999	Graham 87	d-detection	1	11.0	60 total
30407	Glover 61	d-detection	1	14.8	25 total

Table 7:	Experimental	database j	for the	(<i>n</i> , <i>t</i>)	cross	sections	(<i>MT105</i>)
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EXFOR ENTRY	Reference	Type of experiment	No. of datapoints	Energy range [MeV]	SER [%]	LER [%]
22156	Katoh 89	activation	4	14.16 - 14.87	18 - 25	4.7
30473	Sudar 79	activation	1	14.4	50 total	

EXFOR ENTRY	Reference	Type of experiment	No. of datapoints	Energy range [MeV]	SER [%]	LER [%]
10852	Traiforos 79	$\sigma(2^+ \rightarrow \text{g.s.})$	19	1.78 - 3.9	5	9
11218	Day 56	$\sigma(2^+ \rightarrow \text{g.s.})$	1	2.56	10 total	
	Larson 85	$\sigma(2^+ \rightarrow \text{g.s.})$	14	2.25 - 11.5	7	7
	Pavlik 91	Evaluation	1	14.0	7 total	

 Table 8:
 Experimental database for the total inelastic cross sections (MT 4)

 Table 9:
 Experimental database for the total non-elastic cross sections of ^{nat}Ni (MT 3)

EXFOR ENTRY	Reference	Type of experiment	No. of datapoints	Energy range [MeV]	SER [%]	LER [%]
11217	Tailor 55	sphere transm.	3	4.7 – 12.7	3	3
11216	Beyster 55	sphere transm.	2	4.0 - 4.5	3	3
11220	Beyster 56	sphere transm.	1	7.0	4 total	
	Pavlik 91	sphere transm.	1	14.0	1 total	

	Part 1: Data for 58	³ Ni			
EXFOR ENTRY	Reference	No. of datapoints	Energy range [MeV]	SER [%]	LER [%]
13523	Smith 91	12	4.5 - 10.0	1 – 2	5
12997	Pedroni 88	1	17.0	5 total	
12752	Budtz 82	50	1.425 - 3.925	5	5
	Pavlik 91	1	14.0	3 total	
	Part 2: Data for "	^{nat} Ni			
10113	Kinney 74	5	4.34 - 8.56	5	7
22048	Olson 87	1	21.6	5 total	
12930	Guss 85	4	7.9 – 13.94	5 – 9	5
10037	Boschung 71	2	5.05 - 5.58	4	4
20019	Holmquist 69	5	4.0 - 8.05	5	5

Table 10: Experimental database for the elastic scattering cross sections (MT 2)

Table 11: Experimental database for the ⁵⁷Co-production cross sections (MT 28 + 104)

EXFOR ENTRY	Reference	Type of experiment	No. of datapoints	Energy range [MeV]	SER [%]	LER [%]
21965	Pavlik 85 a	Activation	12	12.76 - 19.57	3 - 6.5	4.5
21965	Pavlik 85 b	Activation	18	13.47 – 14.83	~ 1.5	2.5
22089	Ikeda 88	Activation	10	13.55 - 14.92	3.3	2.6
30604	Raics 81	Activation	5	13.52 - 14.80	4.0	3.0
30979	Viennot 91	Activation	7	13.77 – 14.83	3.0	3.0
31444	Lu Hanlin 94	Activation	4	13.55 – 14.85	2.0	2.2
41240	Filatenkov 97	Activation	15	13.43 - 14.86	2 - 4	2.7

	Part 1: Data for 58	Ni				
EXFOR ENTRY	Reference	Type of Experiment	No. of datapoints	Energy range [MeV]	SER [%]	LER [%]
10933	Kneff 86	He-acc.	1	15.0	7 total	
13598	Haight 96	He-acc.	1	10.0	16 total	
10827	Grimes 79	α-detection	1	15.0	15 total	
12999	Graham 87	α -detection	3	8 - 11	17 - 20	7
	Haight 97	α -detection	32	1.75 – 19.5	2.5 - 10	7
	Tsabaris 97	α-detection	7	5.0 - 15.6	15	7
	Part 2: Data for ^{na}	"Ni				
10827	Grimes 79	α-detection	1	15.0	16 total	
21658	Paulsen 81	α-detection	11	4.9 - 10.0	~ 6	7
21873	Wattecamps 83	α-detection	1	14.0	10 total	
	Baba 94	α-detection	13	4.2 - 14.1	10 - 12	7
13598	Haight 96	He-acc.	1	10.0	13 total	
	Sanami 98	α -detection	8	4.81 - 6.51	7.3 – 10	7

 Table 12: Experimental database for the total ⁴He-production cross sections (MT 22 + 107)

MT =	1		total cross	section		
Neut	ron			cross	std.dev.	std.dev.
(in	MoV)			(in have)	OI SIGMA(E)	(12 %)
(111)	Mev)			(III DarII)	(III DarII)	(111 6)
1.0000)E-11	_	8.1000E-01	0.0000E+00	0.000E+00	0.00
8.1000)E-01	-	1.0000E+00	3.1812E+00	1.238E-01	3.89
1.0000)E+00	-	1.2000E+00	2.9956E+00	7.077E-02	2.36
1.2000)E+00	-	1.4000E+00	3.6350E+00	6.723E-02	1.85
1.4000)E+00	-	1.6000E+00	3.3086E+00	4.641E-02	1.40
1.6000)E+00	-	1.8000E+00	3.2147E+00	4.413E-02	1.37
1.8000)E+00	-	2.0000E+00	2.9129E+00	2.958E-02	1.02
2.0000)E+00	-	2.2000E+00	3.0913E+00	3.063E-02	0.99
2.2000)E+00	-	2.4000E+00	3.2336E+00	2.933E-02	0.91
2.4000)E+00	-	2.6000E+00	3.1906E+00	2.583E-02	0.81
2.6000)E+00	-	2.8000E+00	3.2127E+00	1.897E-02	0.59
2.8000)E+00	-	3.0000E+00	3.3675E+00	1.894E-02	0.56
3.0000)E+00	-	3.5000E+00	3.2831E+00	1.876E-02	0.57
3.5000)E+00	-	4.0000E+00	3.4885E+00	1.410E-02	0.40
4.0000)E+00			3.5007E+00	1.582E-02	0.45
4.2500)E+00			3.5129E+00	1.092E-02	0.31
4.7500)E+00			3.5775E+00	1.080E-02	0.30
5.2500)E+00			3.6719E+00	1.210E-02	0.33
5.7500)E+00			3.6751E+00	1.216E-02	0.33
6.5000)E+00			3.6516E+00	1.214E-02	0.33
7.5000)E+00			3.5528E+00	1.094E-02	0.31
8.5000)E+00			3.4234E+00	1.055E-02	0.31
9.5000)E+00			3.2888E+00	1.067E-02	0.32
1.0500)E+01			3.1756E+00	1.035E-02	0.33
1.1500)E+01			3.0349E+00	1.061E-02	0.35
1.2500)E+01			2.9039E+00	1.115E-02	0.38
1.3250)E+01			2.8162E+00	1.248E-02	0.44
1.3750)E+01			2.7420E+00	1.265E-02	0.46
1.4250)E+01			2.6870E+00	1.156E-02	0.43
1.4750)E+01			2.6229E+00	1.248E-02	0.48
1.5500)E+01			2.5650E+00	1.151E-02	0.45
1.6500)E+01			2.4819E+00	1.172E-02	0.47
1.7500)E+01			2.4310E+00	1.130E-02	0.46
1.8500)E+01			2.3875E+00	1.157E-02	0.48
1.9500)E+01			2.3537E+00	1.827E-02	0.78
2.0000)E+01			2.3728E+00	6.655E-02	2.80

Table 13 Evaluated cross sections for neutron induced reactions on ⁵⁸Ni

MT =	2		elastic	cross s	section			
Neut	ron			(cross	std.dev.	std.dev	· .
ene	ergy			S	ection	of sigma(E)		
(in	MeV)			(i)	n barn)	(in barn)	(in %	;)
1.0000)E-11	-	8.1000E-01	0.0	0000E+00	0.0000E+00	0.0	0
8.1000)E-01	-	1.0000E+00	3.3	1705E+00	1.2376E-01	3.9	0
1.0000)E+00	-	1.2000E+00	2.9	9811E+00	7.0793E-02	2.3	7
1.2000)E+00	-	1.4000E+00	3.0	6153E+00	6.7265E-02	1.8	б
1.4000)E+00	-	1.6000E+00	3.3	1715E+00	4.7218E-02	1.4	8
1.6000)E+00	-	1.8000E+00	2.	7702E+00	5.0848E-02	1.8	3
1.8000)E+00	-	2.0000E+00	2.1	3828E+00	3.9520E-02	1.6	б
2.0000)E+00	-	2.2000E+00	2.4	4574E+00	4.0578E-02	1.6	5
2.2000)E+00	-	2.4000E+00	2.	5568E+00	3.9773E-02	1.5	5
2.4000)E+00	-	2.6000E+00	2.4	4656E+00	3.7932E-02	1.5	4
2.6000)E+00	-	2.8000E+00	2.4	4004E+00	3.0078E-02	1.2	5
2.8000)E+00	-	3.0000E+00	2.4	4522E+00	3.2941E-02	1.3	4
3.0000)E+00	-	3.5000E+00	2.1	1915E+00	3.8216E-02	1.7	4
3.5000)E+00	-	4.0000E+00	2.1	1767E+00	4.2874E-02	1.9	7
4.0000)E+06			2.1	1474E+00	3.7644E-02	1.7	5
4.2500)E+06			2.1	1116E+00	4.8392E-02	2.2	.9
4.7500)E+06			2.0	0355E+00	4.5938E-02	2.2	.6
5.2500)			2.0	0557E+00	3.5163E-02	1.7	Т.
5./500) 111 + 06			2.0	0035E+00	3.3502E-02	1.6	. /
6.5000) 111 + 06			2.0	JUI8E+00	3.6918E-U2	1.8	.4
7.5000				2.0		3.4008E-02	1.0	1
0.5000				1 0	9903E+00	3.3047E-UZ 2 2105〒 02	1.0	9
1 0500				1.0	00000000000000000000000000000000000000	1060 ± 02	1.7	±
1 1500)E+07			1.0	5257E+00	5 5796F-02	2.5	2
1 2500)E+07			1.0	4758F+00	5.3790E-02 5 1932F-02	3.4	2
1 3250)E+07			1	3677E+00	3.9519E - 02	2.8	3
1 3750)E+07			1	3109E+00	3.1168E = 02	2.0	8
1 4250)E+07			1	2857E+00	1 7583E - 02	1 3	7
1.4750)E+07			1.1	2528E+00	1.9280E-02	1.5	4
1.5500)E+07			1.1	2104E+00	3.4863E-02	2.8	8
1.6500)E+07			1.1	1225E+00	3.7988E-02	3.3	8
1.7500)E+07			1.0	0485E+00	4.4490E-02	4.2	4
1.8500)E+07			1.0	0069E+00	4.1477E-02	4.1	.2
1.9500)E+07			9.	5042E-01	4.5366E-02	4.7	7
2.0000)E+07			9.4	4686E-01	5.2757E-02	5.5	7

