

INDC(BLR)-0022

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July 2024

IAEA Nuclear Data Section Vienna International Centre, A-1400 Vienna, Austria

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Abstract

The diverse measured data base of $n+^{243}$ Am was evaluated using a statistical theory and genera-lized least squares codes. Consistent description of total, capture and fission measured data provides an important constraint for the inelastic scattering cross section. Important constraints for the measured capture cross section in the 0.15-300 keV energy range come from the average radiative and neutron S⁰ and S¹ strength functions. The evaluated inelastic cross sections of available evaluations are in severe disagreement, predicted change of the inelastic cross section shape at $E_n \sim 1.5$ MeV is attributed to the sharp increase of the level density of the residual odd-even nuclide ²⁴¹Am due to the onset of three-quasi-particle excitations.

The influence of exclusive (n, xnf) pre-fission neutrons on prompt fission neutron spectra (PFNS) and (n, xn) spectra is modelled. Contributions of emissive/non-emissive fission and exclusive spectra of (n, xnf) reactions are defined by a consistent description of the ²⁴¹Am(n, F), ²⁴¹Am(n, 2n).

This work is performed under the project Agreement B-1604 during 2008-2011 with the International Science and Technology Center (Moscow). The financing party is EU. Partial support of International Atomic Energy Agency under Research Contract 14809 is acknowledged. Data file is at https://www-nds.iaea.org/minskact/data/original/za095243

Contents

1. Introduction

Americium-243 ($t_{1/2}$ =7370 yr) evolves in Pu-containing nuclear fuels at increased burn-up, after β—decay of ²⁴¹Pu (t_{1/2} = 14.4 yr) in a chain, starting from ²⁴¹Am. The transmutation of the 241 Am in thermal power reactors is accompanied by the neutron capture cross sections in the reaction chains ²⁴¹Am(n, γ) ^{242m(g)}Am. The neutron capture reaction ²⁴¹Am(n, γ) populates either the 16-h ground state $242g$ Am or the $242m$ Am isomer with $t_{1/2}$ =141 yr, in both cases build-up of 243 Am is possible. The former state ^{242g}Am subsequently β ⁻-decays to ²⁴²Cm. The capture reaction ²⁴¹Am(n, γ)^{242m}Am influences the neutron activity of the spent fuel due to spontaneous fission of ^{242m}Am. It gives a path for the ²⁴⁴Cm yield via ^{242m}Am(n,γ)²⁴³Am(n,γ)^{244m}Am(β ⁻(ε))²⁴⁴Cm(²⁴⁴Pu) or ^{242m}Am(n,γ)²⁴³Am(n,γ)^{244g}Am(β⁻)²⁴⁴Cm. If not the forbidden β⁻⁻-decay of ^{242m}Am state, the major path of ²⁴⁴Cm build-up would not exist. The yield of the ^{244m(g)}Am states influences both alpha- and neutron activity of the spent fuel [1, 2].

Repository or transmutation of ²⁴³Am as one of the constituent of the spent fuel needs rather diverse knowledge base. Namely, the ²⁴³Am neutron-induced fission, capture, inelastic scattering, $(n,2n)$ cross sections, branching ratio for the yields of short-lived ^{244m}Am and long-lived ^{244g}Am states of ²⁴³Am(n, γ) reaction, branching ratio for the yields of short-lived ^{242g}Am and long-lived $242m$ Am states of 243 Am(n, 2n) reaction. Prompt fission neutron spectrum (PFNS) and prompt fission neutron multiplicity are another important items, measurements of the former for the $^{243}Am(n, F)$ reaction are unavailable at the moment.

The improvements of the nuclear reaction modeling and nuclear parameter systematic, developed based on neutron data description of neutron data for major actinides 232 Th, 233 U, 235 U, ²³⁸U, ²³⁹Pu and Z-odd target ²³⁹Np provide a sound basis for critical assessment of the (n, F), (n, γ), (n, n) , (n, n') cross sections and secondary neutron spectra for the $n+243$ Am interaction. The main reasons of improvement might be consistent description of total, fission and capture data in 0.15 $keV - 300 keV$ energy range. For neutron capture reaction on ²⁴³Am target nuclide in the unresolved resonance and fast neutron energy ranges the methods, proven in case of ²³²Th(n,γ) [3], ²³⁸U(n, γ) [4] and 237 Np [5] data analysis would be used. Disentangling of the model deficiencies and model parameter uncertainties, when measured cross section data base fits are rather poor, especially when the data are scattering and there are systematic shifts between different data sets, turns out to be a major problem in case of Z-odd actinides like ²³⁷Np or ^{241,243}Am. Important constraints for the calculated capture cross section come from the average radiation width and neutron strength functions S_0 and S_1 . For the ²⁴³Am+n interaction we have used almost the same optical potential, which allowed consistent description of total, fission and partial inelastic scattering data in $1~3~MeV$ incident neutron energy range for ²³⁷Np target nuclide. It provided an important constraint for the absorption cross section, which is quite important for the robust estimate of the capture cross section in keV- energy range.

Consistent description of ²⁴¹Am(n, 2n) and ²⁴¹Am (n, F) cross sections was considered an important constraint in view of large scatter and systematic shifts of fission data. ²⁴³Am (n, F) observed fission cross section data are scattered even more, calculated cross section is represented as a superposition of the (n, f) and (n, xnf) reactions, with simultaneous calculation of exclusive neutron spectra of (n, xn) and (n, xnf) reactions. That approach provided a robust estimates of prompt fission neutron spectra and their average energies for major actinides 232 Th, 233 U, 235 U, 238 U, 2^{239} Pu [6, 7] and Z-odd target 2^{37} Np [5, 7]. The average energies of prompt fission neutron spectra (PFNS) and PFNS itself $[5, 7]$ for $^{237}Np(n, F)$ reaction are consistent with measured data base. That is a strong impetus to provide a new evaluation of PFNS for 243 Am (n, F).

Realistic assessment of the uncertainties of 243 Am evaluated data should take into account the results of the consistent description of total, fission, capture and inelastic scattering cross sections

with nuclear reaction theory. Purpose of the present evaluation is to clear out whether the available data on total and partial cross sections and average resonance parameters could be described (reproduced) consistently.

2. Resonance Parameters

Here we will briefly review the status of resolved neutron resonance parameters of 243 Am. Resolved and unresolved resonance parameters are adopted from our previous evaluation [8], i.e., resolved resonance parameters for multilevel Breit-Wigner formalism (up to 150 eV) are adopted. Thermal total, capture and fission cross sections and resonance integrals are shown in Table 2.1.

Reaction σ^{th} , barn		RI	σ^{th} , barn	RI	σ th , barn	RI
	Present		JENDL-4.0		ENDF/B-VII.0	
Total	84.232		85.831		83.6875	
Elastic	7.4642		6.49		8.53775	
Fission	.00638	7.4654	.00816	6.31	.007389	8.63501
Capture	76.704	1781.18	79.259	2040	75.0759	1814.44

Table 2.1 Thermal total, elastic, capture and fission cross sections and resonance integrals

3. Evaluation of neutron capture and fission cross sections for ²⁴³Am with generalized leastsquares method

The approach developed by W. Poenitz, the GMA code and database of experimental results were used in the last evaluation of the neutron cross section standards [9, 10]. The most measurements of the neutron capture and fission cross sections at 243 Am have been done relative these standard reactions. These standards can be used in new evaluation of ²⁴³Am(n, γ) and ²⁴³Am(n, f) reaction cross sections in two ways. First, the results of standards evaluation (cross sections and covariance matrices of their uncertainties) may be used as a prior in a Bayesian approach. Uninformative prior should be assigned to ²⁴³Am(n, γ) and ²⁴³Am(n, f) cross sections. Using Bayesian procedure a posterior evaluation for combined standards and 243 Am cross sections can be obtained by the least-squares fit adding the experimental data. In the second method, the generalized least-squares fit can be done for combined standard and ²⁴³Am(n, γ) and ²⁴³Am(n, f) cross sections. The final evaluation will contain the standards, which probably will be slightly modified, and evaluated ²⁴³Am(n, γ) and ²⁴³Am(n, f) cross sections with covariance matrix of their uncertainties, including the blocks with all cross-reaction correlations. The results obtained in both approaches should be almost coincident.

The combined fit with only standard for $197Au(n, \gamma)$ was used in the evaluation of capture cross section ²⁴³Am(n, γ). Because the ²⁴³Am(n, γ) experimental data include only the results of shape cross section measurements and absolute ratio of ²⁴³Am(n, γ) to ¹⁹⁷Au(n, γ) cross sections, this is a rather good approximation. This is endorsed by the result of such evaluation when changes in the values of the ¹⁹⁷Au(n, γ) reaction standard due to influence of the ²⁴³Am(n, γ) data are within 0.1 -0.2% .

3.1 ²⁴³Am capture cross section evaluation

The experimental data used in the evaluation are retrieved from EXFOR database and given

in Table 1. Because the measurements of thermal capture cross section were de-coupled from measurements at other energies and include mostly Maxwellian neutron spectrum averaged cross section with kT=0.0253 eV, the evaluation at thermal energy point 0.0253 eV were done separately. The energy measurements were done by two groups, by L.W. Weston and J.H. Todd [11], which because of their normalization can be used only as shape type of data (see comment in table 1). Data by K. Wisshak and F. Kaeppeler [12], which presents detailed studies with variable parameters of measurement (16 data sets), but because of this, their systematical uncertainties are strongly correlated.

The result of the evaluation are shown at Fig. 3.1 and 3.2 together with experimental data and latest evaluation of ²⁴³Am capture cross section done for JENDL-4.0 [13] library. Data on Fig. 3.1 are shown in the log-log scale. Weston and Todd [11] shape type data taken at their experimental energy nodes tuned with the normalization coefficient obtained in the fit with GMA. Wisshak et al. [12] data are converted from ratio to ¹⁹⁷Au(n, γ) using ¹⁹⁷Au(n, γ) cross section obtained in this combined fit, which, as it was mentioned before, differs from previously evaluated standard only in few points at 0.1 – 0.2 % level. The small uncertainty of ²⁴³Am(n, γ) cross section is at the level of 5 – 6 % below 10 keV, then reduces to $2 - 3$ % in the energy range $10 - 80$ keV, and increases again to $4 - 6$ % in 80 – 230 keV energy range. Coefficients of the correlation matrix of the evaluated uncertainties are varied between 0.2 – 0.6 for range where Weston et al. [11] data determine the evaluation and are low for part of the matrix describing correlations between uncertainties of the data above and below 80 keV. General chi-square per degree of freedom in the fit is at the level of 0.9. Data at Fig 3.2 are shown as cross section multiplied by square root from the incident neutron energy, to remove close to "*1/*v" energy dependence observed at these energies.

Evaluation of the same experimental data were done independently (including analysis of experimental data and their uncertainties) using PADE analytical model approximation. In this evaluation Weston et al. [11] data were considered as shape type of data; this explains the difference in the low-energy part of the cross section. The results of Weston et al. [12] measurements show some fluctuations, which may have physical origine because of the low level density for capture channel in this energy region. It is interesting to mention, that JENDL-4.0 evaluation in the energy range between 80 and 200 keV is about 10% higher GMA and PADE evaluations.

3.2 ²⁴³Am fission cross section evaluation

Data from JENDL-4.0 [13] library for 243 Am(n,f) reaction were used as a prior for ofr experimental data [14-27] to the energy nodes in the GMA fit. The experimental data selected for the fit given in the Table 3.2. Some data presented by the authors as results of absolute measurements (data set 7020 and 7023) were used as shape data, because of obvious problems with the normalization. The results of the GMA fit in comparison with JENDL-4.0 [13] evaluation and experimental data are shown in Figs. $3.3 - 3.7$. When uncertainties assigned by authors are used, the chi-squared value per degree of freedom obtained in the fit for 243 Am(n, f) is about 4, with the chisquared value per degree of freedom for all data in the fit at the level of 1. The outlaying data were determined as data deviating from the result of the fit at more that 3σ -level in separate points and more than 2σ in few sequential energy points. The additional medium energy range correlation components of the uncertainties were added to the covariance matrices of the uncertainties of these data. As a result, the final chi-squared value per degree of freedom obtained in the fit of the data sets for 243 Am(n, f) cros section was of the order of 1.

Fig. 3.1. Comparison of the results of the GMA evaluation with experimental data and JENDL-4.0 and PADE evaluation. GMA evaluation was smoothed using simple 3-point smoothing scheme.

Fig. 3.2. Comparison of the results of the GMA evaluation with experimental data and JENDL-4.0 and PADE evaluations. Non-smoothed GMA evaluation shown by dashed curve.

