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Centre d'Etudes de Bruyères-le-Châtel

ON THE TRANSFORMATION OF ANGULAR SCATTERING PROBABILITIES BETWEEN REFERENCE SYSTEMS : SURVEY AND NUMERICAL ANALYSIS

bу

Olivier BERSILLON, Alois SCHETT, Béatrice CAPUT

- October 1983 -

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et le progrès pour but. (A.COMTE)

RESUME

L'objet du présent travail est l'étude de la transformation des probabilités de diffusion angulaire lors des passages des référentiels du laboratoire au centre de masse, en particulier à l'aide de matrices de transformation T, T^{-1} .

Un examen des méthodes existantes pour le calcul de ces matrices montre qu'aucune d'entre elles est satisfaisante quant à l'analyse et l'exploitation numériques.

Cette étude est donc destinée à l'élaboration et à la vérification d'une méthode numérique sure (sous contrôle numérique) et efficace pour calculer les matrices de transformation T, T^{-1} .

De nombreux calculs comparant l'efficacité relative des différentes méthodes montrent que la méthode basée sur un développement en série de Taylor est manifestement plus sure (stabilité due aux erreurs d'arrondi) et plus économique (temps de calcul).

Le développement en série de Taylor est utilisé pour établir des tables numériques des matrices T, T⁻¹. Il apparait que les tables correspondantes figurant dans la littérature, par trop erronées, sont inutilisables. De plus les matrices données dans le fichier ENDF/B4 doivent être utilisées avec précaution, du moins pour les éléments légers. Ceci est démontré par des calculs du transport de neutrons dans des sphères de deutérium.

Outre les propriétés des matrices T, T^{-1} , sont également présentés de nouveaux résultats relatifs à des formules de récurrence, des intégrales et à la ramification possible vers d'autres branches des mathématiques.

ABSTRACT

The present study deals with the transformation of angular scattering probabilities between the laboratory- and center-of-mass-system, in particular it deals with the transformation matrices T, T^{-1} .

A survey of the methods for the calculation of these matrices shows that none of the methods is satisfactory either as far as mathematical analysis or numerical exploration is concerned.

This work is thus centered on the elaboration and testing of a reliable (accuracy controlled) and efficient method to compute the transformation matrices T, T^{-1} .

Extensive calculations and performance-comparisons of the various methods show that the so-called Taylor series method is manifestly superior as regards reliability (round-off stability) and efficiency (computing time).

The Taylor series method has been applied to calculate tables of the matrices T, T^{-1} . It turns out that the corresponding tables found in literature are to be discarded as they are too erroneous. Moreover, the matrices given in ENDF/B4 file for light elements have to be used with precaution. That is also demonstrated by comparative neutron transport calculations across deuterium-spheres.

Besides results of numerical analysis, properties of the matrices T, T⁻¹, new relations of integrals as well as new recurrence relations are presented and ramification to other mathematical disciplines are discussed.

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1.0 INTRODUCTION.

1.1 HISTORICAL BACKGROUND ON NUCLEAR DATA.

Since the beginning of nuclear industry a vast amount of nuclear data has been accumulated. These data have been determined experimentally or calculated using nuclear models. On the basis of these data, the so-called Evaluated Data Files were established. The most commonly used is the Evaluated Neutron Data File (ENDF) [KI79].

These files contain items such as resonance parameters, integrated cross sections, secondary neutron spectra, angular distributions, γ -ray production spectra, ..., in the usual energy range 10⁻⁵ eV - 20 MeV.

A substantial part of these data concerns the **neutron scattering angular distrib**utions.

1.2 BASIC NOTIONS.

For a given reaction the scattering angular distribution probabilities are **represented in two forms:**

- Pointwise: The scattering probability is tabulated as a function of the independent variables: Incident particle energy, scattering angle.
- Analytical: The scattering probability is represented as a truncated series of Legendre polynomials, the coefficients of which are tabulated as a function of the independent variable: Incident particle energy.

The latter representation has three main advantages:

• It permits **space-saving** storage. Given the large amount of scattering data this is not at all negligible.

- An analytical representation of such data is **more appropriate** for **further use**, for example, for neutron transport calculation.
- It gives information on the partial wave contribution to the total scattering probability.

Two **reference** systems are commonly used for representing the angular distribution scattering probabilities: the center-of-mass system and the laboratory system.

This, of course, requires **transformation prescriptions** for passing from one system to the other. Quite naturally the transformation procedure for the pointwise and the analytical representation will be different. The former is in fact carried out with the help of the so-called **kinematic formulae**, whereas the latter by means of the so-called **transformation matrices**: T, T^{-1} , where the matrix T permits transformation from the center-of-mass to the laboratory system and the matrix T^{-1} performs the inverse transformation.

We have focused our study on the latter transformation procedure; more particularly, on the calculation of the transformation matrices.

1.3 PRESENT STATUS OF THE TRANSFORMATION MATRIX CALCULATION.

This matter has seen rather a great deal of attention in literature [ZW54], [AM56], [AM58], [AM64], [GE63], [BE65] and [BE77].

Several methods have been proposed therein for the calculation of the transformation matrices. These methods can be classified into **three categories**:

- Recurrence relation connecting elements of the transformation matrices
 [AM56] and [BE65]: New elements of the transformation matrix are computed
 from elements calculated anteriorly. This recurrence relation contains an
 infinite sum.
- Closed form expression [GE63]: The matrix elements are expressed as a four-fold product of finite sums.

• **Taylor series expansion** [AM58], [AM64] and [BE77]: The matrix elements are developed in a Taylor series.

In addition to these algorithms, voluminous numerical tables of these transformation matrices have been published in [LA59] and in ENDF [K179]. Moreover, the first three leading terms of the power series representation of the elements of the transformation matrices T, T^{-1} of dimension (7,7) are given in [PE63].

A priori, one would thus believe that this subject has already been studied exhaustively. This is, however, not at all the case, as **Table 1.1** makes apparent. We give there a summary of the present status of the methods so far used for calculating the transformation matrices.

Table 1.1: Present status of methods so far used for calculation of the transformation matrices T, T⁻¹.

Method	Recurrence relation connecting matrix elements	Closed form expression	Taylor series expansion		
Error-analysis	no	_	по		
Validity-range (γ-range) defined?	no	no	no		
Convergence investigated ?	по	_	no		
Reliability (stability) tested ?	по	no	по		
Matrices treated	T, T ⁻¹	T	T		
Numerically explored ?	partly	partly	partly		
Efficiency studied ?	по	no	no		
Used for production ?	yes (ENDF and tables)	partly	partly		

From this table we can readily see that **none** of **the methods** used to the present time for the computation of the transformation matrices is **numerically defined**. An error analysis has not been made for any of them, and such important items as validity range, convergence and stability have not been considered.

Furthermore, two of the methods give formula only for the matrix T, but not for T^{-1} . Moreover, **no comparison** has been made of the **efficiency** of each of the methods. Note that such a performance comparison is only feasible if an error analysis and a reliability check have been carried out prior to it.

The present status concerning the calculation of the transformation matrices is, thus, far from satisfactory. One can not even be confident that the extensive numerical tables of the transformation matrices are sufficiently correct for applications.

In summary, one can say that, surprisingly, there does not at present exist any numerically well-defined and operational method for the calculation of the transformation matrices T, T^{-1} . This situation has prompted the present investigation.

1.4 OBJECTIVES OF THE PRESENT STUDY.

In the present work we have fixed ourselves the following main goals:

- To establish a numerically well-defined method (error-analysis, reliability) for the calculation of both the matrix T and T⁻¹.
- This method should at the very least permit treatment of the angular distribution scattering probabilities contained in **ENDF**.
- The method should be efficient as far as computer time is concerned (performance comparison).
- As a primary application of this method both the tables for T and T⁻¹ given in the literature as well as those given in ENDF should be verified.

We have concentrated our investigation on the **Taylor series expansion method** for the following reasons:

- It avoids wasteful computation as it is, by its nature, numerically adapted to
 each case to be treated, i.e., for a small variable one needs less terms in the
 series to compute than for a large variable. This property is inherent in
 power series, whereas the two other methods in question do not reveal this
 advantage.
- The coefficients of the Taylor series are evidently constants for a given matrix element of T or T⁻¹. They have thus to be computed only once and can henceforth be stored as a permanent file. The actual computation of the matrix elements is thus reduced to the calculation of the variable part, i.e., the sum of terms consisting of powers of the variable multiplied by the respective coefficients. The other two methods in question do not allow such a time-saving computer separation of the calculation procedure.
- As the data to be transformed are always only known to within a certain accuracy, the transformation matrix does not need to be known exactly either. The power series can thus be curtailed at a certain point. A matrix element is thus calculated just to the accuracy required, and not beyonā. This, of course, demands a tight accuracy-control algorithm.

The main merit of the Taylor series expansion method is, for our aim, its natural adaptability to a specific problem considered. This is in turn intimately connected with the **economical aspect** (computer time). Thus this method seems, a priori, peculiarly suited for the calculation of the transformation matrices.

It in fact turns out that the Taylor series expansion method is most satisfactory in terms of accuracy, reliability and efficiency.

1.5 INTRODUCTORY COMMENTS ON THE CONTENT OF THE PRESENT WORK.

This report contains five chapters and four annexes. Each chapter is usually divided into sections which in turn are divided into subsections; for example, 3.1.2 denotes the second subsection of the first section of chapter 3.

A number in **brackets** [] refers to the **bibliography** at the end of the report and [GR65] denotes the author **GRADSHTEYN** and the publishing date 19**65**.

In **CHAPTER 2** we give the physical and mathematical **definition of the problem** and discuss the merits of the two transformation methods used.

In **CHAPTER 3** the **Taylor series expansion method** is treated. Recurrence relations of the coefficients of the Taylor series are given. They permit the calculation of the matrices T and T⁻¹ to any accuracy required. An accuracy-control algorithm was derived. Furthermore, it could be shown that the Taylor series converge within a radius $\gamma \leq 1$ (for definition of γ see (2.5)). This convergence range covers in fact all but exotic cases in ENDF. The method has been extensively numerically tested and pertinent results of these test-runs are given in this chapter.

The whole transformation procedure is fully accuracy-controlled. Typical examples of transformations are presented in **Section 3.7.**

A verification of the existing numerical tables of the transformation matrices [LA59] leads to the conclusion that all of them must be discarded as they are far too inaccurate and parts of them are even seriously erroneous. This also holds for the leading terms of the transformation matrix elements published in [PE63].

Besides these more practical results a series of interesting mathematical relations have been obtained. They are summarized in Subsection 3.8.3.

In **CHAPTER 4** we present results of the **performance-comparison** of the three available methods: The Taylor series method, the method based on recurrence formula connecting matrix elements and the closed form method which expresses the matrix elements as a four-fold product of finite sums.

This **efficiency comparison** clearly points out the superiority of the Taylor series method particularly in that which concerns computer time and reliability (round-off stability).

In CHAPTER 5 we summarize the results of this study and give an outlook.

A verification of the transformation matrices given in ENDF/B4 shows that the lighter the element, the more seriously incorrect they become. The matrix given there for deuterium is much too erroneous. A detailed analysis of ENDF with respect to the accuracy of the transformation matrices for elements with A < 60 is given in Annex-1.

As an example of the **repercussions of our study in neutron transport** calculation, we have carried out comparative computations of neutron transport across a **deutellum-sphere** having a point-source at its centre. More precisely, for one computer run we used the transformation matrix as calculated with the aid of the Taylor series method presented in Chapter 3 (our standard method) and for the other run the transformation matrix as given in ENDF/B4. The results of these two comparative runs are discussed in **Annex-2**.

The **prcgram system** for the complete transformation procedure which has been developed in our laboratory on the basis of the Taylor series expansion method is written in **FORTRAN**. It is available upon request. A detailed description of it is given in **Annex-3**.

A **formulary** which is intended to obviate the need for seeking in the literature is presented in **Annex-4**.

1.6 PERSPECTIVES RESULTING FROM THIS STUDY.

In the course of the present study we have touched on several fields which would be of interest for further investigation. They are, however, beyond the scope of this work. A summary of them is given in Subsection 3.8.4 and in **CHAPTER 5.**

One of the items concerns the **extension** of the Taylor series method to a γ -variable range beyond the value $\gamma = 1$. One would naturally attempt to cover this range by an analytical continuation process. However, this is not feasible as the matrix elements are discontinuous at $\gamma = 1$. This is, by the way, one important result steming from the present study.

A preliminary investigation already undertaken by us indicates that, for the range $\gamma > 1$, the definition of the matrices T, T⁻¹ have presumably to be redefined

and none of the available methods for calculation of the transformation matrices can be applied as they stand.

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1.7 BRIEF SUMMARY.

All in all, we can conclude that the present work presents a comprehensive, and hopefully a thorough, study of the transformation of scattering angular distribution probabilities between the two reference systems used applying transformation matrices. It is valid for a γ -range: [0,1]. This covers in general all cases in common use.

The ultimate objective would of course be a study covering the entire γ -range, i.e., $\gamma \in [0,\infty]$.

1.8 TECHNICAL REMARK.

The edition of this report has been greatly facilitated by using the computer supported IBM-program-system **SCRIPT/VS** [SC81].

2.0 DEFINITION OF THE PROBLEM.

2.1 BASIC NOTIONS AND STATUS OF SCATTERING DATA.

The present study concerns the representation of angular distribution probabilities of nuclear reactions. The nuclear reaction type we deal with is sketched in Figure 1 on page 10.

The probability of such reactions can be determined experimentally or be calculated by means of nuclear models. For reasons of simplicity the latter is done using the center-of-mass system, while the experimental determination is naturally carried out in the laboratory system.

For reasons of nuclear research, but primarily in order to satisfy the strong demand of angular distributions of neutrons scattered by nuclei forwarded by nuclear industry, an impressive amount of such data has been measured, calculated and evaluated. Neutron scattering probabilities are now available for all nuclei of importance for nuclear industry and for neutron energies of main interest, i.e., up to about 20 MeV.

To permit an efficient use of these data they have been stored, in the context of international collaboration, in a computer treatable format. There are in fact two distinct main files:

- The Experimental neutron data files updated and maintained according to international agreements. They contain neutron scattering angular distribution data in both the laboratory and the center-of-mass systems.
- The Evaluated Neutron Data Files. They are established on the basis of the experimental and calculated data. Again, both frame of reference systems are in use there.

These files provide data to feed computer programs which are related to neutron transport problems. In general, they accept neutron scattering angular distribution data in either frame of reference. However, data in the center-of-mass system for neutron transport problems are always transformed in the laboratory system prior to further processing.



Figure 1. Nuclear reaction with which we deal.

The generation of scattering angular distributions is usually performed pointwise. Originally one thus has either theoretically or experimentally determined data in the form of tables. An analytical representation, or more precisely an approximation, of angular distributions can only be done once this function is known pointwise.

Scattering angular distributions in data files are thus quite naturally represented either pointwise in the form of tables or analytically, i.e., as coefficients of a series approximation using Legendre polynomials.

Evidently, as the scattering angular distributions are given in either of the two frames of reference, a transformation algorithm between these two systems is necessarily required.

The two ways of representation of such data, i.e., the pointwise and the analytical, naturally demand two adequate transformation procedures. Before dealing with them, let us fix the **notation** of the quantities appearing in the two frames of reference :

- All quantities marked with a bar belong to the center-of-mass system.
- Those without a bar are understood as belonging to the laboratory system.

We now describe in detail both of the transformation procedures in question.

2.2 TRANSFORMATION PROCEDURES.

2.2.1 Transformation procedure for a pointwise representation of scattering angular distributions.

In this case the following so-called kinematic formulae are applied [EV55] (non-relativistic description):

$$\frac{d\sigma}{d\mu}(\mu, E) = \frac{d\bar{\sigma}}{d\bar{\mu}}(\bar{\mu}, \bar{E}) \frac{d\bar{\mu}}{d\mu} , \qquad (2.1)$$

where

 $\mu = \cos \theta ; \mu \in [-1,1] .$

E is the laboratory incident particle energy.

$$\bar{E} = \frac{m_2}{m_1 + m_2} E$$
 (2.2)

is the total kinetic energy available in the center-of-mass system.

$$\bar{\mu} = \gamma(\mu^2 - 1) + \mu[\gamma^2(\mu^2 - 1) + 1]^{1/2}$$
or
(2.3)

$$\mu = (\gamma + \bar{\mu}) (1 + 2\gamma \bar{\mu} + \gamma^2)^{-1/2} . \qquad (2.4)$$

We thus have to transform both the dependent and independent variables.

The parameter γ reads

$$\gamma = \left(\frac{m_1 m_3}{m_2 m_4} \frac{\bar{E}}{\bar{E} + Q}\right)^{1/2} \text{ or } \gamma = \left(\frac{m_1 m_3}{m_2 m_4} \frac{1}{1 + \frac{m_1 + m_2}{m_2} \frac{Q}{\bar{E}}}\right)^{1/2} , \quad (2.5)$$

where Q is the so-called Q-value (level energy for inelastic neutron scattering, for example).

For elastic scattering we have thus Q = 0 and therefore

$$\gamma = \frac{\mathrm{m}_1}{\mathrm{m}_2} \tag{2.6}$$

is independent of incident energy.

Recall (see Figure 1 on page 10) that

- m₁ mass of incident particle,
- m₂ mass of target nucleus,
- m, mass of the scattered particle of which one is measuring the angular distribution,
- m4 mass of the residual nucleus.

Notice that (2.1) is **not unambiguous** for $\gamma > 1$ [EV55]. We will come back to this problem later in this chapter (**Section 2.4**).

We see that knowing a function-value in one of the reference systems concerned, it can be readily and exactly transformed to the other reference system using (2.1) to (2.4). These equations are thus suitable for a point-by-point transformation of an angular distribution of scattering data.

2.2.2 Transformation procedure for scattering angular distributions represented analytically.

Mathematically such angular distributions are continuous, finite and positive functions defined in the interval [-1,+1]. Naturally, they can therefore be well approximated by means of Legendre polynomials as they are defined in the same interval and have the advantageous property of being orthogonal. Furthermore, such a representation also results from nuclear models. Formally, the angular distribution concerned reads thus in the laboratory system

$$\frac{d\sigma}{d\mu}(\mu, E) = \frac{\sigma(E)}{2\pi} \sum_{\ell=0}^{\infty} (2\ell+1) a_{\ell}(E) P_{\ell}(\mu) , \qquad (2.7)$$

and in the center-of-mass system

$$\frac{d\bar{\sigma}}{d\bar{\mu}}(\bar{\mu},\bar{E}) = \frac{\bar{\sigma}(\bar{E})}{2\pi} \sum_{m=0}^{\infty} (2m+1) \bar{a}_{m}(\bar{E}) P_{m}(\bar{\mu}) , \qquad (2.8)$$

where P_i are Legendre polynomials and a_ℓ and \bar{a}_m are the coefficients of the **infi**nite series representing the angular distribution.

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Owing to the invariance of the total scattering probability we have

$$\sigma(\mathbf{E}) = \overline{\sigma}(\overline{\mathbf{E}})$$

Here we have taken the notation of the Evaluated Neutron Data File (ENDF). Consequently, a_{ℓ} and \bar{a}_{m} are dimensionless and $a_{0} = \bar{a}_{0} = 1$.

The **indices** ℓ and m are mnemonic, i.e., ℓ and m refer to the <u>l</u>aboratory and center-of-mass reference system, respectively.

Formally we have thus to deal with infinite series. In practice, however, ℓ , as well as m, has a finite upper limit for the following reasons:

- Angular distributions are simple functions from a mathematical point of view. Their representation does, therefore, not require a very high order approximation.
- Physically, neither experiments nor calculations can determine angular distributions exactly. They are therefore known only to an accuracy within a few percents. It makes, therefore, no sense to use an approximation far beyond this accuracy.

The transformation from one frame of reference to the other is, in practice, reduced to the transformation of a finite number of coefficients. We should, however, mention that the upper limit L for ℓ and the upper limit M for m are not necessarily equal. Given one of them in the original frame of reference the other must be determined on the basis of certain criteria. Roughly speaking, an **accuracy control** of both the transformation matrix elements (see (2.13) and (2.15)) as well as the transformation itself will permit us (see **CHAPTER 3**) to determine the upper limit of the index of the coefficients resulting from a transformation.

Note that the coefficients (a, \bar{a}) representing the angular distributions given in the original frame of reference system are applied as they appear in a file.

We are now going to establish the transformation from the representation (2.8) to that of (2.7), i.e., from the center-of-mass system to the laboratory system. This

can readily be performed thanks to the orthogonality of the Legendre polynomials. We obtain from (2.7)

$$a_{\ell}(E) = \frac{\pi}{\sigma(E)} \int_{-1}^{+1} P_{\ell}(\mu) \frac{d\sigma}{d\mu}(\mu, E) d\mu , \qquad (2.9)$$

and with (2.1)

$$a_{\ell}(E) = \frac{\pi}{\sigma(E)} \int_{-1}^{+1} P_{\ell}(\mu) \frac{d\sigma}{d\mu}(\mu, E) d\mu = \frac{\pi}{\sigma(E)} \int_{-1}^{+1} P_{\ell}(\mu) \frac{d\bar{\sigma}}{d\bar{\mu}}(\bar{\mu}, \bar{E}) d\bar{\mu} , \quad (2.10)$$

which becomes using (2.8)

$$a_{\ell}(E) = \frac{1}{2} \sum_{m=0}^{\infty} (2m+1) \bar{a}_{m}(\bar{E}) \int_{-1}^{+1} P_{\ell}(\mu) P_{m}(\bar{\mu}) d\bar{\mu} . \qquad (2.11)$$

Following the conventional notation we finally have

$$a_{\ell}(E) = \sum_{m=0}^{\infty} T_{\ell m} \tilde{a}_{m}(\tilde{E}) , \qquad (2.12)$$

where the matrix elements read

$$T_{\mathcal{A}m} = T_{\mathcal{A}m}(\gamma) = \frac{2m+1}{2} \int_{-1}^{+1} P_{\mathcal{A}}(\mu) P_{m}(\bar{\mu}) d\bar{\mu} \qquad (2.13)$$

The inverse transformation can be derived analogously. The results are

$$\bar{a}_{m}(\bar{E}) = \sum_{\ell=0}^{\infty} T_{m\ell}^{-1} a_{\ell}(E) , \qquad (2.14)$$

where

$$T_{m\ell}^{-1} = T_{m\ell}^{-1}(\gamma) = \frac{2\ell+1}{2} \int_{-1}^{+1} P_{m}(\tilde{\mu}) P_{\ell}(\mu) d\mu \qquad (2.15)$$

Formally, (2.12) to (2.15) define the transformation procedure we are seeking.

The main problem of this transformation procedure is the calculation of the transformation matrices T and T⁻¹, whose elements depend only on the variable γ . That

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seems a priori a simple task, but in practice it involves quite laborious algorithms, requires an error-analysis and leads to numerical stability problems.

A series of publications exist on this subject. Various algorithms have been proposed for the calculation of T and T^{-1} . They can essentially be classified into three main categories:

- Closed form expression of the matrix elements: In [ZW54] such expressions are given for the elements: T₁₀, T₁₁, T₂₀, T₂₁. In [AM56] and [AM58] T_{1m} are dealt with, and in [GE63] T_{1m} for any *l*, m are analytically represented as a multiple finite sum expression.
- Recurrence relation connecting different T-matrix (T-1-matrix) elements. Such relations are given in [AM56] and [BE65].
- 3. Expansion of the functions $T_{\ell m}(\gamma)$ and $T_{m\ell}^{-1}(\gamma)$ in powers of γ . This method is applied in [AM58], [AM64] and [BE77].

In summary, we thus have two transformation procedures at our disposal which are defined by (2.1) and (2.7) as well as (2.8), respectively. In principle one would be sufficient, but in practice both are necessary.

2.3 THE MERITS OF THE TWO TRANSFORMATION PROCEDURES.

Leaving details aside, one would be inclined to give preference to the transformation procedure defined in (2.1) rather than to that prescribed in (2.7) and (2.8). The former is in fact simple and exact. It requires, however, an appropriate tabulation of the angular distribution prior to the transformation and a subsequent fit to the transformed distribution if one wishes its parameterized representation; this is generally the case, especially if the data are prepared for later use in neutron transport calculations. Furthermore, the analytical representation has the advantage of permitting a considerable gain of computer storage-space.

Looking closer at the problem there are additional arguments which also fully justify the procedure using transformation matrices. Such arguments are:

- In the case of elastic scattering, the transformation matrix is independent of the incident particle energy as $\gamma = m_1/m_2$. This matrix therefore remains constant for a given reaction, even with various incident particle energies. Note that when using a point-by-point transformation, i.e., when using (2.1), (2.3) and (2.4), all transformation steps have to be performed for each incident energy: generation of an adequate $\mu(=\cos\theta)$ -distribution prior to the transformation, the transformation itself and a fit to the transformed distribution.
- Many angular distribution data in literature, and thus in the data files (experimental data, evaluated data), are in fact represented in analytical form. The application of transformation matrices for passing from one frame of reference system to the other one is in this case more appropriate.
- There are nuclear reactor codes (ETOG-1, MC²-A, AMPX) which make direct use of transformation matrices [HE71].
- The number of rows L of the transformation matrix T is related to the order of the so-called P_N-approximation used in neutron transport calculation. More precisely, N is put equal to L [WI76]. The determination of L is thus crucial for such calculations.

2.4 OBJECTIVES OF THE PRESENT STUDY.

The **present work** is in fact **devoted** to the transformation procedure of angular distribution probabilities which applies **transformation matrices**.

The main objectives of our study are:

- Seeking an economical method for calculating the matrices.
- Carrying out an error analysis for both the computation of the matrix elements and the transformation itself (size of matrix required for ensuring a given accuracy).

 Developing a method which allows treatment of the large amount of existing scattering angular distribution data, especially those in the Evaluated Neutron Data Files.

The quantity which predominantly determines the transformation from one given reference system to the other is γ which is defined in (2.5). According to this relation γ mathematically covers the interval $[-\infty,\infty]$. In physics, however, only positive values of γ are considered: $\gamma \in [0,\infty]$. The ultimate objective would of course be the study of the transformation matrices $T(\gamma)$ and $T^{-1}(\gamma)$ for $\gamma \in [0,\infty]$. However, for physical and mathematical reasons which will become more apparent in **CHAPTER 3** (see also the definition of (2.1)), we confine our investigation to a γ -range: $\gamma \in [0,1]$. This in fact already comprises a large variety of angular distributions of scattering probabilities; all but exotic cases in the Evaluated Neutron Data Files.