MT = 3	nonelastic cross section		
Neutron	cross	std.dev.	std.dev.
energy	section	of sigma(E)	
(in MeV)	(in barn)	(in barn)	(in %)
5.0000E+05	1.1174E-03	2.2313E-04	19.97
9.0000E+05	1.0627E-02	1.8222E-03	17.15
1.1000E+06	1.4450E-02	2.0760E-03	14.37
1.3000E+06	1.9654E-02	2.5811E-03	13.13
1.5000E+06	1.3713E-01	1.1158E-02	8.14
1.7000E+06	4.4452E-01	2.6541E-02	5.97
1.9000E+06	5.3010E-01	2.6776E-02	5.05
2.1000E+06	6.3391E-01	2.6184E-02	4.13
2.3000E+06	6.7677E-01	2.7082E-02	4.00
2.5000E+06	7.2502E-01	2.8358E-02	3.91
2.7000E+06	8.1234E-01	2.3574E-02	2.90
2.9000E+06	9.1535E-01	2.7505E-02	3.00
3.2500E+06	1.0916E+00	3.2031E-02	2.93
3.7500E+06	1.3118E+00	3.8836E-02	2.96
4.0000E+06	1.3533E+00	3.5660E-02	2.63
4.2500E+06	1.4013E+00	4.7722E-02	3.41
4.7500E+06	1.5420E+00	4.5230E-02	2.93
5.2500E+06	1.6162E+00	3.4570E-02	2.14
5.7500E+06	1.6716E+00	3.3137E-02	1.98
6.5000E+06	1.6498E+00	3.6575E-02	2.22
7.5000E+06	1.5107E+00	3.3452E-02	2.21
8.5000E+06	1.4251E+00	3.3431E-02	2.35
9.5000E+06	1.3910E+00	3.2795E-02	2.36
1.0500E+07	1.3519E+00	4.1401E-02	3.06
1.1500E+07	1.4082E+00	5.5131E-02	3.91
1.2500E+07	1.4281E+00	5.1238E-02	3.59
1.3250E+07	1.4485E+00	3.7817E-02	2.61
1.3750E+07	1.4311E+00	2.9010E-02	2.03
1.4250E+07	1.4013E+00	1.4514E-02	1.04
1.4750E+07	1.3701E+00	1.5186E-02	1.11
1.5500E+07	1.3546E+00	3.3145E-02	2.45
1.6500E+07	1.3594E+00	3.6848E-02	2.71
1.7500E+07	1.3825E+00	4.3585E-02	3.15
1.8500E+07	1.3806E+00	4.0306E-02	2.92
1.9500E+07	1.4033E+00	4.2605E-02	3.04
2.0000E+07	1.4041E+00	5.3564E-02	3.81
MT = 4	inelastic cross section		
------------	-------------------------	-------------	----------
Neutron	cross	std.dev.	std.dev.
energy	section	of sigma(E)	
(in MeV)	(in barn)	(in barn)	(in %)
1.5000E+06	1.1205E-01	1.0800E-02	9.64
1.7000E+06	4.1290E-01	2.6358E-02	6.38
1.9000E+06	4.8535E-01	2.6544E-02	5.47
2.1000E+06	5.7044E-01	2.5730E-02	4.51
2.3000E+06	5.8904E-01	2.6567E-02	4.51
2.5000E+06	6.0763E-01	2.7403E-02	4.51
2.7000E+06	6.6334E-01	2.2252E-02	3.35
2.9000E+06	7.3205E-01	2.5734E-02	3.52
3.2500E+06	8.5143E-01	2.9400E-02	3.45
3.7500E+06	9.8573E-01	3.4284E-02	3.48
4.0000E+06	9.8832E-01	3.5558E-02	3.60
4.2500E+06	9.9658E-01	4.8037E-02	4.82
4.7500E+06	1.0722E+00	4.6120E-02	4.30
5.2500E+06	1.0558E+00	3.5960E-02	3.41
5.7500E+06	1.0457E+00	3.4763E-02	3.32
6.5000E+06	9.5248E-01	3.7408E-02	3.93
7.5000E+06	7.9633E-01	3.5333E-02	4.44
8.5000E+06	7.2557E-01	3.5608E-02	4.91
9.5000E+06	6.9311E-01	3.4732E-02	5.01
1.0500E+07	6.3304E-01	4.1817E-02	6.61
1.1500E+07	5.8777E-01	4.4673E-02	7.60
1.2500E+07	4.5400E-01	3.5949E-02	7.92
1.3250E+07	3.7592E-01	2.9362E-02	7.81
1.3750E+07	3.4016E-01	2.6034E-02	7.65
1.4250E+07	3.0915E-01	9.8524E-03	3.19
1.4750E+07	2.8211E-01	1.0484E-02	3.72
1.5500E+07	2.4765E-01	1.5395E-02	6.22
1.6500E+07	2.1852E-01	1.8303E-02	8.38
1.7500E+07	1.9521E-01	2.1765E-02	11.15
1.8500E+07	1.8000E-01	2.1104E-02	11.72
1.9500E+07	1.6530E-01	2.0065E-02	12.14
2.0000E+07	1.5856E-01	2.5492E-02	16.08

MT = 16	(n,2n) cross section		
Neutron	cross	std.dev.	std.dev.
(in MeV)	(in barn)	(in barn)	(in %)
1.2410E+01	0.0000E+00	0.000E+00	0.00
1.3000E+01	4.5420E-03	8.001E-04	17.62
1.3300E+01	9.4701E-03	6.281E-04	6.63
1.3600E+01	1.4399E-02	5.113E-04	3.55
1.3800E+01	1.8737E-02	4.175E-04	2.23
1.4000E+01	2.3121E-02	4.127E-04	1.78
1.4200E+01	2.6762E-02	4.179E-04	1.56
1.4400E+01	3.1782E-02	5.566E-04	1.75
1.4600E+01	3.5539E-02	7.091E-04	2.00
1.4800E+01	3.9009E-02	5.317E-04	1.36
1.5000E+01	4.2235E-02	2.555E-03	6.05
1.5500E+01	5.0738E-02	3.069E-03	6.05
1.6000E+01	5.7574E-02	2.147E-03	3.73
1.6500E+01	6.3100E-02	3.220E-03	5.10
1.7000E+01	6.6415E-02	2.586E-03	3.89
1.7500E+01	6.9124E-02	2.141E-03	3.10
1.8000E+01	7.2658E-02	3.136E-03	4.32
1.8500E+01	7.6685E-02	3.310E-03	4.32
1.9000E+01	7.9219E-02	3.314E-03	4.18
1.9500E+01	8.1746E-02	3.420E-03	4.18
2.0000E+01	8.4293E-02	3.525E-03	4.18

n,na) cross section		
cross section	std.dev. of sigma(E)	std.dev.
(in barn)	(in barn)	(in %)
0.0000E+00	0.000E+00	0.00
8.5484E-08	8.548E-08	100.00
2.2760E-05	6.738E-06	29.60
2.5965E-04	6.683E-05	25.74
1.0899E-03	2.622E-04	24.06
5.5952E-03	1.541E-03	27.54
2.1867E-02	3.769E-03	17.24
4.3756E-02	6.928E-03	15.83
7.5785E-02	6.122E-03	8.08
	cross section (in barn) 0.0000E+00 8.5484E-08 2.2760E-05 2.5965E-04 1.0899E-03 5.5952E-03 2.1867E-02 4.3756E-02 7.5785E-02	n,na) cross section cross std.dev. section of sigma(E) (in barn) (in barn) 0.0000E+00 0.000E+00 8.5484E-08 8.548E-08 2.2760E-05 6.738E-06 2.5965E-04 6.683E-05 1.0899E-03 2.622E-04 5.5952E-03 1.541E-03 2.1867E-02 3.769E-03 4.3756E-02 6.928E-03 7.5785E-02 6.122E-03