Data set	First author	EXFOR entry, date	Data	Type of measurem	Energy range covered, MeV	Comments
numb						
7001	P.A. Seeger	10063 (1970)	$\sqrt[243]{\text{Am}}(n,\text{f})$	Absolute	49 eV -30 MeV	Only data above 0.1 MeV are used in GMA fit because of large
						uncertainty and background below 0.1 MeV. 235U (n,f) was used for
						flux normalization. Because
						systematical uncertainty is substantially larger than the
						uncertainty of the standard data were not converted to
						$^{243}Am(n,f)/^{235}U(n,f)$ ratio
7002	J.W. Behrens	10652 (1981)	$\sqrt[243]{\text{Am}(n, f)}$ $^{235}U(n,f)$	Shape of ratio	$0.2 - 30 \text{ MeV}$	Shape of ratio type of data was used because authors normalized
						data through ratio of cross sections
						in a wide energy interval (1.75 - 4.0 MeV). Shape of ratio was a
						primarely measured quantity
7003	D.K. Butler	12543	$^{243}Am(n,f)$	Shape	$0.03 - 1.67$	Shape data with minimal error
		(1961)			MeV	assigned 5 % . No nunerical data about $^{235}U(n,f)$ monitor used.
7004	K.Wisshak	21863013 (1983)	$^{243}Am(n,f)/$ $^{235}U(n,f)$	Absolute ratio	$0.0125 - 0.08$ MeV	Data from runs \overline{I} – IV, correlated with data sets 7005, 7006, 7007
7005	K.Wisshak	21863014	$^{243}Am(n,f)/$	Absolute	$0.0125 - 0.08$	Data from runs V and VI,
		(1983)	$^{235}U(n,f)$	ratio	MeV	correlated with data sets 7004, 7006, 7007
7006	K.Wisshak	21863015 (1983)	$\sqrt[243]{\text{Am}(n, f)}$ $^{235}U(n,f)$	Absolute ratio	$0.035 - 0.2$ MeV	Data from runs V and VI, correlated with data sets 7004,
						7005, 7007
7007	K.Wisshak	21863016	$^{243}Am(n,f)/$	Absolute	$0.035 - 0.225$	Data from runs V and VI,
		(1983)	$^{235}U(n,f)$	ratio	MeV	correlated with data sets 7004, 7005, 7006
7008	H.Terayama	22024 (1986)	$\sqrt[243]{243}Am(n,f)/$ $^{235}U(n,f)$	Absolute ratio	$4.31 - 6.83$ MeV	d-d neutron source. Correlated with data sets 7009
7009	H.Terayama	22024	$\sqrt[243]{\text{Am}(n,f)}$	Absolute	$1.06 - 2.88$	p-T neutron source. Correlated
7010	H. Knitter	(1986) 22032	$^{235}U(n,f)$ $\sqrt[243]{243}Am(n,f)$	ratio Absolute	MeV $3.76 - 9.92$	with data sets 7009 d-d neutron source. Taken as
		(1988)			MeV	absolute because of large
						uncertainty comparing with
						235 U(n,f) standard changes in this energy range. Correlated with data
						set 7011 and 7012.
7011	H. Knitter	22032 (1988)	$^{243}Am(n,f)$	Absolute	$0.897 - 3.96$ MeV	p-T neutron source. Taken as absolute because of large
						uncertainty comparing with
						235 U(n,f) standard changes in this
						energy range. Correlated with data set 7010 and 7012.
7012	H. Knitter	22032	$\sqrt[243]{243}$ Am(n,f)	Absolute	$0.335 - 1.132$	p- ⁷ Li neutron source. Taken as
		(1988)			MeV	absolute because of large uncertainty comparing with
						235 U(n,f) standard changes in this

Table 3.2. The data sets for $^{243}Am(n,f)$ reaction cross section included in the GMA combined fit.

Fig. 3.3. Comparison of the results of the GMA evaluation with JENDL-4.0 [13] and experimental data. Experimental data shown as symbols connected by lines are non-normalized shape type of data. X4 is a number of EXFOR entry (or sub-entry). Data given as the ratio of cross sections are transformed to ²⁴³Am(n, F) cross section using standard cross section obtained in this combined fit.

Fig. 3.4. The same as at Fig. 3.3 but for detailed view of the cross sections in the energy range from 0.015 to 0.8 MeV.

Fig. 3.4. The same as at Fig. 3 but for detailed view of the cross sections in the energy range from 4 to 7 MeV.

Fig. 3.6 Comparison of GMA' evaluated fission cross section of ²⁴³Am with previous evaluations and measured data.

Fig. 3.7 Comparison of GMA' evaluated fission cross section of ²⁴³Am with previous evaluations and measured data.

The data presented at Fig. $3.3 - 3.7$ show, that the experimental data have a rather large spread. GMA evaluation in the energy range above 1 MeV is below JENDL-4.0 evaluation, because of large influence of data by Terayama et al. [17] and lays slightly below data by Fursov et al. [22]. Largest differences with JENDL-4.0 evaluation were observed in the sub-threshold region, where uncertainties of the data are large.

As we see from figures 3.6 and 3.7, there is rather large spread of experimental data in the MeV region. New measurements are needed in the energy range $100 \text{ eV} - 100 \text{ keV}$ and in the 14 -20 MeV energy range.

4. Unresolved resonance parameters (0.250 - 96.8 keV)

Here we will briefly review the status of unresolved neutron resonance parameters of 243 Am and provide a cross section parameterization of total, capture, elastic and inelastic scattering cross sections. The average resonance parameters were determined as described in [8] to reproduce average cross sections in the energy range of 0.25 keV-96.8 keV. Provided are energy dependent average resonance parameters.

We assume that the the upper energy is 96.8 keV, twice higher than in previous evaluations [8], the lower is 250 eV. We suppose s-, p- and d-wave neutron-nucleus interactions to be effective (see Tables 4.1).

	D_{obs} , eV	Γ_{γ} , meV	$S_0 \times 10^{-4}$	$S_1 \times 10^{-4}$	R, fm
JENDL-4.0	.4356	39			
RIPL	.730	39	.98		
Present	0.621	33	.9009	2.205	9.236

Table 4.1 Average neutron resonance parameters for ²⁴³Am

4.1 Neutron resonance spacing

Neutron resonance spacing *Dobs* was calculated with the phenomenological Ignatyuk' model [28], which takes into account the shell, pairing and collective effects. The main parameter of the model, asymptotic value of level density parameter *a*, was normalized to the observed neutron resonance spacing $D_{obs} = 0.621$ eV. Other parameters are provided in [29].

4.2 Neutron width

Average neutron width is calculated as follows

$$
\left\langle \Gamma_n^U \right\rangle = S_l \left\langle D \right\rangle_J E_n^{\ 1/2} P_l V_n^U, \tag{4.1}
$$

where E_n is the incident neutron energy, P_l is the transmission factor for the 1-th partial wave, which was calculated within black nucleus model, v_n^U is the number of degrees of freedom of the Porter-Thomas distribution. The p-wave neutron strength function $S_1 = 2.205 \times 10^{-4}$ at 250 eV was calculated with the optical model, using the deformed optical potential, described below. Figure 4.1 compares the average reduced neutron widths for the particular (*l, J)-* state, which is excited in the unresolved resonance energy range. The $\langle \Gamma_n^{\text{0U}} \rangle$ $\binom{0.00}{n}$ values for s-wave neutrons in ENDF/B-VII.0 [27] or JENDL-4.0 [13] data file are much less energy-dependent than those of present evaluation.

4.3 Radiative capture width

Energy and angular momentum dependence of radiative capture widths are calculated within a two-cascade γ-emission model with allowance for the $(n, \gamma n')$ [3] and $(n, \gamma f)$ [4, 31] reactions competition to the $(n, \gamma\gamma)$ reaction. The $(n, \gamma\gamma)$ reaction is supposed to be a radiation capture reaction. The radiation capture width was normalized to the value of $\Gamma_{\gamma} = 33$ meV, adopted here to describe the neutron capture cross section data. Detailed treatment is described below.

4.4 Neutron inelastic width

Average neutron inelastic width is calculated as follows

$$
\left\langle \Gamma_{n'}^U \right\rangle_s = S_l \left\langle D \right\rangle_J (E_n - E')^{1/2} P_l (E_n - E') \nu_{n'}^U,
$$
\n(4.2)

where $v_{n'}^U$ is number of degrees of freedom of Porter-Thomas distribution. Excited levels of ²⁴³Am are taken from Nuclear Data Sheets [32].

Fig. 4.1 Reduced neutron width of ²⁴³Am, $l=0$, $J=2$.

4.5 Fission width

Fission widths are calculated within a double-humped fission barrier model by Strutinsky [33]. Energy and angular momentum dependence of fission width is defined by the transition state spectra at inner and outer barrier humps as in [5]. We constructed transition spectra by supposing the triaxiality of inner saddle and mass asymmetry at outer saddle.

4.6 Total cross section in the region 0.25 keV-96.8 keV

Total cross section were calculated with the rigid rotator optical model. Coupled channel parameters, fitting the measured data are those defined for the $^{237}Np+n$ interaction [5]. In the energy ranges 0.15 -20 keV and 20-96.8 keV the optical model calculations of the total cross section were reproduced assuming a decreasing trends of *So, S¹* and *S²* strength function values as the latter and potential radius, which was adopted from the optical model calculations, define total cross section up to E_n = 93.998 keV.

To reproduce the ²⁴³Am total cross section, calculated with the optical model, we assume S_0 value linearly decreasing starting from 0.25 keV to 0.86885 \times 10⁻⁴, while S_I decreases linearly to 1.9090×10^{-4} at 96.8 keV (see Fig. 4.2). The d-wave neutron strength function was assumed to be equal to $S_2 = 1.0909 \times 10^{-4}$.

4.7 Elastic scattering cross section

The elastic scattering cross section is composed of shape elastic (see Fig. 4.3) and compound elastic contributions. Compound elastic scattering cross section estimate is rather insensitive to the ²⁴³Am fission cross section estimate. Present and JENDL-4.0 [13] estimates from 0.25 keV and up to 96.8 keV, shown on Fig. 4.3 differ a lot below 100 keV.

Fig. 4.2 Total cross section of ²⁴³Am.

4.8 Capture cross section

The description of capture cross section data by Weston et al. [11] and Wisshak et al. [12] in the energy range of 0.25 keV–200 keV is very sensitive to the shape of the neutron absorption cross section. It was shown in [5] that around E_n ^{\sim}1 MeV the total cross section of Z-odd target nuclide is virtually insensitive to the lowering/increasing of the neutron absorption cross section. Lowering of the absorption cross section, simulated by the decrease of the imaginary surface potential term *WD*, was cross-checked by the consistency of fission and inelastic scattering cross sections.

Measured data for the ²⁴³Am(n, γ) reaction cross section [11, 12] shown on Figs. 4.4, 4.5 are scattering a lot, or there are a systematic shifts between different data sets. At lower energy the GMA fits are inconsistent with statistical model calculations, defined by estimate of radiation strength function and neutron absorption cross section. Figure 4.5 shows the calculated curve,

Fig. 4.4 Capture cross section of ²⁴³Am.

Fig. 4.5 Capture cross section of ²⁴³Am.

corresponding to the consistent description of the total, fission and inelastic scattering cross section with $\langle \Gamma \gamma \rangle = 33$ meV and $\langle D_{obs} \rangle = 0.621$ eV.

To follow a much higher lying data trend of the GMA-fit one would need rather large values of *s*-wave neutron strength function S0.

The important peculiarity of the calculated ²³⁸U(n, γ) and ²³²Th(n, γ) [3, 4] capture cross sections, Wigner cusp above first excited level threshold, is pronounced in case of calculated ²⁴³Am(n, γ) reaction cross section differently, because of larger number of levels in odd residual ²⁴¹Am nuclide. The pattern of *s-*, *p-* and *d-*wave entrance channel contributions to the capture cross section in the energy range of $0.25 - 96.8$ keV is different from that of ²³²Th [3] or ²³⁸U [4] target nuclides (see Fig. 4.5). That peculiarity may be traced to higher fissility of ²⁴⁴Am compound nuclide as well. In case of ²³⁸U(n, γ) reaction main contribution comes from p-wave neutrons above ~10 keV. The p-wave contribution to the ²⁴³Am(n, γ) reaction cross section is higher than that of *s-*wave above ~30 keV, while that of *d-*wave neutrons is the lowest.

4.9 Inelastic scattering cross section

Calculated inelastic scattering cross section is very close to previous evaluation of ENDF/B-VII.0 [30], but much different from that of JENDL-4.0 [13] (see Fig. 4.7). Conventional ENDF/B processing codes exemplify Hauser-Feshbach-Moldauer formalism. Figure 4.6 shows partial contributions to the inelastic scattering coming from different *(l, J)-*channels. Major contribution, unlike in case of 238 U+n interaction [4], comes from *s*-wave channels (decay of 2⁻ and 3⁻ states), the intermediate comes from *p*-wave channel (decay of $0^+, 1^+, 2^+, 3^+, 4^+$ compound nucleus states) and the lowest comes from d -wave neutrons (decay of 0 , 1 , 2 , 3 , 4 , 5 compound nucleus states). At E_n > 60 keV, the contribution from *p*-wave channel (decay of 0^+ , 1^+ , 2^+ , 3^+ , 4^+ compound nucleus states) becomes the largest, as shown on Fig. 4.7. However, that might be considered as imposed by the fitting procedures employed. Because Hauser-Feshbach-Moldauer formalism is adopted

Fig. 4.6 Inelastic cross section of ²⁴³Am.

Fig. 4.7 Fission cross section of ²⁴³Am.

in conventional ENDF/B processing codes, the direct excitation of the 0.0424 MeV, *J ^π=7/2-* level is not accounted for explicitly. To compensate for that relevant strength function S_2 for inelastic scattering exit channel was increased at 96.8 keV up to 2.989×10^{-4} . That helped to attain, using conventional processing codes, the fit of relevant capture cross section, calculated with the Hauser-Feshbach-Moldauer formalism.