To illustrate the different characters of transformation, one will have to deal with the different γ -ranges we represent in **Figure 2** on page 18 $\mu(\gamma)$ as a function of $\bar{\mu}(\gamma)$, i.e., $\mu(\gamma) = f[\bar{\mu}(\gamma)]$, (2.4), for several γ -values.

Figure 2 on page 18 reveals three categories of functions f characterized by γ -values from the following γ -ranges:

1. $\gamma \in [0, 1^{-}]$ 2. $\gamma = 1$ 3. $\gamma \in [1^{+}, \infty]$

where 1- and 1+ denote the left- and right-side boundary of γ = 1, respectively.

Taking into account the definition of $T(\gamma)$, (2.13), and of $T^{-1}(\gamma)$, (2.15), one can immediately see that this behaviour of the function f has implications on the behaviour of the functions $T_{\ell m}(\gamma)$ and $T_{m\ell}^{-1}(\gamma)$ and thus manifestly affects the transformation itself.

Having now defined the transformation procedures at our disposal and indicated the main objectives of our study, we deal in the next chapter with the **calculation** of the transformation matrices using the power series expansion method and the



Figure 2. The functions $\mu[\hat{\mu}(\gamma)]: \gamma = 0, .4, .8, .95, 1, 1.05, 1.25, 2.$

determination of their size for practical applications. Both of necessity require an error-analysis.

3.0 TAYLOR SERIES EXPANSION METHOD.

3.1 GENERAL REMARKS.

In this method the functions $P_{\ell}[\mu(\gamma)]$ or $P_{\ell}[\bar{\mu}(\gamma)]$ are, in the vicinity of $\gamma = \gamma_1$, expanded in the form of Taylor series. Using the basic relation $\mu = \bar{\mu}, \gamma_1=0$, both integrals under study, (2.13) and (2.15), can be represented as power series in γ , the coefficients of which are in our case calculated by means of a recurrence formula. Such a representation of the integrals $T_{\ell m}$ and $T_{m\ell}^{-1}$ can be expected to be of practical usefulness in the neighbourhood of the point $\gamma = \gamma_1$ as long as the power series converge rapidly. **The main goals of this chapter are:**

- To find the convergence radius G of the Taylor series.
- To give a close-fitting error estimation of the calculated elements $T_{\ell m}$ and $T_{m\ell}^{-1}$.
- To determine the **speed of convergence** for $\gamma \leq G$. This can in fact be considered as a measure of the practical usefulness of the present method.
- To discuss the **applicability of this method** in nuclear physics, especially in the context of the Evaluated Neutron Data Files.

Before giving details of these investigations, a brief historical review on this method might be instructive.

The method was proposed for the first time by AMSTER, [AM58] and [AM64]. The author only applies this method formally in [AM58]. He does not discuss the convergence range of the series expansion nor does he give any error estimation analysis. In this form the method is of limited, practical use. AMSTER gives in [AM64] tables for some of the Taylor series expansion coefficients. However, these tables have to be used with care, as some of the values given are incorrect.

Much later BERSILLON et al.[BE77], for the particular case $\gamma = 0.01$, have shown that the Taylor series expansion method is much superior for numerical use than the recurrence formula method for the matrix elements T_{fm} , which is applied in [BE65]. This is, however, not surprising as it can generally be said that the Taylor series expansion method is, from a numerical point of view, usually superior to any other method of calculating a function in close proximity to the point of expansion.

In none of the above-mentioned references have such important items as convergence radius, error estimation and speed of convergence been investigated. The present method is, however, for practical use, only appropriate if we know in which range the Taylor series is convergent, are able to give a reasonable error estimation and know the behavior of convergence within the convergence radius.

In **Sections 3.2** and **3.3** we treat the functions $T_{\ell m}(\gamma)$. In Section 3.2 we give the mathematical formalism of the method, consider properties of the Taylor series coefficients, and study the convergence range of the series. Section 3.3 is devoted to the numerical calculation of the matrix elements $T_{\ell m}(\gamma)$. Special attention is paid to the error estimation of the $T_{\ell m}(\gamma)$.

In Sections 3.4 and 3.5 the functions $T_{m\ell}^{-1}(\gamma)$ are considered. In Section 3.4 we present the mathematical formalism and in Section 3.5 we discuss the numerical aspects, in particular, the problem of the error estimation of the computed $T_{m\ell}^{-1}(\gamma)$.

In **Section 3.6** we mention properties of the matrices T, T^{-1} , study their product, discuss the error due to the truncation of the infinite matrices and give some typical tables of these matrices together with the accuracy to which their elements are computed.

In Section 3.7 we discuss the applicability of the Taylor series expansion method for practical cases in physics, in particular in view of the treatment of Evaluated Neutron Data Files. The results are summarized in a table where we also give the speed of computation for various values of γ which is in fact a measure of the practical usefulness of the present method.

In Section 3.8 we summarize the essential results of CHAPTER 3, recapitulate interesting mathematical relations which have been derived and briefly discuss possible extensions of the Taylor series method to the range $\gamma > 1$.

3.2 TAYLOR SERIES REPRESENTATION OF THE FUNCTIONS T $_{fm}(\gamma)$.

3.2.1 General formalism.

We recapitulate here briefly the formalism as it is given in detail in [AM58] and [BE77]. The functions $T_{\rho_m}(\gamma)$ are defined as follows

$$T_{\ell m}(\gamma) = \frac{2m+1}{2} \int_{-1}^{+1} P_{\ell}[(\gamma + \bar{\mu})(1 + 2\gamma \bar{\mu} + \gamma^2)^{-1/2}] P_{m}(\bar{\mu}) d\bar{\mu} , \qquad (3.1)$$

where ℓ , m = 0, 1, 2, ...,

P, are Legendre polynomials,

 γ and $\bar{\mu}$ are variables already defined in **CHAPTER 2**, (2.3 to 2.5).

The variable μ in the laboratory system is related to the variable $\bar{\mu}$ in the center-of-mass system as follows

$$\mu = (\gamma + \overline{\mu}) (1 + 2\gamma \overline{\mu} + \gamma^2)^{-1/2}$$
which becomes, for $\gamma = 0$

$$\mu = \overline{\mu} \qquad (3.3)$$

This basic relation suggests a representation of

$$\mathbb{P}_{\rho}[(\gamma+\bar{\mu})(1+2\gamma\bar{\mu}+\gamma^2)^{-1/2}]$$

in (3.1) in the form of Taylor series about the point $\gamma_1 = 0$ as the integrant then reads $P_{\rho}(\bar{\mu})P_{m}(\bar{\mu})$ and thus the integral is analytically well known.

 ${\tt P}_{{}_{\sigma}}(\mu)$ represented as a power series then reads

$$P_{\ell}[\mu(\gamma)] = \sum_{r=0}^{\infty} \frac{\gamma^{r}}{r!} \frac{\partial^{r} P_{\ell}[\mu(\gamma=0)]}{\partial \gamma^{r}} , \qquad (3.4)$$

where the notation $\mu(\gamma=0)$ means γ is equalised to zero **after** the derivation.

The r-th derivative of P $_{
m \prime}(\mu)$ with respect to γ is given by the relation

$$\frac{\partial^{r} P_{\ell}[\mu(\gamma,\bar{\mu})]}{\partial \gamma^{r}} = (1+2\gamma\bar{\mu}+\gamma^{2})^{-1/2} r! \sum_{p=|\ell-r|}^{\ell+r} b_{\ell p}^{r} P_{p}(\mu)$$
(3.5)

which becomes, for $\gamma = 0$

$$\frac{\partial^{r} P_{\ell}[\mu(\gamma,\bar{\mu})]}{\partial \gamma^{r}} = r! \sum_{p=|\ell-r|}^{\ell+r} b_{\ell p}^{r} P_{p}[\mu(\gamma=0)]$$
(3.6)

and with (3.3)

$$= r! \sum_{p=|\ell-r|}^{\ell+r} b_{\ell p}^{r} P_{p}(\bar{\mu})$$

Putting this expression into (3.4), (3.1) becomes

$$\mathbb{T}_{\ell m}(\gamma) = \frac{2m+1}{2} \int_{-1}^{+1} \sum_{r=0}^{\infty} \frac{\gamma^{r}}{r!} r! \sum_{p=|\ell-r|}^{\ell+r} \mathbf{b}_{\ell p}^{r} \mathbf{P}_{p}(\bar{\mu}) \mathbf{P}_{m}(\bar{\mu}) d\bar{\mu} \quad . \tag{3.7}$$

The integral appearing in (3.7) is well known [GR65,p.820]

$$\int_{-1}^{+1} P_{p}(\bar{\mu}) P_{m}(\bar{\mu}) d\bar{\mu} = \frac{2}{2m+1} \delta_{pm}$$
(3.8)

which is nothing other than the orthogonality relation of the Legendre polynomials.

Using (3.8), the relation (3.7) becomes

$$T_{\ell m}(\gamma) = \sum_{r=|\ell-m|}^{\infty} \gamma^{r} b_{\ell m}^{r} \qquad (3.9)$$

The coefficients $b_{\mathcal{I}m}^{\mathbf{r}}$ can be calculated by means of the following recurrence formula

$$b_{\ell,m}^{r+1} = \frac{(m+1)(m+2-r)}{(r+1)(2m+3)} b_{\ell,m+1}^{r} - \frac{m(m+r-1)}{(r+1)(2m-1)} b_{\ell,m-1}^{r} , \qquad (3.10)$$

with the initial values

$$b_{\ell m}^{0} = \delta_{\ell m} \qquad (3.11)$$

A rather lengthy proof of the recurrence relation (3.10) has been sketched in [AM58] and given more explicitly in [BE77]. We propose a more compact proof of this relation.

$$\frac{\partial^{r+1}}{\partial \gamma^{r+1}} P_{\ell}[\mu(\gamma,\bar{\mu})] = (1+2\gamma\bar{\mu}+\gamma^{2})^{-\frac{r+1}{2}} (r+1)! \sum_{p=|\ell-r-1|}^{\ell+r+1} b_{\ell o}^{r+1} P_{p}[\mu(\gamma)] =$$

$$= \frac{\partial}{\partial \gamma} \{\frac{\partial^{r}}{\partial \gamma^{r}} P_{\ell}[\mu(\gamma,\bar{\mu})]\} = (3.12)$$

$$= (1+2\gamma\bar{\mu}+\gamma^{2})^{-\frac{r+1}{2}} (r+1)! \sum_{p=|\ell-r|}^{\ell+r} b_{\ell p}^{r} \frac{p(p+1-r)}{(r+1)(2p+1)} P_{p-1}(\mu)$$

$$= \frac{\ell+r}{p=|\ell-r|} b_{\ell p}^{r} \frac{(p+1)(p+r)}{(r+1)(2p+1)} P_{p+1}(\mu)].$$

By putting $\gamma = 0$ in (3.12), multiplying the resulting equation by $P_{m}(\bar{\mu})$ and then integrating it one obtains

$$\frac{\mathcal{A}+r+1}{\Sigma} \qquad b_{\mathcal{A}p}^{r+1} \int_{-1}^{+1} P_{p}(\bar{\mu}) P_{m}(\bar{\mu}) d\bar{\mu} = \\
= \frac{\mathcal{A}+r}{\Sigma} \qquad b_{\mathcal{A}p}^{r} \frac{p(p+1-r)}{(r+1)(2p+1)} \int_{-1}^{+1} P_{p-1}(\bar{\mu}) P_{m}(\bar{\mu}) d\bar{\mu} - \\
- \frac{\mathcal{A}+r}{\Sigma} \qquad b_{\mathcal{A}p}^{r} \frac{(p+1)(p+r)}{(r+1)(2p+1)} \int_{-1}^{+1} P_{p+1}(\bar{\mu}) P_{m}(\bar{\mu}) d\bar{\mu} .$$
(3.13)

Using relation (3.8) one obtains (3.10) directly from (3.13).

We now discuss some properties of the Taylor series coefficients $b_{\ell m}^r$.

3.2.2 Properties of the coefficients $b_{\ell m}^r$.

1.

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$$b_{\ell m}^{0} = \delta_{\ell m} . \qquad (3.14)$$

This follows directly from (3.4) and (3.8).

2.

$$b_{\ell m}^{r} = 0$$
 (3.15)

for: a)
$$|l-m| > r$$
;
b) $|l-m| < r$ r-odd and $l+m$ -even, or
r-even and $l+m$ -odd.

Using (3.10) and supposing that (3.15) is true for r, one can show that it is also true for r+1, hence for any r.

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$$b_{0m}^{r} = 0$$
(3.16)
for any m and r > 0.

This can again be shown by the induction method using (3.10).

4.

$$b_{\ell m}^{r} = 0$$
 (3.17)
for r > 2 and r-even, m = 1, 3, 5, ...,r-3
r-odd, m = 0, 2, 4, ...,r-3.

This can be shown by using (3.10) taking into account that the coefficients of $b_{f,m+1}^{r}$ are equal to zero when m+2 = r.

5.

$$\sum_{m=|\ell-r|}^{\ell+r} b_{\ell m}^{r} = 0 \qquad (3.18)$$

This follows from (3.5). Putting $\frac{\partial^{r-1}}{\partial \gamma^{r-1}} P_{\mathcal{A}}[\mu(\gamma,\bar{\mu})] = h[\mu(\gamma,\bar{\mu})] \text{ and } \frac{\partial}{\partial \gamma} h[\mu(\gamma,\bar{\mu})] = \frac{\partial h}{\partial \mu} \frac{\partial \mu}{\partial \gamma} ,$

now $\partial \mu / \partial \gamma (\gamma = 1) = 0$, thus (3.18) is valid.

6.

$$b_{\ell m}^{r} = 0 \qquad (3.19)$$
for ℓ -odd and $m < (\ell-1)/2$
for ℓ -odd and $m \ge (\ell-1)/2$ and $r > m+1$.

7.

Both cases follow from properties 2 and 4.

This property is of particular importance, as from it follows that the T_{m} (*2-cdd*) are polynomials and T_{m} (*2-cven*) are represented as infinite series.

$$\sum_{r=|2n+1-m|}^{\infty} b_{2n+1,m}^{r} = T_{2n+1,m}(\gamma=1) = (3.20)$$

$$= (-1)^{n+m+1} \frac{2^{n+1}}{n!} (2n+1)!! \frac{(2m-2n-3)!!}{(2m+2n+3)!!} (2m+1) \frac{(m+n)!}{(m-n)!},$$

$$\sum_{r=|2n-m|}^{\infty} b_{2n,m}^{r} = T_{2n,m}(\gamma=1) = (3.21)$$

$$= (-1)^{n+m-1} \frac{(2m+1)}{2^{n}} \frac{n!}{(n-m)!} \frac{(2n+2m-1)!!}{(2n-1)!!} \frac{(2n-2m-3)!!}{(n+m+1)!}.$$

As we will see later (Subsection 3.3.3), these are central relations for the study of convergence of the Taylor series as well as for the error estimation of the computed $T_{\ell m}$. We have verified (3.20) and (3.21) numerically using the identity

$$T_{\ell m}(\gamma=1) = (-1)^{m} 2(2m+1) \int_{0}^{1} P_{\ell}(\mu) P_{m}(1-2\mu^{2}) \mu d\mu \qquad (3.22)$$

which follows from (3.1) and (3.22) using an analytical evaluation of the integral which will be shown later (see in 3.2.4.2).

We now investigate the important problem of the properties of the Taylor series (3.9).

3.2.3 Convergence of the Taylor series (3.9).

For this purpose let us write down once more the formula (3.9)

$$T_{\ell m}(\gamma) = \sum_{r=|\ell-m|}^{\infty} \gamma^{r} b_{\ell m}^{r} \qquad (3.9)$$
We know from property 6, (3.19), that the $T_{\ell m}(\gamma)$ are represented by polynomials for ℓ -odd. The functions $T_{\ell m}(\gamma)$ have thus finite values for ℓ -odd. For ℓ -even, however, the $T_{\ell m}(\gamma)$ are represented by infinite series. In fact we have ℓ series to which ℓ convergence radii correspond. Here, we are not interested in finding the convergence radius for each series, but in determining a common convergence radius for all series. As we have already pointed out in **Section 2.4**, the present study is limited to the γ -range $0 \leq \gamma \leq 1$. This actually covers a large variety of cases in physics and is sufficient for our purpose, particularly in view of the application of this method for the treatment of Evaluated Neutron Data Files.

The computation of $T_{\ell m}(\gamma)$ shows that, for a given accuracy, the number of terms of the series to be calculated increases rapidly when γ is approaching the value equal to 1 (see **Figure 3** on page 27). We can thus assume that the series (3.9) converge within the radius $\gamma = 1$. In fact, according to (3.20) and (3.21) the series (3.9) have definite values for $\gamma = 1$, i.e., they are still convergent for $\gamma = 1$ and therefore also convergent for $0 \le \gamma < 1$. This of course does not mean that the Taylor series expansion method is still of practical usefulness when γ is approaching the value 1. We will investigate this problem in 3.3.4.2.

3.2.4 Annex to Section 3.2.

3.2.4.1 DETAILS OF THE CALCULATION OF $\partial^r P_{\mu}(\bar{\mu})/\partial \gamma^r$.

Using (3.1) and (3.4) the functions T _m read

$$T_{\ell m}(\gamma) = \frac{2m+1}{2} \int_{-1}^{+1} \sum_{r=0}^{\infty} \frac{\gamma^{r}}{r!} \frac{\partial^{r} P_{\ell}(\mu(\gamma=0))}{\partial \gamma^{r}} P_{m}(\bar{\mu}) d\bar{\mu}$$

and for $\partial^r P_{\mu}(\mu)/\partial \gamma^r$ one obtains:

$$\frac{\mathbf{r} = 1}{\frac{\partial P_{\ell}[\mu(\gamma, \bar{\mu})]}{\partial \gamma}} = (1 + 2\gamma \bar{\mu} + \gamma^2)^{-1/2} \frac{\ell(\ell+1)}{2\ell+1} \left[P_{\ell-1}(\mu) - P_{\ell+1}(\mu) \right]$$

$$\mathbf{r} = 2$$



Figure 3. Number of non-vanishing terms: The number of non-vanishing terms of the series $T_{Am}(\gamma)$, (3.9), to be calculated in dependence on the variable γ for a fixed accuracy ($\leq 10^{-4}$, relative error) demonstrated for the matrix element $T_{2\gamma}$.

$$\frac{\partial^{2} P_{\ell}[\mu(\gamma,\bar{\mu})]}{\partial \gamma^{2}} = (1+2\gamma\bar{\mu}+\gamma^{2})^{-1} \frac{\ell(\ell+1)}{2\ell+1} \left\{ \frac{(\ell-1)^{2}}{2\ell-1} P_{\ell-2}(\mu) - \left[\frac{(\ell-1)(\ell+1)}{2\ell-1} + \frac{(\ell+1)(\ell+3)}{2\ell+3} \right] P_{\ell}(\mu) + \frac{(\ell+2)^{2}}{2\ell+3} P_{\ell+2}(\mu) \right\} .$$

$$r = 3$$

$$\frac{\partial^{3} P_{\ell}[\mu(\gamma,\bar{\mu})]}{\partial \gamma^{3}} = (1+2\gamma\bar{\mu}+\gamma^{2})^{-3/2} \frac{\ell(\ell+1)}{2\ell+1} \left\{ \frac{(\ell-3)(\ell-2)(\ell-1)^{2}}{(2\ell-3)(2\ell-1)} P_{\ell-3}(\mu) - \frac{(\ell-1)\ell(\ell+1)(6\ell^{2}+7\ell+7)}{(2\ell-1)(2\ell+1)(2\ell+3)} P_{\ell-1}(\mu) + \frac{(\ell+1)(\ell+2)(12\ell^{4}+56\ell^{3}+65\ell^{2}-16\ell-34)}{(2\ell-1)(2\ell+1)(2\ell+3)(2\ell+5)} P_{\ell+1}(\mu) - \frac{(\ell+2)^{2}(\ell+3)(\ell+4)}{(2\ell+3)(2\ell+5)} P_{\ell+3}(\mu) \right\} .$$

These terms already show the gradual way the Equation (3.5) is built up.

$$\frac{\partial^{2} P_{\ell}[\mu(\gamma,\bar{\mu})]}{\partial \gamma^{r}} = (1+2\gamma\bar{\mu}+\gamma^{2})^{-r/2} r! \sum_{p=|\ell-r|}^{\ell+r} b_{\ell p}^{r} P_{p}(\mu) .$$

3.2.4.2 PARTICULAR CASES.

3.2.4.2.1
$$T_{\ell m}(\gamma)$$
 for $\gamma = 1$.

For $\gamma = 1$, formula (3.1) reads

$$T_{\ell m}(\gamma=1) = \frac{2m+1}{2} \int_{-1}^{+1} P_{\ell}[(\frac{1+\bar{\mu}}{2})^{1/2}] P_{m}(\bar{\mu}) d\bar{\mu} . \qquad (3.23)$$

Using the relation between μ and $\bar{\mu}$ (3.2) we obtain, for $\gamma = 1$ $\bar{\mu}^2 = 2\mu^2 - 1$. (3.24)

Replacing the variable $\bar{\mu}$ in (3.23) by μ , using relation (3.24), yields

$$\mathbb{T}_{\ell m}(\gamma=1) = (2m+1) \begin{cases} +1 \\ P_{\ell}(\mu) P_{m}(1-2\mu^{2}) \mu \, d\mu \end{cases}$$
(3.25)

This integral can be evaluated analytically replacing either $P_{\ell}(\mu)$ (Method A) or $P_{m}(1-2\mu^{2})$ (Method B) by their explicit polynomial expression:

Method A.

$$P_{f}(\mu) = \sum_{j=0}^{\ell} a_{\ell j} \mu^{j} , \qquad (3.26)$$

-

where

$$\mathbf{a}_{\ell j} = (-1)^{\frac{\ell-j}{2}} \frac{(\ell+j)!}{2^{\ell} (\frac{\ell+j}{2})! (\frac{\ell-j}{2})! j!} \qquad (3.27)$$

Method B.

$$P_{m}(1-2\mu^{2}) = \sum_{j=0}^{m} b_{mj} \mu^{2j}, \qquad (3.28)$$

where

$$b_{mj} = (-1)^{j} {\binom{m+j}{j}} {\binom{m}{j}} , {\binom{m}{j}} = \frac{m!}{j!(m-j)!} .$$
 (3.29)

Inserting (3.26) into (3.25) we have

$$T_{\ell m}(\gamma=1) = (-1)^{m} 2(2m+1) \sum_{j=0}^{\ell} a_{\ell j} \int_{0}^{1} \mu^{j} P_{m}(1-2\mu^{2}) d\mu \qquad (3.30)$$

This type of integral is tabulated in [GR65,p.823]. $T_{\chi m}(\gamma=1)$ can thus be expressed in terms of Γ functions

$$T_{\ell m}(\gamma=1) = (2m+1) \sum_{j=0}^{\ell} a_{\ell j} \frac{\Gamma(\frac{j+2}{2})^2}{\Gamma(\frac{j+2}{2} + m+1) \Gamma(\frac{j+2}{2} - m)} . \qquad (3.31)$$

Inserting (3.28) into (3.25) and using the analytical expression for the integral of the form

$$\int_0^1 \mu^{\Gamma} P_{\mathfrak{m}}(\mu) d\mu ,$$

as given in [GR65,p.796] we obtain, for (3.25)

$$T_{\ell m}(\gamma=1) = (-1)^{m} 2(2m+1) \sum_{j=0}^{m} b_{mj} \frac{\sqrt{\pi} \Gamma(2j+2)}{2^{2j+2} \Gamma(1+\frac{2j+1-\ell}{2}) \Gamma(\frac{3}{2}+\frac{2j+1+\ell}{2})}.(3.32)$$

Equs.(3.31) (Method A) and (3.32) (Method B) are equivalent to the corresponding closed form expressions (3.20) and (3.21). This identity leads to a new representation of the integrals of the form

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$$\int_{0}^{1} x^{r} P_{s}(x) dx \text{ and } \int_{0}^{1} x^{r} P_{s}(1-2x^{2}) dx$$

3.2.4.2.2 Explicit expressions of ${\rm T}_{\ell m}$ for some special $\ell,$ m.

In the following Table we summarize the results given above.

Table: First terms of T_{2n.0}.

	γ^2	γ^4	γ ⁶	γ ⁸	γ ¹⁰
^T 20	1 5	$\frac{1}{5.7}$	<u>э</u> 5.7.9	<u>3</u> 7.9.11	<u>Э</u> 9.11.13
^T 40		$-\frac{1}{7.9}$	$-\frac{6}{7.9.11}$	$-\frac{45}{7.9.11.13}$	$-\frac{60}{9.11.13.15}$
^т 60			<u>Э</u> 9.11.13	<u>5</u> 11.13.15	$\frac{70}{11.13.15.17}$
^т во				$-\frac{15}{11.13.15.17}$	$-\frac{420}{11.13.15.17.19}$

Only the functions $T_{\ell 0}(\gamma)$ appear in the transformation of an angular distribution which is **isotropic** in the center-of-mass to the laboratory system. This transformation reads

$$a_{\ell} = T_{\ell 0} \cdot \bar{a}_{0}$$
 ,

and the corresponding kinematic formula has the form

$$\frac{d\sigma}{d\omega}(\mu) = \frac{(1+2\gamma\bar{\mu}+\gamma^2)^{3/2}}{|1+\gamma\bar{\mu}|} \frac{d\bar{\sigma}}{d\bar{\omega}}(\bar{\mu}) , \text{ here } \frac{d\bar{\sigma}}{d\bar{\omega}} \approx \frac{\sigma}{2\pi} ,$$

and using (2.7)

$$\sum_{\ell=0}^{\infty} (2\ell+1) a_{\ell} P_{\ell}(\mu) = \frac{(1+2\gamma\bar{\mu}+\gamma^2)^{3/2}}{|1+\gamma\bar{\mu}|}$$

We thus obtain

$$\frac{d\sigma}{d\omega}(\mu=1) = (1+\gamma)^2 , \qquad \sum_{\ell=0}^{\infty} (2\ell+1) T_{\ell 0} = (1+\gamma)^2 , \qquad ,$$

$$\frac{d\sigma}{d\omega}(\mu=0) = (1-\gamma^2)^{1/2} , \qquad \sum_{\ell=0}^{\infty} (2\ell+1) P_{\ell}(\mu=0) T_{\ell 0} = (1-\gamma^2)^{1/2} , \qquad ,$$

$$\frac{d\sigma}{d\omega}(\mu=-1) = (1-\gamma)^2 , \qquad \sum_{\ell=0}^{\infty} (-1)^{\ell} (2\ell+1) T_{\ell 0} = (1-\gamma)^2 .$$

These relations can be used for calculating the exact value of the rest of the Taylor series representing the functions $T_{J0}(\gamma)$.