MT = 28	(n,np) cross section		
Neutron	cross	std.dev.	std.dev.
energy	section	of sigma(E)	
(in MeV)	(in barn)	(in barn)	(in %)
8.3134E+00	0.0000E+00	0.000E+00	0.00
9.2361E+00	0.0000E+00	0.000E+00	0.00
9.2361E+00	2.1246E-06	5.077E-07	23.89
9.5000E+00	7.8931E-05	1.860E-05	23.56
9.8939E+00	2.3758E-03	5.431E-04	22.86
1.0500E+01	2.6534E-02	5.674E-03	21.38
1.1000E+01	7.0586E-02	1.356E-02	19.22
1.1233E+01	1.0116E-01	1.821E-02	18.00
1.1500E+01	1.4082E-01	2.224E-02	15.79
1.2000E+01	2.2814E-01	2.824E-02	12.38
1.2534E+01	3.3634E-01	2.608E-02	7.75
1.3000E+01	4.2395E-01	2.324E-02	5.48
1.3500E+01	4.9929E-01	7.978E-03	1.60
1.4000E+01	5.6422E-01	8.240E-03	1.46
1.4500E+01	6.1954E-01	8.783E-03	1.42
1.5000E+01	6.6283E-01	1.060E-02	1.60
1.5500E+01	6.9451E-01	2.798E-02	4.03
1.6000E+01	7.2840E-01	3.285E-02	4.51
1.6152E+01	7.3272E-01	2.945E-02	4.02
1.6500E+01	7.4710E-01	3.125E-02	4.18
1.7000E+01	7.6819E-01	2.777E-02	3.61
1.7500E+01	7.7422E-01	3.591E-02	4.64
1.8000E+01	7.7989E-01	3.075E-02	3.94
1.8500E+01	7.8380E-01	2.900E-02	3.70
1.9000E+01	7.9708E-01	2.954E-02	3.71
1.9500E+01	7.9674E-01	2.723E-02	3.42
2.0000E+01	7.8754E-01	4.355E-02	5.53