4.10 Fission cross section

Evaluated fission cross section describes the trend, predicted by data [14-27], specifically of Knitter et al. [18], Terayama et al. [17], Fursov et al. [22], Aiche et al. [20]. We estimated fission cross section in the unresolved resonance energy region using for transition state spectra of 244 Am, fission barrier parameters were obtained fitting fission cross section data in the first plateau region (see Fig. 4.8). The fission cross section, calculated with the Hauser-Feshbach-Moldauer formalism, reproduces the GMA evaluation within assigned errors in the incident neutron energy range of 0.25 keV~96.8 keV.

5. Optical potential

Calculated total, elastic scattering and absorption cross sections were obtained with the coupled-channel potential parameters, obtained for the ²³⁷Np, as described in [5]. The experience of describing the capture cross section of 232 Th [3] was the motivation to decrease the real volume potential term V_R by 0.5 MeV. Rotational levels of ground state band $5/2$ ⁻⁻⁷/2⁻-9/2⁻-11/2⁻ are assumed coupled (see Table 5.1).

Deformation parameters were tuned to fit S ^{*o*} and S ^{*I*} strength function values. Optical model potential parameters are defined as follows:

Fig. 6.2 Total and elastic cross section of ²⁴³Am.

Partitioning of the total cross section into absorption (reaction) and scattering cross sections allows get reasonable description of available fission and capture cross sections.

6. Total and elastic scattering cross section

Optical potential fitting Phillips and Howe [34] measured $^{241}Am+n$ total cross section in the energy range of 0.4-25 MeV was adopted for 243 Am+n. In case of ENDF/B-VII.0 [30] the elastic scattering was simply adjusted to balance total and partial cross sections (see Fig. 6.1).

7. Statistical model

We calculated neutron cross sections within Hauser-Feshbach theory, coupled channel optical model and double-humped fission barrier model.

Hauser-Feshbach-Moldauer [35] and Tepel-Hoffman-Weidenmuller [36] statistical theory is employed for partial cross section calculations below emissive fission threshold. Fissioning and residual nuclei level densities as well as fission barrier parameters are key ingredients, involved in actinide neutron-induced cross section calculations.

In case of fast neutron ($E_n \le 6$ MeV) interaction with ²⁴³Am target nucleus, the main reaction channel is the fission reaction and fission cross section data description serves as a major constraint, except those of GMA-fits, for the neutron inelastic scattering and radiative neutron capture cross section estimates. Below there is an outline of the statistical model employed. At incident neutron energy lower than cut-off energy of discrete level spectra, neutron cross sections are calculated with Hauser-Feshbach formalism and width fluctuation correction by Moldauer [35]. For width fluctuation correction only Porter-Thomas fluctuations are taken into account. Effective number of degrees of freedom for fission channel is defined at the higher fission barrier saddle as $v_f^{J\pi} = T_f^{J\pi}$ $T_{\text{fmax}}^{K\pi}$ where $T_{\text{fmax}}^{JK\pi}$ is the maximum value of the fission transmission coefficient. At higher incident neutron energies the Tepel et al. [36] approach is employed, it describes cross section behavior in case of large number of open channels correctly.

7.1 Level Density

Level density is the main ingredient of statistical model calculations. Level density of fissioning, residual and compound nuclei define transmission coefficients of fission, neutron scattering and radiative decay channels, respectively. The level densities were calculated with a phenomenological model by Ignatyuk et al. [28], which takes into account shell, pairing and collective effects in a consistent way

$$
\rho(U, J^{\pi}) = K_{rot}(U, J)K_{vib}(U)\rho_{qp}(U, J^{\pi}), \qquad (7.1)
$$

where quasi-particle level density is defined as

$$
\rho_{qp}\left(U,J^{\pi}\right) = \frac{(2J+1)\omega_{qp}(U)}{4\sqrt{2\pi}\sigma_{\perp}^2 \sigma} \exp\left[-\frac{J(J+1)}{2\sigma_{\perp}^2}\right],\tag{7.2}
$$

 $\mathcal{P}_{qp}(U, J^{\pi})$ is the state density, $K_{rot}(U, J)$ and $K_{vib}(U)$ are factors of rotational and vibrational enhancement of the level density. The closed-form expressions for thermodynamic temperature and other relevant equations which one needs to calculate $\rho(U, J^{\pi})$ provided by Ignatyuk' model.

To calculate the residual nucleus level density at the low excitation energy, i.e. just above the last discrete level excitation energy where $N^{exp}(U) \approx N^{theory}(U)$, we employ a Gilbert-Cameron-type

approach. The procedure is as follows. First, level density parameters are defined, using neutron resonance spacing $\langle D_{obs} \rangle$ estimate for ²⁴³Am target nuclide. Constant temperature level density parameters T_0 , E_0 , U_c (see below for details) are defined by fitting cumulative number of low-lying levels of ²⁴³Am (see Fig. 7.1). Figure 7.2 shows the estimate of cumulative number of low-lying levels of ²⁴⁴Am, obtained using systematic of constant temperature level density parameters *T*o, *E*o, U_c . On this figure levels of odd-odd ²⁴⁴Am nuclide are compared with constant temperature model estimate. The constant temperature approximation of the level density

$$
\rho(U) = \frac{dN(U)}{dU} = \frac{1}{T} \exp\left(\frac{U - U_o}{T}\right) \tag{7.3}
$$

is extrapolated up to the matching point U_c to the $\rho(U)$ value, calculated with a phenomenological model by Ignatyuk with the condition

$$
U_c = U_o - Tln(T\rho(U_c)).
$$
\n(7.4)

In this approach $U_o \approx -m\Delta_o$, where Δ_o is the pairing correlation function, $\Delta_o = 12/\sqrt{A}$, A is the mass number, $m = 2$ for odd-odd, 1 for odd-even nuclei, i.e. U_o has the meaning of the odd-even energy shift. The value of nuclear temperature parameter *T* obtained by the matching conditions of Eq. (7.4) at the excitation energy *Uc*.

The modeling of total level density

$$
\rho(U) = K_{rot}(U, J)K_{vib}(U)\frac{\omega_{qp}(U)}{\sqrt{2\pi}\sigma} = \frac{1}{T}\exp\left(\frac{U - U_o}{T}\right)
$$
\n(7.5)

in Gilbert-Cameron-type approach looks like a simple renormalization of quasi-particle state density $\omega_{qp}(U)$ at excitation energies U< U_c . The cumulative number of observed levels for odd-even 243 Am and odd-odd nuclide 244 Am [32] are compared with constant temperature approximations for ²⁴³Am and ²⁴⁴Am on Figs. 7.1 and 7.2, respectively. Missing of levels above ~ 0.5 MeV is pronounced in case ²⁴³Am.

Few-quasi-particle effects due to pairing correlations are essential for state density calculation at low intrinsic excitation energies only for equilibrium ²⁴³Am deformations. Few-quasiparticle effects in fissioning nuclide ²⁴⁴Am are unimportant because of its odd-odd nature.

The partial n-quasi-particle state densities for odd 243 Am, which sum-up to intrinsic state density of quasi-particle excitations, could be modelled using the Bose-gas model prescriptions [37, 38]. The intrinsic state density of quasi-particle excitations $\omega_{qp}(U)$ could be represented as a sum of n-quasi-particle state densities $\omega_{nap}(U)$:

$$
\omega_{qp}(U) = \sum_{n} \omega_{nqp}(U) = \sum_{n} \frac{g^{n}(U - U_{n})^{n-1}}{((n/2)!)^{2}(n-1)!},
$$
\n(7.6)

where $g = 6a_{cr}/\pi^2$ is a single-particle state density at the Fermi surface, n is the number of quasiparticles. The important model parameters are threshold values *U*ⁿ for excitation of n-quasi-particle configurations employed, as applied for fission, inelastic scattering or capture reaction calculations, is provided in [39, 40].In case of and odd-odd nucleus ²⁴²Am Gilbert-Cameron-type approximation of $\rho(U)$ is employed. Nuclear level density $\rho(U)$ of odd nuclide ²⁴¹Am at equilibrium deformation, as compared with the Gilbert-Cameron-type approximation of $\rho(U)$ is shown on Fig. 7.3. The arrows on the horizontal axis of Fig. 7.3 indicate the excitation thresholds of odd n-quasi-particle configurations.

Fig. 7.1 Cumulative sum of levels of ²⁴³Am.

Fig. 7.2 Cumulative sum of levels of ²⁴⁴Am.

Fig. 7.3 Level density of ²⁴³Am.

Main parameters of the level density model for equilibrium, inner and outer saddle deformations are as follows: shell correction δW , pairing correlation functions Δ and Δ_f , at equilibrium deformations $\Delta_0 = 12/\sqrt{A}$, quadrupole deformation ε and momentum of inertia at zero temperature F_0/h^2 are given in Table 7.1. For ground state deformations the shell corrections were calculated as $\delta W = M^{\text{exp}} - M^{\text{MS}}$, where M^{MS} denotes liquid drop mass (LDM), calculated with Myers-Swiatecki parameters [41], and M^{exp} is the experimental nuclear mass. Shell correction values at inner and outer saddle deformations $\delta W_f^{A(B)}$ are adopted following the comprehensive review by Bjornholm and Lynn [42].

*) for axially asymmetric deformations, 1.5 MeV for axially symmetric deformations; **) $\delta = \Delta_f$ - Δ_o value is defined by fitting fission cross section in the plateau region.

7.2 Fission cross section

Fission data, processed with GMA-code [9, 10], are used as a major constraint for capture, elastic and inelastic scattering, (n,2n) and (n,3n) cross sections as well as secondary neutron spectrum estimation. Description of measured fission cross section might justify a validity of level density description and fission barrier parameterization.

7.2.1 Fission Channel

Fission barrier of Am is double-humped, in the first ''plateau'' region and at higher energies we can use double-humped barrier model and relevant barrier parameters. Even at lower energies we could describe the general shape of the fission cross section starting from 0.250 keV.

Neutron-induced fission in a double humped fission barrier model is a two-step process, i.e. a successive crossing over the inner hump A and over the outer hump B. Hence, the transmission coefficient of the fission channel $T_f^{J\pi}(U)$ represented as

$$
T_f^{J\pi}(U) = \frac{T_{fA}^{J\pi}(U)T_{fB}^{J\pi}(U)}{T_{fA}^{J\pi}(U) + T_{fB}^{J\pi}(U)}.
$$
\n(7.7)

The transmission coefficient $T_f^{\text{J}\pi}(U)$ is defined by the level density $\rho_{f_i}(\varepsilon, J, \pi)$ of the fissioning nucleus at the inner and outer humps $(i = A, B, respectively)$:

$$
T_{fi}^{J\pi}(U) = \sum_{K=-J}^{J} T_{fi}^{JK\pi}(U) + \int_0^U \frac{\rho_f(\varepsilon, J, \pi) d\varepsilon}{1 + \exp\left(2\pi(E_{fi} + \varepsilon - U)/h\omega_i\right)},
$$
(7.8)

where the first term denotes the contribution of low-lying collective states and the second term that coming from the continuum levels at the saddle deformations, *ε* is the intrinsic excitation energy of fissioning nucleus. The first term contribution due to discrete transition states depends upon saddle symmetry. The total level density $\rho_{\hat{f}}(\varepsilon, J, \pi)$ of the fissioning nucleus is determined by the order of symmetry of nuclear saddle deformation.

Inner and outer fission barrier heights and curvatures as well as level densities at both saddles are the model parameters. They are defined by fitting fission cross section data at incident neutron energies below emissive fission threshold. Fission barrier height values and saddle order of symmetry are interdependent. The symmetry of nuclear shape at saddles was defined by Howard and Moller [43] within shell correction method (SCM) calculation. We adopt the saddle point asymmetries from SCM calculations. According to shell correction method (SCM) calculations of Howard and Moller [43] the inner barriers were assumed axially asymmetric. Outer barriers for the americium nuclei are assumed mass-asymmetric.

7.2.2 Fission transmission coefficient, level density and transition state spectrum

Adopted level density description allows describe shape of measured fission cross section data of ²⁴³Am (see Figs. 7.4-7.7). One- and two-quasi-particle states in odd residual nuclide ²⁴³Am could be excited. The transition state spectra of odd-odd ²⁴⁴Am nuclide for the band-heads of Table 7.2 were constructed using values of F_o/h^2 at the inner and outer saddles shown in Table 7.1.

We construct the discrete transition spectra up to 175 keV, using collective states of Table 7.2. The discrete transition spectra, as well as continuous level contribution to the fission

Fig.7.4 Fission cross section of ²⁴³Am.

Fig. 7.5 Fission cross section of ²⁴³Am.

Fig. 7.6 Fission cross section of 243 Am.

We construct the discrete transition spectra up to 175 keV, using collective states of Table 7.2. The discrete transition spectra, as well as continuous level contribution to the fission transmission coefficient are dependent upon the order of symmetry for fissioning nucleus at inner and outer saddles. With transition state spectra defined as described, the fission barrier parameters are obtained.

Inner saddle A		Outer saddle B		
K^{π}	$E_{K\pi}$, MeV	K^{π}	$E_{K\pi}$, MeV	
2^+		2^+		
3^+	0.05	3^+	0.05	
\mathcal{F}	0.05	3.	0.05	
	0.05		0.05	

Table 7.2 Transition spectra band-heads, Z-odd, N-even nuclei

7.3 Fission data analysis

Fission cross section is calculated within statistical model from 0.25 keV up to the emissive fission threshold. Measured fission data [14-27] analysis was accomplished within GMA approach [9, 10], as described above. Calculated cross section is consistent with data by Wsshak et al. [12], Knitter et al. [18], Terayama et al. [17], Fursov et al. [22], Fomushkin et al. [21, 23], Aiche et al. [20], Seeger et al. [44].