•

.

$$\begin{aligned} \frac{1}{2} - even, \ m = 1 \\ T_{21} &= -6.3 \sum_{k=0}^{\infty} (k+1) \frac{(2k-3)!!}{(2k+5)!!} \gamma^{2k+1} , \\ T_{41} &= 6.3.5 \sum_{k=1}^{\infty} (k+1)k \frac{(2k-3)!!}{(2k+7)!!} \gamma^{2k+1} , \\ T_{61} &= -\frac{6}{2} \cdot 3 \cdot 5 \cdot 7 \sum_{k=2}^{\infty} (k+1)k(k-1) \frac{(2k-3)!!}{(2k+9)!!} \gamma^{2k+1} , \\ T_{81} &= \frac{6}{2 \cdot 3} \cdot 3 \cdot 5 \cdot 7 \cdot 9 \sum_{k=3}^{\infty} (k+1)k(k-1)(k-2) \frac{(2k-3)!!}{(2k+11)!!} \gamma^{2k+1} , \\ T_{2n,1} &= (-1)^{n} 6 \frac{(2n+1)!!}{(n-1)!!} \sum_{k=n-1}^{\infty} \frac{(k+1)!}{(k-n+1)!} \frac{(2k-3)!!}{(2k+2n+3)!!} \gamma^{2k+1} \\ \hline \\ \frac{1}{2} = 3 \\ T_{3m} &= \frac{m(m+2)(5m+11)}{2(2m+3)(2m+5)} (-\gamma)^{m+1} - \frac{m(m-1)(5m+8)}{(2m-1)(2m+3)} (-\gamma)^{m-1} + \\ &+ \frac{5m(m-1)(m-2)}{2(2m-1)(2m-3)} (-\gamma)^{m-3} . \end{aligned}$$

$$\begin{array}{l} \boxed{ \mbox{$\ell=5$} \end{tabular}} \\ \hline \mbox{I_{5m}} = - \frac{1}{8} \frac{m(m-1)(m+2)(2m+1)(21m^2+119m+158)}{(2m+1)(2m+3)(2m+5)(2m+7)} (-\gamma)^{m+1} + \\ + \frac{1}{8} \frac{m(m-1)(m-2)(2m+1)(2m+3)(2m+1)(2m+3)}{(2m+1)(2m+3)(2m+5)} (-\gamma)^{m-1} - \\ - \frac{7}{6} \frac{m(m-1)(m-2)(m-3)(2m+1)(9m+14)}{(2m-3)(2m-1)(2m+1)(2m+3)} (-\gamma)^{m-5} \\ + \frac{21}{8} \frac{m(m-1)(m-2)(m-3)(m-4)(2m+1)}{(2m-5)(2m-3)(2m-1)(2m+1)} (-\gamma)^{m-5} \\ \hline \mbox{I_{7m}} = \frac{1}{80} \frac{m(m-1)(m-2)(m-3)(2m+1)(143m^3+1452m^2+4705m+4796)}{(2m+1)(2m+3)(2m+5)(2m+7)(2m+9)} (-\gamma)^{m-1} \\ - \frac{1}{80} \frac{m(m-1)(m-2)(m-3)(2m+1)(143m^3+1089m^2+2644m+2048)}{(2m-1)(2m+1)(2m+3)(2m+5)(2m+7)} (-\gamma)^{m-1} \\ + \frac{3}{80} \frac{m(m-1)(m-2)(m-3)(m-4)(2m+1)(143m^3+1089m^2+2644m+2048)}{(2m-3)(2m-1)(2m+1)(2m+3)(2m+5)} (-\gamma)^{m-3} \\ - \frac{11}{260} \frac{m(m-1)(m-2)(m-3)(m-4)(m-5)(2m+1)(13m+20)}{(2m-3)(2m-1)(2m+1)(2m+3)} (-\gamma)^{m-5} \\ + \frac{11.13}{80} \frac{m(m-1)(m-2)(m-3)(m-4)(m-5)(m-6)(2m+1)}{(2m-7)(2m-5)(2m-3)(2m-1)(2m+1)} (-\gamma)^{m-7} \\ \hline \mbox{I_{5m}} = -\frac{1}{2668} (-\gamma)^{m-9} (m-3)(m-2)(m-1)m \\ \hline \mbox{I_{5m}} = -\frac{1}{2668} (-\gamma)^{m-9} (m-3)(m-2)(m-1)m \\ \hline \mbox{I_{2m}} = -\frac{1}{(2m-1)(2m+1)(2m+3)(2m+5)(2m+7)(2m+9)(2m+11)} \\ \hline \mbox{I_{2m}} = -\frac{1}{(2m-1)(2m+1)(2m+3)(2m+5)(2m+7)(2m+9)(2m+11)} \\ \hline \mbox{I_{2m}} = -\frac{1}{2668} (-\gamma)^{m-9} (m-3)(m-2)(m-1)m \\ \hline \mbox{I_{2m}} = -\frac{1}{(2m-1)(2m+1)(2m+1)(2m+3)(2m+5)(2m+7)(2m+9)(2m+11)} \\ \hline \mbox{I_{2m}} = -\frac{1}{2668} (-\gamma)^{m-9} (m-3)(m-2)(m-1)m \\ \hline \mbox{I_{2m}} = -\frac{1}{(2m-1)(2m+1)(2m+3)(2m+5)(2m+7)(2m+9)(2m+1)} \\ \hline \mbox{I_{2m}} = -\frac{1}{2668} (-\gamma)^{m-9} (m-3)(m-2)(m-1)m \\$$

11.13.17 $\frac{(m-4)(m-5)(m-6)(m-7)(m-8)(2m+1)}{(2m-9)(2m-7)(2m-5)(2m-3)(2m-1)(2m+1)}$].

3.3 NUMERICAL EVALUATION OF THE POWER SERIES EXPRESSION OF T $_{fm}(\gamma)$.

Once the coefficients $b_{\ell m}^r$ of the power series (3.9) are known, the functions $T_{\ell m}(\gamma)$ are also known. The infinite series (3.9) have, of course, to be curtailed and it will be one of our main tasks in this section to find a **close estimation of the error** which is caused by such a truncation.

We turn first to the computation of the power series coefficients b_{Am}^{r} .

3.3.1 Computation of the matrices b_{m}^{r} .

By means of the recurrence formula (3.10) and the initial values (3.11) the coefficients $b_{\ell m}^{r}$ can be evaluated. This computation has been carried out on a **CDC-7600** using the program **MICOF** (see **Annex-3**). The matrices $b_{\ell m}^{r}$ for r = 1, 2, ..., 6 and $\ell = 1, 2, ..., 11, m = 0, 1, ..., 11$ are given in **Table 3.1**.

	REILO	1	~ ~ ~	2		5			9	a	10	11
1	2		-2			0					0	
2	3	6	3 0	-6	0	0	0	0	0	0	0	0
3	0	5	12	5	-12	0	0	0	0	0	0	0
4	0	0	7	20	7	-27)	0	0	0	0	0	0
5	0	0	c	-9 0	30	-9	-30	0	0	0	0	0
6	0	0	0	0	11 0	42	11 0	-42	0	0	0	o
7	o	0	0	0	0	13 0	56	13 0	-56	0	0	0
8	o	0	0	0	0	0	15 0	72	15 0	-72	0	0
9	0	0	0	0	0	0	0	17 0	90	17 0	90	0
10	o	0	0	0	0	0	0	0	19 0	110	19 0	-110
11	0	0	0	0	0	0	0	0	0	21 0	132	21 0
			······								23	
LH	R = 2 0	1	2	3	4	5	6	7	8	9	10	11
1	0	3	0	35	0	0	0	0	0	0	0	0
2	15	0	-11	0	48 35	٥	٥	0	0	0	0	¢
3	0	24 35	0	-46 15	0	50 21	0	0	0	0	0	0
4	o	0	10	0	390 77	0	40 11	0	0	0	0	¢
5	0	0	0	80 33	0	-295 39	0	735 143	0	0	0	0
6	0	0	0	0	525 143	0	-581 55	0	448 65	0	0	0
7	0	0	0	0	0	336 65	0	-3108 221	0	756 85	0	0
8	0	0	0	0	0	O	588 85	0	-1716 95	0	3600 323	0
9	0	o	0	0	0	0	0	2880 323	0	-2685 119	٥	1815 133
10	0	0	0	٩	0	0	0	0	1485 133	0	-12045 437	0
11	0	0	0	0	0	0	0	0	0	2200 161	0	-5786 175
·												
LH	R = 3 0	1	2	Э	4	5	6	7	8	9	10	11
1	0	0	\$	0	-7	0	0	0	0	0	0	0
2	0	-12 35	0	28 15	0	-32 21	0	0	0	0	0	0
3	0	0	-4	0	48 11	0	~100 33	0	0	0	0	0
4	0	21	0	-112 33	0	2300 273	0	-2240 429	0	0	0	0
5	0	0	160 231	0	-6900 1001	0	476 33	0	-1176 143	0	0	0
6	0	0	0	700 429	0	-476 39	0	55272 2431	0	-2688 221	0	0
7	0	0	0	0	448 143	0	-18424 935	0	41664 1235	0	-5544 323	0
8	0	0	0	0	0	1176 221	0	-124992 4199	0	5688 119	0	52800 2261
9	O	0	D	0	0	0	2688 323	0	-5688 133	0	485100 7429	0
10	0	D	0	0	0	0	0	3960 323	0	-23100 391	0	8228 95
11	0	0	0	0	0	٥	0	0	52800 3059	0	-172788 2185	0

LM	R = 4 0	1	2	3	4	5	6	7	8	9	10	11
1	0	0	0	الم	0	59	0	0	0	0	0	C
2	35	0	3 7	Û	-816 385	0	128 77	0	0	0	0	0
3	D	0	0	65 33	0	-220 39	C	525 143	0	0	0	0
4	-1 63	0	-340 693	0	5787 1001	0	-8480 693	•	8960 1287	0	0	0
5	0	0	٥	80 39	0	521 39	C	-5145 221	0	2646 221	0	0
6	0	0	25 143	0	-795 143	0	4970 187	0	-109760 2717	0	80640 4199	0
7	0	0	0	896 1287	0	-120736 9945	0	2202606 46189	0	-72336 1105	0	9438 323
8	0	0	C	0	4410 2431	0	-82320 3553	0	19590 247	0	-747360 7429	0
9	0	0	0	0	0	16128 4199	0	-1183680 29393	0	340626 2737	0	-335049 2261
10	o	0	0	0	0	0	2310 323	0	-28545 437	0	6926931 37145	0
11	0	0	0	0	0	0	0	633600 52003	0	-274912 2737	0	107393 399
					·····							
LM	R = 5 0	1	2	3	4	5	6	7	8	9	10	11
1	0	0	0	0	6 11	0	-6 11	0	0	0	0	0
2	0	-2 35	0	-82 165	0	640 273	0	-256 143	0	0	0	0
3	0	0	0	0	-372 143	0	76 11	0	-56 13	0	0	0
4	0	77	0	124 143	0	-776 91	0	40000 2431	0	-21504 2431	0	0
5	0	0	0	0	582 143	0	-4078 187	0	8428 247	0	5292 323	0
6	0	-2 143	0	-266 429	0	8156 663	o	-2200100 46189	0	155904 2431	0	-118272 4199
7	0	0	0	. 0	-6720 2431	0	528024 17765	0	-115056 1235	0	831600 7429	0
8	0	0	0	392 2431	0	-33712 4199	0	169200 2717	0	-50184 299	0	297792 1615
9	0	0	0	0	32256 46189	0	-66816 3553	C	4692204 39767	0	- 45 8172 1615	0
10	0	0	0	0	0	8316 4199	٥	~3712500 96577	0	17622 85	0	*******
11	0	0	0	0	0	0	33792 7429	0	-1091904 15295	0	38267944 111435	0
r 									<u> </u>			
L M 1	R=6 0	0	2	<u>3</u> 0		-7	6 0	7	8	9	10	110
2	1	0	17	0	2784	13 0	-2944	13	4096	0	0	0
3	105	0	231	0	5005	42	1155 0	-1806	2145	84	0	0
4	-2	0	-290	0	~1308	13	45520	221	-171520	17 0	501760	0
5	231	0	3003	0	1001	-1491	3927	135345	8151	-798	46189	6930
	1	0	22	0	2414	221	-237670	4199	620480	17	-100364544	323
7	429		429	۰ م	2431	144349	10659	-745977	8151	313120	1062347	-1420054
		•	-20		-22768	20995	77560	4199	-436390	1955	7869990	8075
	J		2431		46189	_7(*	3553	3767594 0	3289	_7/0100	25415	V
, ,	0	0	0	0	0	221		3/5/5360 6760 39	0	-/40190 2737	0	37 (8346 6783
10	0	0	0	0	630 4199	0	-80010 7429	0	36729 299	0		0
11	0	0	0	0	0	67584 96577	0	-90583584 3380195	0	an a	0	an a

From **Table 3.1** one can see that many of the matrix elements $b_{\ell m}^{\Gamma}$ are zero as it was pointed out in the Subsection 3.2.2 which treats the properties of these matrices. As one knows which elements of $b_{\ell m}^{\Gamma}$ do not vanish, one can considerably reduce the storage space of the matrices $b_{\ell m}^{\Gamma}$ (see Annex-3).

Note that these coefficients are variable-independent and thus have only to be computed once. The computation of the functions $T_{\ell m}(\gamma)$ is thus split up into two parts when using the Taylor series method, the computation of constants, i.e., the matrices $b_{\ell m}^{r}$, and the simple summation of the power series. In practice the computation of the functions $T_{\ell m}(\gamma)$ is therefore simply limited to the summation of the power series.

This even makes the Taylor series expansion method attractive when γ approaches the value equal to 1, i.e., when it approaches the common convergence radius. However, this point will be investigated more precisely in 3.3.4.2.

To summarize, the most interesting numerical aspects of the Taylor series expansion method are:

- 1. Separation of the computation procedure into the determination of constants and the summation of the power series in γ .
- Considerable reduction in the storage space for the constants (the matrices b^r_{sm}), due to their properties.

This leads to a more convenient manipulation of the coefficients b_{Am}^{r} and a considerable reduction in computation time.

3.3.2 Computation of the functions $T_{fm}(\gamma)$.

Having computed the constants $b_{\ell m}^{r}$, the functions $T_{\ell m}(\gamma)$ can in principle be computed for any γ lying in the range $0 \leq \gamma \leq 1$ by means of (3.9). Let us for illustration purposes give the first terms of the Taylor series representation of $T_{\ell m}(\gamma)$ for some explicit ℓ , m:

$$T_{55}(\gamma) = 1 - \frac{295}{39} \gamma^2 + \frac{521}{39} \gamma^4 - \frac{1491}{221} \gamma^6$$
(3.33)

(there are no other terms, see (3.19)),

Note that the functions $T_{\ell m}(\gamma)$ for ℓ -odd are polynomials and for ℓ -even infinite series as it follows from property 5 of the matrices $b_{\ell m}^{r}$, (3.19).

For completeness, we give in **Table 3.2** the $T_{\ell m}(\gamma)$ as represented in the form of power series for ℓ , m = 1, 2, ..., 11 and up to the term r = 6.

Table 3.2: Leading terms of $T_{fm}(\gamma)$, (3.9); ℓ , m = 1, 2, ..., 11 and r = 1, 2, ...,

	_				-				
LI	1 1	R =	0	1	2	3	4	5	6
1 0	>		C	23	0	0	0	0	C
1 1	L J		1	0	-3 5	0	0	0	0
1 2	2		0	-2 3	0	4	0	0	0
1 3	•		0	0	3 5	0	-59	0	0
14	•		0	0	0	-4	0	6 11	0
1 5	5		0	0	0	0	59	0	-7 13
16	• I		0	0	0	0	0	- 6 11	0
17			0	0	0	0	0	0	7 13
18	•		0	0	0	0	0	0	0
19	2		0	0	0	0	0	0	0
1 10)		0	0	0	0	0	0	0
1 11			0	0	0	0	0	0	0
LM	1 F	1 =	0	1	2	3	4	5	6
20	1		0	0	15	0	35	0	105
2 1			0	6 5	0	-12 35	0	2 35	0
22			1	0	-1 <u>1</u> 7	0	3 7	0	17 231
23			0	-6 5	0	28 15	0	-82 165	0
24	·		0	0	48 35	0	-816 385	0	2784 5005
25	'		0	0	0	-32 21	0	640 273	0
. 6			0	0	0	0	128 77	0	-2944 1155
27	·		0	0	0	0	0	-256 143	0
28			0	0	0	0	0	0	4096 2145
29	'		0	0	0	0	0	0	0
2 10	<u>۱</u>		0	0	0	0	0	o	¢
2 11			0	0	0	0		0	C
LM	I F	2 =	0	1	2	3	4	5	6
3 0	7		0	0	0	0	0	0	0
31			0	0	24 35	0	0	0	0
32			0	1 <u>2</u> 7	o	-4 3	0	0	0
33			1	0	-46 15	0	65 33	0	0
34			0 -	-12 7	0	48 11	0	-372 143	0
35			0	0	50 21	0	-220 39	0	42 13
36			0	0	0	-100 33	0	76 11	0
37			0	0	0	0	525 143	0	-1806 221
38			0	0	0	C	0	-56 13	0
39	'		0	0	0	0	0	0	84 17
3 10			0	0	0	0	0	0	0
3 11	: L		0	0	0	0	0	0	0

P							
LH	R = 0	1	2	3	4	5	6
4 0	0	0	0	0	-1 63	0	231
4 1	0	0	0	21	0	#	0
4 2	0	0	10 7	0	-340 693	0	290 3003
43	0	20 9	0	-112 33	0	124 143	0
4 4	1	0	-390 77	0	5787 1001	Q	-1306 1001
4 5	0	~20 9	0	2300 273	0	-776 91	0
4 6	0	0	40 11	0	8480 693	0	45520 3927
4 7	0	0	9	-2240 429	0	40000 2431	0
48	0	0	0	0	8960 1287	0	-171520 8151
4 9	0	0	0	0	0	-21504 2431	0
4 10	0	0	0	0	0	0	501760 46189
4 11	0	0	0	0	0	0	0
LM	R = 0	1	2	3	4	5	6
50 51	0	8	8	8	0	0	0
52	0	0	0	160 231	0	0	0
53	0	0	80 33	0	-80 39	0	0
54	0	30 11	0	~6900 1001	0	582 143	0
55	1	0	-295 39	0	521	0	-1491
56	0	-30 11	0	476	0	-4078 187	0
57	0	0	735 143	0	-5145 221	0	135345 4199
58	0	0	0	-1176 143	0	8428 247	0
59	0	0	0	0	2646 221	0	798 17
5 10	0	0	0	0	0	-5292 323	0
5 11	0	0	0	0	0	0	6930 323
6 0	R = 0 0	0	2	3	4	- 5	<u>6</u>
6 1	o	0	0	0	0	-2	429 0
6 2	0	0	0	0	25	143 0	23
63	0	0	0	700	143	-266	429
6 4	· •	۰ ۱	626	429	-795	429	3414
		43	143	-476	143	B164	2431
		13	5 01	-4/6		663	0
00	1	U	-581	0	4970 187	0	10659
67	O	-42	0	55272 2431	0	-2200100 46189	0
68	0	0	448	0	-109760 2717	0	620480 8151
69	0	0	0	-2688 221	0	155904 2431	0
6 10	0	0	0	0	80640 4199	0-	100364544 1062347
6 11	0	0	0	0	0	~118272 4199	0

LH	R =	0	1	2	3	4	5	6
70		0	0	0	0	0	0	0
7 1		0	0	0	0	0	0	0
7 2	ł	0	0	0	0	0	0	0
73		0	0	0	0	896 1287	0	0
74	[0	0	0	448 143	0	-6720 2431	0
75		0	0	336 65	0	-120736 9945	0	144368 20995
76	}	0	56 15	0	-18424 935	0	528024 17765	0
77		1	0	3.08 221	0	2202606 46189	0	-2^5932 +199
78		0	-56 15	0	41664 1235	0	-115056 1235	0
79		0	0	756 85	0	-72336 1105	0	313128 1955
7 10]	0	0	0	-5544 323	0	831600 7429	0
7 11	L	0	0	0		9438 323	0	-1420056 8075
LM	R =	0	1	2	3	4	5	6
80		0	9	0	0	0	0	0
8 1		0	0	0	0	0	0	0
82	ļ	0	0	0	0	0	0	-28 2431
83	}	0	0	0	Ű	0	392 2431	0
84		0	0	0	0	4410 2431	0	-33768 46189
85	j	0	0	0	1176 221	0	-33712 4199	0
86	1	0	0	588 85	0	~82320 3553	0	77560 3553
87		0	72 17	0	-124992 4199	0	169200 2717	0
88		1	0	-1716 95	0	19590 247	0	~436380 3289
89	[0	-72 17	0	5688 119	0	-50184 299	0
8 10		0	0	3600 323	0	-747 3 60 7429	0	7853328 25415
8 11	l	•	0	0	-52800 2261	0	297792 1615	0
LM	R =	0	1	2	3	4	5	6
90	r	0	0	0	0	0	0	0
91		0	0	0	0	0	0	0
92		0	0	0	0	0	0	0
93	1	0	0	0	0	0	0	0
94	1	0	0	0	Q	0	32256 46189	0
95		0	0	0	0	16128 4199	0	-768 221
96	1	0	0	0	2688 323	0	-66816 3553	0
97	}	0	0	2880 323	0	-1183680 29393	0	37575360 676039
98		0	90 19	0	-5688 137	0	46°2204 39767	0
99	ļ	1	0	-2685 119	0	340626 2737	0	-740190 2737
9 10		0	-90 19	0	485100 7429	0	-458172 1615	0
9 11		0	0	1815 133	0	- 335049 2261	0	3778346 6783

L

10 0

10 1

10 2

10 3 10 4

10 5

10

M R

-	5	4	3	2	1	0	-
_	C	0	0	0	0	0	
	0	0	0	0	0	0	
	0	0	0	0	0	0	
	0	0	0	0	0	0	
	0	0	0	0	0	0	
	8316 4199	D	D	٥	0	0	
	0	2310 323	0	0	0	0	
	-3712500	0	3960	0	0	C	

0	17622 85	0	-23100 391	0	110 21	0	10 9
	0	6926931 37145	0	-12045 437	0	1	10 10
 0	******	0	8228 95	0	-110 21	0	10 11
 	5		3	2	1	R = 0	
 0	. 0	0				0	11 0
0	0	0	0	0	0	0	11 1
0	0	0	0	0	0	0	11 2
0	0	0	0	0	0	0	11 3
0	0	0	0	0	0	0	11 4
67584 96577	0	0	0	0	0	0	11 5
0	33792 7429	0	0	0	0	0	11 6
90883584 3380195	0	633600 52003	0	0	0	0	11 7
0	~1091904 15295	0	52800 3059	0	0	0	11 8
*******	0	-274912 2737	0	2200 161	0	0	11 9
0	38267944 111435	0	~172788 2185	0	132 23	0	11 10
*******	0	107393 399	0	-5786 175	0	1	11 11

A similar table for r = 1, 2, ..., 6 and ℓ , m = 0, 1, ..., 9 was also published in [AM64]. However, some of the values given there are incorrect.

Furthermore, such terms for r = 0, 1, 2 are also published in [PE63,p.50-51]. However, all but the diagonal elements of the matrices T and T⁻¹ given there are erroneous.

From Table 3.2 one can immediately see that for ℓ -odd, the $T_{\ell m}(\gamma)$ become polynomials with $(\ell+3)/2 - (\ell-m)$ and $(\ell+3)/2$ non-vanishing terms for $m \leq \ell$ and for $m > \ell$, respectively. The number of terms of these polynomials are for $\ell = 5, 9, 13$ and 19 given in the following Table.

6

0

0

0 0

o

0 36729

630 4199

İ	<i>1</i> \ m	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	
	5	1	2	3	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	
1	9			1	2	3	4	5	6	6	6	6	6	6	6	6	6	6	6	6	
I	13						1	2	3	4	5	6	7	8	8	8	8	8	8	8	
1	19								1	2	3	4	5	6	7	8	9	10	11	11	

Table: Number of terms of the polynomials $T_{\ell-\text{odd},m}(\gamma)$ for $\ell = 5, 9, 13$ and 19.

Relation (3.19) tells us also that for ℓ -even, the $T_{\ell m}(\gamma)$ are infinite power series in γ . These series have the following characteristics:

- The infinite series is alternating in sign for r < m+2; all other terms are positive for m-even and negative for m-odd.
- The coefficients of the series are, with increasing r, first monotonically increasing and then monotonically decreasing.

These properties are illustrated in the following **Table** where we list the coefficients $b_{\ell m}^{r}$ for $\ell \approx 14$, m = 15 and 16 and r = 0, 1, 2, ..., 299.

The series have, in practice, to be curtailed at a certain r = R, where R is defined by the accuracy to which one wishes to calculate the $T_{\ell m}(\gamma)$. However, imposing an accuracy on the computation requires the knowledge of the remainder in the power series. This is in fact the second major problem of the present analysis; the first being the determination of a common convergence radius of the series.