MT =	51
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energysectionof sigma(E)(in MeV)(in barn)(in barn)(in1.4753E+000.000E+000.000E+000.1.4763E+007.2075E-026.949E-039.1.6717E+004.0166E-012.565E-026.1.8084E+004.5594E-012.494E-025.1.9029E+004.8628E-012.733E-025.1.9728E+005.1524E-012.418E-024.2.0864E+005.6918E-012.566E-024.2.5031E+006.5962E-012.591E-023.2.9505E+005.9817E-012.444E-024.2.9915E+005.4922E-012.432E-024.3.0912E+004.2170E-012.287E-025.3.4799E+003.8221E-012.133E-025.3.6844E+003.2727E-011.892E-025.3.9612E+002.7484E-011.779E-026.4.1789E+002.3845E-011.997E-025.3.9612E+002.7484E-011.779E-026.4.1789E+002.3845E-011.927E-025.4.6175E+002.328E-011.928E-025.5.5000E+001.8962E-016.959E-033.6.0000E+001.4586E-017.143E-034.6.5000E+001.0184E-015.525E-035.7.900E+009.3769E-025.432E-035.7.900E+008.1118E-024.577E-035.	_v.
$\begin{array}{llllllllllllllllllllllllllllllllllll$	
1.4753E+00 $0.000E+00$ $0.000E+00$ $0.$ $1.4763E+00$ $7.2075E-02$ $6.949E-03$ $9.$ $1.6717E+00$ $4.0166E-01$ $2.565E-02$ $6.$ $1.8084E+00$ $4.5594E-01$ $2.494E-02$ $5.$ $1.9029E+00$ $4.8628E-01$ $2.733E-02$ $5.$ $1.9728E+00$ $5.1524E-01$ $2.418E-02$ $4.$ $2.0864E+00$ $5.6918E-01$ $2.566E-02$ $4.$ $2.5031E+00$ $6.0792E-01$ $2.081E-02$ $3.$ $2.8287E+00$ $6.5962E-01$ $2.591E-02$ $3.$ $2.9505E+00$ $5.9817E-01$ $2.442E-02$ $4.$ $3.0912E+00$ $4.2170E-01$ $2.432E-02$ $4.$ $3.0912E+00$ $3.8221E-01$ $2.133E-02$ $5.$ $3.4799E+00$ $3.2727E-01$ $1.892E-02$ $5.$ $3.4799E+00$ $3.2727E-01$ $1.892E-02$ $5.$ $3.6834E+00$ $2.9770E-01$ $1.750E-02$ $5.$ $3.9612E+00$ $2.7484E-01$ $1.779E-02$ $6.$ $4.1789E+00$ $2.3845E-01$ $1.237E-02$ $5.$ $4.6175E+00$ $2.2328E-01$ $1.92E-02$ $5.$ $4.8841E+00$ $1.8962E-01$ $6.959E-03$ $3.$ $5.5000E+00$ $1.5901E-01$ $6.016E-03$ $3.$ $6.0000E+00$ $1.4586E-01$ $7.143E-03$ $4.$ $7.0000E+00$ $1.0184E-01$ $5.525E-03$ $5.$ $7.9836E+00$ $8.1118E-02$ $4.577E-03$ $5.$	응)
1.4763E+00 $7.2075E-02$ $6.949E-03$ $9.$ $1.6717E+00$ $4.0166E-01$ $2.565E-02$ $6.$ $1.8084B+00$ $4.5594E-01$ $2.494E-02$ $5.$ $1.9029E+00$ $4.8628E-01$ $2.733E-02$ $5.$ $1.9728E+00$ $5.1524E-01$ $2.418E-02$ $4.$ $2.0864E+00$ $5.6918E-01$ $2.566E-02$ $4.$ $2.5031E+00$ $6.0792E-01$ $2.081E-02$ $3.$ $2.8287E+00$ $6.5962E-01$ $2.591E-02$ $3.$ $2.9505E+00$ $5.9817E-01$ $2.444E-02$ $4.$ $2.9915E+00$ $5.4922E-01$ $2.432E-02$ $4.$ $3.0912E+00$ $4.2170E-01$ $2.287E-02$ $5.$ $3.3201E+00$ $3.8221E-01$ $2.133E-02$ $5.$ $3.4799E+00$ $3.5695E-01$ $1.997E-02$ $5.$ $3.6834E+00$ $3.2727E-01$ $1.892E-02$ $5.$ $3.8401E+00$ $2.9770E-01$ $1.750E-02$ $5.$ $3.8401E+00$ $2.3845E-01$ $1.237E-02$ $5.$ $4.6175E+00$ $2.2328E-01$ $1.92E-02$ $5.$ $4.6175E+00$ $1.5901E-01$ $6.959E-03$ $3.$ $5.5000E+00$ $1.5901E-01$ $6.959E-03$ $3.$ $6.0000E+00$ $1.4586E-01$ $7.143E-03$ $4.$ $7.0000E+00$ $1.9769E-02$ $5.432E-03$ $5.$ $7.9836E+00$ $8.1118E-02$ $4.577E-03$ $5.$.00
1.6717E+00 $4.0166E-01$ $2.565E-02$ $6.$ $1.8084E+00$ $4.5594E-01$ $2.494E-02$ $5.$ $1.9029E+00$ $4.8628E-01$ $2.733E-02$ $5.$ $1.9728E+00$ $5.1524E-01$ $2.418E-02$ $4.$ $2.0864E+00$ $5.6918E-01$ $2.566E-02$ $4.$ $2.5031E+00$ $6.0792E-01$ $2.081E-02$ $3.$ $2.8287E+00$ $6.5962E-01$ $2.591E-02$ $3.$ $2.9505E+00$ $5.9817E-01$ $2.444E-02$ $4.$ $2.9915E+00$ $5.4922E-01$ $2.432E-02$ $4.$ $3.0912E+00$ $4.2170E-01$ $2.287E-02$ $5.$ $3.4799E+00$ $3.8221E-01$ $1.392E-02$ $5.$ $3.6834E+00$ $3.2727E-01$ $1.892E-02$ $5.$ $3.8401E+00$ $2.9770E-01$ $1.750E-02$ $5.$ $3.8401E+00$ $2.3845E-01$ $1.237E-02$ $5.$ $4.6175E+00$ $2.3845E-01$ $1.237E-02$ $5.$ $4.6175E+00$ $1.8962E-01$ $6.959E-03$ $3.$ $5.5000E+00$ $1.5901E-01$ $6.016E-03$ $3.$ $6.0000E+00$ $1.4586E-01$ $7.443E-03$ $4.$ $7.0000E+00$ $1.0184E-01$ $5.525E-03$ $5.$ $7.9836E+00$ $8.1118E-02$ $4.577E-03$ $5.$.64
1.8084E+00 $4.5594E-01$ $2.494E-02$ $5.$ $1.9029E+00$ $4.8628E-01$ $2.733E-02$ $5.$ $1.9728E+00$ $5.1524E-01$ $2.418E-02$ $4.$ $2.0864E+00$ $5.6918E-01$ $2.566E-02$ $4.$ $2.5031E+00$ $6.0792E-01$ $2.081E-02$ $3.$ $2.8287E+00$ $6.5962E-01$ $2.591E-02$ $3.$ $2.9505E+00$ $5.9817E-01$ $2.444E-02$ $4.$ $2.9915E+00$ $5.9817E-01$ $2.432E-02$ $4.$ $3.0912E+00$ $4.9850E-01$ $2.499E-02$ $5.$ $3.3201E+00$ $4.2170E-01$ $2.287E-02$ $5.$ $3.4799E+00$ $3.8221E-01$ $2.133E-02$ $5.$ $3.6834E+00$ $3.2727E-01$ $1.892E-02$ $5.$ $3.8401E+00$ $2.9770E-01$ $1.750E-02$ $5.$ $3.9612E+00$ $2.3845E-01$ $1.997E-02$ $5.$ $4.6175E+00$ $2.2328E-01$ $1.927E-02$ $5.$ $4.6175E+00$ $1.5901E-01$ $6.959E-03$ $3.$ $5.5000E+00$ $1.5901E-01$ $6.016E-03$ $3.$ $6.0000E+00$ $1.726E-01$ $5.432E-03$ $4.$ $6.5000E+00$ $1.0184E-01$ $5.525E-03$ $5.$ $7.9836E+00$ $8.1118E-02$ $4.577E-03$ $5.$.38
1.9029E+00 $4.8628E-01$ $2.733E-02$ $5.$ $1.9728E+00$ $5.1524E-01$ $2.418E-02$ $4.$ $2.0864E+00$ $5.6918E-01$ $2.566E-02$ $4.$ $2.5031E+00$ $6.0792E-01$ $2.081E-02$ $3.$ $2.8287E+00$ $6.5962E-01$ $2.591E-02$ $3.$ $2.9505E+00$ $5.9817E-01$ $2.444E-02$ $4.$ $2.9915E+00$ $5.4922E-01$ $2.432E-02$ $4.$ $3.0912E+00$ $4.2170E-01$ $2.287E-02$ $5.$ $3.4799E+00$ $3.8221E-01$ $2.133E-02$ $5.$ $3.5854E+00$ $3.5695E-01$ $1.997E-02$ $5.$ $3.6834E+00$ $3.2727E-01$ $1.892E-02$ $5.$ $3.9612E+00$ $2.7484E-01$ $1.779E-02$ $6.$ $4.1789E+00$ $2.3845E-01$ $1.916E-02$ $7.$ $4.3743E+00$ $2.2328E-01$ $1.92E-02$ $5.$ $4.6175E+00$ $2.3845E-01$ $1.92E-02$ $5.$ $4.6175E+00$ $1.5901E-01$ $6.959E-03$ $3.$ $5.5000E+00$ $1.5901E-01$ $6.016E-03$ $3.$ $6.0000E+00$ $1.686E-01$ $7.143E-03$ $4.$ $7.0000E+00$ $1.0184E-01$ $5.525E-03$ $5.$ $7.9836E+00$ $8.1118E-02$ $4.577E-03$ $5.$.47
1.9728E+00 $5.1524E-01$ $2.418E-02$ $4.$ $2.0864E+00$ $5.6918E-01$ $2.566E-02$ $4.$ $2.5031E+00$ $6.0792E-01$ $2.081E-02$ $3.$ $2.8287E+00$ $6.5962E-01$ $2.591E-02$ $3.$ $2.9505E+00$ $5.9817E-01$ $2.444E-02$ $4.$ $2.9915E+00$ $5.4922E-01$ $2.432E-02$ $4.$ $3.0912E+00$ $4.2870E-01$ $2.499E-02$ $5.$ $3.3201E+00$ $4.2170E-01$ $2.287E-02$ $5.$ $3.4799E+00$ $3.8221E-01$ $2.133E-02$ $5.$ $3.6834E+00$ $3.2727E-01$ $1.892E-02$ $5.$ $3.6834E+00$ $2.9770E-01$ $1.750E-02$ $5.$ $3.9612E+00$ $2.4901E-01$ $1.916E-02$ $7.$ $4.1789E+00$ $2.3845E-01$ $1.237E-02$ $5.$ $4.6175E+00$ $2.2328E-01$ $1.92E-02$ $5.$ $4.6175E+00$ $1.5901E-01$ $6.016E-03$ $3.$ $5.5000E+00$ $1.5901E-01$ $6.016E-03$ $3.$ $6.0000E+00$ $1.726E-01$ $5.403E-03$ $4.$ $7.0000E+00$ $1.0184E-01$ $5.525E-03$ $5.$ $7.5000E+00$ $9.3769E-02$ $5.432E-03$ $5.$ $7.9836E+00$ $8.1118E-02$ $4.577E-03$ $5.$.62
$\begin{array}{cccccccccccccccccccccccccccccccccccc$.69
2.5031E+00 $6.0792E-01$ $2.081E-02$ $3.$ $2.8287E+00$ $6.5962E-01$ $2.591E-02$ $3.$ $2.9505E+00$ $5.9817E-01$ $2.444E-02$ $4.$ $2.9915E+00$ $5.4922E-01$ $2.432E-02$ $4.$ $3.0912E+00$ $4.9850E-01$ $2.499E-02$ $5.$ $3.201E+00$ $4.2170E-01$ $2.287E-02$ $5.$ $3.4799E+00$ $3.8221E-01$ $2.133E-02$ $5.$ $3.5854E+00$ $3.5695E-01$ $1.997E-02$ $5.$ $3.6834E+00$ $3.2727E-01$ $1.892E-02$ $5.$ $3.8401E+00$ $2.9770E-01$ $1.750E-02$ $5.$ $3.9612E+00$ $2.4901E-01$ $1.916E-02$ $7.$ $4.1789E+00$ $2.3845E-01$ $1.237E-02$ $5.$ $4.6175E+00$ $2.2328E-01$ $1.192E-02$ $5.$ $4.6175E+00$ $1.5901E-01$ $6.016E-03$ $3.$ $6.0000E+00$ $1.4586E-01$ $7.143E-03$ $4.$ $6.5000E+00$ $1.0184E-01$ $5.525E-03$ $5.$ $7.5000E+00$ $9.3769E-02$ $5.432E-03$ $5.$ $7.9836E+00$ $8.1118E-02$ $4.577E-03$ $5.$.51
2.8287E+00 $6.5962E-01$ $2.591E-02$ $3.$ $2.9505E+00$ $5.9817E-01$ $2.444E-02$ $4.$ $2.9915E+00$ $5.4922E-01$ $2.432E-02$ $4.$ $3.0912E+00$ $4.9850E-01$ $2.499E-02$ $5.$ $3.201E+00$ $4.2170E-01$ $2.287E-02$ $5.$ $3.4799E+00$ $3.8221E-01$ $2.133E-02$ $5.$ $3.5854E+00$ $3.5695E-01$ $1.997E-02$ $5.$ $3.6834E+00$ $3.2727E-01$ $1.892E-02$ $5.$ $3.8401E+00$ $2.9770E-01$ $1.750E-02$ $5.$ $3.9612E+00$ $2.7484E-01$ $1.779E-02$ $6.$ $4.1789E+00$ $2.3845E-01$ $1.237E-02$ $5.$ $4.6175E+00$ $2.2328E-01$ $1.192E-02$ $5.$ $4.8841E+00$ $1.5901E-01$ $6.016E-03$ $3.$ $5.5000E+00$ $1.4586E-01$ $7.143E-03$ $4.$ $6.5000E+00$ $1.0184E-01$ $5.525E-03$ $5.$ $7.5000E+00$ $9.3769E-02$ $5.432E-03$ $5.$ $7.9836E+00$ $8.1118E-02$ $4.577E-03$ $5.$.42
2.9505E+00 $5.9817E-01$ $2.444E-02$ $4.$ $2.9915E+00$ $5.4922E-01$ $2.432E-02$ $4.$ $3.0912E+00$ $4.9850E-01$ $2.499E-02$ $5.$ $3.3201E+00$ $4.2170E-01$ $2.287E-02$ $5.$ $3.4799E+00$ $3.8221E-01$ $2.133E-02$ $5.$ $3.5854E+00$ $3.5695E-01$ $1.997E-02$ $5.$ $3.6834E+00$ $3.2727E-01$ $1.892E-02$ $5.$ $3.8401E+00$ $2.9770E-01$ $1.750E-02$ $5.$ $3.9612E+00$ $2.7484E-01$ $1.779E-02$ $6.$ $4.1789E+00$ $2.3845E-01$ $1.237E-02$ $5.$ $4.6175E+00$ $2.2328E-01$ $1.92E-02$ $5.$ $4.8841E+00$ $1.8962E-01$ $6.959E-03$ $3.$ $5.5000E+00$ $1.4586E-01$ $7.143E-03$ $4.$ $6.5000E+00$ $1.0184E-01$ $5.525E-03$ $5.$ $7.5000E+00$ $9.3769E-02$ $5.432E-03$ $5.$ $7.9836E+00$ $8.1118E-02$ $4.577E-03$ $5.$.93
$\begin{array}{cccccccccccccccccccccccccccccccccccc$.09
$\begin{array}{cccccccccccccccccccccccccccccccccccc$.43
3.3201E+00 $4.2170E-01$ $2.287E-02$ $5.$ $3.4799E+00$ $3.8221E-01$ $2.133E-02$ $5.$ $3.5854E+00$ $3.5695E-01$ $1.997E-02$ $5.$ $3.6834E+00$ $3.2727E-01$ $1.892E-02$ $5.$ $3.8401E+00$ $2.9770E-01$ $1.750E-02$ $5.$ $3.9612E+00$ $2.7484E-01$ $1.779E-02$ $6.$ $4.1789E+00$ $2.4901E-01$ $1.916E-02$ $7.$ $4.3743E+00$ $2.3845E-01$ $1.237E-02$ $5.$ $4.6175E+00$ $2.2328E-01$ $1.192E-02$ $5.$ $4.8841E+00$ $1.8962E-01$ $6.959E-03$ $3.$ $5.5000E+00$ $1.4586E-01$ $7.143E-03$ $4.$ $6.5000E+00$ $1.0184E-01$ $5.525E-03$ $5.$ $7.5000E+00$ $9.3769E-02$ $5.432E-03$ $5.$ $7.9836E+00$ $8.1118E-02$ $4.577E-03$ $5.$.01
$\begin{array}{cccccccccccccccccccccccccccccccccccc$.42
3.5854E+00 $3.5695E-01$ $1.997E-02$ $5.$ $3.6834E+00$ $3.2727E-01$ $1.892E-02$ $5.$ $3.8401E+00$ $2.9770E-01$ $1.750E-02$ $5.$ $3.9612E+00$ $2.7484E-01$ $1.779E-02$ $6.$ $4.1789E+00$ $2.4901E-01$ $1.916E-02$ $7.$ $4.3743E+00$ $2.3845E-01$ $1.237E-02$ $5.$ $4.6175E+00$ $2.2328E-01$ $1.192E-02$ $5.$ $4.8841E+00$ $1.8962E-01$ $6.959E-03$ $3.$ $5.5000E+00$ $1.5901E-01$ $6.016E-03$ $3.$ $6.0000E+00$ $1.4586E-01$ $7.143E-03$ $4.$ $7.0000E+00$ $1.0184E-01$ $5.525E-03$ $5.$ $7.5000E+00$ $9.3769E-02$ $5.432E-03$ $5.$ $7.9836E+00$ $8.1118E-02$ $4.577E-03$ $5.$.58
$\begin{array}{cccccccccccccccccccccccccccccccccccc$.59
3.8401E+00 $2.9770E-01$ $1.750E-02$ $5.$ $3.9612E+00$ $2.7484E-01$ $1.779E-02$ $6.$ $4.1789E+00$ $2.4901E-01$ $1.916E-02$ $7.$ $4.3743E+00$ $2.3845E-01$ $1.237E-02$ $5.$ $4.6175E+00$ $2.2328E-01$ $1.192E-02$ $5.$ $4.8841E+00$ $1.8962E-01$ $6.959E-03$ $3.$ $5.5000E+00$ $1.5901E-01$ $6.016E-03$ $3.$ $6.0000E+00$ $1.4586E-01$ $7.143E-03$ $4.$ $7.0000E+00$ $1.0184E-01$ $5.525E-03$ $5.$ $7.5000E+00$ $9.3769E-02$ $5.432E-03$ $5.$ $7.9836E+00$ $8.1118E-02$ $4.577E-03$ $5.$.78
3.9612E+002.7484E-011.779E-026.4.1789E+002.4901E-011.916E-027.4.3743E+002.3845E-011.237E-025.4.6175E+002.2328E-011.192E-025.4.8841E+001.8962E-016.959E-033.5.5000E+001.5901E-016.016E-033.6.0000E+001.4586E-017.143E-034.6.5000E+001.0184E-015.525E-035.7.5000E+009.3769E-025.432E-035.7.9836E+008.1118E-024.577E-035.	.88
4.1789E+00 $2.4901E-01$ $1.916E-02$ $7.$ $4.3743E+00$ $2.3845E-01$ $1.237E-02$ $5.$ $4.6175E+00$ $2.2328E-01$ $1.192E-02$ $5.$ $4.8841E+00$ $1.8962E-01$ $6.959E-03$ $3.$ $5.5000E+00$ $1.5901E-01$ $6.016E-03$ $3.$ $6.0000E+00$ $1.4586E-01$ $7.143E-03$ $4.$ $6.5000E+00$ $1.0184E-01$ $5.525E-03$ $5.$ $7.5000E+00$ $9.3769E-02$ $5.432E-03$ $5.$ $7.9836E+00$ $8.1118E-02$ $4.577E-03$ $5.$.47
4.3743E+002.3845E-011.237E-025.4.6175E+002.2328E-011.192E-025.4.8841E+001.8962E-016.959E-033.5.5000E+001.5901E-016.016E-033.6.0000E+001.4586E-017.143E-034.6.5000E+001.1726E-015.403E-034.7.0000E+001.0184E-015.525E-035.7.5000E+009.3769E-025.432E-035.7.9836E+008.1118E-024.577E-035.	.69
4.6175E+002.2328E-011.192E-025.4.8841E+001.8962E-016.959E-033.5.5000E+001.5901E-016.016E-033.6.0000E+001.4586E-017.143E-034.6.5000E+001.1726E-015.403E-034.7.0000E+001.0184E-015.525E-035.7.5000E+009.3769E-025.432E-035.7.9836E+008.1118E-024.577E-035.	.19
4.8841E+001.8962E-016.959E-033.5.5000E+001.5901E-016.016E-033.6.0000E+001.4586E-017.143E-034.6.5000E+001.1726E-015.403E-034.7.0000E+001.0184E-015.525E-035.7.5000E+009.3769E-025.432E-035.7.9836E+008.1118E-024.577E-035.	.34
5.5000E+001.5901E-016.016E-033.6.0000E+001.4586E-017.143E-034.6.5000E+001.1726E-015.403E-034.7.0000E+001.0184E-015.525E-035.7.5000E+009.3769E-025.432E-035.7.9836E+008.1118E-024.577E-035.	.67
6.0000E+001.4586E-017.143E-034.6.5000E+001.1726E-015.403E-034.7.0000E+001.0184E-015.525E-035.7.5000E+009.3769E-025.432E-035.7.9836E+008.1118E-024.577E-035.	. 78
6.5000E+001.1726E-015.403E-034.7.0000E+001.0184E-015.525E-035.7.5000E+009.3769E-025.432E-035.7.9836E+008.1118E-024.577E-035.	.90
7.0000E+001.0184E-015.525E-035.7.5000E+009.3769E-025.432E-035.7.9836E+008.1118E-024.577E-035.	.61
7.5000E+00 9.3769E-02 5.432E-03 5. 7.9836E+00 8.1118E-02 4.577E-03 5.	.43
/.9836E+UU 8.1118E-U2 4.5//E-U3 5.	. 79
	.64
8.5000E+00 7.9305E-02 5.100E-03 6.	.43
9.0000E+00 7.5040E-02 5.978E-03 7.	.97
9.2301E+00 $7.4700E-02$ $7.057E-03$ 9.	.44 22
9.5000E+00 7.5122E-02 0.165E-03 6.	.43 60
9.0939 ± 00 7.0232 ± 02 3.945 ± 03 $5.$.02
$1.0500 \pm 01 \qquad 0.2990 \pm 02 \qquad 7.990 \pm 03 \qquad 12. \\1.000 \pm 01 \qquad 5.4702 \pm 02 \qquad 9.505 \pm 03 \qquad 15$.09 69
1.1000E+01 $5.1201E-02 8.000E-03 15.$	58
$1.1235 \pm 01 \qquad 5.1221 \pm 02 \qquad 0.495 \pm 05 \qquad 10.$ $1.1500 \pm 01 \qquad 4.6632 \pm 02 \qquad 7.183 \pm 03 \qquad 15$. 50
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	51
1.2000 ± 01 1.1502 ± 02 2.005 ± 03 $0.$	51
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	18
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	35
$\begin{array}{cccccccccccccccccccccccccccccccccccc$.18
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	97
1.5000E+01 $4.5264E-02$ $7.761E-03$ $17.$.15
$\begin{array}{cccccccccccccccccccccccccccccccccccc$.56
1.6000E+01 4.0360E-02 6.492E-03 16.	.09
1.6500E+01 $4.0319E-02$ $4.854E-03$ 12.	.04
1.7000E+01 3.9635E-02 2.122E-03 5.	.35
1.7500E+01 3.6846E-02 5.314E-03 14.	.42
1.8000E+01 3.4461E-02 6.752E-03 19.	.59
1.8500E+01 3.2205E-02 7.573E-03 23.	.52
1.9000E+01 3.0061E-02 8.013E-03 26.	.66
1.9500E+01 2.8079E-02 8.160E-03 29.	.06
2.0000E+01 2.6663E-02 8.099E-03 30.	.37