Statistical model calculations in the energy of .25 keV~6 MeV are maintained, calculated cross sections deviate from the GMA evaluation within the GMA-estimated uncertainties, except part of the threshold range.

NEUTRON ENERGY, MeV

Fig. 7.9 Inelastic cross section of $2nd$ level of $2⁴³Am$.

Fig. 7.10 Inelastic cross section of $3rd$ level of $2⁴³$ Am.

Fig. 7.11 Inelastic cross section of ²⁴³Am.

Fig. 7.12 Inelastic cross section of ²⁴³Am(continuum contribution)..

Fig. 7.13 Inelastic cross section of ²⁴³Am(continuum contribution)..

We fit the trend of the fission cross section data above $E_n \approx 3$ MeV increasing the correlation function value at outer saddle, which controls the 243 Am (n, f) cross section shape. For incident neutron energies up to $E_n \approx 3$ MeV the threshold shape is roughly reproduced by varying the density of one-quasi-particle states of the residual nuclide ²⁴³Am (see Figs. 7.4-7.6). Smooth statistical model calculations are adopted as evaluated fission cross section in the energy range of 0.15 keV~5.5 MeV.

7.4 Inelastic scattering

Fission data fit largely defines the compound inelastic neutron scattering contribution to the total inelastic scattering cross section. The relative contribution of direct discrete level excitation cross sections is much higher than in case of say ²³⁸U target nuclide due to much higher fission competition to the compound neutron scattering. That explains the sensitivity of the 243Am compound inelastic scattering cross section to the fission competition and modeling of the residual nuclide level density.

7.4.1 Neutron Channel

The lumped transmission coefficient of the neutron scattering channel is given by equation

$$
T_n^{J\pi}(U) = \sum_{l'j'q'} T_{l'j'}^{J\pi}(E - E_{q'}) + \sum_{l'j'l'} \int_0^{U - U_c} T_{l'j'}^{J\pi}(E')\rho(U - E', I'^{\pi})dE', \qquad (7.9)
$$

where $\rho(U - E', I'^{\pi})$ is the level density of the residual nucleus. Levels of residual nuclide ²⁴¹Am are provided in Table 5.1. The entrance channel neutron transmission coefficients $T_{\mu\nu}^{J\pi}(E)$ $\int_{l'j'}^{J\pi} (E')$ are calculated within a rigid rotator coupled channel approach. The compound and direct inelastic scattering components summed incoherently. The exit channel neutron transmission coefficients $T^{J\pi}_{l'j'}(E')$ $\int_{l'j'}^{J\pi}(E')$ were calculated using the re-normalized deformed optical potential of entrance channel without coupling, which describes a neutron absorption cross section.

7.4.2 Ground State Rotational Band

Predicted discrete level excitation cross section shape, calculated within a rigid rotator model, depends upon optical potential used. We assume strong missing of levels above excitations of 0.313 MeV (see Fig. 7.1), so only 10 excited levels up to this excitation energy were included when calculating inelastic scattering cross sections. Predicted discrete level excitation cross section shape, calculated within a rigid rotator model, strongly depends upon optical potential used. Calculated compound contribution is controlled mainly by fission competition (see Figs. 7.8-7.13). Figures 7.8, and 7.10 show that direct scattering essentially defines the excitation cross section of J^π=7/2⁻ and J^π=9/2⁻ levels of the ground state band levels at $E_n \ge 1$ MeV. Discrepancies with previous evaluations are due to both compound and direct contributions differences. The compound component tends to be zero above incident neutron energy of ~3 MeV (see Fig. 7.9).

7.4.3 Total inelastic cross section

Direct inelastic contributions added incoherently to Hauser-Feshbach calculated values of compound nucleus inelastic scattering cross sections. Present calculation based on the fits of the fission cross section. The evaluated inelastic cross sections of ENDF/B-VII.0 [30] and JENDL-4.0 [13] evaluations are in severe disagreement with our evaluation in the energy range $0.30 \text{ MeV} - 2$ MeV) (see Fig. 7.11).

Upward trend of the inelastic data at $E_n \ge 1.5$ MeV might be explained by the sharp increase of the level density of the residual nuclide 243 Am due to the onset of three-quasi-particle excitations [37, 38], that conclusion is qualitatively supported by the measured data by Kornilov et al [45] for 237 Np target nuclide [5] (see Figs. 7.11-7.13). The total inelastic scattering cross section of JENDL-4.0 [13] is much lower, than present evaluation. The continuum levels contribution to the total inelastic scattering cross section is shown on Figs. 7.12, 7.13.

7.5 Capture cross sections

We have demonstrated by the analysis of measured capture cross sections of ²³⁸U(n, γ), ²³²Th(n, γ) and ²³⁷Np(n, γ) [3, 4, 5] that neutron capture data could be described within a Hauser-Feshbach-Moldauer [35] statistical model, reproducing delicate variations of the measured cross sections with the increase of the incident neutron energies. Specifically, in a few-keV energy region calculated capture cross section is defined by the radiative strength function value $S_{\gamma} = \Gamma_{\gamma}/D$. At incident neutron energies above $E_n \approx 100 \text{ keV}$ calculated capture cross section shape is defined by the energy dependence of the radiative strength function S_y . Energy dependence of S_y is controlled mainly by the energy dependence of the level density of the compound nuclide ²⁴⁴Am. Alongside with neutron emission at the second γ -cascade rather low fission threshold for the ²⁴⁴Am nuclide defines appreciable competition of fission [31], i.e. after first γ-quanta emission.

Then "true" capture reaction cross section $(n, \gamma\gamma)$ is defined using transmission coefficient $T^{J\pi}_{\nu}(E)$ $\chi^{J\pi}_{\gamma\gamma}(E)$, which is defined in a two-cascade approximation as

$$
T_{\gamma}^{J\pi}(E) = \frac{2\pi C_{\gamma 1}}{3(\pi \hbar c)^2} \int_0^{E_{\pi}+B_{\pi}} \varepsilon_{\gamma}^2 \sigma_{\gamma}(\varepsilon_{\gamma}) \sum_{I=|J-1|}^{I=J+1} \rho \big(U-\varepsilon_{\gamma},I,\pi\big) \frac{T_{\gamma}^{1\pi}(U)}{T_{f}^{1\pi}(U)+T_{n}^{1\pi}(U)+T_{\gamma}^{1\pi}(U)} d\varepsilon_{\gamma}. \tag{7.10}
$$

The last term of the integrand describes the competition of fission, neutron emission and γ -emission at excitation energy $(U - \varepsilon_\gamma)$ after emission of first γ -quanta, $C_{\gamma 1}$ is the normalizing coefficient. That means that transmission coefficients $T_f^{I\pi}(U)$, $T_{\pi'}^{I\pi}(U)$, $T_{\nu}^{I\pi}(U)$ γ $\pi(\mathbf{I}I)$ $\mathbf{T}^{I\pi}(\mathbf{I}I)$ $\mathbf{T}^{I\pi}$ $T_f^{\text{I}\pi}(U), T_{n'}^{\text{I}\pi}(U), T_{\gamma}^{\text{I}\pi}(U)$ are defined at excitation energy $(U - \varepsilon_{\gamma})$. The neutron emission after emission of first γ-quanta strongly depends on the ²⁴¹Am residual nuclide level density at excitations around the pair-breaking threshold in odd nuclide U3. The contribution of (n, γ f)-reaction to the fission cross section is defined by $T_{\gamma}^{J\pi}(E)$ *f* $\chi_{\text{f}}^{J\pi}(E)$ value. The energy dependence of (n γ f) reaction transmission coefficient $T_{\alpha}^{J\pi}(E)$ *f* $\chi^{J\pi}_{\pi}(E)$ was calculated with the expression

$$
T_{\mathcal{J}}^{J\pi}(E) = \frac{2\pi C_{\gamma 1}}{3(\pi\hbar c)^2} \int_{0}^{E_{n}+B_{n}} \varepsilon_{\gamma}^{2} \sigma_{\gamma}(\varepsilon_{\gamma}) \sum_{I=|J-1|}^{I=J+1} \rho \big(U-\varepsilon_{\gamma},I,\pi\big) \frac{T_{f}^{I\pi}(U)}{T_{f}^{I\pi}(U)+T_{n}^{I\pi}(U)+T_{\gamma}^{I\pi}(U)} d\varepsilon_{\gamma}.
$$
 (7.11)

Competition of (n, γn') reaction is taken into account in a similar way. Above neutron energy 5.5 MeV capture cross section is assumed to be 0.001 barn.

Trends of the measured data by Weston et al. [11] and Wisshak et al. [12] are inconsistent with each other. Measured data for the ²⁴³Am(n, γ) reaction cross section [11, 12] shown on Figs. 3.1, 3.2 are scattering a lot, or there are a systematic shifts between different data sets. The GMA-fit follows the data by Weston et al. [11]. In the incident neutron energy range of 20-300 keV, the calculated capture

Fig. 7.14 Capture cross section of ²⁴³Am

Fig. 7.15 Capture cross section of ²⁴³Am

cross section closely follows the GMA-fit. The trend predicted by the data of Wisshak et al. [12] is divergent with the former one at *En*< 20 keV. However, the data in the range of 10~100 keV support the theoretical calculation, based on consistent description of fission measured data, as well as the estimate of radiation strength function ($\langle \langle \Gamma_{\gamma} \rangle = 33$ meV and $\langle D_{obs} \rangle = 0.621$ eV) and absorption cross section (see Figs. 7.14, 7.15).

Finally, Fig. 7.15 shows calculated capture cross section and competition of ²⁴³Am(n, γ f) and ²⁴³Am (n, γn') reactions to the "true" capture reaction ²⁴³Am(n, γ γ), they define the capture cross section shape at $E_n \geq 2$ MeV.

7.6 Branching ratio of short-lived 244mAm (1-) and long-lived 244gAm (6-) states of ²⁴⁴Am

The neutron capture reaction ²⁴³Am(n, γ) populates either the 10.1-h ground state ^{244g}Am or the ^{244m}Am isomer with T_{1/2} = 26 min. Experimental information on (n,γ) reaction excitation function for the target actinide 243 Am [1, 11, 12, 46-60] is devoted to measurements of thermal capture cross sections. Only in two experiments [11, 12] the ²⁴³Am(n, γ)^{244m+g}Am reaction excitation function was investigated in the energy range of 0.258 – 226 keV. We analyzed and corrected experimental cross section data to modern standards and evaluated the isomeric cross section ratio for the yields of metastable state (t_{1/2}=26 min) ^{244m}Am, having spin J^{π}=1⁻ and ground state (t_{1/2}=10.1 h) state ^{244g}Am, having spin J^π=6⁻: ²⁴³Am(n, γ)^{244g}Am/²⁴³Am(n, γ)^{244m+g}Am.

All reviewed experimental data, if possible, were renormalized to the new standards for the decay data and cross sections for the monitor reactions. Direct measurements of the 243 Am(n, γ)^{244m}Am reaction cross-section is not feasible. Analysis of the experiments for determination of the 243 Am thermal capture cross-sections show, that most representative are experimental data by Gavrilov et al. [56] and Marie et al. [1]. Evaluated 243 Am thermal capture crosssections are given below in Table 7.1.

Cross-section	Evaluated value,		
᠊ᡪᢅᢄ	$5.2 \pm 31.62\%$		
	$76.39 \pm 6.15\%$		
τ^{m+g}	$81.59 + 3.75\%$		

Table 7.1. Evaluated the ²⁴³Am(n, γ)^{244m}Am, ²⁴³Am(n, γ)^{244g}Am and ²⁴³Am(n, γ)^{244m(g)}Am cross sections at E_n = 0.0253 eV

The isomeric cross-section ratio $\sigma^{g}(E_n)/\sigma^{m+g}(E_n)$ for the reaction $^{243}Am(n,\gamma)$ may be determined from the evaluated experimental data at the thermal point 0.0253 eV and in the resonance energy range between 0.5 eV and about 1 MeV on the basis of experimental data by Schuman [52].

Calculated from the evaluated experimental data (Table 7.1) isomeric cross-section ratio at 0.0253 eV is equal to $\sigma^{g}(0.0253 \text{ eV})/\sigma^{m+g}(0.0253 \text{ eV})$ = 0.064 \pm 7.20%. The isomeric cross-section ratio obtained in the resonance energy range from experimental data by Schuman [52] equals to $\sigma^{g}(E_n)/\sigma^{m+g}(E_n) = 0.051 \pm 13.07\%$, there E_n ranges from 0.5 eV to ~1 MeV. It is necessary to mention, that measured by Schuman [52] thermal caprure cross section $\sigma^{g}(0.0253 \text{ eV}) = 5.9 \text{ b} \pm 33\%$ agrees satisfactory with new experimental data by Marie et al. [1] σ ^g(0.0253 eV) = 5.2 b \pm 31.62%.