3.3.3 Error estimation of the $T_{\mu}(\gamma)$ computed.

The power series representation of the $T_{fm}(\gamma)$, (3.9), can be written

$$T_{\ell m}(\gamma) = \sum_{r=|\ell-m|}^{R} \gamma^{r} b_{\ell m}^{r} + \sum_{r=R+1}^{\infty} \gamma^{r} b_{\ell m}^{r} . \qquad (3.34)$$

In practice only the first summation term in (3.34) is computed. In order to make such computations meaningful one has to find an estimation of the second summation

Table: Coefficients $b_{\ell m}^{r}$ for $\ell = 14$, m = 15 and 16 and r = 0, 1, 2, ..., 299.

L = 14	H=15	L								
RO	_	1	2	3	4	5	6	7	8	9
0 0. 10 0. 20 0. 30 0. 40 0. 50 0. 60 0. 70 0. 80 0. 90 0. 110 0. 120 0. 130 0. 150 0. 150 0. 170 0. 2200 0. 2210 0. 2210 0. 2210 0. 2250 0. 2260 0. 2270 0. 230 0.	ݫݐݵݨݕݪݨݙݵݨݷݪݸݕݷݨݷݪݡݞݡݪݡݞݵݸݕݵݕݱݷݱݷݑݷݑݭݡݔݲݡݪݡݪ <u>ݞ</u> ݞ	2414E+00 3831E+04 1139E+01 0242E-01 8882E-02 3879E-02 049E-02 1411E-03 8894E-03 8894E-03 8894E-03 8894E-03 8894E-03 8894E-03 8894E-03 8894E-04 21889E-04 2188E-04 2188E-04 2742E-04 8690E-04 8590E-04 8590E-04 9955E-05 7927E-05 792	0.0000000000000000000000000000000000000	2.1749E+02 -2.6209E+04 -7.2356E+00 -7.2356E+00 -7.2356E+00 -5.9844E+02 -5.9844E+02 -7.9844E+02 -7.7495E+03 -7.7495E+03 -8.6745E+03 -8.6745E+04 -4.5195E+04 -3.1383E+04 -2.1298E+04 -2.1298E+04 -1.5199E+04 -1.1271E+04 -7.6039E+05 -7.6058E+05 -7.6058E+05 -7.6058E+05 -7.6058E+05 -7.6058E+05 -7.6058E+05 -7.6058E+05 -7.6058E+05 -7.6058E+05 -7.6058E+05 -7.6058E+05 -7.6058E+05 -7.6058E+05 -7.6058E+058E+05 -7.6058E+058E+058E+058E+058E+058E+058E+058E+		-2.12291+00 9.84022+00 -2.12298-00 -2.12298-00 -2.12298-00 -2.1298-00 -2.12988-00 -2.4.63366-00 -2.4.63366-00 -2.4.61366-00 -2.4.61366-00 -2.4.61366-00 -2.4.61366-00 -2.4.61366-00 -2.4.61366-00 -2.4.61366-00 -4.12001-04 -4	0.0000000000000000000000000000000000000	9.7410E+03 -1.0263E+00 -1.5292+00 -1.5292+00 -1.5292+00 -1.5292+00 -1.5292+00 -1.5292+00 -1.5292+00 -2.4811E-032 -3.6562E-033 -1.49561E-033 -7.6642E-033 -7.6642E-033 -7.6642E-033 -7.6642E-033 -7.6642E-033 -7.6642E-033 -7.6642E-04 -2.3978E-04 -2.3978E-04 -2.3978E-04 -1.422E-04 -2.3978E-05 -7.2448E-05 -5.76577E-05 -5.76572E-05 -4.6582E-05 -4.6582E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -5.76572E-05 -4.2143E-05 -4.2143E-05 -5.76572E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -5.76572E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -5.76572E-05 -4.2143E-05 -4.2143E-05 -4.2143E-05 -5.76572E-05 -5.7677E-05 -5.767	0.0000000000000000000000000000000000000	-2.4137[=+04 -2.4137[=+01 -1.06595[=022 -1.1334[=00] -1.29351[=022 -2.9351[=022 -2.9351[=022 -3.30405[=023 -3.30405[=033 -3.30405[=044 -3.30405[=044 -3.30405[=044 -3.30405[=044 -3.30405[=044 -3.30405[=044 -3.30405[=044 -3.30405[=044 -1.3934[=045]=04 -1.3934[=045]=04 -1.3934[=045]=04 -1.3934[=045]=04 -1.3934[=045]=04 -1.3934[=045]=04 -1.3934[=045]=04 -1.3934[=045]=04 -1.3934[=045]=04 -1.3934[=055]=04 -1.3934[=055]=04 -1.3934[=055]=04 -1.3934[=055]=04 -1.3934[=055]=04 -1.3934[=045]=05 -5.65328[=055]=05 -5.65455[=055]=05 -4.55545[=055]=04 -4.1325[=055]=04 -4.1325[=055]=04 -4.1325[=055]=04 -4.1325[=055]=04 -4.1325[=055]=04 -4.1325[=055]=04 -4.1325[=055]=04 -4.1325[=055]=04 -4.1325[=055]=04 -4.1325[=055]=04 -4.1325[=040]=03 -5.65455[=044]=04 -7.8673[=055]=04 -7.8673[=0

	= 14 H=16]							
R	0	1 2	3	4	5	6	7	8	9
0 100 300 500 600 800 100 1100 1300 1400 1300 1400 100	$\begin{array}{c} 0\\ + 9818E+0.6\\ + 4561E+02\\ 0\\ - 14960E+00\\ 0\\ - 14960E+00\\ 0\\ - 14920E+002\\ 0\\ - 0\\ - 14120E-022\\ 0\\ - 0\\ - 0\\ - 0\\ - 0\\ - 0\\ - 0\\ -$	2 9900-01 -6.4834-04 -7.0898-01 -7.0898-01 -7.0898-01 -7.0898-01 -7.0898-01 -7.0898-01 -7.2844-02 -7.4456-03 -7.4668-04 -7.4668-04 -5.82371-04 -5.82571-05 -5.32581-05 -5.32				5.4777E+03 -1.6921E+04 5504E+00 2.8891E+01 5.0372F=02 2.0377E-02 2.0377E-02 2.0377E-02 2.0377E-02 2.0377E-02 2.0377E-02 2.0377E-02 2.0377E-02 2.0377E-02 2.0377E-02 2.0377E-02 2.0377E-02 2.0377E-02 3.1862E-03 1.8627E-04 3.3231E-04 2.250E-04 1.6040E-04 1.3747E-05 8.0081E-05 5.1080E-	0.0000	-2.2117:+04 1.6948:-01 1.9848:-01 1.9848:-01 1.9848:-01 1.9556:-02 1.70536:-02 1.70536:-02 1.70536:-03 1.71938:-03 1.71938:-03 1.71938:-03 1.71938:-03 1.71938:-03 1.71938:-04 1.9155:-02 1.71938:-03 1.71938:-04 1.9155:-04 1.95551:-04 1.9552:-0552:-055 1.9552:-0552:-0552:-0552:-0552:-0552:-0552:-0552:-0552:-0552:-0552:-0552:-0552:-0552:-0552:-0552:-0552:-05	0.0000000000000000000000000000000000000

term. This estimated value should be as near to the real value as possible to avoid unnecessary computation. This represents the real difficulty of this problem.

Henceforth we will consider the absolute value of the remainder in (3.34)

$$\begin{vmatrix} & \\ & \\ & \\ & \\ & \\ & r=R+1 \end{matrix} \stackrel{r}{\not = r} = \epsilon_{\ell m} \qquad (3.35)$$

It is well known that the remainder of the Taylor series satisfies the following inequality

$$\begin{vmatrix} \infty & & \\ \Sigma & \gamma^{r} & b_{\ell m}^{r} \\ r = R+1 & & \\ \end{vmatrix} \leq A_{\ell m} & \gamma^{R+1} , \qquad (3.36)$$

where $A_{\ell m}$ is a constant matrix. We know that the Taylor series considered converge within the common convergence radius G = 1. For this boundary value of γ (3.36) becomes

$$\begin{vmatrix} \mathbf{x} & \mathbf{b}_{\ell m}^{\mathbf{r}} \\ \mathbf{r} = \mathbf{R} + 1 \end{vmatrix} \leq \mathbf{A}_{\ell m} \qquad (3.37)$$

Furthermore we have the identity

$$\begin{vmatrix} \mathbf{x} & \mathbf{p}^{\mathbf{r}} - \mathbf{R} \\ \mathbf{\Sigma} & \mathbf{p}^{\mathbf{r}} - \mathbf{\Sigma} & \mathbf{p}^{\mathbf{r}} \\ \mathbf{r} = |\ell - \mathbf{m}| & \mathbf{r} = |\ell - \mathbf{m}| \end{vmatrix} = \begin{vmatrix} \mathbf{x} & \mathbf{p}^{\mathbf{r}} \\ \mathbf{r} = \mathbf{R} + \mathbf{1} \end{vmatrix} .$$
(3.38)

We remember that

$$\sum_{r=|\ell-m|}^{\infty} b_{\ell m}^{r} = T_{\ell m}(\gamma=1)$$
(3.39)

Thanks to the relations (3.20) and (3.21) or their equivalent representations (3.31) and (3.32), $T_{\ell m}(\gamma=1)$ can be computed exactly and thus the right-hand side of (3.38) is also known precisely.

Thus, knowing the exact value of $T_{\ell m}(\gamma)$ at the boundary $\gamma = 1$, one is able to estimate the remainder (3.35) of the Taylor series.

3.3.4 Annex to Section 3.3: Details of the numerical calculation.

3.3.4.1 THE COMPUTATION OF THE PRECISION MATRICES R , OF T $_{m}(\gamma)$.

The computation of the functions $T_{\ell m}(\gamma)$ is, a priori, fast and simple once the coefficients of the Taylor series are known because it consists in summing up terms of the power series in γ . However, determining the number of terms to be summed up for a given accuracy requires some more numerical work. Let us suppose that the relative error, $\epsilon_{\ell m}$, for a given element $T_{\ell m}$ has been fixed prior to its computation. Then the number of terms R of the power series to be summed up is

determined ipso facto. As R will vary with 4, m and γ it is convenient to use the matrix notation $R_{fm}(\gamma)$.

The relative error, $\epsilon_{\ell m}$, of a matrix element $T_{\ell m}$ is in our case defined as follows: $\begin{vmatrix} \infty & \gamma^{r} b_{\ell m}^{r} - \sum_{r=|\ell-m|}^{R} \gamma^{r} b_{\ell m}^{r} \rangle / \sum_{r=|\ell-m|}^{\infty} \gamma^{r} b_{\ell m}^{r} \end{vmatrix} \approx \frac{1}{2} \sum_{r=|\ell-m|}^{\infty} \gamma^{r} b_{\ell m}^{r} / \sum_{r=|\ell-m|}^{R} \gamma^{r} b_{\ell m}^{r} \end{vmatrix} \approx (3.40)$

Using (3.36), (3.37) and (3.38) we obtain, for the error check condition,

$$\begin{vmatrix} & & & \\ & & & \\ & & & \\ & & r = |\ell - m| & \\ & & & & \\ & & & \\ & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & &$$

Equ.(3.41) yields an element $R_{\ell m}$ of what we call the precision matrix R for every ℓ , m. These matrix elements indicate the speed of convergence of the power series and are, in a certain sense, a measure of the computing time.

For R_{μ} the following inequality is valid

 $R_{\ell m}(\gamma_1) < R_{\ell m}(\gamma_2) \quad \text{for} \quad \gamma_1 < \gamma_2 \quad . \tag{3.42}$

In order to give some idea of how these precision matrices look, we give them in **Table 3.3.** for some typical γ -values and a given relative error.

Table 3.3: Precision matrices $R_{\ell m}$ of the functions $T_{\ell m}$ for $\gamma = 0.01, 0.1, 0.5, 0.9$ and a constant relative error $\epsilon_{\ell m} = \epsilon \le 10^{-4}$. The number on the left side of a column indicates the number of non-vanishing terms of the series, whereas that on the right side is $R_{\ell m}$.

HAT	RIX R	GANNA = .010	EPS =	1.000E-04	PIMAX = 1	40		_		
LM	0	1	2	3	4	5	6	7	8	9
01234567 890111 123145 1667 178 190	1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0	0 0 2 3 3 2 5 0 7 0 9 0 11 0 1 5 0 7 0 9 0 11 0 1 5 0 17 0 9 0 1 1 0 1 5 0 17 0 9 0 2 1 0 3 0 2 1 0 3 2 3 3 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3	02223436080020106080020 1002002020303030303030303030303030303030	0 4 3 2 3 4 5 4 7 0 9 0 11 0 2 2 2 2 2 1 2 0 9 0 11 0 15 0 17 0 9 0 12 1 0 3 0 19 0 1 3 0 19 0 1 1 0 0 1 0 0 1 1 0 0 1 0 0 1 0 0 1 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 0 1 0	05432345658000106018020 000000000000000000000000000000000	06543234567690110130709 0222222234567690110130709	07654323456787100120408	08765432345678981013015	09876543234567891991201	0009876543234567890111013
LM	10	11	12	13	14	15	16	17	18	19
012334566789011112314516678901111231451667890111123145166789011112314516678900111123145166789001111231451667890011112314516678900111123145166789001111231451667890011112314516678900000000000000000000000000000000000	0110987651437345678901112 077777777777777777777777777777777	0777777777777777777777777777777	0321109876543234567890 0222209876543234567890	0413211109876674323466789 022222222	0547711098765472345678 022200000000000000000000	0654321109876543234567	0776543210987654323466 077757777777777777777777777	08765543211098765432345 0227672222222	09874554921098746549294 022220202020202020202020202	0093755437109876644323
MAT	RIX R	GANMA = .100	EPS =	1.000E-04	PIMAX = 1	40	<u></u>			
LM	0	1	2	3	4	5	6	7	<u> </u>	<u> </u>
1234567 89101 112 13145 167 18190 20	1 60800030 1004 140 1 6080030 1004 140 1 60800200 1 4040 200 2 400 2 400 50505 50505	223277090330507090330507 130304040404050505 27	23436380004040404060505	2454547490110507092302 2233332313030404040505 25	xxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxx	x77654567696103070902	78769696787071060800 200333433332313040404	x89876565678981810109 x777733334333773240404	209876767678909129408 199876767678919129408	vo 111098787678789001110 vv3333334444433339901110305
LH	10	11	12	13	14	15	16	17	18	19
0 1 2 3 4 5 6 7 8 9 0 10 11 12 3 4 5 6 7 8 9 0 10 11 23 4 5 6 7 8 9 0 10 11 23 4 5 6 7 8 9 0 10 11 23 4 5 6 6 7 8 9 0 10 11 23 4 5 6 6 7 8 9 0 10 11 11 11 11 11 11 11 11 11 11 11 1	01121109878767878901112114 0233333334444433333333201112114	02333333344444443333333	022333333444454445444591091112	0445432110110987878989011011 0777777777774444454444737	0233333334444445444444	0474514371711098989898911 04888888888911	07876543232109898989890 028785543211109898989890	02	0202221451451471110910910910910910910910910910910910910	0021209876565472110110909 022298776565472110110909

HAT	RIX R	GANNA = .500	EPS =	1.000E-04	PIMAX = 1	140 <u>F</u>	<u> </u>		e	
L 0 1234 5667 899 101112 1131 14516 167 18 199 20	0 1 1 1 5 0 0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 5 1 9 2 6 1309 8 0 190 2 0 10 2 10 2 10 2 10 3 10 2 10 3 10 3 10 3 10 3 10 3 10 3 10 3 10 3	2 0 0 0 2 3 6 10 3 5 10 3 5 10 3 6 0 0 8 0 0 2 4 0 0 2 8 0 0 2 4 0 0 0 10 2 8 0 0 2 4 0 0 0 11 3 2 0 0 0 1 1 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3 0 0 0 2 4 4 6 11 3 4 4 6 13 4 4 6 1 4 4 7 17 0 8 21 0 29 9 0 29 9 0 29 9 0 29 10 29 10 29 10 29 10 30 11 30 12 37 13 41	* 0 0 5 2 5 4 12 5 4 5 2 0 2 6 1 12 5 4 5 2 0 2 8 0 2 2 0 8 0 2 2 0 8 0 2 2 0 1 1 0 1 2 0 3 6 0 0 1 1 0 1 2 0 3 6 0 0 1 1 0 1 2 0 3 6 0 0 1 1 0 1 2 0 3 6 0 0 1 1 0 1 2 0 3 6 0 0 1 1 0 1 2 0 3 6 0 0 1 1 0 1 2 0 3 6 0 0 1 1 0 1 2 0 3 6 0 0 1 1 0 1 2 0 3 6 0 0 1 1 0 1 2 0 3 6 0 0 1 1 0 1 2 0 3 6 0 0 1 1 0 1 2 0 3 6 0 0 1 1 0 1 2 0 3 6 0 0 1 1 0 1 2 0 3 6 0 0 1 1 0 1 2 0 3 6 0 0 1 0 1 1 0 0 1 0 1 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0	> 0263136 747362136 626136 136261 136261 16670 2009 2009 10012 307 1237	0 0 0 7 6 14 7 6 6 17 6 17 6 17 6 17 6 17 6 17 6 17 6 17 6 17 6 17 6 17 6 16 17 20 9 26 90 30 10 30 11 34	<pre></pre>	8 0 2 9 6 3 16 9 7 5 16 9 7 16 9 8 5 16 9 1 9 4 6 3 16 9 8 5 16 9 9 5 16 9	7 00071050500000000000000000000000000000
LM	10	11	12	13	14	15	16	17	18	19
01234567890112134567 101121345671890	0 0 11 13 11 14 11 15 11 16 11 16 11 16 11 16 11 16 11 16 11 16 11 16 11 16 11 16 11 16 11 16 11 16 11 16 11 16 16	0 0 26 19 36 12 47 12 58 12 77 12 68 12 77 12 74 12 77 12 85 12 74 12 73 6 12 74 12 73 12 74 12 74 12 73 12 74 12 7	02636465869701388564613885646	$\begin{array}{c} 0\\ 2\\ 6\\ 3\\ 6\\ 4\\ 6\\ 1\\ 1\\ 1\\ 7\\ 6\\ 9\\ 7\\ 1\\ 1\\ 2\\ 1\\ 4\\ 1\\ 2\\ 1\\ 4\\ 9\\ 6\\ 7\\ 1\\ 1\\ 2\\ 1\\ 4\\ 9\\ 6\\ 7\\ 5\\ 6\\ 1\\ 7\\ 5\\ 6\\ 1\\ 7\\ 5\\ 6\\ 1\\ 7\\ 5\\ 6\\ 1\\ 7\\ 5\\ 6\\ 1\\ 1\\ 1\\ 4\\ 7\\ 5\\ 6\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\$	052636465760150150150150150150150150150150150150150	0 06 233 16 3 6 21 16 4 6 16 7 16 16 16 11 18 16 10 7 21 16 10 7 21 16 10 7 21	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0 08 26336 2336 4618 5718 1018 1109 123 1018 1123 1133 1133 113 11	0 9969144 19229122 19249192 1922912 1922912 1922914 192291	02636465768798022202202202202202202202202202202202202
NATE	IX R	GAMMA = .900	EPS =	1.000E-04	PIHAX = 1	40				
LM	0	1	2	3	4	5	6	7	8	9
0123456789011234567890	$\begin{array}{c} 1 & 0 \\ 1 & 1 \\ 1^{7} & 3^{4} \\ 0 & 2^{6} & 5^{4} \\ 0 & 0 & 0 \\ 32 & 68 \\ 0 & 0 & 0 \\ 33 & 82 \\ 0 & 0 & 0 \\ 34 & 92 \\ 0 & 0 & 0 \\ 54 & 104 \\ 0 & 51 \\ 114 \\ 0 & 51 \\ 122 \\ 0 & 51 \\ 132 \\ 0 & 51 \\ 132 \\ 0 & 51 \\ 132 \\ 0 & 51 \\ 140 \\ 14$	$\begin{array}{c} 0 & 0 \\ 2 & 31 \\ 1 & 1 \\ 22 & 45 \\ 0 & 31 \\ 22 & 45 \\ 0 & 65 \\ 31 & 65 \\ 0 & 79 \\ 0 & 0 \\ 101 \\ 0 \\ 0 & 101 \\ 0 \\ 0 \\ 101 \\ 0 \\ 101 \\ 0 \\ 50 \\ 101 \\ 0 \\ 101 \\ 0 \\ 50 \\ 101 \\ 0 \\ 101 \\ 0 \\ 50 \\ 101 \\ 0 \\ 101 \\ 0 \\ 50 \\ 101 \\ 0 \\ 101 \\ 0 \\ 50 \\ 101 \\ 0 \\ 0$	0 2 50 3 40 3 54 0 22 20 1 26 50 3 40 3 20 1 26 50 3 40 3 20 1 26 50 77 0 68 60 75 0 108 0 53 110 8 0 55 110 8 0 55 110 8 0 55 110 8 0 55 0 55	0 4 53 4 53 4 53 4 53 4 55 9 0 4 53 4 55 9 0 4 5 3 4 5 5 9 0 0 3 0 0 5 1 1 1 0 3 0 0 5 0 5 0 5 0 5 0 5 0 5 0 5 0 5 0	02739384550520400 273938224190080900 3003090060309006 300309006030057128	0 27 27 29 40 57 67 67 67 67 67 67 67 67 67 6	0 2 2 7 3 0 4 0 7 5 6 7 6 0 7 5 8 7 4 0 4 0 4 0 4 0 4 0 4 0 4 0 5 1 114	0 8 57 8 38 8 58 8 33 8 59 8 57 8 31 4 33 5 33 4 31 3 8 59 8 57 8 71 0 9 10 5 10 10 10 10 10 10 10 10 10 10 10 10 10	0 9 58 9 44 9 68 9 70 9 70 9 46 9 68 9 70 9 70 9 66 9 80 9 70 9 70 9 66 9 70 9 70 9 66 9 70 9 70	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
LM	10	11	12	13	14	15	16	17	18	19
01234567890111234567891112345678	0116011701182 273334054463118 4054463118	0 2 27 34 43 129 127 127 129 127 33 4 43 59 127 127 129 127 129 127 129 127 129 125 129 125 125 125 125 125 125 125 125 125 125	0 2 134 138 138 138 138 138 138 138 138 138 138	0465454794771477147714771477147714771477147714	01661011818158158158158158	0 2 3 3 4 5 7 1 6 9 7 1 6 9 7 1 6 9 7 1 6 9 7 1 6 9 7 1 6 9 7 1 6 9 7 1 6 1 6 5 6 7 1 6 5 6 7 1 6 5 7 1 6 7 7 1 6 7 7 1 6 8 1 6 5 6 5 7 7 1 6 7 7 1 6 7 7 1 6 7 7 1 6 7 7 1 6 7 7 7 1 6 7 7 1 6 7 7 1 6 7 7 7 1 8 7 7 7 1 8 7 7 7 1 8 7 7 7 7 1 8 7 7 7 7 7 7 7 7 7 7 7 7 7	0 2 8 3 3 6 4 5 7 8 1 7 8 1 7 8 1 7 4 3 6 0 7 4 8 8 4 9 7 9 7 7 2 7 8 1 7 7 8 1 8 1	0 08 28 36 34 18 57 18 57 18 187 57 18 187 57 18 187 57 18 187 57 18 187 187 187 187 187 187 187 1	0 28 33 44 58 64 79 19 94 95 19 19 19 19 19 19 19 29 19 20 20 20 20 20 20 20 20 20 20 20 20 20	0 20 28 710 33 79 29 33 4 4 5 9 20 120 20 120 20 120 20 20 20 20 20 20 20 20 20

From these tables one can conclude:

- R varies, in general, from element to element,
- \mathbf{R}_{cm} increases with increasing γ . The number of terms to be taken into account, however, remains quite reasonable when γ approaches the boundary value 1.

In 3.6.3.1 we obtain for a certain submatrix $(T^{-1}.T)$ the relation $T^{-1}.T = I$. This permits verification of the quality of the error estimation (3.41). It turns out that (3.41) works quite well.

5.3.4.2 THE COMPUTATION OF $T_{\mu}(\gamma=1, \mu \in [-1,1])$.

For the computation of these matrix elements formula (3.31) (Method A) or formula (3.32) (Method B) or the equivalent representations (3.20) and (3.21) can be used. From the numerical point of view Method A and Method B are distinct in various aspects. These are summarized in the following **Table** for some matrix elements.

Table: The differences between Method A and Method B.

LM		0		1		2	1	3		4	r i	5	6		7		8		9		10	
0]=	1=		2~		3~		4-		5-		6~		7~		8~		9~		10~		11~
1	1=	1=	1=	2~	1=	3~	1=	4-	1=	5~	1=	6~	1=	7~	1=	8~	1=	9~	1=	10~	1=	11~
2	2~	1=	1=	2~		3~		4-		5-		6~		7~		8~		9~		10~		11~
3	2~		2~	1=	2=	2~	2=	3~	2=	4-	2-	5~	2=	6~	2=	7~	2=	8~	2=	9~	2=	10~
4	3~	1=	2~	2=	1=	2~		4-		5-		6~		7~		8~		۴		10~		11~
5	3~		3~		3~	1=	3=	2~	3=	3~	3=	4~	3=	5~	3=	6~	3=	7~	3=	8~	3*	9~
6	4~	1=	3~	2=	2~	3=	1-	4~		5~		6~		7~		8~		٩.		10~		11~
7	4.		4		4~	_	4.	1=	4=	2~	4=	3~	4=	4~	4=	5~	4=	6~	4=	7~	4=	8~
8	5~	1=	4~	2=	3~	3=	2~	4=	1=	5~		6~		7~		8~		9~		10-		11~
9	5~		5.		5.		5~		5~	1=	5=	2~	5=	3~	5=	4-	5=	5~	5=	6~	5=	7~
10	6~	1=	5~	2-	4.	3=	3~	4 m	2~	5=	1=	6~		7~		8~		9~		10~		11~

To explain this table, let us take the box l = 9, m = 5:

Data below the diagonal concern Method A and those above the diagonal Method B. 5= means **five** terms in the series (3.30 or 3.32) have been used and the sign of each term is **equal**. 2~ means that **two** terms in the series have been used and the sign of the terms **changes**. No data given for a method means that the method is not applicable.