Neutron cross std.dev. std.dev.	lev.
energy section of sigma(F)	
(in MeV) (in barn) (in barn) (in	1 %)
2.5028E+00 0.0000E+00 0.000E+00	0.00
2.5051E+00 2.8022E-03 4.795E-04 1	7.11
2.8287E+00 3.8253E-02 3.800E-03	9.93
2.9505E+00 4.9527E-02 4.940E-03	9.97
2.9915E+00 5.2176E-02 5.751E-03 1	L.02
3.0912E+00 5.8145E-02 6.203E-03 1).67
3.3201E+00 7.5580E-02 7.628E-03 1	0.09
3.4799E+00 8.7294E-02 1.044E-02 1	L.96
3.5854E+00 9.1486E-02 1.094E-02 1	L.96
3.6834E+00 9.5460E-02 1.208E-02 1	2.65
3.8401E+00 9.8254E-02 1.257E-02 1	2.80
3.9612E+00 9.4459E-02 1.342E-02 1	4.21
4.1789E+00 8.9753E-02 1.478E-02 1	5.47
4.3743E+00 8.6051E-02 1.482E-02 1	7.22
4.6175E+00 7.9712E-02 1.286E-02 1	5.14
4.8841E+00 7.4012E-02 7.896E-03 1	0.67
5.5000E+00 6.4209E-02 7.734E-03 1	2.04
6.0000E+00 5.4502E-02 7.452E-03 1	3.67
6.5000E+00 4.3466E-02 7.103E-03 1	5.34
7.0000E+00 3.4713E-02 5.126E-03 1	1. 77
7.5000E+00 2.6861E-02 4.634E-03 1	7.25
7.9836E+00 2.0761E-02 3.342E-03 1	5.10
8.5000E+00 1.6209E-02 3.487E-03 2	L.51
9.0000E+00 1.3863E-02 3.367E-03 2	1.29
9.2361E+00 1.2960E-02 3.324E-03 2	5.65
9.5000E+00 1.2072E-02 3.277E-03 2	7.15
9.8939E+00 1.0962E-02 3.206E-03 2	9.25
1.0500E+01 9.8227E-03 2.941E-03 2	9.94
1.1000E+01 9.1807E-03 2.848E-03 3	L.02
1.1233E+01 8.9249E-03 2.815E-03 3.	L.54
1.1500E+01 8.6815E-03 2.785E-03 3.	2.08
1.2000E+01 8.4032E-03 2.746E-03 3.	2.68
1.2534E+U1 8.1831E-U3 2./15E-U3 3.	3.18
1.3000E+01 /.8810E-03 2.648E-03 3.	3.60
1.3500E+01 7.6319E-03 2.583E-03 3.	3.85
1.4000E+01 7.41/6E-03 2.524E-03 3	±.02
1.4500E+01 7.0342E-03 2.480E-03 3.	5.25
1.5000E+01 0.0186E-03 2.441E-03 3 1.5000E+01 6.0206E-02 2.225E 02 2	
$1.5500 \pm 01 \qquad 5.0090 \pm 0.0390 \pm 0.03900 \pm 0.03$	3.50
1.60000 ± 01 5.0910 ± 03 2.209 ± 03 4	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2.02
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	ככ.כ 1 דד
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5 88
1 8500E+01	7 00
1 9000E+01	3 1 3
1.9500 ± 01 4.8312 ± 03 2.357 ± 03 4	2.26
2.0000E+01 4.7745E-03 2.404E-03 5).35