The neutron capture reaction ²⁴³Am(n, γ) populates either the T_{1/2} = 10.1h ground state ^{244g}Am with $J^{\pi}=1^-$ or the ^{242m}Am isomer $J^{\pi}=5^-$ with $T_{1/2}=26$ min. The ground state ^{244g}Am β^- -decays to ²⁴⁴Cm via ^{242m}Am(n, γ)²⁴³Am(n,γ)^{244g}Am(β⁻)²⁴⁴Cm. It gives a path for the ²⁴⁴Cm yield also via ^{242m}Am(n, γ)²⁴³Am(n, γ)^{244m}Am(β⁻(ε))²⁴⁴Cm(²⁴⁴Pu).

Ground $242g$ Am and isomer $242m$ Am states of the residual nuclide 242 Am are excited in the

reaction $243 \text{Am}(n, 2n)$ $242 \text{g}(m)$ Am as well. The same approach as in case of capture reaction is applied to predict the branching ratio $r(E_n) = \sigma_{n2n}^g(E_n) / \sigma_{n2n}^m(E_n)$ in ²³⁷Np(n, 2n) reaction, as described in [5]. The branching ratio $r(E_n) = \sigma_\gamma^s(E_n) / \sigma_\gamma^m(E_n)$ *n* $r(E_n) = \sigma_\gamma^s(E_n) / \sigma_\gamma^m(E_n)$ from thermal energy to 20 MeV could be defined by the ratio of the populations of two lowest states in 244 Am [61]. These populations are defined by the γ-decay of the excited states, described by the kinetic equation, developed by Strutinsky et al. [62]. The branching ratio $r(E_n)$ is defined by the ratio of the populations of the two lowest states, ^{244g}Am, with spin $J = 6$ and ^{244m}Am, with spin $J = 1$. The integral equation in the code STAPRE [63] solved as a system of linear equations, the integration range is binned, in the assumption that there are no γtransitions inside the bins as described in [5].

The isomer branching ratio depends mostly on the low-lying levels scheme and relevant γtransitions probabilities. Though experimental data are available for 244 Am [32], we will use a simplified approach, since level scheme and gamma-decay branching ratios are still incomplete. Modeling of low-lying levels of ²⁴⁴Am in [61] is accomplished based on the assumption that ground and first few excited states are of two-quasi-particle nature. For actinides with quadrupole deformations the superposition principle is usually adopted, the band-head energies of the doublyodd nucleus are generated by adding to the each unpaired configuration (Ω_p, Ω_n) , as observed in the isotopic/isotonic (A-1) nucleus, the rotational energy contribution and residual (n−p) interaction energy contribution. The angular momenta of neutron and proton quasi-particles could be parallel or anti-parallel. In the independent quasi-particle model the two-quasi-particle states, $K^+ = |K_n + K_p|$ and $K^- = |K_n - K_p|$, are degenerate. Gallaher-Moshkowski doublets [61] appear because of (n−p) residual interaction. Figure 7.16 shows employed band-head energies for the two-quasi-particle states expected in the odd-odd nuclide ²⁴⁴Am up to 700 keV. The spectroscopic properties of two pairs of proton and neutron single particle states were derived from those experimentally observed in the isotopic $(Z=95)$ and isotonic $(N=147)$ odd-mass nuclei with mass $(A-1)$. Figure 7.16 shows levels expected, which have similar ordering as experimentally observed [32]. For the band-heads, shown on Figure 7.16, the rotational bands were generated as

$$
E_{JK\pi} = E_{JK} + 5.5[J(J+1) - K(K+1)].
$$
\n(7.10)

Obviously, the schema presented on Fig. 7.16 does not represent a complete set to allow the calculation of absolute yields of ²⁴³Am (n,γ)^{244m}Am and ²⁴³Am (n,γ)^{244g}Am reactions. Rotational bands were constructed up to 700 keV excitation, modeling levels with spins $J^{\pi} \le 10$, in total up to 70 levels. It was shown in [23], that simple estimate of the number of levels in odd-odd nuclei as

$$
N(U) = e^{2\Delta_0 / \sqrt{U - 1}}, \tag{7.11}
$$

predicts up to 280 level at $U \sim 700$ keV, $T=0.388$ MeV, $\Delta = 12/A^{1/2}$, MeV. We assume that the modeled angular momentum distribution would not be much different from realistic estimates. Since the complete data on the γ-transitions are missing, we assumed the simple decay scheme: only

E1, E2 and M1, M2, M3 transitions are allowed in a continuum excitation energy range. Inter-band transitions are not allowed, i.e., only γ-transitions within the rotational bands are possible. In that approach the populations of the lowest five level doublets could be calculated. Then we assumed that the transition to the isomer state $J^{\pi} = 6^-$ or low-spin, short-lived ground state $J^{\pi} = 1^-$ is defined by the "minimal multipolarity" rule. That means the states with spins $J > 3$ should populate the ground state, while those with $J \leq 3$ should feed the isomer state. Then the branching ratio is obtained as the ratio of the populations, derived from Eq. (7.12):

Fig. 7.17 Isomeric cross section ratio for the ²⁴³Am(n, γ)^{242g}Am and ²⁴³Am(n, γ)^{242(m+g)}Am reactions

$$
r(E_n) = \frac{\sum_{J > (J_i + J_s)/2} W(U, J^{\pi})}{\sum_{J \ge (J_i + J_s)/2} W(U, J^{\pi})}
$$
(7.12)

Figure 7.17 show the branching ratio, calculated for the modeled level schema, presented at Fig. 7.16.

The measured data reproduced assuming lihear extrapolation up to incident neutron energy 100 keV.

8. Fission cross section above emissive fission threshold

At incident neutron energies when fission of 243 Am or 242 Am nuclides is possible, as well as fission of ²⁴⁴Am, after emission of 1 or 2 pre-fission neutrons, the observed ²⁴³Am(n, F) fission cross section is a superposition of non-emissive or first chance fission of ²⁴⁴Am

$$
\sigma_{\rm nf}(E_{\rm n}) = q(E_{\rm n}) \frac{\pi \hbar^2}{2(2I+1)} \sum_{IJ_{\pi}} (2J+1) T_{\rm l} (E_{\rm n}) P_{\rm f}^{J\pi}(E_{\rm n}), \tag{8.1}
$$

and xth -chance fission contributions as

$$
\sigma_{\text{nF}}(E_n) = \sigma_{\text{nf}}(E_n) + \sum_{x=1}^{X} \sigma_{\text{n,xnf}}(E_n).
$$
\n(8.2)

The contributions to the observed fission cross section $\sigma_{n,xnf}(E_n)$, coming from (n, *x*nf), *x*= 1, 2, 3...X, fission of relevant equilibrated americium nuclei are weighted with a probability of *x* neutron emission before fission. These cross sections are calculated as

$$
\sigma_{n,\text{xnf}}(E_n) = \sum_{J\pi}^{U_{\text{max}}}\int_{0}^{U_{\pi\text{ax}}} W_{x+1}^{J\pi}(U) P_{f(x+1)}^{J\pi}(U) dU , \qquad (8.3)
$$

where $W_x^{J\pi}$ is the population of $(x+1)^{th}$ nucleus at excitation energy *U* after emission of *x* neutrons, excitation energy U_{max} is defined by the incident neutron energy E_n and the energy, removed from the composite system ²⁴⁴Am by the ²⁴³Am(n, *xnf*) pre-fission neutrons.

Contribution of first-chance fission $\sigma_{\rm nf}(E_n)$ is defined by the pre-equilibrium emission of the first neutron and the fission probability P_f of the ²⁴²Am nuclide

$$
\sigma_{f1} = \sigma_c (1 - q(E)) P_{f1}. \tag{8.4}
$$

Once the contribution of first neutron pre-equilibrium emission $q(E)$ is fixed, the firstchance fission probability *Рf1* of the ²⁴⁴Am is defined by the level densities of fissioning ²⁴⁴Am and residual ²⁴³Am nuclides. Actually, it depends on the ratio of shell correction values $\delta W_{A(B)}$ and δW_n . Different theoretical calculations of the shell corrections as well as of the fission barriers vary by 1-2 MeV. The same is true for the experimental shell corrections, which are obtained with a smooth component of potential energy calculated according to the liquid-drop or droplet model. However the isotopic changes of $\delta W_{f(A|B)}$ and δW_n are such that P_{fI} viewed as a function of the difference $(\delta W_{A(B)} - \delta W_n)$ is virtually independent on the choice of smooth component of potential energy. Therefore, we shall consider the adopted $\delta W_{A(B)}$ estimates to be effective, provided that δW_n are obtained with the liquid drop model. In the first "plateau" region and at higher energies we can safely use double-humped barrier model and relevant barrier parameters (see Table 8.1).

Consistent description of a most complete set of measured data on the (n, F), (n,2n), (n,3n) and $(n,4n)$ reaction cross sections for the ²³⁸U target nuclide up to 20 MeV $\overline{64}$ enables one to consider the estimates of first neutron spectra emitted from the composite ²⁴⁴Am nuclide as fairly

realistic. In case of 243 Am(n, F) cross section, for which there are systematic discrepancies in measured data [12−27], calculated cross section is consistent with data by Knitter et al.[18], Fursov et al. [22], Fomushkin et al. [21, 23], Terayama et al. [17], Aiche et al. [20].

Table 8.1 Fission barrier parameters of Am nuclei

Figures 8.1-8.2 demonstrate the fission data fit from 100 keV up to 20 MeV. The contributions of emissive $243 \text{Am}(n, n f)$ and $243 \text{Am}(n, 2n f)$ fission to the total fission cross section are shown.

9. (n,2n) and (n,3n) cross section

The reaction chain ²⁴³Am(n,2n)^{242m(g)}Am was used to measure the yield of lower spin ^{242g}Am state, by Norris-Gancartz (1982) [65] at \sim 15 MeV. From the ratio of the calculated yields at \sim 15 MeV it follows that the yield of low spin state is higher than that of high spin state. Near the threshold the ratio is defined by the relative position of states and feeding from the higher laying levels.

9.1 Branching ratio of short-lived 242gAm (1-) and long-lived 242mAm (5-) states in ²⁴³Am(n,2n) reaction

Ground $242g$ Am and isomer $242m$ Am states of the residual nuclide $242Am$ are excited in the reaction ²⁴³Am(n, 2n)^{242g(m)}Am. The ²⁴³Am(n,2n)^{242m(g)}Am reaction populates either the T_{1/2} = 16h ground state ^{242g}Am with J^π=1⁻ or the ^{242m}Am isomer J^π=5⁻ with $T_{1/2}$ =141y. The ground state ^{242g}Am mostly β⁻-decays to ²⁴²Cm, or goes to ²⁴²Pu via electron capture. The yield of the ^{242g}Am short-lived ground state in the reaction chains ²⁴³Am(n,2n)^{242g}Am(β ⁻²⁴²Cm and ²⁴¹Am(n, γ) ^{242g}Am(β⁻)²⁴²Cm influences the α–activity and neutron activity of the spent fuel due to emerging nuclides 242 Cm and 238 Pu. The yield of the 242 ^mAm long-lived isomer state, which due to large and odd value of $J^{\pi}=5^-$ may decay to ^{242g}Am via isomeric transition IT only, emerging in reactions ²⁴³Am(n,2n)^{242g}Am(β ⁻²⁴²Cm and ²⁴¹Am(n, γ)^{242m}Am influences the neutron activity of the spent fuel due to spontaneous fission of $242m$ Am. It gives a path for the 244 Cm yield via ^{242m}Am(n,γ)²⁴³Am(n,γ)^{244m}Am(β⁻(ε))²⁴⁴Cm(²⁴⁴Pu) or ^{242m}Am(n,γ)²⁴³Am(n,γ)^{244g}Am(β⁻)²⁴⁴Cm. If not the forbidden β^- -decay of ^{242m}Am state, the major path for the ²⁴⁴Cm build-up, would be closed.

The approach applied for the modeling ratio of the yields of short-lived (1⁻) and long-lived (6⁻) of ²³⁷Np(*n*,2*n*)^{236s(l)}Np reaction $r(E_n) = \sigma_{n2n}^l(E_n)/\sigma_{n2n}^s(E_n)$ *n* $r(E_n) = \sigma_{n2n}^l(E_n) / \sigma_{n2n}^s(E_n)$ from threshold energy up to 20 MeV allowed to infer the yields of the short-lived state ^{236}Np in $^{237}Np(n,2n)$ reaction. The consistent description of the data

base on cross sections ²³⁷Np(n,F), ²³⁷Np(n,2n)^{236s}Np was achieved [5]. The branching ratio $r(E_n)$ was obtained by modeling the residual nuclide ²³⁶Np levels. Excited levels of ²³⁶Np are modeled using predicted Gallher-Moshkowski doublets.

In case of ²⁴³Am(n,2n)^{242m(g)}Am reaction the branching ratio $r(E_n) = \sigma_{n2n}^m(E_n) / \sigma_{n2n}^g(E_n)$ n ^{*y*} o_{n2n} $r(E_n) = \sigma_{n2n}^m(E_n) / \sigma_{n2n}^g(E_n)$ and are of interest. The branching ratio $r(E_n) = \sigma_{n2n}^m(E_n) / \sigma_{n2n}^g(E_n)$ from threshold energy to 20 MeV could be defined by the ratio of the populations of two lowest states in 242 Am [61]. These populations are defined by the γ -decay of the excited states, which is described by the kinetic equation, developed by Strutinsky et al. [62]. The branching ratio $r(E_n)$ is defined by the ratio of the populations of the two lowest states, ^{242g}Am, with spin $J = 1^-$ and ^{242m}Am, with spin $J = 5^-$.