It is, generally speaking, advisable to use the method for which the term of the series have equal signs in order to avoid disturbing numerical effects due to the difference caused by almost equal numbers. That is to say Method A should be used for $\ell \leq 2m$ and Method B for $\ell > 2m$.

3.4 TAYLOR SERIES REPRESENTATION OF THE FUNCTIONS $T_{m,\ell}^{-1}(\gamma)$.

In analogy to the formalism for $T_{\chi m}(\gamma)$ we will represent the functions $T_{m\ell}^{-1}(\gamma)$ in the form of power series in γ and derive a recurrence formula for their coefficients. As this formalism has, to the best of our knowledge, never been published we present it here in more detail than was done for $T_{\ell m}(\gamma)$ in Subsection 3.2.1.

3.4.1 General formalism.

The functions $\operatorname{T}_{\mathfrak{m}\ell}^{-1}(\gamma)$ are defined as follows

$$T_{m\ell}^{-1}(\gamma) = \frac{2\ell+1}{2} \int_{-1}^{+1} P_m[(\gamma(\mu^2-1)+\mu(1-\gamma^2(1-\mu^2))^{1/2}] P_\ell(\mu) d\mu , \quad (3.43)$$

where m, l = 0, 1, 2, ...,

P, are Legendre polynomials,

 γ and μ are variables already defined in **CHAPTER 2**, (2.3 to 2.5).

The variable $\bar{\mu}$ in the center-of-mass system is related to the variable μ in the laboratory system as follows

$$\bar{\mu} = \gamma(\mu^2 - 1) + \mu [1 - \gamma^2 (1 - \mu^2)]^{1/2}$$
which for $\gamma = 0$ again becomes
(3.44)

$$\bar{\mu} = \mu$$
 (3.45)
(see (3.3)).

This key relation quite naturally suggests a Taylor series expansion of $P_{m}[\tilde{u}(\gamma)]$ about the point $\gamma = 0$, which will permit the elimination of the integral in (3.43).

Expanding $P_m[\bar{\mu}(\gamma,\mu)]$ in a Taylor series around $\gamma \approx 0$ one obtains (see Subsection 3.4.4)

$$P_{m}[\bar{\mu}(\gamma,\mu)] = \sum_{r=0}^{\infty} \frac{\gamma^{r}}{r!} \frac{\partial^{r} P_{m}[\bar{\mu}(\gamma=0)]}{\partial \gamma^{r}} = \sum_{r=0}^{\infty} \frac{\gamma^{r}}{r!} r! \sum_{p=|\ell-r|}^{\ell+r} q_{\ell p}^{r} P_{p}(\bar{\mu}=\mu) .(3.46)$$

Inserting this relation into (3.43) one obtains

$$T_{m\ell}^{-1}(\gamma) = \frac{2\ell+1}{2} \int_{-1}^{+1} \sum_{r=0}^{\infty} \gamma^{r} \sum_{p=|m-r|}^{m+r} q_{mp}^{r} P_{p}(\mu) P_{\ell}(\mu) d\mu \qquad (3.47)$$

which similarly to the formalism for T_{fm} leads to the relation

$$\mathbf{T}_{\mathbf{m}\ell}^{-1}(\gamma) = \sum_{\mathbf{r}=|\mathbf{m}-\ell|}^{\infty} \gamma^{\mathbf{r}} \mathbf{q}_{\mathbf{m}\ell}^{\mathbf{r}} \qquad (3.48)$$

For the coefficients $q_{m_{\ell}}^{r}$ it was possible to derive the following recurrence relation (see Subsection 3.4.4)

$$q_{m\ell}^{r} = \frac{m(m+1-r)}{(2m+1)(r+1)} q_{m+1,\ell}^{r} - \frac{(m+1)(m+r)}{(2m+1)(r+1)} q_{m-1,\ell}^{r}$$
(3.49)

with
$$q_{m,\ell}^0 = \delta_{m,\ell}$$

which can either be shown by the induction method (see in 3.4.4.1) or rendered plausible by simple considerations of symmetry as follows:

The expressions

$$T_{\ell m} \approx \frac{2m+1}{2} \int_{-1}^{+1} P_{\ell}(\mu) P_{m}(\bar{\mu}) d\bar{\mu} \text{ and } T_{m\ell}^{-1} \approx \frac{2\ell+1}{2} \int_{-1}^{+1} P_{\ell}(\mu) P_{m}(\bar{\mu}) d\mu$$

reveal a certain symmetry with respect to the labels m and ℓ . This property permits the formal derivation of the recurrence formula for $q_{m\ell}^r$ from that for $b_{\ell m}^r$. In order to do this one starts from the well known recurrence formula for $b_{\ell m}^r$, (3.10), one transposes the indices and transforms the coefficients of this recurrence formula adequately. More precisely, we have

$$b_{\ell m}^{r} = c_{1}(m,r) \ b_{\ell,m+1}^{r} + c_{2}(m,r) \ b_{\ell,m-1}^{r} ,$$

$$q_{m',\ell'}^{r} = c_{1}'(m',r) \ q_{m'+1,\ell'}^{r} + c_{2}'(m',r) \ q_{m'-1,\ell'}^{r} ,$$

$$c_{1}(m,r) \ \frac{m+1 \longrightarrow m'}{\longrightarrow} \ c_{1}'(m',r) ,$$

$$c_{2}(m,r) \ \frac{m-1 \longrightarrow m'}{\longrightarrow} \ c_{2}'(m',r) ,$$

$$c_{1} = \frac{(m+1)(m+2-r)}{(2m+3)(r+1)} , \qquad c_{2} = \frac{m(m+r-1)}{(2m-1)(r+1)} ,$$

$$c_{1}' = \frac{m'(m'+1-r)}{(2m'+1)(r+1)} , \qquad c_{2}' = \frac{(m'+1)(m'+r)}{(2m'+1)(r+1)}$$

which we wished to demonstrate.

3.4.2 Properties of the coefficients $q_{m\ell}^r$.

1.

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$$q_{m\ell}^0 = \delta_{m\ell} . \qquad (3.50)$$

.

2.

$$q_{m\ell}^{r} = 0$$
for: a) $|m-\ell| > r$;
b) $|m-\ell| < r$ r-odd and $m+\ell$ -even, or
r-even and $m+\ell$ -odd.

з.

$$q_{0\ell}^{r} = 0$$
 (3.52)

for any ℓ and for r > 0.

4.

$$q_{m\ell}^{r} = 0$$
 (3.53)
for r > 2 and r-odd, m = 1, 3, 5, ..., r-2

$$r-even, m = 0, 2, 4, ..., r-2.$$

5.
$$\begin{array}{c} m+r \\ \Sigma \\ \ell = \left|m-r\right| \\ m\ell \end{array} = 0 \quad .$$
 (3.54)

6.

$$\sum_{r=|m-\ell|}^{\infty} q_{m\ell}^{r} = \sum_{r=|m-\ell|}^{M} q_{m\ell}^{r}$$
(3.55)

for *l*-even; i.e., for *l*-even, the $T_{m\ell}^{-1}(\gamma)$ are polynomials.

The proofs of properties 1 to 6 are analogous to those of the matrices $b_{\ell m}^r$.

7.

$$\sum_{r=|m-\ell|}^{\infty} \gamma^{r}(=1^{-}) q_{m,2n}^{r} = T_{m,2n}^{-1}(\gamma=1^{-}) =$$

$$= \frac{(-1)^{m+n}}{2} \frac{2^{n}(2n-1)!!}{n!} (4n+1) \frac{(2m-2n-1)!!}{(2m+2n+1)!!} \frac{(m+n)!}{(m-n)!} ,$$
(3.56)

$$\sum_{r=|m-\ell|}^{\infty} \gamma^{r}(=1^{-}) q_{m,2n+1}^{r} = T_{m,2n+1}^{-1}(\gamma=1^{-}) =$$

$$= \frac{(-1)^{m+n}}{2^{n+2}} \frac{n!}{(n-m)!} (4n+3) \frac{(2n-2m-1)!!}{(2n+1)!!} \frac{(2n+2m+1)!!}{(n+m+1)!} +$$

$$+ (-1)^{m+\ell+n} \frac{2\ell+1}{2} \frac{(2n-1)!!}{2^{n+1}(n+1)!} ,$$
(3.57)

where $\gamma = 1^{-1}$ indicates the left-side boundary, i.e., $\gamma = 1 - \epsilon$, where ϵ is positive and arbitrarily small.

These are key relations for the study of the convergence of the power series (3.48) as well as the error analysis. We have verified these formulae numerically using the identity

$$T_{m\ell}^{-1}(\gamma=1) = \frac{2\ell+1}{2} (-1)^{\ell} \int_{-1}^{+1} P_{\ell}(\mu) P_{m}(1-2\mu^{2}) d\mu , \qquad (3.58)$$

an integral which can be evaluated analytically (see in 3.4.4.4).

We will see later that $T_{m\ell}^{-1}(\gamma=1^-) \neq T_{m\ell}^{-1}(\gamma=1)$.

8.

$$q_{\ell,\ell-r}^{r} = b_{\ell-r+1,\ell+1}^{r}$$
 (3.59)

The proof can be established by the induction method using the recurrence relation for $q_{m,\ell}^r$ and $b_{\ell m}^r$.

These properties of the matrices $q_{m,\ell}^r$ do enable us to save considerable storage space.

3.4.3 Convergence of the power series (3.48).

As in the case of $T_{\ell m}$, we are again looking for a common convergence radius of the power series (3.48) representing the functions $T_{m,\ell}^{-1}(\gamma)$. Numerical experience shows that when the variable γ approaches the value $\gamma = 1$ the convergence slows considerably. This is illustrated by **Figure 4** on page 54.

However, the power series are still convergent at $\gamma = 1^{-}$, i.e., on the left-hand side of the boundary value $\gamma = 1$, as these series have, according to (3.56) and (3.57), finite values for $\gamma = 1^{-}$. We can thus consider $\gamma = 1^{-}$ as the common convergence radius for the power series (3.48). We will see later (in 3.4.4.4) that the functions $T_{m\ell}^{-1}(\gamma)$ are discontinuous at $\gamma = 1$ and that the inequality $T_{m\ell}^{-1}(\gamma = 1^{-}) \neq T_{m\ell}^{-1}(\gamma = 1)$

is valid, where 1- denotes the left side of the boundary $\gamma = 1$. This indicates that, at this boundary value and for $\gamma > 1$, the usual definition of the transformation matrix T⁻¹ is probably no longer valid.

3.4.4 Annex to Section 3.4.

3.4.4.1 DETAILS OF THE CALCULATION.

We treat the expression

$$T_{m,\ell}^{-1}(\gamma) = \frac{2\ell+1}{2} \sum_{r=0}^{\infty} \frac{\gamma}{r!} \int_{-1}^{+1} \frac{\partial^{r} P_{m}[\bar{\mu}(\gamma=0)]}{\partial \gamma^{r}} P_{\ell}(\mu) d\mu \quad . \tag{3.59a}$$



To evaluate the integral we have to know the explicit expression for

$$d^{r}P[\bar{\mu}(\gamma=0)] / d\gamma^{r}$$

which implicitly contains the derivatives

$$d^{r}P_{\ell}(\bar{\mu}) / d\bar{\mu}^{r}$$

Let us, therefore, first consider these derivatives.

3.4.4.1.1 The derivatives of $P_{\mu}(\bar{\mu})$ with respect to $\bar{\mu}$.

$$\frac{\mathbf{r} = 1}{d\tilde{\mu}} \frac{dP_{\ell}(\tilde{\mu})}{d\tilde{\mu}} = \frac{1}{1 - \tilde{\mu}^2} \frac{\ell(\ell+1)}{2\ell+1} \left(P_{\ell-1} - P_{\ell+1} \right) .$$

$$\frac{\mathbf{r} = 2}{d^2 P_{\ell}(\tilde{\mu})} \frac{d^2 P_{\ell}(\tilde{\mu})}{d\tilde{\mu}^2} = \frac{1}{(1 - \tilde{\mu}^2)^2} \frac{\ell(\ell+1)}{2\ell+1} \left\{ \frac{(\ell-1)(\ell+2)}{2\ell-1} P_{\ell-2} - \left[\frac{\ell(\ell-3)}{2\ell-1} + \frac{(\ell+1)(\ell+4)}{2\ell+3} \right] P_{\ell} + \frac{(\ell-1)(\ell+2)}{2\ell+3} P_{\ell+2} \right\} .$$

$$\frac{\mathbf{r} = 3}{2\ell}$$

$$\frac{d^{3}P_{\ell}(\bar{\mu})}{d\bar{\mu}^{3}} = \frac{1}{(1-\bar{\mu}^{2})^{3}} \frac{\ell(\ell+1)}{2\ell+1} \left\{ \frac{(\ell-1)(\ell+2)}{2\ell-1} \frac{(\ell-2)(\ell+3)}{2\ell-3} P_{\ell-3} - \left[\frac{(\ell-1)(\ell+2)}{2\ell-1} \frac{(\ell-1)(\ell-6)}{2\ell-3} + \left(\frac{\ell(\ell-3)}{2\ell-1} + \frac{(\ell+1)(\ell+4)}{2\ell+3} \right) \frac{\ell(\ell+5)}{2\ell+1} \right] P_{\ell-1} + \left[\frac{(\ell-1)(\ell+2)}{2\ell+3} \frac{(\ell+2)(\ell+7)}{2\ell+5} + \left(\frac{\ell(\ell-3)}{2\ell-1} + \frac{(\ell+1)(\ell+4)}{2\ell+3} \right) \frac{(\ell+1)(\ell-4)}{2\ell+1} \right] P_{\ell+1} - \frac{(\ell-1)(\ell+2)}{2\ell+3} \frac{(\ell-2)(\ell+3)}{2\ell+5} P_{\ell+3} \right\}$$

which shows the gradual built-up of the r-th derivative

$$\frac{d^{r}P_{\ell}(\bar{\mu})}{d\bar{\mu}^{r}} = \frac{1}{(1-\bar{\mu}^{2})^{r}} \sum_{p=|\ell-r|}^{\ell+r} a_{\ell p}^{r} P_{p}(\bar{\mu}) \qquad \text{with} \qquad (3.60)$$

$$a_{\ell p}^{r+1} = \frac{(p+1)(p+2+2r)}{2p+3} a_{\ell,p+1}^{r} - \frac{p(p-1-2r)}{2p-1} a_{\ell,p-1}^{r}$$
(3.61)

and

$$a_{\ell p}^{0} = \delta_{\ell p}$$

This recurrence formula for the $a_{\ell m}^r$ can easily be proved as follows:

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$$\frac{d^{r+1}P_{\ell}(\tilde{\mu})}{d\tilde{\mu}^{r+1}} = \frac{1}{(1-\tilde{\mu}^2)^{r+1}} \frac{\ell^{r+r+1}}{p=|\ell-r-1|} a_{\ell p}^{r+1} P_{p}(\tilde{\mu}) = \frac{2r\tilde{\mu}}{(1-\tilde{\mu}^2)^{r+1}} \frac{\ell^{r+r}}{p=|\ell-r|} a_{\ell p}^{r} P_{p}(\tilde{\mu}) + \frac{1}{(1-\tilde{\mu}^2)^{r+1}} \sum_{p=|\ell-r|}^{\ell+r} a_{\ell p}^{r} P_{p}(\tilde{\mu}) + \frac{1}{(1-\tilde{\mu}^2)^{r+1}} \sum_{p=|\ell-r|}^{\ell+r} \frac{p(p+1)}{2p+1} a_{\ell p}^{r} [P_{p-1}(\tilde{\mu}) + P_{p+1}(\tilde{\mu})]$$

Using now in the first sum the recurrence formula connecting Legendre polynomials of different orders (see Annex-4)

$$\bar{\mu} P_{p}(\bar{\mu}) = \frac{p+1}{2p+1} P_{p+1}(\bar{\mu}) + \frac{p}{2p+1} P_{p-1}(\bar{\mu})$$

yields

$$\frac{l+r+1}{\Sigma} = a_{lp}^{r+1} P_{p}(\bar{\mu}) = \frac{l+r}{\Sigma} \frac{(p+1)(2r-p)}{2p+1} a_{lp}^{r} P_{p+1}(\bar{\mu}) + \frac{l+r}{\Sigma} \frac{p(2r+p+1)}{2p+1} a_{lp}^{r} P_{p-1}(\bar{\mu}) + \frac{l+r}{2p+1} = \frac{p(2r+p+1)}{2p+1} a_{lp}^{r} P_{p-1}(\bar{\mu}) .$$

Multiplying this equation by $P_k(\bar{\mu})$ and then integrating it, and applying the orthogonality relation (3.8), one directly obtains (3.61).

Explicitly, for the coefficients $a_{\ell m}^r$ we thus obtain

$$\begin{bmatrix} \mathbf{r} = 1 \end{bmatrix}$$

$$\mathbf{a}_{\ell,\ell-1}^{1} = \frac{\ell(\ell+1)}{2\ell+1} , \quad \mathbf{a}_{\ell,\ell+1}^{1} = -\frac{\ell(\ell+1)}{2\ell+1} .$$

$$\begin{bmatrix} \mathbf{r} = 2 \end{bmatrix}$$

$$\mathbf{a}_{\ell,\ell-2}^{2} = \frac{(\ell-1)(\ell+2)}{2\ell-1} \frac{\ell(\ell+1)}{2\ell+1} , \quad \mathbf{a}_{\ell,\ell+2}^{2} = \frac{(\ell-1)(\ell+2)}{2\ell+3} \frac{\ell(\ell+1)}{2\ell+1} ,$$

$$\mathbf{a}_{\ell,\ell}^{2} = -\frac{(\ell+1)(\ell+4)}{2\ell+3} \frac{\ell(\ell+1)}{2\ell+1} - \frac{\ell(\ell-3)}{2\ell-1} \frac{\ell(\ell+1)}{2\ell+1} .$$

$$\begin{bmatrix} \mathbf{r} = 3 \end{bmatrix}$$

$$\mathbf{a}_{\ell,\ell-3}^{3} = \frac{(\ell-2)(\ell+3)}{2\ell-3} \frac{(\ell-1)(\ell+2)}{2\ell-1} \frac{\ell(\ell+1)}{2\ell+1} ,$$

$$\mathbf{a}_{\ell,\ell-3}^{3} = -\frac{\ell(\ell+1)}{2\ell+1} \{\frac{(\ell-1)(\ell-6)}{2\ell-3} \frac{(\ell-1)(\ell+2)}{2\ell-1} + \frac{\ell(\ell+5)}{2\ell+1} [\frac{(\ell+1)(\ell+4)}{2\ell+3} + \frac{\ell(\ell-3)}{2\ell-1}]\} ,$$

$$a_{\ell,\ell+1}^{3} = \frac{\ell(\ell+1)}{2\ell+1} \{ \frac{(\ell+2)(\ell+7)}{2\ell+5} \frac{(\ell-1)(\ell+2)}{2\ell+3} + \frac{(\ell-4)(\ell+1)}{2\ell+1} [\frac{(\ell+1)(\ell+4)}{2\ell+3} + \frac{\ell(\ell-3)}{2\ell-1}] \},$$

$$a_{\ell,\ell+3}^{3} = -\frac{(\ell-2)(\ell+3)}{2\ell-3} \frac{(\ell-1)(\ell+2)}{2\ell-1} \frac{\ell(\ell+1)}{2\ell+1} \quad .$$

Tables of $a_{\ell m}^r$ coefficients are given in Subsection 3.8.3.

3.4.4.1.2 The derivatives of $\bar{\mu}$ with respect to γ .

In the following we give the derivatives of $\bar{\mu}$ with respect to γ up to the order of 10 in the left column, and the corresponding values at $\gamma = 0$ in the right column.

			<u> </u>
ū	=	$\gamma y + \mu (\gamma^2 y + 1)^{1/2}$ $y = \mu^2 + 1$	μ
$\frac{\partial \overline{\mu}}{\partial \gamma}$	=	$y[1+\mu\gamma(\gamma^2y+1)^{-1/2}]$	-(1-µ ²)
$\frac{\partial^2 \bar{\mu}}{\partial \gamma^2}$	=	$\mu y \frac{1}{(\gamma^2 y+1)^{3/2}}$	$-\mu(1-\mu^2)$
$\frac{\partial^3 \overline{\mu}}{\partial \gamma^3}$	=~	$3\mu y^2 \frac{\gamma}{(\gamma^2 y+1)^{5/2}}$	o
$\frac{\partial^4 \overline{\mu}}{\partial \gamma^4}$	=-	$3\mu y^2 \frac{1-4\gamma^2 y}{(\gamma^2 y+1)^{7/2}}$	$-3\mu(1-\mu)^2$
$\frac{\partial^5 \overline{\mu}}{\partial \gamma^5}$	=~	$15\mu y^3 \frac{4\gamma^3 y - 3\gamma}{(\gamma^2 y + 1)^{9/2}}$	o
<u> 2⁶μ</u> 2γ ⁶	=-	$45\mu y^{3} \frac{-8\gamma^{4}y^{2}+12\gamma^{2}y-1}{(\gamma^{2}y+1)^{11/2}}$	$-45\mu(1-\mu^2)^3$
$\frac{\partial^7 \overline{\mu}}{\partial \gamma^7}$	±~	$315\mu y^{4} \frac{8\gamma^{5}y^{2} - 20\gamma^{3}y + 5\gamma}{(\gamma^{2}y + 1)^{13/2}}$	о
<u>θ⁸μ</u> θγ ⁸	=-	$315\mu y^{4} \frac{-64\gamma^{6}y^{3}+240\gamma^{4}y^{2}-120\gamma^{2}y+5}{(\gamma^{2}y+1)^{15/2}}$	$-1575\mu(1-\mu^2)^4$
<u>θ⁹μ</u> θγ ⁹	z	$\frac{2835\mu y^5}{(\gamma^2 y+1)^{17/2}} \frac{\frac{64\gamma^7 y^3 - 336\gamma^5 y^2 + 280\gamma^3 y - 35\gamma}{(\gamma^2 y+1)^{17/2}}$	о
$\frac{\partial^{10}\overline{\mu}}{\partial\gamma^{10}}$	=~	$\frac{2835\mu y^5}{(\gamma^2 y+1)} \frac{640\gamma^8 y^4 + 3584\gamma^6 y^3 - 5600\gamma^4 y^2 + 1400\gamma^2 y - 35}{(\gamma^2 y+1)^{19/2}}$	$-99225\mu(1-\mu^2)^5$

which for $\gamma = 0$ give

$$\frac{\partial^{k} \mu(\gamma=0)}{\partial \gamma^{k}} = -\frac{(k-1)!!^{2}}{k-1} \mu(1-\mu^{2})^{k/2} , \ k \ge 2 .$$
 (3.62)

3.4.4.1.3 The Taylor series coefficients of (3.59a).

$$\begin{split} \overline{\mathbf{r}} &= 1 \\ \hline \frac{\partial P_{m}(\bar{\mu})}{\partial \gamma} &= \frac{m(m+1)}{2m+1} \left[P_{m-1}(\mu) - P_{m+1}(\mu) \right] \\ \cdot \\ \hline \overline{\mathbf{r}} &= 2 \\ \hline \frac{\partial^{2} P_{m}(\bar{\mu})}{\partial \gamma^{2}} &= \frac{m(m+1)}{2m+1} \frac{m-1}{2m-1} (m+1) P_{m-2}(\mu) \\ &- \frac{m(m+1)}{2m+1} \left[\frac{m(m-2)}{2m-1} + \frac{(m+1)(m+3)}{2m+3} \right] P_{m}(\mu) \\ &+ \frac{m(m+1)}{2m+1} \frac{m(m+2)}{2m+3} m P_{m+2}(\mu) \\ \cdot \\ \hline \overline{\mathbf{r}} &= 3 \\ \hline \frac{\partial^{3} P_{m}(\bar{\mu})}{\partial \gamma^{3}} &= \frac{(m-1)m(m+1)(m+2)}{2m+1} \left\{ - \frac{m(m-2)}{(2m-1)(2m-3)} P_{m-3}(\mu) + \\ &+ \frac{1}{2m-1} \left[\frac{(m-1)(m-3)}{2m-3} + \frac{2m(m+2)}{2m+3} \right] P_{m-1}(\mu) \\ &- \frac{1}{2m+3} \left[\frac{2(m+1)(m-1)}{2m-1} + \frac{(m+2)(m+4)}{2m+5} \right] P_{m+1}(\mu) \\ &+ \frac{(m+1)(m+3)}{(2m+3)(2m+5)} P_{m+3}(\mu) \right\} \end{split}$$

In analogy to the formula (3.6) we obtain

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$$\frac{\partial^{r} P_{m}[\bar{\mu}(\gamma=0)]}{\partial \gamma^{r}} = r! \sum_{p=|m-r|}^{m+r} q_{mp}^{r} P_{p}(\mu) .$$

Recall, that $P_{p}(\mu) = P_{p}(\bar{\mu})$ for $\gamma = 0$.