MT = 53	(n,n'3) cross section		
Neutron	cross	std.dev.	std.dev.
energy	section	of sigma(E)	
(in MeV)	(in barn)	(in barn)	(in %)
2.8284E+00	0.0000E+00	0.000E+00	0.00
2.8314E+00	1 3967E = 0.2	1 831E-03	13 11
2.9505E+00	1 0005E-01	1 305E - 02	13 04
2 9915E+00	1 0053E 01	1.061E - 02	10 56
3 0912E+00	1 2048F - 01	1 216F-02	10.00
3 3201F+00	1 4499F-01	1 421F-02	9 80
3.4799F+00	1 4903F-01	1 432F-02	9 61
3 5854F+00	1.5024 F = 01	1 444F-02	9 61
3 6834E+00	1 4663E - 01	1.374E = 02	9 37
3 8401E+00	1 4531E - 01	1.371E - 02	9 44
3 9612E+00	1 3469E-01	1.597E = 02	11 86
4 1789E+00	1 1984E = 01	1 888E-02	15 75
4 3743E+00	1 0807E - 01	1 933E-02	17 89
4 6175E+00	95040E-02	1 730E-02	18 20
4 8841E+00	7 7527E = 02	1.255E-02	16 19
5,5000E+00	5 2156E-02	1 156E-02	22 16
6 0000E+00	4 4846E-02	8 826E-03	19 68
6.5000E+00	3,2898E-02	6.785E-03	20.63
7 0000E+00	2 3593E-02	4 0.03E - 0.3	16 96
7 5000E+00	1 8018E - 02	3 367E-03	18 69
7.9836E+00	1.3192E - 02	2.358E-03	17.87
8.5000E+00	8.5043E-03	1.855E-03	21.81
9.0000E+00	5.8918E-03	1.386E-03	23.52
9.2361E+00	4.9702E-03	1.205E-03	24.25
9.5000E+00	4.0626E-03	1.026E-03	25.27
9.8939E+00	2.8802E-03	8.054E-04	27.96
1.0500E+01	1.7942E-03	5.378E-04	29.98
1.1000E+01	1.2855E-03	4.142E-04	32.22
1.1233E+01	1.1007E-03	3.661E-04	33.26
1.1500E+01	9.2401E-04	3.183E-04	34.44
1.2000E+01	6.7040E-04	2.456E-04	36.64
1.2534E+01	4.7675E-04	1.857E-04	38.96
1.3000E+01	3.5643E-04	1.462E-04	41.03
1.3500E+01	2.6284E-04	1.136E-04	43.20
1.4000E+01	1.9474E-04	8.836E-05	45.37
1.4500E+01	1.4445E-04	6.875E-05	47.59
1.5000E+01	1.0745E-04	5.356E-05	49.84
1.5500E+01	8.0350E-05	4.408E-05	54.86
1.6000E+01	5.9950E-05	3.590E-05	59.89
1.6500E+01	4.4828E-05	2.911E-05	64.94
1.7000E+01	3.3713E-05	2.359E-05	69.98
1.7500E+01	2.5421E-05	1.906E-05	74.99
1.8000E+01	1.9206E-05	1.536E-05	80.00
1.8500E+01	1.4537E-05	1.236E-05	85.00
1.9000E+01	1.1026E-05	9.923E-06	90.00
1.9500E+01	8.3839E-06	7.965E-06	95.00
2.0000E+01	6.3917E-06	6.391E-06	100.00

MT = 91	(n,n'cont) cross section		
Neutron energy	cross section	std.dev. of sigma(E)	std.dev.
(in MeV)	(in barn)	(in barn)	(in %)
3.5854E+00	0.0000E+00	0.000E+00	0.00
4.0000E+00	8.2117E-02	1.629E-02	19.84
4.5000E+00	2.1900E-01	3.796E-02	17.33
5.0000E+00	3.8162E-01	4.977E-02	13.04
5.5000E+00	5.3854E-01	4.878E-02	9.06
6.0000E+00	6.0214E-01	4.534E-02	7.53
6.5000E+00	6.2502E-01	4.360E-02	6.98
7.0000E+00	5.6813E-01	3.788E-02	6.67
7.5000E+00	5.8379E-01	3.788E-02	6.49
8.0000E+00	6.2882E-01	3.614E-02	5.75
8.5000E+00	5.7757E-01	3.691E-02	6.39
9.0000E+00	5.6179E-01	3.838E-02	6.83
9.5000E+00	5.7350E-01	3.584E-02	6.25
1.0000E+01	4.9647E-01	3.886E-02	7.83
1.1000E+01	5.8165E-01	5.078E-02	8.73
1.2000E+01	4.5027E-01	4.155E-02	9.23
1.3000E+01	3.2902E-01	3.021E-02	9.18
1.4000E+01	2.5443E-01	9.028E-03	3.55
1.5000E+01	2.0527E-01	1.422E-02	6.93
1.6000E+01	1.7347E-01	1.823E-02	10.51
1.7500E+01	1.4578E-01	2.079E-02	14.26
2.0000E+01	1.2019E-01	2.392E-02	19.90

Neutron	cross	std.dev.	std.dev.
energy	section	of sigma(E)	(
(IN MeV)	(in barn)	(in barn)	(111 3)
1 0000E-11	0 0000E+00	0 000E+00	0 00
5,5000E-01	0 0000E+00	0 000E+00	0 00
5,5000E-01	9 2254E-03	1 843E-03	19 97
6 0000E = 01	9 1000E-03	1 818E-03	19 97
65000E - 01	9 0189E-03	1 801E-03	19 97
7 0000 = 01	8 9750E-03	1 793E-03	19 97
75000E-01	8 9630E-03	1 790E-03	19 97
8.0000E-01	8.9790E-03	1.793E-03	19.97
8.5000E-01	9.0202E-03	1.801E-03	19.97
9.0000E-01	9.0843E-03	1.814E-03	19.97
9.5000E-01	9.1671E-03	1.830E-03	19.97
1.0000E+00	9.2690E-03	1.851E-03	19.97
1.1000E+00	9.5227E-03	1.996E-03	20.96
1.2000E+00	9.8315E-03	2.158E-03	21.95
1.2500E+00	1.0000E-02	2.245E-03	22.45
1.3000E+00	1.0181E-02	2.336E-03	22.94
1.3500E+00	1.0372E-02	2.431E-03	23.43
1.4000E+00	1.0573E-02	2.530E-03	23.93
1.4500E+00	1.0774E-02	2.632E-03	24.43
1.4797E+00	1.1638E-02	2.877E-03	24.72
1.5000E+00	8.9114E-03	2.222E-03	24.93
1.5500E+00	7.9332E-03	2.018E-03	25.43
1.6000E+00	7.3921E-03	1.918E-03	25.94
1.7000E+00	6.6507E-03	1.793E-03	26.96
1.8000E+00	6.1477E-03	1.720E-03	27.97
1.9000E+00	5.8207E-03	1.687E-03	28.99
2.0000E+00	5.6141E-03	1.684E-03	30.00
2.1000E+00	5.4924E-03	1.655E-03	30.13
2.2000E+00	5.4262E-03	1.641E-03	30.25
2.3000E+00	5.4098E-03	1.643E-03	30.36
2.4000E+00	5.4318E-03	1.656E-03	30.49
2.5000E+00	5.4841E-03	1.6/9E-03	30.61
2.51098+00	5.4041E-U3	1.000E-03	20.03
2.0000E+00 2.7000E+00	4.0430E-03	1.42/E-03	20.74
2.7000E+00 2.8000E+00	4.44546-03	1.372E-03	30.87
2 8238F+00	4 3061F-03	1 336F-03	31.00
2 9000E+00	3 9644E-03	1.334E = 03	31.03
2 9505E+00	3 8874E-03	1.231E 03 1.210E-03	31.13
3 0000E+00	3 6627E-03	1 146E-03	31 28
3.0912E+00	3.4933E-03	1.097E-03	31.41
3.3201E+00	3.0777E-03	9.671E-04	31.42
3.4799E+00	2.8486E-03	9.096E-04	31.93
3.5000E+00	2.7939E-03	8.928E-04	31.95
3.5854E+00	2.7007E-03	8.658E-04	32.06
3.6199E+00	2.6228E-03	8.408E-04	32.06
4.0000E+00	2.0058E-03	6.514E-04	32.48
4.5000E+00	1.5737E-03	5.201E-04	33.05
5.0000E+00	1.3339E-03	4.480E-04	33.59
5.5000E+00	1.0803E-03	3.692E-04	34.17
6.0000E+00	9.3305E-04	3.248E-04	34.81
6.5000E+00	8.7226E-04	3.095E-04	35.49
7.0000E+00	8.3369E-04	3.017E-04	36.19