The γ-decay of the excited nucleus described by the kinetic equation $[46]$ as further developed by Dovbenko et al. [66]:

$$
\frac{\partial \omega_k(U, J^\pi, t)}{\partial t} = \sum_{J^\pi, J_0}^{U_g} \omega_{k-1}(U', J^{\pi\tau}, t) \frac{\Gamma_\gamma(U', J^{\pi\tau}, U, J^\pi)}{\Gamma(U', J^{\pi\tau})} dt - \omega_k(U, J^\pi, t) \frac{\Gamma_\gamma(U, J^\pi)}{\Gamma(U, J^\pi)},
$$
(9.1)

here $\omega_k(U, J^{\pi}, t)$ is the population of the state J^{π} at excitation U at time t, after emission of *k* γ quanta; $\Gamma_{\gamma}(U', J^{\pi}, U, J^{\pi})$ is the partial width of γ -decay from the (U', J^{π}) to the state (U, J^{π}) , while $\Gamma(U, J^{\pi})$ is the total decay width of the state (U, J^{π}) . For any state (U, J^{π}) with the excitation energy $0 \le U \le U_g$, the initial population is

$$
\omega_k(U, J^{\pi}, t = 0) = \delta_{k_0} \omega_0(U, J^{\pi}).
$$
\n(9.2)

That equation means in the initial state we deal with the ensemble of states (U, J^{π}) , excited in ²⁴³Am(n,2n) reaction. Integrating the Eq. (9.1) over *t*, one gets the population $W(U, J^{\pi})$ of the state (U, J^{π}) after emission of *k* γ-quanta:

$$
\omega_k(U, J^\pi, \infty) - \omega_k(U, J^\pi, 0) = \sum_{J' \pi} \int_{U}^{U_s} \frac{\Gamma_\gamma(U', J^\pi', U, J^\pi)}{\Gamma(U', J^\pi)} \int_0^\infty \omega_{k-1}(U', J^\pi', t) dt dU' - \frac{\Gamma_\gamma(U, J^\pi)}{\Gamma(U, J^\pi)} \int_0^\infty \omega_k(U, J^\pi, t) dt
$$
\n(9.3)

Denoting the population of the state (U, J^{π}) after emission of *k* γ -quanta

$$
W_k(U, J^{\pi}) = \frac{\Gamma_{\gamma}(U, J^{\pi})}{\Gamma(U, J^{\pi})} \int_0^{\infty} \omega_k(U, J^{\pi}, t) dt,
$$
\n(9.4)

and taking into account the condition that $\omega_k(U, J^{\pi}, \infty) = 0$ for any state, belonging to ensemble (U, J^{π}) , Eq. (9.3) could be rewritten as

$$
W_k(U, J^{\pi}) = \sum_{J:\pi} \int_{U}^{U_s} \frac{\Gamma_{\gamma}(U', J^{\pi}, U, J^{\pi})}{\Gamma(U', J^{\pi})} W_{k-1}(U', J^{\pi}) dU' + \omega_k(U, J^{\pi}, 0).
$$
(9.5)

The population of any state (U, J^{π}) after emission of any number of γ -quanta is a lumped sum

$$
W(U, J^{\pi}) = \sum_{k} W_{k}(U, J^{\pi}), \qquad (9.6)
$$

then from Eq. (9.5) one easily gets

$$
W(U, J^{\pi}) = \sum_{J' \pi'} \int_{U}^{U_s} \frac{\Gamma_{\gamma}(U', J^{\pi'}, U, J^{\pi})}{\Gamma(U', J^{\pi'})} W(U', J^{\pi'}) dU' + W_0(U, J^{\pi}). \tag{9.7}
$$

The integral equation (9.7) in the code STAPRE [63] is solved as a system of linear equations, the integration range (U, U_g) is binned, in the assumption that there are no γ -transitions inside the bins.

The isomer branching ratio depends mostly on the low-lying levels scheme and relevant γtransitions probabilities. Though experimental data are available for 242 Am [32], we will use a simplified approach, since experimental level scheme and gamma-decay intensities are still incomplete. Modeling of low-lying levels of ²⁴²Am in [61] is accomplished based on the assumption that ground and first few excited states are of two-quasi-particle nature. For actinides with quadrupole deformations the superposition principle is usually adopted, the band-head energies of the doubly-odd nucleus are generated by adding to the each unpaired configuration (Ω_p, Ω_n) , as observed in the isotopic/isotonic (A-1) nucleus, the rotational energy contribution and residual (n-p) interaction energy contribution. The angular momenta of neutron and proton quasi-particles could be parallel or anti-parallel. In the independent quasi-particle model the two-quasi-particle states, $K^+ = |K_n + K_p|$ and $K^- = |K_n - K_p|$, are degenerate. Gallaher-Moshkowski doublets [61] appear because of (n-p) residual interaction. Fig 9.1 shows employed band-head energies for the two-quasiparticle states expected in the odd-odd nuclide ²⁴²Am up to 700 keV. The spectroscopic properties of two pairs of proton and neutron single particle states were derived from those experimentally observed in the isotopic ($Z=95$) and isotonic ($N=147$) odd-mass nuclei with mass (A-1). Figure 9.1 shows levels expected, which have similar ordering as experimentally observed [32]. For the bandheads, shown on Figure 9.1, the rotational bands were generated as

$$
E_{JK\pi} = E_{JK} + 5.5[J(J+1) - K(K+1)].
$$
\n(9.8)

Obviously, the schema presented on Fig. 9.1 does not represent a complete set to allow the calculation of absolute yields of ²⁴²Am (n,γ)^{242m}Am and ²⁴²Am (n,γ)^{242g}Am reactions. Rotational bands were constructed up to 700 keV excitation, modeling levels with spins $J^{\pi} \le 10$, in total up to 70 levels. The simple estimate [29] of the number of levels in odd-odd nuclei as

$$
N(U) = e^{2\Delta_0 / \tau} (e^{U / \tau} - 1), \qquad (9.9)
$$

predicts up to 280 level at $U \sim 700$ keV, $T=0.388$ MeV, $\Delta = 12/A^{1/2}$, MeV. We assume that the modeled angular momentum distribution would not be much different from realistic estimates. Since the complete data on the γ -transitions are missing, we assumed the simple decay scheme: only E1, E2 and M1 transitions are allowed in a continuum excitation energy range. Inter-band transitions forbidden, i.e., only γ-transitions within the rotational bands are possible. In that approach the populations of the lowest five level doublets could be calculated. Then we assumed that the transition to the isomer state $J^{\pi} = 5^-$ or low-spin, short-lived ground state $J^{\pi} = 1^-$ is defined by the "minimal multipolarity" rule. That means the states with spins $J < 3$ should populate the ground state, while those with $J \leq 3$ should feed the isomer state. Then the branching ratio could be obtained as the ratio of the populations, derived from Eq. (9.7):

$$
r(E_n) = \frac{\sum_{J < (J_I + J_s)/2} W(U, J^{\pi})}{\sum_{J \ge (J_I + J_s)/2} W(U, J^{\pi})}
$$
(9.10)

Fig. 8.1 Fission cross section of 243 Am(n, f).

Fig. 8.2 Fission cross section of 243 Am(n, f).

Fig. 9.1 Levels of 242 Am.

Fig. 9.2 Branching ratio of ²⁴³Am(n,2n)^{242m}Am(²⁴³Am(n,2n)^{242g}Am reaction

Fig. 9.3 Cross section of ²⁴³Am (n, 2n) reaction

Fig. 9.4 Cross section of 243 Am (n, 3n) reaction

Figure 9.2 show the branching ratio, calculated for the modeled level schema, presented at Fig. 9.1. The modeled level scheme appears to be quite compatible with the measured data on the 242 gAm ground state yield [65].

Figure 9.2 shows, that the yields of the ^{242g}Am and ^{242m}Am at ~15 MeV are still comparable, the latter being lower, as it should be for higher spin state in (n,2n) reaction. In calculation of [5] the ratio is opposite different. The branching ratio for $^{237}Np(n,2n)$ reaction shown on Fig. 9.2 is much different from that calculated here for $^{243}Am(n,2n)^{242m(g)}Am$ reaction. It is explained by the level spectra differences for residual nuclei. Figure 9.3 shows respective cross sections for the $^{243}Am(n,2n)^{242m(g)}Am$ reaction. Calculated $^{243}\overline{Am(n,3n)}$ cross section is shown on Fig. 9.3. It should be stressed once again, that we base our evaluation of fission cross section on simultaneous statistical model description of both $(n,2n)$ and (n, F) reactions for ^{241,243}Am.

10. Evaluation of prompt neutron yield in ²⁴³Am(n, F)

Average prompt neutron yield in neutron−induced fission of ²⁴³Am target nuclide was evaluated in a non-model least−squares fit of the experimental data with the use of the GMA code. The experimental data obtained by two groups. Data by Khokhlov et al. [67], measured relative $^{252}Cf(sf)$ prompt neutron yield, were renormalized to the latest evaluation recommended as standard [10]. Data by Frehaut et al. [68], which are not available in EXFOR data base, were digitized from the figure given in the [68]. They are in good agreement with data [67] in the overlapping energy region. Non-model least squares fit done with the GMA code [9, 10]. Chi−squared value per degree of freedom is about 1. For final presentation of the evaluation, 2-nd order polynomial fit was done for the GMA evaluated values below ~15 MeV and data of model calculations [64] above ~15 MeV. The thermal value adopted equal to value stemming from the fit at 0.1 keV, taking into account common for most nuclides energy dependence of prompt fission neutron yields in the resonance region [10].

The evaluated data are shown at Fig. 10.1 in comparison with experimental data, non-model fit and values from various evaluated data libraries. The uncertainties of evaluated data vary inbetween 0.6% and 2% in the range where experimental data are available. The thermal value of $\langle V_{d} \rangle$ is evaluated as 3.155±0.035, it is lower than that of ENDF/B-VII.0 [30] evaluation but consistent with JENDL-4.0 value.

We applied more complicated theoretical approach, than just linear extrapolation of V_p , with incorporation of the pre-fission neutron emission and contributing fission chances. At incident neutron energies above emissive fission threshold the number of prompt fission neutron V_p calculated as

$$
\nu(E_n) = \sum_{x=1}^{X} \left(\nu_x(E_{nx}) + (x-1) \right) \cdot \beta_x(E_n), \tag{10.1}
$$

here $x =1, \ldots X$ is the multiplicity for the *x*−chance fission of the nuclei A+1, A, A-1, A-2 after emission of $(x-1)$ pre-fission neutrons, $\beta_x(E_n)$ is the *x*-chance contribution to the observed fission cross section, $v_x(E_{nx})$ - prompt neutron multiplicity for x-th fissioning nucleus. The excitation energy of A, A-1, A-2 nuclides, which emerge after emission of $(x-1)$ pre-fission neutrons is defined

Fig. 10.1 Prompt fission neutron number of ²⁴³Am

Fig. 11.1 Delayed fission neutron number of 243 Am

$$
E_{nx} = E_n - \sum_j B_{nj} - \langle E_{xj} \rangle, \qquad (10.2)
$$

here B_{nj} - neutron binding energy for the $(A+1-j)$, j=1, 2, 3, nucleus, $\langle E_{xy} \rangle$ - average energy of j-th pre-fission neutron. The incident neutron energy dependence of neutron multiplicity in the energy range $E_n \le 6$ MeV for all fissioning ^{244, 243, 242, 241}Am nuclei was taken from evaluation by Malinovskij [69], to reproduce the measured data on v_p (see Table 10.1). We assumed that excitation energy E_{nx} is brought into A_j nuclide with the reaction: n+(A_j -1) \rightarrow fission. Incident neutron energy in this hypothetical reaction equals to $(E_{nj} - B_{nAj})$. In this way the $v_x(E_{nx})$ functions for all nuclides in the mass chain $242,241,240,239$ Am were calculated. Energy dependence of v_p versus incident neutron energy estimated with this equationis compared on Fig. 10.2 with previous present GMA-evaluation and previous evaluations. Relevant partial contributions to v_p are shown on Fig. 10.1. "Step" in v_p around (n,nf) reaction threshold is due to the pre-fission neutrons, emitted in 243 Am(n,nf) reaction. The similar behavior was evidenced in measured data for $^{232}Th(n, F)$ and $^{238}U(n,f)$, it was reproduced with the present model [64].

Target	$v_{\rm p}^{\rm th}$	$v_p(E_n \text{ MeV})$	$v_p(6 \text{ MeV})$
243 Am	$3.260*$	3.709(3.0)	4.150
242 Am	3.257	3.696(3.0)	4.127
^{241}Am	$3.090*$	3.624(3.0)	4.047
240 Am	3.205	3.623(3.0)	4.034

Table 10.1 Evaluated [64] first chance v_p –values for ^{243,242,241,240}Am target nuclides

*)tuned to measured data **11. Evaluation of averaged delayed neutron yields for ²⁴³Am (n, F)**

There is only one result of direct measurements of total average delayed neutron yield for 243 Am(n, f) - measurements by Saleh et al. [70] for thermal neutron spectrum. In these conditions, the results of evaluation given in ENDF/B-VII.0 [30] and JENDL-4 [13] and shown at Fig. 11.1 are rather discrepant. JENDL-4 evaluation obtained in calculations with account of contribution from (n, f), (n, nf) and (n, 2nf) chances of the observed fission, considering accordingly the evaluated data available for ²⁴³Am(n, f) below the threshold of (n, n'f) reaction, $242m$ Am(n, f) and 241 Am(n, f). The energy dependence of the delayed neutron yield for the first chance fission was assumed negligible and the respective yield has a constant value for excitations below the threshold of (n, n'f) reaction. In present evaluation, the energy dependence of average delayed neutron yield was modeled comparing the values of the group yields for 243 Am and 237 Np at thermal energy and relative energy dependence of the group yields known for ²³⁷Np [71]. The results of the final evaluation are shown in Fig. 11.1.