Using the explicit expressions of

$$\partial^{r} P_{m}(\bar{\mu}) / \partial \gamma^{r}$$

as given above, one immediately obtains, for the coefficients $q_{m,\ell}^r$, r = 1, 2, 3:

$$\frac{\mathbf{r} = 1}{\mathbf{q}_{m,m-1}^{1}} = -\frac{\mathbf{m}(\mathbf{m}+1)}{2\mathbf{m}+1} , \qquad \mathbf{q}_{m,m+1}^{1} = \frac{\mathbf{m}(\mathbf{m}+1)}{2\mathbf{m}+1} .$$

$$\frac{\mathbf{r} = 2}{\mathbf{r} = 2}$$

$$2 \ \mathbf{q}_{m,m-2}^{2} = \frac{(\mathbf{m}-1)\mathbf{m}(\mathbf{m}+1)^{2}}{(2\mathbf{m}-1)(2\mathbf{m}+1)} , \qquad 2 \ \mathbf{q}_{m,m+2}^{2} = \frac{\mathbf{m}^{2}(\mathbf{m}+1)(\mathbf{m}+2)}{(2\mathbf{m}+1)(2\mathbf{m}+3)} ,$$

$$2 \ \mathbf{q}_{m,m}^{2} = -\frac{\mathbf{m}(\mathbf{m}+1)}{2\mathbf{m}+1} \left[\frac{(\mathbf{m}-2)\mathbf{m}}{2\mathbf{m}-1} + \frac{(\mathbf{m}+1)(\mathbf{m}+3)}{2\mathbf{m}+3} \right] .$$

$$\frac{\mathbf{r} = 3}{\mathbf{r} = 3}$$

$$3! \ \mathbf{q}_{m,m-3}^{3} = -\frac{\mathbf{m}(\mathbf{m}+1)}{2\mathbf{m}+1} \frac{(\mathbf{m}-1)(\mathbf{m}+2)}{2\mathbf{m}-1} \frac{(\mathbf{m}-2)\mathbf{m}}{2\mathbf{m}-3} ,$$

$$3! \ \mathbf{q}_{m,m-1}^{3} = \frac{\mathbf{m}(\mathbf{m}+1)}{2\mathbf{m}+1} \frac{(\mathbf{m}-1)(\mathbf{m}+2)}{2\mathbf{m}-1} \frac{\mathbf{m}(\mathbf{m}+2)}{2\mathbf{m}-3} ,$$

$$3! \ \mathbf{q}_{m,m+1}^{3} = -2 \frac{\mathbf{m}(\mathbf{m}+1)}{2\mathbf{m}+1} \frac{(\mathbf{m}-1)(\mathbf{m}+2)}{2\mathbf{m}-1} \frac{(\mathbf{m}-1)(\mathbf{m}+1)}{2\mathbf{m}+3} ,$$

$$3! \ \mathbf{q}_{m,m+1}^{3} = -\frac{\mathbf{m}(\mathbf{m}+1)}{2\mathbf{m}+1} \frac{(\mathbf{m}-1)(\mathbf{m}+2)}{2\mathbf{m}+3} \frac{(\mathbf{m}+2)(\mathbf{m}+4)}{2\mathbf{m}+5} ,$$

$$3! \ \mathbf{q}_{m,m+3}^{3} = -\frac{\mathbf{m}(\mathbf{m}+1)}{2\mathbf{m}+1} \frac{(\mathbf{m}-1)(\mathbf{m}+2)}{2\mathbf{m}+3} \frac{(\mathbf{m}+1)(\mathbf{m}+3)}{2\mathbf{m}+5} .$$

The matrix $T^{-1}(\gamma)$ thus reads

$$T_{m\ell}^{-1}(\gamma) = \frac{2\ell+1}{2} \sum_{r=0}^{\infty} \frac{\gamma^r}{r!} \int_{-1}^{+1} r! \sum_{p=|m-r|}^{m+r} q_{mp}^r P_p(\mu) P_{\ell}(\mu) d\mu$$

The integral vanishes unless $p = \ell$.

For
$$r = 1$$
 one has the coefficients $q_{m,m-1}^{1}$ and $q_{m,m+1}^{1}$; or as $\ell = m - r$, $q_{\ell+1,\ell}^{1}$ and $q_{\ell+1,\ell}^{1}$; where
 $q_{\ell-1,\ell}^{1}$, where
 $q_{\ell+1,\ell}^{1} = -\frac{(\ell+1)(\ell+2)}{2\ell+3} = -\frac{(\ell+1)(\ell+2)}{2\ell+3} q_{\ell,\ell}^{0}$,
 $q_{\ell-1,\ell}^{1} = \frac{\ell(\ell-1)}{2\ell-1} = \frac{\ell(\ell-1)}{2\ell-1} q_{\ell,\ell}^{0}$.

.

For r = 2 one has the coefficients: $q_{m,m-2}^2$, $q_{m,m}^2$ and $q_{m,m+2}^2$; or, as l = m - r, $q_{l+2,l}^2$; $q_{l,l}^2$ and $q_{l-2,l}^2$; hence

$$2 q_{\ell+2,\ell}^{2} = -\frac{(\ell+3)^{2}}{2\ell+5} q_{\ell+1,\ell}^{1} ,$$

$$2 q_{\ell,\ell}^{2} = -\frac{\ell(\ell+1)}{2\ell+1} \left[\frac{\ell(\ell-2)}{2\ell-1} + \frac{(\ell+1)(\ell+3)}{2\ell+3} \right]$$

$$2 q_{\ell-2,\ell}^{2} = \frac{(\ell-2)^{2}}{2\ell-3} q_{\ell-1,\ell}^{1} .$$

Similarly, for r = 3 one obtains

$$3 q_{\ell+3,\ell}^{3} = \frac{(\ell+4)(\ell+5)}{2\ell+7} q_{\ell+2,\ell}^{2}$$

$$3 q_{\ell-3,\ell}^{3} = \frac{(\ell-3)(\ell-4)}{2\ell-5} q_{\ell-2,\ell}^{2}$$

Coefficients with higher indices are thus related to coefficients with lower indices.

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In analogy to the recurrence relation for the coefficients $b_{\ell m}^{r}$ and taking into account the ℓ , m symmetry of $T_{m\ell}^{-1}$ relative to that of $T_{\ell m}$, one can write the following formal recurrence relation for the coefficients $q_{m\ell}^{r}$:

$$(r+1) q_{m,\ell}^{r+1} = a(m,r) q_{m+1,\ell}^{r} - b(m,r) q_{m-1,\ell}^{r}$$

For r = 0, 1, 2 we thus obtain

$$q_{m,\ell}^{1} = \frac{(m+1)m}{2m+1} q_{m+1,\ell}^{0} - \frac{(m+1)m}{2m+1} q_{m-1,\ell}^{0} ,$$

$$2 q_{m,\ell}^{2} = \frac{m \cdot m}{2m+1} q_{m+1,\ell}^{1} - \frac{(m+1)(m+1)}{2m+1} q_{m-1,\ell}^{1} ,$$

$$3 q_{m,\ell}^{3} = \frac{m(m-1)}{2m+1} q_{m+1,\ell}^{2} - \frac{(m+1)(m+2)}{2m+1} q_{m-1,\ell}^{2} .$$

From these relations the quantities a(m,r) and b(m,r) can be directly read off. They are given in the following **Table**.

This yields the recurrence relation

$$(r+1) q_{m,\ell}^{r+1} = \frac{m(m+1-r)}{2m+1} q_{m+1,\ell}^r - \frac{(m+1)(m+r)}{2m+1} q_{m-1,\ell}^r$$
with $q_{m,\ell}^0 = \delta_{m,\ell}$.

Table: The quantities a(m,r) and b(m,r).

		the second s							
r	a(m,r)	b(m,r)							
0	$\frac{m(m+1)}{2m+1}$	$\frac{(m+1)m}{2m+1}$							
1	<u>m.m</u> 2m+1	<u>(m+1)(m+1)</u> 2m+1							
2	$\frac{m(m-1)}{2m+1}$	$\frac{(m+1)(m+2)}{2m+1}$							
which render apparent the general structure of $a(m,r)$ and $b(m,r)$									
r	$\frac{m(m+1-r)}{2m+1}$	<u>(m+1)(m+r)</u> 2m+1							

3.4.4.2 ANOTHER POSSIBLE REPRESENTATION OF (3.59a).

The following general relation is valid [GR65,p.19]

$$\frac{\partial^{r} P_{\boldsymbol{\ell}}[\bar{\boldsymbol{\mu}}(\boldsymbol{\gamma})]}{\partial \boldsymbol{\gamma}^{r}} = \Sigma \frac{r!}{\frac{1}{2}! \frac{1}{2}! \cdots \frac{1}{5}!} \frac{\partial^{h} P_{\boldsymbol{\ell}}(\bar{\boldsymbol{\mu}})}{\partial \bar{\boldsymbol{\mu}}^{h}} \left(\frac{\partial \bar{\boldsymbol{\mu}}}{\partial \boldsymbol{\gamma}}\right)^{1} \left(\frac{\partial^{2} \bar{\boldsymbol{\mu}}}{2! \partial \boldsymbol{\gamma}^{2}}\right)^{2} \cdots \left(\frac{\partial^{5} \bar{\boldsymbol{\mu}}}{5! \partial \boldsymbol{\gamma}^{5}}\right)^{1} s , \quad (3.63)$$

where the sum runs over all solutions in non-negative integers of the equation $i_1+2i_2+3i_3+\cdots+si_s = r$ and $i_1+i_2+i_3+\cdots+i_s = h$.

Equ.(3.63) are Bell polynomials [RI68].

We know from (3.62) that $\partial^{j}\bar{\mu}/\partial\gamma^{j}\Big|_{\gamma=0} = 0$ for $j \ge 3$ and odd.

Hence, using (3.62) we obtain

$$\begin{bmatrix} \left(\frac{\partial \bar{\mu}}{\partial \gamma}\right)^{i_{1}} \left(\frac{\partial^{2} \bar{\mu}}{2! \partial \gamma^{2}}\right)^{i_{2}} \left(\frac{\partial^{3} \bar{\mu}}{3! \partial \gamma^{3}}\right)^{i_{3}} \cdots \left(\frac{\partial^{s} \bar{\mu}}{s! \partial \gamma^{s}}\right)^{i_{s}} \end{bmatrix}_{\gamma=0} =$$

$$\begin{bmatrix} \left(\frac{\partial \bar{\mu}}{\partial \gamma}\right)^{i_{1}} \left(\frac{\partial^{2} \bar{\mu}}{2! \partial \gamma^{2}}\right)^{i_{2}} \left(\frac{\partial^{4} \bar{\mu}}{4! \partial \gamma^{4}}\right)^{i_{4}} \cdots \left(\frac{\partial^{s} \bar{\mu}}{s! \partial \gamma^{s}}\right)^{i_{s}} \end{bmatrix}_{\gamma=0} =$$

$$= \left(-\left(1-\mu^{2}\right)\right)^{i_{1}} \left(c_{2}\mu\left(1-\mu^{2}\right)\right)^{i_{2}} \left(c_{4}\mu\left(1-\mu^{2}\right)^{2}\right)^{i_{4}} \cdots \left(c_{s}\mu\left(1-\mu^{2}\right)^{s/2}\right)^{i_{s}}$$

where
$$c_{k} = -\frac{(k-1)!!^{2}}{k!(k-1)}, \quad k = 2, 3, 4, ...$$

$$\left[\left(\frac{\partial \mu}{\partial \gamma}\right)^{i_{1}}\left(\frac{\partial^{2} \mu}{2!\partial \gamma^{2}}\right)^{i_{2}}\left(\frac{\partial^{3} \mu}{3!\partial \gamma^{3}}\right)^{i_{3}}... \left(\frac{\partial^{5} \mu}{s!\partial \gamma^{5}}\right)^{i_{5}}\right]_{\gamma=0} = \mu^{I}(1-\mu^{2})^{\frac{\Gamma+i_{1}}{2}} \frac{s/2}{\prod_{k=1}^{l} c_{2k}} c_{2k}^{i_{2k}}$$

$$I = i_{2}+i_{4}+i_{6}+...+i_{5} = h-i_{1}. \qquad (3.64)$$

Equ.(3.63) thus reads

$$T_{m\ell}^{-1}(\gamma) = \frac{2\ell+1}{2} \sum_{r=0}^{\infty} \frac{\gamma^{r}}{r!} \Sigma \frac{r!}{i_{1}!i_{2}!\cdots i_{s}!} (\prod_{k=1}^{s/2} i_{2k}^{2k}).$$
$$\cdot \int_{-1}^{+1} \mu^{I} (1-\mu^{2})^{\frac{r+1}{2}} \frac{d^{h}P_{m}[\tilde{\mu}(\gamma=0)=\mu]}{d\tilde{\mu}^{h}} P_{\ell}(\mu) d\mu \qquad (3.65)$$

with

$$\frac{d^{h}P_{m}(\bar{\mu})}{d\bar{\mu}^{h}}\bigg|_{\gamma=0} = (2h-1)!! \ C_{m-h}^{h+1/2}(\mu) , \text{ where } C_{m-h}^{h+1/2}(\mu)$$

are Gegenbauer polynomials [GR65,p.1031]. The integral in (3.65) becomes

$$(2h-1)!! \int_{-1}^{+1} \mu^{I} (1-\mu^{2})^{\frac{r+1}{2}} C_{m-h}^{h+1/2}(\mu) P_{\ell}(\mu) d\mu$$

.

and, with the relation [GR65,p.1031]

$$P_{\ell}(\mu) = C_{\ell}^{1/2}(\mu)$$

we have

$$(2h-1)!! \int_{-1}^{+1} \mu^{I}(1-\mu^{2})^{\frac{r+1}{2}} c_{m-h}^{h+1/2}(\mu) c_{\ell}^{1/2}(\mu) d\mu \quad . \tag{3.66a}$$

In principle this integral can be reduced to one of the form

$$\int_{-1}^{+1} \mu^{a} C_{n}^{1/2}(\mu) d\mu = \int_{-1}^{+1} \mu^{a} P_{n}(\mu) d\mu$$

which is known [WH52, p. 310]; or to an integral of the form

$$\int_{-1}^{+1} \mu^{a} (1-\mu^{2})^{\beta} P_{\ell}(\mu) d\mu$$

which is also known [ER54,Vol.2,p.314].

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Using the relation (3.60) we get yet another representation of the integral (3.65); it reads

$$\int_{-1}^{+1} \mu^{h-i_{1}} (1-\mu^{2})^{\frac{r+i_{1}}{2} - h} \sum_{p=|m-h|}^{m+h} a_{mp}^{h} P_{p}(\mu) P_{\ell}(\mu) d\mu .$$
 (3.66b)

By means of the relation

$$\mu P_{p}(\mu) = \frac{p+1}{2p+1} P_{p+1}(\mu) + \frac{p}{2p+1} P_{p-1}(\mu)$$
(3.66c)

this integral can again be reduced to one which is known [GR65,p.820], i.e., to the integral

$$\int_{-1}^{+1} P_{p}(\mu) P_{\ell}(\mu) d\mu .$$

However, all these reductions lead to additional summations in (3.65). The representation of $T_{m,\ell}^{-1}(\gamma)$ as given in (3.65) is thus less practical for numerical calculations than that given in (3.48).

Nevertheless, relation (3.65) has other interesting aspects, particularly from the point of view of number theory.

To investigate this let us consider, in more detail, the coefficients d_{rh} which are defined by the relation

$$\Sigma \frac{1}{i_{1}!i_{2}!\cdots i_{s}!} \prod_{k=1}^{s/2} c_{2k}^{i_{2k}} = \Sigma d_{rh} \qquad (3.67)$$

We recall that

 $i_1 + 2i_2 + 3i_3 + \dots + si_s = r$ and $i_1 + i_2 + i_3 + \dots + i_s = h$.

Using the notations of (3.66b) and (3.67), (3.65) becomes

$$T_{m\ell}^{-1}(\gamma) = \frac{2\ell+1}{2} \sum_{r=0}^{\infty} \gamma^{r} d_{rh} \int_{-1}^{+1} \mu^{h-1} (1-\mu^{2})^{\frac{r+1}{2}} - h$$

$$\cdot \sum_{p=|\ell-h|}^{\ell+h} a_{mp}^{h} P_{p}(\mu) P_{\ell}(\mu) d\mu \quad . \quad (3.67a)$$

The coefficients d_{rh} and the possible summation indices together with the exponents h-i₁, (r+i₁)/2 and (r+i₁)/2-h which appear in the integrant (3.67a) are given in the following **Tables**.

Tables of the coefficients d_{rh} defined in (3.67) and appearing in (3.65). $R = i_1 + 2i_2 + 3i_3 + \ldots + si_s$, $M = i_1 + i_2 + i_3 + \ldots + i_s$, $M1 = h - i_1$, $M2 = (r + i_1)/2 - M$, $d_{11} = 1$.





Taylor

	R	= 1	4			10	10			M4		1	D/C -		1
	1 00N00N400N0N44	2 0100N100107N10	4 00010000110000	6 000000100000	8 00000001111111	10 00011110000000	12 011100000000000000000000000000000000	14 100000000000000000000000000000000000	H 12323452344567	H1 12123212324321	12 05554445443333		D(R,I	1) 2048 2048 2048 2048 2048 2048 1024 6144 2048 2048 6144 2048 6144	
	60N00N40N4680N0N460N46800N46801	0100210432101032105432107654321	0000111100000770000011111110000000	000000000000000000000000000000000000000	100000000000000000000000000000000000000	000000000000000000000000000000000000000		000000000000000000000000000000000000000	734345656789455678678901178901123	132343254321435432654326543217654321	344433332222223332222222222222222222222		אשרישיר - 'שלשלהלישלישלישלישלי	18442 1024 1024 1024 2048 1024 2048 3012 6144 1036 2048 6144 6144 6144 6144 6144 6144 92160 30720 92160 92160 92160 1935360 1935360 29030400 1935360 29030400 1935360 29030400 1935360 29030400 1935360 29030400 1935360 29030400 1935360 29030400 1935360 1935360 29030400 1935360 29030400 1935360 29030400 1935360 29030400 1935360 29030400 29030400 29030400 29030400 1935360 29030400 1935360 29030400 29030000 29030000 290300000 290300000000000000000000000000000000000	
	14 R -	0 - 1	0 6]	0	<u> </u>	_0	0	0	14	0	0		1	87178291200	
ł	1	2	4	6	8	10	12	14	16	H	M1	H2	D	R,H)	
	00100140010146001001401468001	01002100103210010021043210021	0001000011000000000111100000100	000000010000000110000000000000000000000	000000000000000000000000000000000000000	000000011111110000000000000000000000000	000111110000000000000000000000000000000	011100000000000000000000000000000000000	100000000000000000000000000000000000000	12323452344567234345656789345	1212321232432123234343254321343	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	29333 322121277777772545645645645645645454541717171	32 32 44 44 48 88 44 44 44 12 12 184 12 184 12 184 12 184 12 184 12 12 184 12 12 184 44 16 16 16 16 16 16 16 16 16 16 16 16 16	768600992200968800800009880000098800000988000000

000000400000460000004600400000400004000046004680000000	R 1	11351313	11311351131357113113513578	R 1
0100210010321001002104321010021010321054321001032	= 1 2	002101072	01002100103210010021043210	= 1 2
000100001100000001110000000010000001110000	8	10002211	000100001100000000111100000	4
000000010000001100000000000011111000000	6	2222211111	00000010000001100000000	6
000000000000000000000000000000000000000	8	000000000000000000000000000000000000000	000000000000000000000000000000000000000	8
000000000000011111111111100000000000000	10	000000000000000000000000000000000000000	000000011111110000000000000000000000000	10
000000011111110000000000000000000000000	12	000000000000000000000000000000000000000	000111100000000000000000000000000000000	12
000111100000000000000000000000000000000	14	000000000000000000000000000000000000000	011000000000000000000000000000000000000	14
01100000000000000000000000000000000000	16	000000000000000000000000000000000000000	100000000000000000000000000000000000000	16
100000000000000000000000000000000000000	18	145675667	23434563455678345456767890	H
12323452344567234345656789343456455678678678801134556	H	134324354	12123212324321232343254325432	M1
1211232123243212324323432343243243243243243243243243243	M1	3544444713	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	M2
877744474400400000744444444444444444444	H2			<u> </u>
-7429 -4333 -331121217-17577777777777777777777777777777	D(R,H		-423311 -2213311 -221277777777777777777777777777777777	D(R,H)
2 3 14 1 1 20 928)	40 40 614 614 122 61	327 40 40 81 81 409 400 400 122 122 122 122 122 122 122 122 122 1	
655346 655346 6163844 1163844 1163844 1163844 1163844 1163844 116384 116		296 196 44 196 88 44	6866226066688880086889875567428	
4600240246802468020246024680024680246802	R 1	57 9 11 13 15 17	5713579111135135791357911111	R 1
100210432106543210103210543210765432109876543210	= 1 2	-6543210	10543210021043210654321087	≖ 1 2
00322211111100000004433333222221111111111	4	0000000	110000004333222222111111100	4
221111111111111111000000000000000000000	6	0000000	111111100000000000000000000000000000000	5
000000000000000000000000000000000000000	8	0000000	000000000000000000000000000000000000000	8 1
000000000000000000000000000000000000000	10 1	0000000	000000000000000000000000000000000000000	10 1
000000000000000000000000000000000000000	12 1	0000000	000000000000000000000000000000000000000	2 1
000000000000000000000000000000000000000	4 1	00000000	000000000000000000000000000000000000000	4 1
	6 18	011 001 001 001 001		6 1
7845676789000112356667897890111289011123445671112	H			I MI
32454365432765432115465437654328765432119876543210	M1			M
445444433333322222222222222222222222222	M2	0000000		2
		-1 -1 -1 -1 -1 -1		D(
	D{F	26 742		R,H)
5 5 116 76644 22 10 10 10 10 10 10 10 10 10 10 10 10 10	(,H)	55296 193536 1393459 19160064 498161666 153487366 124513853	307 6451 6451 366 922 6386688 3645 3645 3645 3686 3686 1290 1290 3686681 4448 3686681 4935 23224 4936161664 103211 38700 397000 307000 307000 307000 307000 30700000000	
24576 66840 49152 16334 49152 16334 49152 12288 12288 12288 12288 12288 12288 12288 12288 12288 12288 12288 12288 12288 12288 12288 12288 12288 12288 1228 1208 1228 1208 1228 1208		00 20 20 20 20 20 20 20 20 20 20 20 20 2	22240446020004644024482492000222	

R = 19		R = 19
12	6 8 10 12 14 16 18 M M1 M2 D(R,H)	1 2 4 6 8 10 12 14 16 18 H H1 H2 D(R,H)
010021001002104971049710100210020000000000000000000000000000	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

R =	20]														
1	2	4	6	8	10	12	14	16	18	20	M	H1	H2		D(R,H)	
000000400000460000004004680000000400004	010021001032100400210432100100210103210	000100001100000000111100000000000000000	0000001000000110000000000001111000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000111110000000000000000000000000000000	011000000000000000000000000000000000000	100000000000000000000000000000000000000	1232345234456723445656567892343456455678	1114231422314324324323432432432432435432	98887778776666687776666555558777666665555	3155999933331131116511113777777195557777777777 2774447 2471		221147 2147 2147 2147 2147 2147 2147 214

R = 20 CONTINUED

K •	21												_	_	_	_	_	_	_	_			 	 			_							_	 						 		
1	2	4	6	8	10	12	12	12	12	12	12	12	1	1		1		1)	1	12	2	14	16	1	8	20	0	L	H	 H1	1	12	ļ	 		 D(R,	<u>, H</u>)			 		
1311361131367113113513513579113113513135713579111351357113571	100210010321001002104321001002002104032105432100210010321002404327065432401002104321010321054321076543	001000110000002111100000000000000000000						000000000111111111111111111111111111111																		110000000000000000000000000000000000000		000000000000000000000000000000000000000		34345634556783454567678903454567566756678978901124567456678956787890112345656787890116778908901113901121	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		8887778776666877766665555587776666665555444444476667665555655544444333333666555444445544443333386665555444455444453333366655554444455444433333366655554444455444433333366655554444455444433333366655554444455444433333366655554444455644433333366655555555			5599333311111151711777711955777777777777			14	14 220 594	13926631333333641332313923436936934949999798877458222986599999693939999631787794746349944637999999992999218632227369	10000000000000000000000000000000000000	71644472088888886097388338880746020278538887203885405000446613866444486678866478866488725533266688520850000114402020126000000000000000000000000

R = 21 CONTINUED

1	2	4	6	8	10	12	14	16	18	20	H	M1	H2	D(R,H)
11351135135791357911313579113579135791135791135791135791	210021043210654321087654321009876543210	000544433333333333333333333333333333333	111000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	1451667898901112901123450011234566781123345667899021	321565476543876543298765432109876543210	NNN5++++33333NNNNNNNNNNNNNNNNNNNNNNNNNN	5109350400 199264665600 20922789888000 1179648 1179648 1179648 884736 2949120 30965760 1114767360 114767360 114767360 30965760 30965760 30965760 154258020 15425800 15455800 15555800 15555

These tables have several interesting features.

• The number of coefficients d_{rh} , i.e., the number of summation terms for a given r, belongs to the sequence of numbers of partitions into parts of 2 kinds p_2 . We have verified this up to r = 150 by comparing our results with the tables of [GU62,p.90]. The subsequent **Table** gives **the number N of coefficients** d_{rh} in dependence on r as calculated by us.

For r even we thus have N(r) = N(r+1) and $N(r) = p_2(r/2,1)$ in the notation of [GU62]. In [GU62] these numbers have been tabulated up to r = 1000.

- Consequently, this relation between the number of summation terms and the number of partitions into parts of 2 kinds together with the tables in [GU62] give us the number of summation terms for any r up to 1000.
- Many of the coefficients d have the same value.
- The denominator of d is a subset of the JORDAN-POLYA numbers [P037,p.209], [ME68,p.25], [SL73] and [LA81]. These denominators, without repetition of

equal values, are given in the subsequent **Table** for r up to 21. We could compare the sequence given in this table with the sequence of JORDAN-POLYA numbers up to the number 1536 as given in [SL73]. We did not find a more extensive table on the JORDAN-POLYA numbers than that given in [SL73].

- It relates different branches of mathematics.
- For the numerical computation of $T_{m\ell}^{-1}(\gamma)$ (3.67a) is not as practical, despite the reduction in the number of terms resulting from the integral due to the orthogonality of the Legendre polynomials, since the number of the coefficients d_{rh} increases rapidly with increasing r. For example, for r = 79 there are 177970 d_{rh} coefficients, whereas only 40 non-vanishing terms of the coefficients $q_{m\ell}^{r}$ (3.48) are needed. Therefore, (3.67a) has not been further exploited for numerical computation of the functions $T_{m\ell}^{-1}(\gamma)$.

r	N	r	N	r	N	r	N	r	N
2	2	32	915	62	35471	92	646193	122	7760854
4	4	34	1212	64	43820	94	770947	124	9061010
6	7	36	1597	66	53963	96	918220	126	10566509
8	12	38	2087	68	66273	98	1091745	128	12308139
10	19	40	2714	70	81156	100	1295971	130	14320697
12	30	42	3506	72	99133	102	1535914	132	16644217
14	45	44	4508	74	120770	104	1817503	134	19323906
16	67	46	5763	76	146785	106	2147434	136	22411641
18	97	48	7338	78	177970	108	2533589	138	25965986
20	139	50	9296	80	215308	110	2984865	140	30053954
22	195	52	11732	82	259891	112	3511688	142	34751159
24	272	54	14742	84	313065	114	4125842	144	40143942
26	373	56	18460	86	376326	116	4841062	146	46329631
28	508	58	23025	8 8	451501	118	5672882	148	53419131
30	684	60	28629	90	540635	120	6639349	150	61537395

Table: Number N of coefficients d rh in dependence on r.