MT = 102 (n,γ) cross section

7.5000E+00	7.7667E-04	2.863E-04	36.87
8.0000E+00	7.2605E-04	2.727E-04	37.55
8.5000E+00	6.8364E-04	2.614E-04	38.24
9.0000E+00	6.4584E-04	2.511E-04	38.88
9.5000E+00	6.1472E-04	2.429E-04	39.51
1.0000E+01	5.8576E-04	2.352E-04	40.15
1.0500E+01	5.4674E-04	2.468E-04	45.14
1.1000E+01	5.1342E-04	2.573E-04	50.12
1.1500E+01	4.4954E-04	2.475E-04	55.07
1.2000E+01	4.0276E-04	2.409E-04	59.81
1.2419E+01	3.8047E-04	2.418E-04	63.55
1.3000E+01	3.7834E-04	2.602E-04	68.77
1.3500E+01	4.2242E-04	3.087E-04	73.09
1.4000E+01	4.9954E-04	3.860E-04	77.27
1.4500E+01	6.1023E-04	4.726E-04	77.44
1.5000E+01	7.4000E-04	5.763E-04	77.88
1.5500E+01	8.6210E-04	6.753E-04	78.34
1.6000E+01	9.5730E-04	7.543E-04	78.80
1.6500E+01	1.0084E-03	7.993E-04	79.26
1.7000E+01	1.0290E-03	8.185E-04	79.54
1.7500E+01	1.0274E-03	8.192E-04	79.74
1.8000E+01	1.0122E-03	8.084E-04	79.86
1.8500E+01	9.9580E-04	7.965E-04	79.98
1.9000E+01	9.7614E-04	7.819E-04	80.10
1.9500E+01	9.5673E-04	7.675E-04	80.22
2.0000E+01	9.3966E-04	7.545E-04	80.29

MT = 103	(n,p) cı	ross section		
Neutron		cross	std.dev.	std.dev.
energy		section	of sigma(E)	
(in MeV)		(in barn)	(in barn)	(in %)
4.0000E-01		0.0000E+00	0.000E+00	0.00
1.0000E+00		2.6476E-03	3.097E-04	11.70
1.4000E+00		1.1663E-02	1.277E-03	10.95
1.8000E+00		2.9135E-02	2.532E-03	8.69
2.2000E+00		6.6905E-02	4.816E-03	7.20
2.6000E+00		1.2554E-01	8.127E-03	6.47
3.0000E+00		1.9260E-01	1.384E-02	7.19
3.4000E+00		2.5484E-01	1.948E-02	7.65
3.8000E+00		3.2166E-01	1.954E-02	6.08
4.2000E+00		3.7651E-01	1.599E-02	4.25
4.6000E+00		4.2038E-01	1.502E-02	3.57
5.0000E+00		4.6542E-01	1.598E-02	3.43
5.4000E+00		5.4312E-01	1.902E-02	3.50
5.8000E+00		5.6778E-01	2.046E-02	3.60
6.2500E+00		6.0757E-01	2.251E-02	3.70
6.7500E+00		6.3522E-01	2.444E-02	3.85
7.5000E+00		6.3739E-01	2.529E-02	3.97
8.5000E+00		6.1946E-01	2.444E-02	3.95
9.5000E+00		6.1243E-01	2.396E-02	3.91
1.0500E+01		6.0122E-01	2.651E-02	4.41
1.1500E+01		5.8220E-01	2.847E-02	4.89
1.2200E+01		5.4942E-01	2.671E-02	4.86
1.2600E+01		5.3376E-01	2.285E-02	4.28
1.3000E+01		5.0151E-01	1.816E-02	3.62
1.3400E+01		4.8761E-01	1.607E-02	3.30
1.3800E+01		4.1983E-01	1.376E-02	3.28
1.4200E+01		3.6645E-01	1.180E-02	3.22
1.4600E+01		2.9930E-01	1.006E-02	3.36
1.5000E+01		2.6996E-01	9.685E-03	3.59
1.5400E+01		2.4130E-01	1.012E-02	4.19
1.5800E+01		2.2836E-01	1.192E-02	5.22
1.6500E+01		1.9436E-01	1.375E-02	7.08
1.7500E+01		1.8226E-01	1.874E-02	10.28
1.8500E+01		1.6258E-01	2.248E-02	13.83
1.9500E+01		1.5335E-01	2.557E-02	16.67
2.0000E+01		1.5711E-01	2.470E-02	15.72

MT = 104	(n,d) cross	s section		
Neutron		cross	std.dev.	std.dev.
(in MeV)		(in barn)	(in barn)	(in %)
6.0498E+00		0.0000E+00	0.000E+00	0.00
9.0413E+00		3.0128E-07	1.202E-07	39.91
9.5000E+00		7.2720E-04	2.688E-04	36.96
1.0000E+01		3.2616E-03	1.269E-03	38.90
1.0474E+01		4.5635E-03	1.753E-03	38.41
1.0500E+01		4.3165E-03	1.607E-03	37.23
1.1000E+01		5.2032E-03	1.854E-03	35.63
1.1500E+01		5.9730E-03	1.958E-03	32.79
1.2000E+01		7.6968E-03	2.942E-03	38.23
1.2500E+01		9.2954E-03	3.424E-03	36.84
1.3000E+01		1.1261E-02	4.032E-03	35.80
1.3500E+01		1.3223E-02	4.654E-03	35.20
1.4000E+01		1.5688E-02	4.706E-03	30.00
1.4500E+01		1.8122E-02	4.200E-03	23.18
1.5000E+01		2.0616E-02	4.579E-03	22.21
1.5500E+01		2.2127E-02	5.732E-03	25.91
1.6000E+01		2.5693E-02	6.327E-03	24.63
1.6500E+01		2.8167E-02	6.754E-03	23.98
1.7000E+01		2.9910E-02	1.092E-02	36.50
1.7500E+01		3.2339E-02	1.167E-02	36.10
1.8000E+01		3.4573E-02	1.229E-02	35.53
1.8500E+01		3.6321E-02	1.281E-02	35.26
1.9000E+01		3.7925E-02	1.315E-02	34.68
1.9500E+01		3.8786E-02	1.336E-02	34.45
2.0000E+01		3.9052E-02	1.351E-02	34.60

MT = 105	(n,t)	cross	section

Neutron	cross	std.dev.	std.dev.
energy	section	of sigma(E)	
(in MeV)	(in barn)	(in barn)	(in %)
1.1255E+01	0.0000E+00	0.000E+00	0.00
1.3500E+01	0.0000E+00	0.000E+00	0.00
1.4000E+01	7.1090E-06	2.663E-06	37.46
1.4500E+01	2.1560E-05	7.782E-06	36.09
1.5000E+01	3.2514E-05	1.620E-05	49.83
1.6000E+01	6.7857E-04	6.096E-04	89.83
1.7000E+01	3.9129E-03	2.260E-03	57.75
1.8000E+01	1.0304E-02	5.195E-03	50.41
1.9000E+01	1.7331E-02	8.868E-03	51.17
2.0000E+01	2.6123E-02	1.347E-02	51.56

MT = 106	(n,3He) cross section		
Neutron energy	cross section	std.dev. of sigma(E)	std.dev.
(in MeV)	(in barn)	(in barn)	(in %)
6.5907E+00	0.0000E+00	0.000E+00	0.00
1.4446E+01	0.0000E+00	0.000E+00	0.00
1.4446E+01	0.0000E+00	0.000E+00	0.00
1.8000E+01	0.0000E+00	0.000E+00	0.00
1.8000E+01	1.8002E-06	1.804E-06	100.00
1.8500E+01	1.3360E-05	1.336E-05	100.00
1.9000E+01	6.3715E-05	6.371E-05	100.00
1.9500E+01	2.2570E-04	2.257E-04	100.00
2.0000E+01	6.4287E-04	6.428E-04	100.00