Fig. 12.1 Components of first neutron spectrum of 243 Am +n interaction

Fig. 12.3 Components of third neutron spectrum of $^{243}Am + n$ interaction for incident neutron energy 20 MeV.

12. Energy distributions of secondary neutrons

Energy distributions for (n, 2nγ), (n,3nγ) and (n, n'γ) reactions were calculated with a Hauser-Feshbach statistical model of cascade neutron emission [5, 64], taking into account exclusive pre-fission (n, xnf) and (n, xnγ) neutron spectra, with the allowance of pre-equilibrium emission of first neutron.

Prompt fission neutron spectra (PFNS) calculated with a phenomenological model, developed for the first-chance fission by Kornilov et al. [72]. The model extended to the emissive fission domain for various targets by Maslov et al. [5, 64, 73] and exclusive prefission neutron spectra of ²⁴³Am(n, xnf) and ²⁴³Am(n, xnγ) being included. Exclusive pre-fission neutron spectra of (n,xnf) reactions, either equilibrium and pre-equilibrium spectra of pre-fission (n,xnf) neutrons are strictly correlated with (n, F) and (n, xn) reaction cross sections. This approach was used previously for the description of the PFNS and neutron emission spectra for ²³⁸U+n [64], ²³⁵U+n [73], ²³²Th+n [64] and 237 Np+n [5] interactions. A number of experimental signatures were revealed and correlated with the exclusive pre-fission (n, xnf) and (n, xnγ) neutron spectra. This validated approach is used for the ²⁴³Am(n, F), ²⁴³Am(n, 2ny) and PFNS description/prediction for n+²⁴³Am interaction for non-emissive and emissive fission domain. Average energies of PFNS would predict distinct lowering in the vicinity of (n, nf) and (n, 2nf) reaction thresholds well known in measured PFNS shapes for major actinides.

12.1 (n,xnγ) and (n,xnf) neutron emission spectra

Exclusive (n, xnγ) and (n,xnf) neutron emission spectra for $x = 1, 2, 3$, reactions are calculated with Hauser-Feshbach model taking into account fission and gamma-emission competition to neutron emission, actually neutron spectra are calculated simultaneously with fission and (n,xn) reaction cross sections. The pre-equilibrium emission of first neutron is fixed by the description of high energy tails of (n,2nγ) reaction cross sections and (n, F) reaction cross sections for ²³⁷Np [5], ²³⁵U [73], ²³⁸U and ²³²Th target nuclides [64].

First neutron spectrum of the ²⁴¹Am(n, nf) or ²⁴¹Am(n, n γ) reactions is the sum of evaporated and pre-equilibrium emitted neutron contributions. Second and third neutron spectra for $^{243}Am(n,$ xnf) and 243 Am(n, xn γ) reactions are assumed to be evaporative. Pre-fission neutron spectrum of 243 Am(n, nf) reaction, especially its hard energy tail, is sensitive to the description of fission probability of 243 Am nuclide near fission threshold.

Components of first neutron spectra for $E_n = 20$ MeV are shown on Fig. 12.1. Components of second neutron spectra for $E_n = 20$ MeV are shown on Fig. 12.2. Components of third neutron spectra for E_n $= 20$ MeV are shown on Fig. 12.3.

That is an illustration of the strong dependence of the partial contributions of the exclusive first neutron spectra on the fissilities of the composite (A+1) nuclides as well as relative fissilities of A, A-1, A-2 nuclides.

Summarizing, we anticipate that partial (n, xnf) pre-fission neutron spectra for ²⁴³Am target nuclide would be pronounced in observed PFNS to a different extent as compared with ²³⁸U+n [64], 235 U+n [73], 232 Th+n [64] and 237 Np+n [5] interactions.

12.2 Prompt Fission Neutron Spectra

PFNS from fission fragments calculated as a superposition of two Watt [74] distributions for heavy and light fission fragments (FF), the partial contributions being equal, while the temperatures of the fragments are different [72]. Fission fragments' kinetic energy is the superimposed phenomenological parameter, generally lower, than total kinetic energy (TKE) of accelerated fission fragments.

The prompt fission neutron spectrum S (ε , E_n) is calculated as a sum of two Watt distributions, modified to take into account the emission of prompt fission neutrons before full acceleration of fission fragments. The neutrons, emitted from heavy and light fission fragments are included with equal weights:

$$
S(\varepsilon, E_n) = 0.5 \cdot \sum_{j=l,h} W_j(\varepsilon, E_n, T_j(E_n), \alpha), \qquad (12.1)
$$

$$
W_j(\varepsilon, E_n, T_j(E_n), \alpha) = \frac{2}{\sqrt{\pi} T_j^{3/2}} \sqrt{\varepsilon} \exp\left(-\frac{\varepsilon}{T_j}\right) \exp\left(-\frac{E_{\nu j}}{T_j}\right) \frac{sh(\sqrt{b_j \varepsilon})}{\sqrt{b_j \varepsilon}}, \quad (12.2)
$$

$$
b_j = \frac{4E_{vj}^0}{T_j^2}, T_j = k_j \sqrt{E_j^*} = k_j \sqrt{E_r - TKE + E_n + B_n},
$$
\n(12.3)

$$
E_{vl}^{0} = \frac{A_{h}}{A_{l}A} \cdot \alpha \cdot TKE \quad E_{vh}^{0} = \frac{A_{l}}{A_{h}A} \cdot \alpha \cdot TKE \quad . \tag{12.4}
$$

The coefficient α is the ratio of the kinetic energies of the fragments at the moment of neutron emission to the kinetic energy of fully accelerated fragments and is, in fact, a free

parameter. The ratio of the temperatures of the light and heavy fragment $r = T \sqrt{T_h}$ is another free parameter, which ensures the model [64] flexibility to reproduce the soft and hard tails of the PFNS. The parameters α =0.808 and *r*=1.248 were fixed in [5] by fitting, in fact, the PFNS for n+²³⁷Np system at E_n =7.8 MeV. For $n+^{243}$ Am they are defined by systematics [72].

Exclusive (n,xnf) pre-fission neutron spectra, as described above, are calculated. At *Eⁿ* higher than the emissive fission threshold $S(\varepsilon, E_n)$ is calculated as a superposition of pre-fission (n, x) neutrons $-d\sigma_{n,mf}^{k}/d\varepsilon$ (x=1, 2, 3, 4; k=1,…,x) and post-fission spectra $S_{A+2-x}(\varepsilon, E_n)$ of the neutrons from the fission fragments:

$$
S(\varepsilon, E_n) = \tilde{S}_{A+1}(\varepsilon, E_n) + \tilde{S}_A(\varepsilon, E_n) + \tilde{S}_{A-1}(\varepsilon, E_n) + \tilde{S}_{A-2}(\varepsilon, E_n) =
$$

\n
$$
v_p^{-1}(E_n) \cdot \left\{ v_{p1}(E_n) \cdot \beta_1(E_n) S_{A+1}(\varepsilon, E_n) + v_{p2}(E_n - \langle E_{nnf} \rangle) \beta_2(E_n) S_A(\varepsilon, E_n) +
$$

\n
$$
+ \beta_2(E_n) \frac{d\sigma_{nnf}^1(\varepsilon, E_n)}{d\varepsilon} + v_{p3}(E_n - B_n^A - \langle E_{n2nf}^1 \rangle) - \langle E_{n2nf}^2 \rangle \beta_3(E_n) S_{A-1}(\varepsilon, E_n) + \beta_3(E_n) \cdot \left[\frac{d\sigma_{n2nf}^1(\varepsilon, E_n)}{d\varepsilon} + \frac{d\sigma_{n2nf}^2(\varepsilon, E_n)}{d\varepsilon} \right] + v_{p4}(E_n - B_n^A - B_n^{A-1} - \langle E_{n3nf}^1 \rangle) - \langle E_{n3nf}^2 \rangle - \langle E_{n3nf}^3 \rangle \cdot \beta_4(E_n) S_{A-2}(\varepsilon, E_n) + \beta_4(E_n) \left[\frac{d\sigma_{n3nf}^1(\varepsilon, E_n)}{d\varepsilon} + \frac{d\sigma_{n3nf}^3(\varepsilon, E_n)}{d\varepsilon} + \frac{d\sigma_{n2nf}^3(\varepsilon, E_n)}{d\varepsilon} \right] \right\}.
$$
 (12.5)

Figures 12.4-12.7 compare present PFNS with those of JENDL-4.0 [13]. Some shape differences for the first- and higher chance fission noticed. Aerage energies (Fig. 12.8) of emitted prompt fission neutron spectra both in first-chance and emissive fission domains are discrepant.

Figure 12.9 shows the partial contributions of ²⁴³Am (n, f) and ²⁴³Am(n, xnf) reactions to the observed PFNS, shown on previous Fig. 12.7. The contribution of $^{243}Am(n, nf)$ reaction in the soft part of the spectrum is systematically lower than that of 243 Am(n, f) reaction. The contribution of (n,nf) reaction is higher in case of JENDL-4.0 [13] for the hard part of the spectrum.

The combined effect of fission chances and exclusive pre-fission neutron spectra leads to the lowering of the average energy of the PFNS of 243 Am (n, F) in the vicinity of the 243 Am (n, nf) and ²⁴³Am (n, 2nf) reaction thresholds. The dips are evidenced in measured PFNS average energy $\langle E \rangle$ of different U nuclei. In JENDL-4.0 [13] the PFNS is calculated with Madland-Nix model [75], the pre-fission neutron spectra are calculated, presumably, as exclusive ones. However, some discrepancies are noticed with measured data for $^{237}Np(n, F)$, a second dip due to $(n, 2nf)$ reaction is not reproduced in JENDL-4.0 [13] both for ²³⁷Np and $243,241$ Am.

12.3 (n,xn) Reactions Neutron Spectra

There is no measured data on neutron emission spectra for 243 Am +n interaction. For incident neutron energy higher than emissive fission threshold, emissive neutron spectra are de-convoluted, components of 1st, 2nd and 3d neutron spectra are provided, where applicable. We have calculated 1st, 2nd and 3d neutron spectra for the (n, nγ), (n, 2n) and (n, 3n) reactions.

According to the ENDF/B-VI format specifications the secondary neutron spectra were summed up and tabular spectra for the $(n, n\gamma)$, $(n, 2n)$ and $(n, 3n)$ reactions were obtained.

Fig. 12.4 Comparison of the prompt fission neutron spectrum for 243 Am (n, F) reaction at incident neutron energy of 10-5 MeV.

Fig. 12.5 Comparison of the prompt fission neutron spectrum for 243 Am (n, F) reaction atincident neutron energy of 2 MeV.

Fig. 12.6 Comparison of the prompt fission neutron spectrum for ²⁴³Am (n, F) reaction at incident neutron energy of 6 MeV.

Fig. 12.7 Comparison of the prompt fission neutron spectrum for 243Am (n, F) reaction at incident neutron energy of 20 MeV.

Fig. 12.8 Dependence of average energy of 243 Am (n, F) and 237 Np(n,F) prompt fission neutron spectra on the incident neutron energy.

Fig. 12.9 Multiple-chance fission contributions to the prompt fission neutron spectrum for ²⁴³Am (n, F) reaction, incident neutron energy 20 MeV.

Fig. 12.11 (n, 3n) reaction neutron spectra of ²⁴³Am +n for incident neutron energy 20 MeV.

Fig. 12.12 Comparison of (n, 3n) reaction neutron spectra for 243 Am +n for incident neutron energy 14 MeV.

Spectrum of (n,nγ) reaction actually is just hard energy tail of 'pre-equilibrium' component of first neutron spectrum (see Figs. 12.1, 12.2, 12.3).

Spectrum of the first neutron of (n,2n) reaction is much softer, although 'pre-equilibrium' component still comprise appreciable part of it. Figures 12.10, 12.11 and 12.12 illustrate the variation of the partial contributions of the 1st and 2nd neutrons to the combined spectrum of 243 Am $(n,2n)$ and $(n,3n)$ reactions. First neutron spectrum of $(n,3n)$ reaction is actually of evaporative nature. First neutron spectrum of (n,nf) reaction has rather long pre-equilibrium high-energy tail. First neutron spectrum of (n,2nf) reaction, as that of (n,3n) reaction, is of evaporative nature. Figures 12.11 ($E_n = 20$ MeV) and 12.12 ($E_n = 14$ MeV) illustrate the variation of the partial contributions of the 1st, 2nd and 3d neutrons to the combined spectrum of ^{241}Am (n,3n) reaction, softening of higher multiplicity neutrons is evident.

13. Conclusion

The diverse measured database of $n+243$ Am is analyzed using a statistical theory and generalized least squares codes. Important constraints for the measured capture cross section comes from the average radiative, S_0 and S_1 strength functions, however, the observed capture cross section needs anomalously high capture width to produce a consistency with measured data, fited with GMA code approach in keV-energy range.