With an eye to thoroughness, we print the first terms of the series (3.65) making use of the tables for the coefficients d_{rh} .

$$T_{m\ell}^{-1}(\gamma) = \frac{2\ell+1}{2} \left\{ \frac{2}{2\ell+1} \delta_{m\ell} + \gamma \right\}_{-1}^{+1} P_m^{(1)}(\mu) P_\ell(\mu) (1-\mu^2) d\mu + (3.68)$$

. .

Table: Sequence of denominators of the coefficients d_{rh} , (3.67), for r up to 21.



$$+\gamma^{2}\left[-\frac{1}{2}\int_{-1}^{+1}P_{m}^{(1)}(\mu)P_{\ell}(\mu)\mu(1-\mu^{2})d\mu+\int_{-1}^{+1}P_{m}^{(2)}(\mu)P_{\ell}(\mu)(1-\mu^{2})^{2}d\mu\right]+$$

+\gamma^{3}\left[-\frac{1}{2}\int_{-1}^{+1}P_{m}^{(2)}(\mu)P_{\ell}(\mu)\mu(1-\mu^{2})^{2}d\mu+\frac{1}{6}\int_{-1}^{+1}P_{m}^{(3)}(\mu)P_{\ell}(\mu)(1-\mu^{2})^{3}d\mu\right]+
+ ...

3.4.4.3 RELATIONS RESULTING FROM THE TWO DIFFERENT REPRESENTATIONS OF (3.59a).

From (3.65) and (3.48) one obtains the identity

$$q_{m\ell}^{\Gamma} = \frac{2\ell+1}{2} \sum_{h} d_{rh} \int_{-1}^{+1} \mu^{h-i_1} (1-\mu^2)^{\frac{r+i_1}{2}} P_{m}^{(h)}(\mu) P_{\ell}(\mu) d\mu \qquad (3.69)$$

By means of this relation and the integral

$$\int_{-1}^{+1} (1-x)^{a} (1+x)^{\nu-1/2} C_{m}^{\mu}(x) C_{n}^{\nu}(x) dx , \quad \operatorname{Re}(a) > -1 \qquad (3.70)$$

where C_{ij} denote Gegenbauer polynomials which are given in an analytical form in [ER54,p.283], formula(16), one can immediately obtain further **analytical representations of integrals which are not given in the usual tables of integrals** [GR65], [ER54] and [GR66].

Such an integral is

$$\int_{-1}^{+1} P_{m}^{(1)}(\mu) P_{\ell}(\mu) \mu(1-\mu^{2}) d\mu = -\frac{4}{2\ell+1} q_{m\ell}^{2} + \int_{-1}^{+1} P_{m}^{(2)}(\mu) P_{\ell}(\mu) (1-\mu^{2})^{2} d\mu$$

$$(3.71) = -\frac{4}{2\ell+1} q_{m\ell}^{2} + 3 \int_{-1}^{+1} c_{m-2}^{5/2}(\mu) c_{\ell}^{1/2}(\mu) (1-\mu^{2})^{2} d\mu .$$

The right-hand side of (3.71) is analytically known (see (3.70)), thus the integral on the left-hand side is also known.

Another integral which can be expressed in a similar manner is

$$\int_{-1}^{+1} P_{m}^{(2)}(\mu) P_{\ell}(\mu) \mu(1-\mu^{2})^{2} d\mu = -\frac{4}{2\ell+1} q_{m\ell}^{3} + \frac{1}{3} \int_{-1}^{+1} P_{m}^{(3)}(\mu) P_{\ell}(\mu) (1-\mu^{2})^{3} d\mu$$

$$(3.72) = -\frac{4}{2\ell+1} q_{m\ell}^{3} + 5 \int_{-1}^{+1} C_{m-3}^{7/2}(\mu) C_{\ell}^{1/2}(\mu) (1-\mu^{2})^{3} d\mu .$$

As the right-hand side is known (see (3.70)), the integral on the left-hand side is also known.

Using the representation (3.60) for
$$P_{m}^{(h)}$$
 the relation (3.69) reads
 $q_{m,\ell}^{r} = \frac{2\ell+1}{2} \sum_{h} d_{rh} \int_{-1}^{+1} \mu^{h-i_{1}} (1-\mu^{2})^{\frac{r+i_{1}}{2}} -h \prod_{p=|m-h|}^{m+h} a_{mp}^{h} P_{p}(\mu) P_{\ell}(\mu) d\mu$
and if the recurrence relation for $q_{m,\ell}^{r}$, (3.49) holds, we obtain
 $\int_{-1}^{+1} \sum_{h} d_{r+1,h}, \mu^{h'-i_{1}} (1-\mu^{2})^{\frac{r+1+i_{1}}{2}} -h \prod_{p=|m-h|}^{m+h} a_{mp}^{h} P_{p}(\mu) P_{\ell}(\mu) d\mu = p_{p}|m-h| \prod_{p=|m-h|}^{+1} \sum_{p=|m-h|}^{+1} a_{m+1,p}^{h} P_{p}(\mu) P_{\ell}(\mu) d\mu = p_{p}|m-h|$

$$b_{2} \int_{-1}^{+1} \sum_{h} d_{rh} \mu^{h-i_{1}} (1-\mu^{2})^{\frac{r+i_{1}}{2}} -h \qquad m+h \\ p = |m-h| \qquad p = |m-h| \qquad h^{h-i_{1}} p_{p}(\mu) p_{\ell}(\mu) d\mu , \quad (3.73)$$
where $b_{1} = \frac{m(m+1-r)}{(2m+1)(r+1)}$; $b_{2} = -\frac{(m+1)(m+r)}{(2m+1)(r+1)}$.

Additional interesting relations result from (3.69) in connection with the properties of the matrices $q_{m,r}^r$, (3.50 to 3.57).

From the **tables for the coefficients** d_{rh} one can immediatly read off the following useful relations for **r-even**

 $h_{r+1} = h_r + 1 , \qquad (h-i_1)_{r+1} = (h-i_1)_r ,$ $(\frac{r+i_1}{2} - h)_{r+1} = (\frac{r+i_1}{2} - h)_r ,$ $d_{r+1,h} = d_{rh} / i_{1,r+1} , \qquad i_{1,r+1} = i_{1,r} + 1 .$

They can be used to check (3.73).

For **r-odd**, however, the corresponding relations are more complicated.

3.4.4.4 PARTICULAR CASES.

3.4.4.4.1
$$T_{m\ell}^{-1}(\gamma \rightarrow 1)$$
.

In order to study this case, let us start from the definition of $T_{m\ell}^{-1}$ which reads $T_{m\ell}^{-1}(\gamma) = \frac{2\ell+1}{2} \int_{-1}^{+1} P_m(\bar{\mu}) P_\ell(\mu) d\mu$ (3.74)

The **Figure 5** on page 76 illustrates the discontinuous behavior of the function $\bar{\mu}[\mu(\gamma)]$.

In particular one can see from there that

 $\lim_{\gamma \to 1^{-}} \overline{\mu}[\mu(\gamma)] \to -1 \text{ for } \mu \in [-1,0] \quad ,$

where 1⁻ indicates the left side of the boundary $\gamma = 1$; whereas at the boundary itself we have (3.44)

 $\bar{\mu} = 2\mu^2 - 1$.



Figure 5. The functions $\bar{\mu}[\mu(\gamma)]$: $\gamma = 0, .2, .4, .6, .8, 1^-, 1$.

Ipso facto the functions $T_{m\ell}^{-1}$ are also discontinuous at $\gamma = 1$.

As we are only interested, for application purposes, in the γ -range in which the functions $T_{m\ell}^{-1}(\gamma)$ are continuous, we will evaluate the integral (3.74) for $\gamma = 1$ -instead of $\gamma = 1$.

Equ.(3.74) then reads

$$T_{m\ell}^{-1}(\gamma=1^{-}) = \frac{2\ell+1}{2} \left\{ \int_{-1}^{0} P_{m}(\bar{\mu}=-1) P_{\ell}(\mu) d\mu + \int_{-1}^{0} P_{m}(2\mu^{2}-1) P_{\ell}(\mu) d\mu \right\}.(3.74a)$$

Both integrals can be represented in analytical form:

The first integral becomes [GR65,p.796]

$$\int_{-1}^{0} P_{m}(-1) P_{\ell}(\mu) d\mu = (-1)^{m+\ell} \int_{0}^{1} P_{\ell}(\mu) d\mu =$$

$$= (-1)^{m+\ell} \left| \begin{array}{c} 0 \quad \text{for } \ell - \text{even and } \ell > 0 \\ 1 \quad \text{for } \ell = 0 \\ \frac{(-1)^{n}(2n-1)!!}{2^{n+1}(n+1)!} \quad \text{for } \ell = 2n+1; n=0, 1, \ldots \end{array} \right|$$

The second integral can be evaluated in two ways which have already been treated in 3.2.4.2, (3.25). This integral can thus be written

$$T_{m\ell}^{-1}(\gamma=1^{-}) = \frac{2\ell+1}{2} \left[T_{m\ell}^{-1}(\gamma=1^{-},\mu \ \epsilon \ [-1,0]) + T_{m\ell}^{-1}(\gamma=1^{-},\mu \ \epsilon \ [0,1], \frac{A}{B}) \right] (3.76)$$

where A, B in the second term on the right-hand side indicates the method used for evaluating the integral (see in 3.2.4.2). Further details on the computation of $T_{m,\ell}^{-1}(\gamma=1^{-})$ are given in 3.5.4.3.

3.4.4.4.2 Explicit expressions of
$$T_{m\ell}^{-1}$$
 for certain m, ℓ .

$$\begin{split} \overline{\mathbf{m}} &= \overline{\mathbf{0}} \\ \overline{\mathbf{m}} &= \overline{\mathbf{0}} \\ \mathbf{T}_{0\ell}^{-1} &= \frac{2\ell+1}{2} \int_{-1}^{+1} \mathbf{P}_{\ell}(\mu) \ d\mu &= \delta_{0,\ell} \\ \mathbf{T}_{m0}^{-1} &= \frac{1}{2} \int_{-1}^{+1} \mathbf{P}_{m}(\overline{\mu}) \ d\mu \\ &= \frac{1}{2} \int_{-1}^{\infty} \mathbf{P}_{m}(\overline{\mu}) \ d\mu \\ &= \frac{1}{2} \sum_{n=0}^{\infty} (-\gamma)^{n} (n+1) \int_{-1}^{+1} \mathbf{P}_{m}(\overline{\mu}) \ \mathbf{P}_{n}(\overline{\mu}) \ d\overline{\mu} \\ &= \frac{m+1}{2m+1} (-\gamma)^{m} \\ \mathbf{T}_{11}^{-1} &= \frac{3}{8\gamma^{3}} \left[\gamma (1+\gamma^{2}) - \frac{1}{2} (1-\gamma^{2})^{2} \log(\frac{1+\gamma}{1-\gamma}) \right] = -3 \sum_{n=0}^{\infty} \frac{1}{(2n-1)(2n+1)(2n+3)} \gamma^{2n} \\ \mathbf{T}_{11}^{-1} (1^{-}) &= 3/4 \\ \end{split}$$

,

$$\begin{split} \hline m = 1, \ \vec{x} = 2 \\ r_{12}^{-1} &= \frac{2\eta^2}{3} \\ r_{11}^{-1} &= -3 \sum_{n=0}^{\infty} \frac{1}{(2n-1)(2n+1)(2n+3)} \gamma^{2n} \\ r_{13}^{-1} &= -3 \sum_{n=0}^{\infty} \frac{1}{(2n-1)(2n+1)(2n+3)} \gamma^{2n} \\ r_{13}^{-1} &= -165 \gamma^4 \sum_{n=0}^{\infty} \frac{(n+1)}{(2n+1)(2n+3)(2n+5)(2n+7)} \gamma^{2n} \\ r_{15}^{-1} &= -\frac{165}{2} \gamma^4 \sum_{n=0}^{\infty} \frac{(n+1)(n+2)}{(2n+5)(2n+7)(2n+9)(2n+1)} \gamma^{2n} \\ r_{17}^{-1} &= \frac{525}{2} \gamma^6 \sum_{n=0}^{\infty} \frac{(n+1)(n+2)(n+2)(n+4)}{(2n+5)(2n+7)(2n+9)(2n+1)(2n+13)(2n+15)} \gamma^{2n} \\ r_{19}^{-1} &= \frac{17955}{2\cdot3\cdot4} \gamma^8 \sum_{n=0}^{\infty} \frac{(n+1)(n+2)(n+2)(n+4)}{(2n+7)(2n+9)(2n+1)(2n+13)(2n+15)} \gamma^{2n} \\ r_{19}^{-1} &= \frac{17955}{2\cdot3\cdot4} \gamma^8 \sum_{n=0}^{\infty} \frac{(n+1)(n+2)(n+2)(n+4)}{(2n+7)(2n+9)(2n+1)(2n+13)(2n+15)} \gamma^{2n} \\ r_{1,2k+1}^{-1} &= (4k+3)(2k+1)!! \\ r_{1,2k+1}^{-1} &= (4k+3)(2k+1)!! \\ r_{1,2k+1}^{-1} &= (4k+3)(2k-3)!! \\ r_{1,2k+1}^{-1} &= (4k+3)(2k-3)!! \\ r_{1,2k+1}^{-1} &= \frac{(2k+1)!!(2k-3)!!}{(2n-1)(2n+1)(2n+3)(2n+5)} \gamma^{2n} \\ r_{1,2k+1}^{-1} &= (4k+3)(2k-3)!! \\ r_{1,2k+1}^{-1} &= \frac{(2k+1)!!}{(2n-1)(2n+1)(2n+1)(2n+3)(2n+5)} \gamma^{2n} \\ r_{23}^{-1} &= -126\gamma \sum_{n=0}^{\infty} \frac{(n+1)^2}{(2n-1)\cdots(2n+1)} \gamma^{2n} \\ r_{25}^{-1} &= 495\gamma^3 \sum_{n=0}^{\infty} \frac{(n+1)(n+2)^2}{(2n+1)\cdots(2n+1)} \gamma^{2n} \\ r_{27}^{-1} &= -1575\gamma^5 \sum_{n=0}^{\infty} \frac{(n+1)(n+2)(n+3)^2}{(2n+3)\cdots(2n+1)} \gamma^{2n} \\ r_{2,2k+1}^{-1} &= \frac{6(4k+3)(2k+1)!!}{k!} \gamma^{2k-1} \sum_{n=0}^{\infty} (n+k) \frac{(n+k)!}{n!} \frac{(2n+2k-5)!!}{(2n+4k+3)!!} \gamma^{2n} \\ r_{2,2k+1}^{-1} &= \frac{6(4k+3)(2k+1)!!}{k!} \gamma^{2k-1} \sum_{n=0}^{\infty} (n+k) \frac{(n+k)!}{n!} \frac{(2n+2k-5)!!}{(2n+4k+3)!!} \gamma^{2n} \\ r_{2,2k+1}^{-1} &= \frac{6(4k+3)(2k+1)!!}{k!} \gamma^{2k-1} \sum_{n=0}^{\infty} (n+k) \frac{(n+k)!}{n!} \frac{(2n+2k-5)!!}{(2n+4k+3)!!} \gamma^{2n} \\ r_{2,2k+1}^{-1} &= \frac{6(4k+3)(2k+1)!!}{k!} \gamma^{2k-1} \sum_{n=0}^{\infty} (n+k) \frac{(n+k)!}{n!} \frac{(2n+2k-5)!!}{(2n+4k+3)!!} \gamma^{2n} \\ r_{2,2k+1}^{-1} &= \frac{6(4k+3)(2k+1)!!}{k!} \gamma^{2k-1} \sum_{n=0}^{\infty} (n+k) \frac{(n+k)!}{n!} \frac{(2n+2k-5)!!}{(2n+4k+3)!!} \gamma^{2n} \\ r_{2,2k+1}^{-1} &= \frac{6(4k+3)(2k+1)!}{k!} \gamma^{2k-1} \sum_{n=0}^{\infty} (n+k) \frac{(n+k)!}{n!} \frac{(2n+2k-5)!!}{(2n+4k+3)!!} \gamma^{2n} \\ r_{2,2k+1}^{-1} &= \frac{6(4k+3)(2k+1)!}{k!} \gamma^{2k-1} \sum_{n=0}^{\infty} (n+k) \frac{(2n+2k-5)!}{n$$

$$\begin{split} \mathbf{T}_{2,2k+1}^{-1}(1^{-}) &= \frac{6(4k+3)(2k-5)!!}{k!} (2k^{2}+3k-3) \\ &\vdots \\ \hline \mathbf{T}_{31}^{-1} &= -72\gamma^{2} \sum_{n=0}^{\infty} \frac{(n+1)(n+2)}{(2n-1)\cdots(2n+7)} \gamma^{2n} \\ &, \\ \mathbf{T}_{31}^{-1} &= -72\gamma^{2} \sum_{n=0}^{\infty} \frac{(n+1)(8n^{2}+8n+5)}{(2n-1)\cdots(2n+7)} \gamma^{2n} \\ &, \\ \mathbf{T}_{33}^{-1} &= 63\gamma^{2} \sum_{n=0}^{\infty} \frac{(n+1)(8n^{2}+8n+5)}{(2n-1)\cdots(2n+7)} \gamma^{2n} \\ &, \\ \mathbf{T}_{35}^{-1} &= -495\gamma^{2} \sum_{n=0}^{\infty} \frac{(n+1)(n+2)(4n^{2}+12n+15)}{(2n-1)(2n+1)\cdots(2n+1)} \gamma^{2n} \\ &, \\ \mathbf{T}_{37}^{-1} &= 1575\gamma^{4} \sum_{n=0}^{\infty} \frac{(n+1)(n+2)(n+3)(8n^{2}+40n+75)}{(2n+1)(2n+3)\cdots(2n+15)} \gamma^{2n} \\ &, \\ \mathbf{T}_{39}^{-1} &= -\frac{17955}{2}\gamma^{6} \sum_{n=0}^{\infty} \frac{(n+1)(n+2)(n+3)(n+4)(2n^{2}+14n+35)}{(2n+3)(2n+5)\cdots(2n+15)} \gamma^{2n} \\ &, \\ \mathbf{T}_{3,11}^{-1} &= \frac{3.3.3.7.11\cdot23}{2}\gamma^{8} \sum_{n=0}^{\infty} \frac{(n+1)\cdots(n+5)(8n^{2}+72n+225)}{(2n+23)} \gamma^{2n} \\ &, \\ \mathbf{T}_{3,2k+1}^{-1} &= k_{k} \sum_{n=0}^{\infty} \frac{(n+k)!}{n!} \frac{(2n+2k-7)!!}{(2n+4k+3)!!} (a_{k}n^{2} + b_{k}n + c_{k}) \gamma^{2n} \\ &, \\ &k_{k} &= \frac{3(4k+3)(2k+1)!!}{k!} , a_{k} &= 8 , b_{k} &= 8(2k-1) , c_{k} &= 5k(2k-1), \\ &\mathbf{T}_{3,2k+1}^{-1} (1^{-}) &= \frac{3(4k+3)(2k-7)!!}{2^{k}(k+4)!} (4k^{4}+12k^{3}-19k^{2}-42k+30) \\ &. \end{split}$$

3.5 NUMERICAL EVALUATION OF THE POWER SERIES EXPANSION OF $T_{m\ell}^{-1}(\gamma)$.

The whole numerics for $T_{m\ell}^{-1}$ is very similar to that for $T_{\ell m}$. Naturally we first compute the constants, i.e., the coefficients of the power series (3.48). They can be stored on disk and called up whenever required. The computation of the functions $T_{m\ell}^{-1}(\gamma)$ then only consists in summing up the power series (3.48) including an accuracy check. It's again the latter on which our particular attention will be focused.

3.5.1 Computation of the matrices q_{m}^r .

Using the recurrence formula (3.49) the matrices $q_{m\ell}^r$ can be computed exactly. This computation was performed on a **CDC-7600** using the program **M1COF** (see **Annex-3**).

For completeness we give some $q_{m,\ell}^r$ matrices in Table 3.4.

HL	R = 1 0	1	2	3	4	5	6	7	8	9	10	11
1	-23	0	23	0	0	0	0	0	0	0	0	0
2	0	-65	0	65	0	0	0	0	0	0	0	0
3	0	0	-12 7	0	12 7	0	0	0	0	0	0	0
4	o	0	0	-20 9	0	20 9	0	0	0	0	0	0
5	0	0	0	0	- 30 11	0	30 11	0	0	0	0	0
6	0	0	0	0	0	-42 13	0	42 13	0	0	0	0
7	0	0	0	0	0	0	-56 15	0	56 15	0	0	0
8	0	0	0	0	0	0	0	-72 17	0	7-	0	0
9	0	0	0	0	0	0	0	0	-90 19	0	90 19	0
10	0	0	Ü	0	0	0	0	0	0	-110 21	0	110 21
11	0	0	0	•	0	0	0	0	0	0	-132 23	0
HL	R = 2 0	1	2	3	4	5	6	7	8	9	10	11
1.	0	- <u>1</u> 5	0	15	0	0	0	0	0	0	0	0
2	35	0	-9 7	0	24 35	0	0	0	0	0	0	0
3	0	48 35	0	-14 5	0	19 7	0	0	0	0	0	0
4	0	0	50 21	0	- 370 77	0	80 33	0	0	0	0	0
5	0	0	0	40 11	0	-95 13	0	525 143	0	0	0	0
6	o	0	0	0	735 143	0	-567 55	0	336 65	0	0	0
7	0	0	0	0	0	448 65	0	- 305 2 221	0	58B 85	0	0
8	0	0	0	0	0	0	756 85	0	-1692 95	0	2880 323	0
9	0	0	0	0	0	0	0	3600 323	0	-2655 119	0	1485 1 33
10	0	0	0	0	0	0	0	0	1815 133	0	-119 3 5 437	0
11	0	0	0	0	0	0	0	0	0	2640 161	0	-5742 175
ML	R = 3 0	1	2	3	4	5	6	7	8		10	11
1	0	0	0	0	0	0	0	0	0	0	0	0
2	0	12 35	0	15	0	21 21	0	0	0	0	0	0
3	-4 7	0	40 21	0	-156 77	0	160 231	0	0	0	0	0
4	0	-32 21	0	52 11	0	-440 91	0	700 429	0	0	0	0
5	O	0	-100 33	0	120 13	0	-28 3	0	448 143	0	0	0
6	0	0	0	-2240 429	0	616 39	0	-38640 2431	0	1176 221	0	0
7	0	0	0	0	-1176 143	0	23184 935	0	-30744 1235	0	2688 323	0
8	0	0	0	C	0	-2688 221	0	153720 4199	0	- 62 4 17	0	3960 323
9	0	0	0	0	0	0	-5544 323	0	6864 133	0	-384120 7429	0
10	0	0	C	0	0	0	0	-52800 2261	0	192060 2737	0	-46728 665
11	0	0	0	C	0	0	0	0	-94380 3059	0	202488 2185	0

HL	$R = 4 \downarrow 0$	1	2	3		5	6	7	8	9	10	11
1	0	-1	0	.2	0		0	0	0	0	0	0
2	0	ر د 0	0	45 0	0	0	0	0	0	0	0	0
3	0	-16 35	0	53 55	0	-62 91	0	25 143	0	0	0	0
4	5	0	-250 99	0	575 143	0	-272 99	0	896 1287	0	0	0
5	0	128 77	0	-992 143	0	970 91	0	-17500 2431	0	4410 2431	0	0
6	0	0	525 143	0	-2142 143	0	21273 935	0	-207648 13585	0	16128 4199	0
7	0	0	0	8960 1287	0	-56000 1989	0	1965250 46189	0	-6300 221	0	2310 323
8	0	0	0	0	2646 221	0	-77868 1615	0	33066 455	0	-19008 391	0
9	0	0	0	0	٥	80640 4199	0	-324000 4199	0	45405 391	0	-125334 1615
10	0	0	0	0	0	0	9438 323	0	-18876 161	0	68926 391	0
11	0	0	0	0	0	0	0	316800 7429	0	-334224 1955	0	122023
ME	$R = 5 \mid 0$	1	2	3	•	5	6	7	a	9	10	11
1	0	0	0	0	0	0	0	0	0	0	0	0
2	٥	2 35	0	55	0	91 91	0	~2 143	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0
•	0	128 231	0	-632 429	0	424 273	0	-5800 7293	0	392 2431	0	D
5	11	0	450 143	0	-954 143	0	1278 187	0	-9408 2717	0	32256 46189	0
6	0	-256 143	٥	1344 143	0	-4260 221	0	902300 46189	0	-23940 2431	0	8316 4199
7	0	0	-56 13	0	4872 221	0	-72184 1615	0	55656 1235	0	-2188032 96577	0
8	0	0	0	-21504 2431	0	188160 4199	0	-4174200 46189	0	461880 5083	0	-7 3656 1615
9	0	0	0	0	-5292 323	0	1404 17	0	-508068 3059	0	6193044 37145	0
10	0	0	0	0	0	-118272 4199	0	13675200 96577	0	-555786 1955	0	138 <u>1226</u> 4845
11	0	0	0	0	0	0	-339768 7429	0	3510936 15295	0	-10260536 22287	0
HL	$R = 6 \mid 0$	1	2		4	5	6	7	8	9	10	11
1	0	105	0	1 55	0	-1 91	0	429	0	0	0	0
2	0	0	0	0	0	0	0	0	0	0	0	0
3	0	-32 385	0	404 2145	0	-44 273	0	164 2431	0	-28 2431	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0
5	o	-640 1001	0	80 39	0	-13330 4641	٥	9250 4199	0	-2170 2431	0	630 4199
6	7	0	-49 13	0	2205 221	0	-22001 1615	0	12784 1235	0	-403200 96577	0
7	0	4096 2145	0	-146944 12155	0	130240 4199	0	-5809300 138567	0	1772820 55913	0	-1338876 104975
8	0	0	84 17	0	-9828 323	0	7332 95	0	-1587612 15295	0	171072 2185	O
9	0	0	0	501760 46189	0	-277760 4199	0	177282000 1062347	0	-1137633 5083	0	54439 323
10	0	0	٥	0	6930 323	0	-965250 7429	0	999702 305 9	0	-29255798 66861	0
11	0	0	0	D	D	3784704 96577	0	-4967424 20995	0	3484096 5865	0-	5581582 16 702525

From **Table 3.4** one can see that many matrix elements vanish as was pointed out in Subsection 3.4.2 where the properties of the matrices $q_{m,\ell}^r$ were treated. These properties permit a space-saving storage of these matrices.