Neutron	cross	std.dev.	std.dev.
energy	section	of sigma(E)	
(in MeV)	(in barn)	(in barn)	(in %)
		(,	
1.0000E-11	0.0000E+00	0.000E+00	0.00
5.0000E-01	1.3194E-07	6.493E-08	49.22
1.0000E+00	1.6838E-05	8.007E-06	47.55
1.0521E+00	2.1173E-05	9.808E-06	46.32
1.1476E+00	3.2269E-05	1.438E-05	44.55
1.1973E+00	4.2035E-05	1.691E-05	40.22
1.4754E+00	1.2809E-04	3.874E-05	30.25
1.6717E+00	1.8892E-04	3.266E-05	17.29
1.8084E+00	2.7805E-04	4.208E-05	15.14
1.9029E+00	3.5313E-04	7.788E-05	22.06
1.9728E+00	4.1394E-04	1.084E-04	26.18
2.0864E+00	4.8861E-04	1.299E-04	26.59
2.5031E+00	1.0230E-03	2.097E-04	20.49
2.9915E+00	4.0685E-03	2.756E-04	6.77
3.5000E+00	6.9117E-03	3.416E-04	4.94
4.0000E+00	1.3926E-02	5.308E-04	3.81
4.5000E+00	2.7943E-02	8.482E-04	3.04
5.0000E+00	3.4235E-02	9.767E-04	2.85
5.5000E+00	5.6022E-02	1.580E-03	2.82
6.0000E+00	6.4380E-02	1.894E-03	2.94
6.5000E+00	7.5076E-02	2.420E-03	3.22
7.0000E+00	7.2877E-02	2.655E-03	3.64
7.5000E+00	7.6188E-02	2.804E-03	3.68
8.0000E+00	7.5015E-02	3.140E-03	4.19
8.5000E+00	7.9389E-02	3.218E-03	4.05
9.0000E+00	7.7487E-02	3.238E-03	4.18
9.5000E+00	8.4010E-02	3.476E-03	4.14
1.0000E+01	8.2435E-02	3.820E-03	4.63
1.0500E+01	8.6185E-02	4.379E-03	5.08
1.1000E+01	8.2536E-02	4.616E-03	5.59
1.1500E+01	9.0843E-02	4.420E-03	4.87
1.2000E+01	9.2094E-02	5.003E-03	5.43
1.2500E+01	9.5887E-02	5.051E-03	5.27
1.3000E+01	9.5348E-02	4.288E-03	4.50
1.3500E+01	9.4620E-02	5.172E-03	5.47
1.4000E+01	9.5240E-02	4.334E-03	4.55
1.4500E+01	8.8421E-02	4.671E-03	5.28
1.5000E+01	9.4678E-02	5.611E-03	5.93
1.5500E+01	8.2679E-02	3.768E-03	4.56
1.6000E+01	7.8411E-02	1.274E-02	16.25
1.6500E+01	7.1291E-02	5.302E-03	7.44
1.7000E+01	6.3899E-02	6.895E-03	10.79
1.7500E+01	6.6655E-02	7.072E-03	10.61
1.8000E+01	5.5131E-02	1.476E-02	26.77
1.8500E+01	5.0814E-02	5.263E-03	10.36
1.9000E+01	5.4190E-02	5.649E-03	10.42
1.9500E+01	4.7992E-02	3.828E-03	7.98
2.0000E+01	4.2685E-02	1.379E-02	32.30

MT = 107 (n,a) cross section

MT = 112	(n,pa) cross	s section		
Neutron energy		cross section	std.dev.	std.dev.
(in MeV)		(in barn)	(in barn)	(in %)
6.4227E+00		0.0000E+00	0.000E+00	0.00
1.3000E+01		0.0000E+00	0.000E+00	0.00
1.3000E+01		4.0030E-06	1.997E-06	49.89
1.3500E+01		1.9242E-05	9.586E-06	49.82
1.4000E+01		7.3712E-05	3.663E-05	49.69
1.4500E+01		2.3255E-04	1.153E-04	49.59
1.5000E+01		6.2171E-04	3.078E-04	49.51
1.5500E+01		1.4200E-03	7.018E-04	49.42
1.6000E+01		2.8513E-03	1.409E-03	49.40
1.6152E+01		3.4329E-03	1.697E-03	49.44
1.6500E+01		5.0364E-03	2.500E-03	49.63
1.7000E+01		8.0017E-03	3.990E-03	49.86
1.7500E+01		1.1545E-02	5.803E-03	50.27
1.8000E+01		1.5445E-02	7.823E-03	50.65
1.8500E+01		1.9486E-02	9.939E-03	51.01
1.9000E+01		2.3548E-02	1.209E-02	51.33
1.9500E+01		2.7524E-02	1.421E-02	51.64
2.0000E+01		3.1402E-02	1.628E-02	51.85

MT = 854	(n,n'4-8)			
Neutron		cross	std.dev.	std.dev.
energy		section	of sigma(E)	
(in MeV)		(in barn)	(in barn)	(in %)
2.9505E+00		0.0000E+00	0.000E+00	0.00
3.0000E+00		5.8436E-02	6.271E-03	10.73
3.2500E+00		1.9849E-01	1.828E-02	9.21
3.5000E+00		3.2930E-01	2.724E-02	8.27
3.7500E+00		3.9571E-01	3.043E-02	7.69
4.0000E+00		4.1030E-01	3.767E-02	9.18
4.2500E+00		3.9689E-01	4.763E-02	12.00
4.5000E+00		3.9337E-01	4.544E-02	11.55
4.7500E+00		4.0211E-01	5.026E-02	12.50
5.0000E+00		3.4185E-01	4.948E-02	14.47
5.5000E+00		2.4767E-01	4.179E-02	16.87
6.0000E+00		1.8398E-01	2.908E-02	15.81
6.5000E+00		1.3384E-01	2.466E-02	18.42
7.0000E+00		9.1127E-02	1.569E-02	17.22
7.5000E+00		7.3894E-02	1.441E-02	19.50
8.0000E+00		5.8595E-02	1.005E-02	17.15
8.5000E+00		4.3981E-02	9.629E-03	21.89
9.0000E+00		3.4907E-02	8.632E-03	24.73
9.5000E+00		2.8352E-02	7.517E-03	26.51
1.0000E+01		2.2779E-02	6.639E-03	29.14
1.0500E+01		1.9378E-02	5.984E-03	30.88
1.1000E+01		1.7211E-02	5.466E-03	31.76
1.1500E+01		1.5571E-02	5.085E-03	32.65
1.2000E+01		1.4650E-02	4.810E-03	32.83
1.2500E+01		1.4107E-02	4.604E-03	32.64
1.3000E+01		1.3597E-02	4.449E-03	32.72
1.3500E+01		1.3236E-02	4.283E-03	32.36
1.4000E+01		1.2861E-02	4.103E-03	31.90
1.4500E+01		1.2021E-02	3.990E-03	33.19
1.5000E+01		1.0955E-02	3.903E-03	35.63
1.6000E+01		9.0962E-03	3.626E-03	39.86
1.7000E+01		7.9992E-03	3.477E-03	43.47
1.8000E+01		7.3245E-03	3.354E-03	45.80
1.9000E+01		7.2129E-03	3.474E-03	48.17
2.0000E+01		6.9299E-03	3.500E-03	50.51



Fig.1 ⁵⁸Ni evaluation-flow chart

Fig. 2 Correction factor for conversion of $\sigma\,(^12^{\scriptscriptstyle +}\!\rightarrow g.s.)$ to σ_{inel}





Fig. 3 Total cross section and comparison with ENDF/B-VI

Fig. 4 Elastic cross section and comparison with ENDF/B-VI



Fig. 5 Nonelastic cross section and comparison with ENDF/B-VI



Fig. 6 Inelastic cross section and comparison with ENDF/B-VI











Fig. 9 (n,d) cross section with ENDF/B-VI as "prior"





Fig. 10 (n,np) cross section and comparison with ENDF/B-VI



Fig. 11 (n,n₁) cross section up to 6 MeV and comparison with ENDF/B-VI



Fig. 12 (n,n₁) cross section (full range) and comparison with ENDF/B-VI



Fig. 13 (n,n₂) cross section and comparison with ENDF/B-VI



Fig. 14 (n,n₃) cross section and comparison with ENDF/B-VI



Fig. 15 Sum of (n,n₄) to (n,n₈) cross section and comparison with ENDF/B-VI



Fig. 16 (n,n_{cont}) cross section and comparison with ENDF/B-VI

Fig. 17 (n,y) cross section and comparison with ENDF/B-VI





Fig. 18 (n,p) cross section and comparison with ENDF/B-VI





Fig. 20 (n,³He) cross section, not available in ENDF/B-VI







Fig. 22 (n,pα) cross section, not available in ENDF/B-VI







Correlation matrix for the (n, 2n) cross section



Incident neutron energy (MeV)


Fig. 26 Correlation matrix for the (n, np) cross section





Fig. 28 Correlation matrix for the (n, n'₂) cross section



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Fig. 29 Correlation matrix for the (n, n'₃) cross section



Fig. 30 Correlation matrix for the $(n, n'_4) + ... + (n, n'_8 cross section$



- 75 -

Fig. 31 Correlation matrix for the (n, n'_{cont}) cross section



Fig. 32 Correlation matrix for the (n, γ) cross section



- 76 -

Fig. 33 Correlation matrix for the (n, p) cross section



Fig. 34 Correlation matrix for the (n, d) cross section



Fig. 35 Correlation matrix for the (n, t) cross section



Correlation matrix for the (n, ³He) cross section Fig. 36



Incident neutron energy (MeV)

Fig. 37 Correlation matrix for the (n, α) cross section



Fig. 38 Correlation matrix for the (n, pa) cross section



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