Evaluated are the 243 Am neutron-induced fission, capture, inelastic scattering, (n,2n) cross sections, branching ratio for the yields of short-lived 244m/Am and long-lived 244m/Am states of ²⁴³Am(n, γ) reaction, branching ratio for the yields of short-lived ^{242g}Am and long-lived ^{242m}Am states of 243 Am(n, 2n) reaction. Prompt fission neutron spectrum (PFNS) and prompt fission neutron

multiplicity are another important items predicted, measurements of the former for the $^{243}Am(n, F)$ reaction are unavailable at the moment.

Prompt fission neutron spectra data for the first-chance fission and emissive fission reactions are predicted. The influence of exclusive (n, xnf) pre-fission neutrons on prompt fission neutron spectra (PFNS) and (n, xn) spectra is modelled. Contributions of emissive/non-emissive fission and exclusive spectra of (n, xnf) reactions are defined by a consistent description of the ²⁴³Am (n, F) , 241 Am (n, F), 241 Am (n, 2n) 241 Am reactions. In 243 Am neutron capture the branching ratio data of the yields of short-lived (1^-) and long-lived (6^-) ²⁴⁴Am states measured at thermal energy is calculated without arbitrary normalizations, though in a simplified manner. Excited levels of 244 Am are modelled using predicted Gallher-Moshkowski doublets. In ²⁴³Am(n, 2n) reaction the branching ratio data of the yields of short-lived (1⁻) and long-lived (6⁻) ²⁴²Am states are calculated without arbitrary normalizations, though in a simplified manner. Excited levels of 242 Am are modelled using predicted Gallher-Moshkowski doublets.

The job supported by the International Science and Technology Center (Moscow) under Project Agreement B-1604.Data file is at https://www-nds.iaea.org/minskact/data/original/za095243

REFERENCES

- 1. Marie F., Letourneau A., Fioni G. et al. Nucl. Instr. and Meth. in Physics Research. A 556, pp. 547-555.
- 2. Bringer O., AlMahamid I., Chabod S., et al. Proc. of Int. Conf. on Nuclear Data for Science and Technology. Nice, France, Vol. 1, p. 619 (2008).
- 3. Maslov V.M., Porodzinskij Yu.V., Baba M., Hasegawa A. Nucl. Sci. Eng. 143, 177 (2003).
- 4. Maslov V. M. In: Proc. of the 13th International Seminar on Interaction of Neutrons with Nuclei, May 25-28, 2005, Dubna, Russia, p. 321.
- 5. Maslov V.M., Pronyaev V.G., Tetereva N.A. et al. INDC(BLR)-021, 2010.
- 6. Maslov V.M., Pronyaev V.M., Tetereva N.A. et al. In: Proc. Intern. Conf. on Nuclear Data for Science and Technology, Jeju, Korea, April 26-30, 2010, Journal of Korean Phys. Soc., **59**, 1337 (2011).
- 7. Maslov V.M., Pronyaev V.M., Tetereva N.A., Granier T., Hambsch F.-J. In: Proc. Intern. Conf. on Nuclear Data for Science and Technology, Jeju, Korea, April 26-30, 2010 Journal of Korean Phys. Soc., **59**, 867 (2011).
- 8. Maslov V.M., Sukhovitskij E.Sh., Porodzinskij Yu.V., Klepatskij A.B., Morogovskij G.B. INDC(BLR)-006, 1996.
- 9. Poenitz W.P., Aumeier S.E., The simultaneous evaluation of the standards and other cross sections of importance for technology, Report ANL/NDM-139 (1997).
- 10. International Evaluation of Neutron Cross-Section Standards, IAEA, Vienna, Austria, IAEA Publication STI/PUB/1291 (2006).
- 11. Weston L.W. and Todd J.H. Nucl. Sci. Eng., 91, 444 (1985).
- 12. Wisshak K., Kappeler F. Nucl. Sci. Eng. 85, 251 (1983).
- 13. Shibata K., Iwamoto O., Nakagawa T. . Nucl. Sci. Techn., 48 (2011) 1.
- 14. Seeger P.A. Fission cross sections from Pommard. LA-4420, 1970, p. 138.
- 15. Behrens J.W., Browne J.C. Nucl. Sci. Engng. 77, 444 (1981)
- 16. Butler D.K. and Sjoblom R.K. Phys. Rev. 124, 1129 (1961).
- 17. Terayama H., Karino Y., Manabe F., Yanagawa M., Kanda K., Hirakawa N. NEANDC(J)- 122, 8609.
- 18. Knitter H.-H., Budtz-Jorgensen C. Nucl. Sci. Engng. 99, 1 (1988).
- 19. Manabe F., Kanda K., Iwasaki T. Terayama H., Karino Y., Baba M., Hirakawa N. Fourn. Fac. of Eng., Tohoku University Tech. Rep. 52, 97, 1988.
- 20. Aiche M. et al. Proc. Intern. Conf. on Nuclear Data for Science and Technology, p. 483, Nice, France, April 22-27, 2007, EDP Sciences.
- 21. Fomushkin E.F., Gutnikova E.K., Zamyatnin Yu.S. et al. Yadernaya Fyzika, 5 (5), 966 (1967).
- 22. Fursov B.I., Baranov E.Yu., Klemyshev M.P. et al. Sov. J. At. Energy 59, 899 (1985).
- 23. Fomushkin E.F., Novoselov G.F., Vinogradov Yu.I. et al. Yadernye Konstanty 57(3), 17 (1984).
- 24. A.A.Goverdovsky, A.K. Gordyushin, B.D. Kuz'minov, V.F.Mitrofanov, A.I.Sergachev, S.M.Solov'ev, T.E.Kuz'mina, Atom. Energ. 67, (1), 30, 1989
- 25. Golovnya V.YA, Bozhko V.P., Oleynik S.N., Shpakov V.P., Kalinin V.A. JINR-E3-419, 293, 1999.
- 26. A.V. Fomichev, V.N. Dushin, S.M. Soloviov, A.A. Fomichev, S.G. Mashnik. LA-UR-05- 1533. 2005
- 27. Laptev A.B., Scherbakov O.A., Vorobyev A.S., Haight R.C., Carlson A.D. Proc. 4-th Intern. Conf. Fission and Properties of neutron-rich nuclei, Sanibel Island, USA, 11-17 November, 2007.
- 28. Ignatjuk A.V., Istekov K.K., Smirenkin G.N. Sov. J. Nucl. Phys. 29, 450 (1979). 1984.
- 29. V.M. Maslov, INDC(BLR)-013/L, 1998, IAEA, Vienna.
- 30. Chadwick M., M. Herman, P. Oblozinsky et al. Nuclear Data Sheets. **112**, 2887-2996 (2011).
- 31. Maslov V.M. In: Proc. 13th International Symposium on capture gamma rays and related topics, Koln, August 25-29, 2008, Germany, American Instituite of Physics, 2009, p. 579.
- 32. Firestone R.B., Table of Isotopes CD-ROM, Eighth Edition, Version 1.0, March 1996, S.Y.Frank Chu, CD-ROM Ed., V.S.Shirley, Ed., Wiley-Interscience, 1996
- 33. Strutinsky V.M. Nucl. Phys.A95 (1967) 420
- 34. Phillips T.W., Howe R.E. Nucl. Sci. Eng. 69, 375 (1979)
- 35. Moldauer P.A. Phys. Rev., C11, 426 (1975).
- 36. Tepel J.W., Hoffman H.M., Weidenmuller H.A. Phys. Lett. 49, 1 (1974).
- 37. Fu C. Nucl. Sci. Eng. 86 (1984) 344.
- 38. Maslov V.M. Yad. Fiz. 63 (2000) 214.
- 39. Maslov V.M. Actinide Neutron-Induced Fission up to 20 MeV, Nuclear Reaction Data and Nuclear Reactors, International Center for Theoretical Physics Lecture Notes, 14 March – 14 April, Trieste, Italy, No.1, pp. 231-268 (2001)
- 40. Ignatyuk A.V., Maslov V.M. Sov. J. Nucl.Phys. .54 , p. 392, 1991.
- 41. Myers W.O. and Swiatecky W.J. Ark. Fyzik. 36 (1967) 243.
- 42. Bjørnholm S. and Lynn J.E. Rev. Mod. Phys. 52 (1980) 725
- 43. Howard W.M. and Möller P. Atomic Data and Nuclear Data Tables 25 (1980) 219.
- 44. Seeger P.A., Hemmendinger A., Diven B.C. Nucl. Phys. A96, 605 9549 (1967).
- 45. Kornilov N.V., Kagalenko A.V., Baryba V.Ya. et al. Ann. Nucl. Energy, 27, 1643 (2000).
- 46. Street K. Jr, Ghiorso A., Seaborg G.T. Phys. Rev. 79, p. 530 (1950).
- 47. Stevens C.M., Studier M.H., Fields P.R., et al. Phys. Rev. 94, p. 974 (1954).
- 48. Harvey B.G., Robinson H.P., Thompson S.G., et al. Phys. Rev. 95, p. 581 (1954).
- 49. Butler J.P., Lounsbury M., Merritt J.S., Canadian J. of Physics 35, pp. 147-154 (1957).
- 50. Vandenbosch R., Fields P.R., Vandenbosch S.E., Metta D. J. Inorg. Nucl. Chem. 26, pp. 219-234 (1964).
- 51. Ice C.H., Production of the transplutonium elements at Savannah River, Report DP-MS-66- 69, 1966.
- 52. Schuman R.P, Resonance Activation Integral Measurements, Report IN-1126, p.19, December 1967.
- 53. Bak M.A.., Krivochatskiy A.S., Petrzhak K.A., et al. Atomnaya Energija (Sov.), Vol. 23, issue 4, pp. 316-319, October 1967 (in Russian).
- 54. Folger R.L., Smith J.A., Brown L.S., et al. Proc. of Conf. Washigton, Vol. 2, p. 1279 (1968).
- 55. Simpson O.D., Simpson F.B., Harvey J.A., et al. Nucl. Sci. Eng. 55, pp.273-279 (1974).
- 56. Gavrilov V.D., Goncharov V.A., Ivanenko V.V., et al. Atomnaya Energya, Vol. 41, issue 3, pp. 185-190, September, 1976.
- 57. Hatsukawa Y., Shinohara N., Kentaro H., Measurements of Neutron Cross Section of the 243 Am(n, γ)²⁴⁴Am, Report JAERI-Conf 98-003, pp. 221-224 1998.
- 58. Ohta M., Nakamura S., Harada H. et al, Nucl. Sci. Eng. 43, pp. 1441-1445 (2006).
- 59. Hori J., Oshima M, Harada H, et al. Report JAERI-C-2009-004, p. 123, April 2009.
- 60. Cricchio A., Ernstberger R., Koch L., Wellum R., Proc. of the Int. Conf. Nuclear Data for Science and Technology, 6-10 September 1982, Antwerp, Holland, D.Reidel Publishing Company, p.175.
- 61. Sood P.C., Singh R.N. Nucl. Phys. A373, 519 (1982.
- 62. Strutinsky V.M., Groshev L.V., Akimova M.K., Atomnaya Energiya, 38, 598 (1960).
- 63. Uhl M., Strohmaier B., A Computer Code for Particle induced Activation Cross Sections and Related QuantitiesIRK-76/01, IRK, Vienna (1976).
- 64. Maslov V.M., Porodzinskij Yu. V., Baba M., Hasegawa A., Kornilov N. V., Kagalenko A. B., Tetereva N.A. Phys. Rev. C, 69, 034607, 2004.
- 65. T.L. Norris, A.J. Gancarz, D.W. Efurd, R.E. Perrin, G.W. Knobeloch, P.W. Oliver, G.F. Grisham, R.J. Prestwood, I., Binder, G.W. Butler, W.R. Daniels, and D.W. Barr. 14-MeV $(n,2n)$ Neutron Cross Sections of ²⁴¹Am and ²⁴³Am. In: Irradiations at the Rotating Target Neutron Source-II, p. 69. UCID-19837-83.
- 66. Dovbenko A.G., Ivanov V.I., Kolesov V.E., Tolstikov V.A., Bulleten Tsentra po Jadernym Dannym 6, pp. 42-46, M: Atomizdat 1969.
- 67. Khokhlov Yu. A., Ivanin I.A., In'kov V.I., et al. In:. Proc. Int. Conf. Nuclear Data for Science and Technology, Gatlinburg, USA, May 9-13, 1994, p. 272, J.K. Dickens (Ed.), ANS, 1994.
- 68. Frehaut J. et al., Progress Report CEA-N-2396, 1984, p. 69.
- 69. Malinovskij V.V. VANT (ser. Yadernie constanty), 1987, No.2, 25.
- 70. Saleh H.H., Parish T.A., Shinohara N., Nucl. Sci. and Eng., 125, p.51 (1997).
- 71. Piksaikin V.M., Balakshev Yu.F., Isaev S.G., Kazakov L.E. et al., Atomnaya Energiya, 85, 51 (1998).
- 72. Kornilov N.V., Kagalenko A. B, Hambsch F.-J.,. Phys. At. Nucl., 1999, 62, 209.
- 73. Maslov V.M., Kornilov N.V., Kagalenko A. B., Tetereva N.A. Nucl. Phys. A760 (2005) 274.
- 74. Watt B.E. Phys. Rev. 87, 1037 (1952).
- 75. Madland D., Nix J., Nucl. Sci. Engng. 81, 213 (1982).

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