We wish once more to underline the fact that the **representation of the functions** $T_{m\ell}^{-1}(\gamma)$ in the form of power series in γ lead to a variable independent part, i.e., the coefficients $q_{m\ell}^{r}$, and a variable dependent one, i.e., the powers in γ . This factorisation of the functions $T_{m\ell}^{-1}(\gamma)$ is very advantageous for numerical calculations, as it saves computer time.

3.5.2 Computation of the functions $T_{m\ell}^{-1}(\gamma)$.

We know from Subsection 3.4.3 that the power series in γ which represent the functions $T_{m\ell}^{-1}(\gamma)$ converge within the radius $\gamma = 1^-$. These functions can, in principle, thus be computed by means of (3.48) for any value of γ from the interval $0 \leq \gamma \leq 1^-$. However, for $\gamma = 1^-$ it is evidently advantageous to use the sum free and exact representation of $T_{m\ell}^{-1}$ (3.56), (3.57) or their identical equation (3.74a) for numerical calculation.

To illustrate how the series (3.48) look we give their leading terms for some explicit values of m, ℓ

 $T_{23}^{-1}(\gamma) = \frac{6}{5}\gamma - \frac{8}{15}\gamma^3 - \frac{6}{55}\gamma^5 - \dots ,$ $T_{34}^{-1}(\gamma) = \frac{12}{7}\gamma - \frac{156}{77}\gamma^3 \quad \text{no more terms,}$ $T_{55}^{-1}(\gamma) = 1 - \frac{95}{13}\gamma^2 + \frac{970}{91}\gamma^4 - \frac{13330}{4641}\gamma^6 + \dots ,$ $T_{56}^{-1}(\gamma) = \frac{30}{11}\gamma - \frac{28}{3}\gamma^3 + \frac{1278}{187}\gamma^5 \quad \text{no other terms.}$ (3.77)

These examples confirm that $\mathbf{T}_{m\ell}^{-1}(\gamma)$ are polynomials for ℓ -even, as stated in (3.55), and they show that the coefficients of the power series can be positive or negative and are relatively large. Hence the convergence is mainly influenced by the value of γ .

For the sake of completeness we give, in **Table 3.5**, the leading terms of the power series in γ representing the functions $T_{m\ell}^{-1}$ for m, $\ell = 0, 1, ..., 11$ and r = 1, 2, ..., 6.

n L n L 1 2 3 4 5 6 1 0 $-\frac{2}{3}$ 0 0 0 0 0 0 1 1 0 $-\frac{2}{3}$ 0 0 0 0 0 1 2 0 $\frac{2}{3}$ 0 0 0 0 0 1 3 0 0 $\frac{1}{5}$ 0 $\frac{2}{3}$ 0 0 0 1 4 0 0 0 0 0 0 0 0 1 5 0 0 0 0 0 0 0 0 1 6 0 0 0 0 0 0 0 0 1 7 0 0 0 0 0 0 0 0 1 1 0 0 0 0 0 0 0 0 1 1 0 0 0 0 0 0 <		D -	~		~				
1 0 $-\frac{2}{3}$ 0 0 0 0 0 1 1 0 $-\frac{1}{5}$ 0 $-\frac{1}{5}$ 0 $-\frac{1}{5}$ 1 2 0 $\frac{2}{3}$ 0 0 0 0 0 1 3 0 0 $\frac{1}{5}$ 0 0 0 0 0 1 5 0 0 0 0 0 0 0 0 1 6 0 0 0 0 0 0 0 0 1 7 0 0 0 0 0 0 0 0 1 1 0 0 0 0 0 0 0 0 1 1 0 0 0 0 0 0 0 0 1 1 0 -5 0 12 3 4 5 6 2 1 0 -5 0 12 0 0 0		π =	0	1		3	•	2	*
1 1 0 -1 0 -1 0 -1 0 -1 1 2 0 $\frac{2}{3}$ 0 0 0 0 0 1 3 0 0 0 0 0 0 0 0 1 4 0 0 0 0 0 0 0 0 1 5 0 0 0 0 0 0 0 0 1 6 0 0 0 0 0 0 0 0 1 $\frac{42}{7}$ 1 8 0	10		0	-2 3	0	0	0	0	o
1 2 0 $\frac{2}{3}$ 0 0 0 0 0 1 3 0 0 0 0 0 0 0 0 1 4 0 0 0 0 0 0 0 0 1 5 0 0 0 0 0 0 0 0 1 6 0 0 0 0 0 0 0 0 1 7 0 0 0 0 0 0 0 0 1 8 0 0 0 0 0 0 0 0 1 1 0 0 0 0 0 0 0 0 1 1 2 3 4 5 6 6 0	1 1		1	0	-1 5	0	-1 35	0	-1 195
1 3 0 0 $\frac{1}{5}$ 0 $\frac{2}{45}$ 0 $\frac{1}{5}$ 1 4 0 0 0 0 0 0 0 1 5 0 0 0 0 $\frac{-1}{63}$ 0 $\frac{-1}{91}$ 1 6 0 0 0 0 0 0 0 1 7 0 0 0 0 0 0 0 1 8 0 0 0 0 0 0 0 0 1 9 0 0 0 0 0 0 0 0 1 1 0 0 0 0 0 0 0 0 1 1 0 -5 0 $\frac{12}{35}$ 0 0 0 0 2 1 0 -5 0 $\frac{12}{35}$ 0 0 0 0 2 1 0 -5 0 $\frac{12}{35}$ 0 0	12		0	23	0	o	0	0	٥
1 4 0 0 0 0 $-\frac{1}{63}$ 0 $-\frac{1}{91}$ 1 6 0 0 0 0 0 0 0 1 7 0 0 0 0 0 0 0 1 7 0 0 0 0 0 0 0 1 7 0 0 0 0 0 0 0 0 1 9 0 0 0 0 0 0 0 0 0 1 10 0 0 0 0 0 0 0 0 1 1 0 -5 0 $\frac{12}{3}$ 0 0 0 0 2 1 0 -5 0 $\frac{12}{35}$ 0 0	1 3		0	0	15	0	2 45	0	55 55
1 5 0 0 0 $-\frac{1}{63}$ 0 $-\frac{1}{91}$ 1 6 0 0 0 0 0 0 0 1 7 0 0 0 0 0 0 0 1 8 0 0 0 0 0 0 0 1 9 0 0 0 0 0 0 0 1 10 0 0 0 0 0 0 0 1 1 0 0 3 0 0 0 0 2 1 0 -5 0 12 0 22 0 2 1 0 -5 0 15 35 0 0 0 2 1 0 -5 0 12 0 23 0 24 0 0 0 2 2 0 0 0 0 0 0 0 0 0 0	14		0	0	0	0	0	0	o
1 6 0	15		0	0	0	0	-1 63	0	-1 91
1 7 0 0 0 0 0 0 0 0 1 8 0 0 0 0 0 0 0 0 1 10 0 0 0 0 0 0 0 0 0 1 10 0 0 0 0 0 0 0 0 1 1 0 0 0 0 0 0 0 0 1 1 0 -6 0 12 0 -2 0 0 0 2 1 0 -6 0 12 0 -2 0 0 0 2 1 0 -6 0 12 0 -5 0 -2 0 <td< td=""><td>16</td><td></td><td>0</td><td>0</td><td>0</td><td>0</td><td>0</td><td>0</td><td>o</td></td<>	16		0	0	0	0	0	0	o
1 8 0 0 0 0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 1 10 0 0 0 0 0 0 0 0 0 0 11 0 0 0 0 0 0 0 0 0 0 M L R = 0 1 2 3 4 5 6 2 0 -6 0 12 0 -2 3 4 5 6 2 1 0 -6 0 12 0 -2 3 0 0 0 0 2 3 0 6 0 -5 0 22 0 <th< td=""><td>17</td><td></td><td>0</td><td>0</td><td>0</td><td>0</td><td>0</td><td>0</td><td>1 429</td></th<>	17		0	0	0	0	0	0	1 429
1 9 0 1 1	18		0	٥	0	0	0	0	0
1 10 0 0 0 0 0 0 0 0 M L R = 0 1 2 3 4 5 6 2 0 0 0 $\frac{3}{5}$ 0 0 0 0 0 2 1 0 $\frac{-6}{5}$ 0 $\frac{12}{35}$ 0 2 2 2 2 1 0 $-\frac{6}{5}$ 0 $\frac{12}{35}$ 0 0 0 2 3 0 $\frac{6}{5}$ 0 $\frac{18}{15}$ 0 $\frac{-6}{55}$ 0 2 4 0 0 $\frac{24}{35}$ 0 0 0 0 2 5 0 0 0 21 0 6 0 2 6 0 0 0 0 0 0 0 0 2 7 0 0 0 0 0 0 0 0 2 8 0 0 0 0 0 0 0 0 0 2 10 0 0 0	19		0	0	0	0	0	0	0
1 0 0 0 0 0 0 0 M L R = 0 1 2 3 4 5 6 2 0 0 0 35 0 0 0 0 2 1 0 -5 0 125 0 25 0 2 2 1 0 -5 0 125 0 0 0 2 3 0 65 0 -8 0 0 0 0 2 4 0 0 24 0 0 21 0 6 0 2 5 0 0 0 21 0 6 0 0 2 6 0 0 0 0 0 0 0 0 0 2 7 0 0 0 0 0 0 0 0 0 0 2 7 0 0 0 0 0	1 10		0	0	0	0	0	0	0
H L R - 0 1 2 3 4 5 6 2 0 0 0 3 0 0 0 0 2 1 0 -6 0 125 0 25 0 2 2 1 0 -9 0 0 0 0 2 3 0 6 0 -8 0 55 0 2 4 0 0 24 0 0 0 0 2 5 0 0 0 0 0 0 0 2 6 0 0 0 0 0 0 0 0 2 7 0 0 0 0 0 0 0 0 0 2 7 0 0 0 0 0 0 0 0 0 0 <t< td=""><td>1 11</td><td></td><td>0</td><td>0</td><td>0</td><td>0</td><td>0</td><td>0</td><td>0</td></t<>	1 11		0	0	0	0	0	0	0
n n	H I	P =			2	3		5	6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2 0		0	0	3	0	0	0	0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21		0	- 2	0	12	0	2	o
2 3 0 $\frac{6}{5}$ 0 $\frac{18}{15}$ 0 $\frac{-6}{55}$ 0 2 4 0 0 $\frac{24}{35}$ 0 0 0 0 2 5 0 0 0 $\frac{24}{35}$ 0 0 0 0 2 5 0 0 0 0 0 0 0 2 6 0 0 0 0 0 0 0 2 7 0 0 0 0 0 0 0 2 8 0 0 0 0 0 0 0 2 9 0 0 0 0 0 0 0 2 10 0 0 0 0 0 0 0 2 11 0 0 4 5 6 3 3 1 0 0 3 3 3 3 3 3 3 3 3 3 3 3	22		1	0	-9	0	0	0	o
2 4 0 0 $\frac{24}{35}$ 0 0 0 0 2 5 0 0 0 $\frac{4}{21}$ 0 $\frac{6}{91}$ 0 2 6 0 0 0 0 0 0 0 2 7 0 0 0 0 0 $\frac{-2}{14.3}$ 0 2 8 0 0 0 0 0 0 0 2 8 0 0 0 0 0 0 0 2 9 0 0 0 0 0 0 0 2 10 0 0 0 0 0 0 0 2 11 0 0 0 0 0 0 0 3 1 0 0 $\frac{48}{35}$ 0 $-\frac{16}{15}$ 0 $-\frac{32}{385}$ 3 2 0 $-\frac{12}{7}$ 0 $\frac{40}{21}$ 0 0 3 3 1	23		0	Ę	0	-8 15	0	-6	o
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2 4		0	0	24 35	0	0	0	o
2 6 0 0 0 0 0 0 0 0 2 7 0 0 0 0 0 $\frac{-2}{143}$ 0 2 8 0 0 0 0 0 0 0 2 9 0 0 0 0 0 0 0 2 9 0 0 0 0 0 0 0 2 10 0 0 0 0 0 0 0 2 11 0 0 0 0 0 0 0 3 1 0 0 48 0 -16 0 -32 3 2 0 -12 0 400 0 0 0 3 3 1 0 -14 5 55 0 2145 3 4 0 12 0 -156 55 0 2145 3 4 0 12	25		0	0	0	21 21	0	6 91	0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	26		0	0	0	0	0	0	0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	27		0	0	0	0	0	-2 143	0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	28		0	0	0	0	0	0	0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	29		0	0	0	0	0	0	0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2 10		0	0	0	0	0	0	0
H L R = 0 1 2 3 4 5 6 3 0 0 0 0 $-\frac{4}{7}$ 0 0 0 3 1 0 0 $\frac{48}{35}$ $-\frac{16}{7}$ 0 0 0 3 1 0 $-\frac{12}{35}$ 0 $\frac{40}{21}$ 0 0 0 3 3 1 0 $-\frac{14}{5}$ 0 $\frac{53}{55}$ 0 $\frac{404}{5}$ 3 4 0 12 0 $-\frac{156}{77}$ 0 0 0 3 5 0 0 10 0 -62 0 $-\frac{44}{273}$ 3 6 0 0 0 0 0 0 0 3 7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 11		0	0	0	0	0	0	0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	ML	R =	0	1	2	3	4	5	6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	30		0	0	0	-	0	0	0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	31		0	0	48 35	0	-16 35	0	32 385
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	32		0	-1 <u>2</u> 7	0	40 21	0	0	0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	33		1	٥	-14 5	0	53 55	0	404 2145
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 4		0	1 <u>2</u> 7	0	-156 77	0	0	o
3 6 0 0 0 160 0 0 0 3 7 0 0 0 0 25 0 166 143 2431	35		0	0	10 7	0	-62 91	0	-44 273
3 7 0 0 0 0 25 0 164 143 2431	36		0	0	0	160 231	0	0	0
	37		0	0	0	0	25 143	0	164 2431
38 0 0 0 0 0 0	38		0	0	0	C	0	0	0
3 9 0 0 0 0 0 -28 2431	39		0	0	0	0	Q	0	-28 2431
	3 10		0	0	0	0	0	0	0
3 10 0 0 0 0 0 0 0	3 11		0	0	0	0	0	0	0
310 0 0 0 0 0 0 0	2 11		, n	~	•	- ^	•	-	-
	3 11		<u> </u>	V	v	v	~	v	

ML	R =	0	1	2	3	4	5	6	
4 0		0	0	0	0	59	0	0	٦
4 1		0	0	0	-32 21	0	128 231	0	
42		٥	0	50 21	0	-250 99	0	0	
43		0	-20	0	52 11	0	-632 429	0	
4 4		1	0	-370 77	0	575 143	0	0	
45		0	20 9	0	-440 91	0	424 273	0	
46		0	0	80 33	0	-272 99	0	0	
47		0	0	0	700 429	0	-5800 7293	0	
48		0	0	0	0	896 1287	0	0	
49		0	0	0	C	0	392 2431	0	
4 10 4 11		ô	0 0	8	00	Ô	00	õ	
ML	R =	0	1	2	3	4	5	6	
5 0		0	0	0	0	0	11	0	7
51		0	0	0	0	128 77	0	-640 1001	
52		0	0	0	-100 33	0	450 143	0	
53		0	0	40 11	0	- 9 92 143	0	80 39	ľ
54		0	- 30 11	0	120 13	0	-954 143	0	
55		1	0	-95 13	0	970 91	0	-1 3330 4641	
56		0	30 11	0	-28 3	0	1278 187	0	
57		0	0	525 143	0	-17500 2431	0	9250 4199	
58		0	0	0	448 143	0	-9408 2717	0	
59		0	0	0	0	4410 2431	0	-2170 2431	
5 10	1	0	0	0	0	0	32256 46189	0	
5 11		0	0	0	0	0	0	630 4199	
M L	R =	0	1	2	3	4	5	6	٦
60		0	0	0	0	0	0	13	٦
61		0	0	0	0	0	-256 143	G	
62		0	0	0	0	525 143	0	-49 13	
63		0	0	o	-2240 429	0	1344 143	0	
64		Q	0	7 3 5 143	0	-2142 143	0	2205 221	
65		0	-42 13	0	616 39	0	-4260 221	0	
66		1	0	-567 55	0	21273 935	0	-22001 1615	
67		0	42 13	0	-38640 2431	0	902300 46189	0	
68		0	0	336 65	0	-207648 13585	0	12784 1235	
69		0	0	0	1176 221	0	-23940 2431	0	
6 10		0	D	•0	0	16128	0	-403200	
6 11		0	0	0	0	0	8316 4199	0	

ML	R =	0	1	2	3	4	5	6	
70		0	0	0	0	0	0	0	
		0	U	U	U	0	U	2145	
72		0	0	0	0	0	-56 13	0	
73		0	0	0	0	8960 1287	0	-146944 12155	
74		0	0	0	-1176 143	0	4872 221	0	
75		. 0	0	448 65	0	-56000 1989	0	130240 4199	
76		0	-56 15	0	23184 935	0	-72184 1615	O	
77		1	0	-3052 221	0	1965250 46189	0	-5809300 138567	
7 B		0	56 15	0	-30744 1235	0	55656 1235	0	
79		0	0	588 85	0	-6300 221	0	1772820 55913	
7 10		0	0	0	2688 323	0	-21880 <u>32</u> 96577	0	
7 11		0	0	0	0	2310 323	0	-1338876 104975	
								6	
9 0	N -	<u> </u>						<u> </u>	
9 V 9 J		Ň	ő	0	0	0		0	
8 2		0	0	0	0	0		84	
8 9		0	0	0	0	0	-21504	17 0	
8 4		ů	0	0	0	2646	2431	-9828	
		•	•	•	-2688	221	189160	323	
• 4		~		761	221	_77869	4199	7222	
• 7		•	_72	185	153720	1615	-4174200	' 95	
• •			-17	-1(00	4199	22014	46189		
		1	U	-1672	0	455	U	15295	
89		0	1 3	0	-624 17	0	461880 5063	0	
8 10		0	0	2880 323	0	-19008 391	0	171072 2185	
8 11		0	0	0	3960 323	•	-7 3656 1615	0	
HL	R =	0	1	2	3	+	5	6	
90		0	0	0	0	0	0	0	_
91		0	0	0	0	0	0	0	
92		0	0	0	0	0	0	0	
9 [.] 3		0	0	0	0	0	0	501760 46189	
94		0	0	0	0	0	-5292 323	0	
95		0	0	0	0	80640 4199	0	-277760 4199	
96		0	0	0	-5544 323	0	1404 17	0	
97		0	0	3600 323	0	-324000 4199	0	177282000 1062347	
98		0	-90 19	0	6864 133	. 0	-508068 3059	0	
99		1	0	-2655 119	0	45405 391	0	-11 3763 3 5083	
9 10		0	90 19	0	-384120 7429	0	6193044 37145	0	I
9 11		0	0	1485 133	0	-125334 1615	0	54439 323	

ML	R =-	0	1	2	3	4	5	6	
10 0		0	0	0	0	0	0	·0	_
10 1		0	0	0	0	0	0	0	
10 2		0	0	0	0	0	0	0	
10 3		0	0	0	0	0	0	0	
10 4	[0	0	0	0	0	0	6930 323	
10 5		0	0	0	0	0	-118272 4199	0	
10 6		0	0	0	0	9438 323	0	-96525 0 7429	
10 7		0	0	0	-52800 2261	0	13675200 96577	o	
10 8		0	0	1815 133	0	-1887 6 161	0	999702 3059	
10 9		0	-110 21	0	192060 2737	0	-555786 1955	0	
10 10		1	0	-11935 437	0	68926 391	0	-29255798 66861	
10 11		0	110 21	0	-46728 665	0	1381226 4845	0	
									_
M.L	R =	0	1	2	3	4	5	6	_
M L 11 0	R =	0	1	2	3	4	5	6	
H L 11 0 11 1	R =	0 0 0	1 0 0	2 0 0	3 0 0	4	5 0	6 0 0	
H L 11 0 11 1 11 2	R =	0 0 0 0	1 0 0 0	2 0 0 0	3 0 0 0	4 0 0 0	5 0 0 0	6 0 0 0	
H L 11 0 11 1 11 2 11 3	R =	0 0 0 0 0	1 0 0 0 0	2 0 0 0 0	3 0 0 0 0	4 0 0 0 0	5 0 0 0 0	6 0 0 0 0	
M L 11 0 11 1 11 2 11 3 11 4	R =	0 0 0 0 0 0	1 0 0 0 0 0	2 0 0 0 0 0	3 0 0 0 0 0 0	4 0 0 0 0 0	5 0 0 0 0 0	6 0 0 0 0 0 0	
H L 11 0 11 1 11 2 11 3 11 4 11 5	R -	0 0 0 0 0 0 0		2 0 0 0 0 0 0 0	3 0 0 0 0 0 0	4 0 0 0 0 0 0 0	5 0 0 0 0 0 0	6 0 0 0 0 3784704 36577	
M L 11 0 11 1 11 2 11 3 11 4 11 5 11 6	R =	0 0 0 0 0 0 0 0 0		2 0 0 0 0 0 0 0 0	3 0 0 0 0 0 0 0		5 0 0 0 0 0 0 -339768 7429	6 0 0 0 0 3784704 \$6577 0	
H L 11 0 11 1 11 2 11 3 11 4 11 5 11 6 11 7	R =	0 0 0 0 0 0 0 0 0		2 0 0 0 0 0 0 0 0	3 0 0 0 0 0 0 0	4 0 0 0 0 0 0 316800 7429	5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6 0 0 0 3784704 95577 0 -4967424 20995	
M L 11 0 11 1 11 2 11 3 11 4 11 5 11 6 11 7 11 8	R =			2 0 0 0 0 0 0 0 0 0 0	3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4 0 0 0 0 0 0 0 316800 7429 0	5 0 0 0 0 0 -339768 7429 0 3510936 15295	6 0 0 0 3784704 96577 0 -4967424 20995 0	
M L 11 0 11 1 11 2 11 3 11 4 11 5 11 6 11 7 11 8 11 9	R =			2 0 0 0 0 0 0 0 0 0 0 264.0 161	3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4 0 0 0 0 0 0 316800 7429 0 -334224 1955	5 0 0 0 0 0 0 0 0 0 7429 0 3510936 3510936 0 0	6 0 0 0 3784704 9577 0 -4967424 20995 0 3484096 5845	
M L 11 0 11 1 11 2 11 3 11 4 11 5 11 6 11 7 11 8 11 9 11 10	R =		1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 0 0 0 0 0 0 0 0 0 0 264.0 161 0	3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4 0 0 0 0 0 0 316800 7429 0 -334224 1955 0	5 0 0 0 0 0 -339768 7429 0 3510936 15295 0 -10260536 22287	6 0 0 0 3784704 96577 0 -4967424 20995 0 3484096 5845 0	

From Table 3.5 one can easily see that $T_{m\ell}^{-1}(\gamma)$ are polynomials for ℓ -even, which confirms (3.55). The polynomials have $(\ell+2)/2 - (\ell-m)$ and $(\ell+2)/2$ non-vanishing terms for $m \leq \ell$ and $m > \ell$, respectively. The number of terms of these polynomials are for $\ell = 4, 8, 12$ and 18 given in the following Table.

Table: Number of terms of the polynomials $T_{m,\ell-\text{even}}^{-1}(\gamma)$ for $\ell = 4, 8, 12$ and 18.

<i>1</i> \ m	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
4 8	1	2	3 1	3 2	3 3	3 4	3 5	35	3 5										
12						1	2	3	4	5	6	7	7	7	7	7	7	7	7
ΤQ								Т	2	3	4	5	ъ		8	9	т0	10	T0

For ℓ -odd and $0 \le \gamma \le 1$ - the functions $T_{m,\ell}^{-1}(\gamma)$ in (3.48) are represented by infinite series.

These series have the following characteristics:

- 1. The series are alternating for r < m. For $r \ge m$ all terms are positive for m-even, and negative for m-odd.
- 2. The coefficients $q_{m\ell}^r$ are first increasing with increasing r and then monotonically decreasing.

These characteristics are apparent in the following **Table**, where we list the coefficients $q_{m\ell}^{r}$ for $\ell = 15$, m = 16 and 17 and r = 0, 1, 2, ..., 299.

Obviously, the infinite series cannot be computed exactly by means of (3.48). They must therefore be curtailed at r = R, where R depends on the accuracy required. In this case an accuracy check is, therefore, necessary.

We will now turn to this error analysis.

3.5.3 Error estimation of the $T_{m,\ell}^{-1}(\gamma)$ computed.

The error analysis for $T_{m\ell}^{-1}(\gamma)$ is very similar to that given for $T_{\ell m}(\gamma)$; see Subsection 3.3.3. We will, therefore, present here only the essential relations.

In analogy to (3.37), for the remainder of the power series (3.48) we have

$$\begin{vmatrix} \sum_{\Sigma} q_{m,\ell}^{S} \gamma^{S} \\ s=S+1 \end{vmatrix} \leq B_{m,\ell} \gamma^{S+1} \qquad (3.78)$$

As the common convergence radius for the power series is equal to 1-, we may put $\gamma = 1$ in (3.78). This leads to the relation

$$\begin{vmatrix} \mathbf{x} & \mathbf{x} \\ \mathbf{\Sigma} & \mathbf{q}_{m\ell}^{S} \\ \mathbf{s}=\mathbf{S}+1 \end{vmatrix} = \begin{vmatrix} \mathbf{x} & \mathbf{q}_{m\ell}^{S} - \mathbf{\Sigma} \\ \mathbf{s}=|\mathbf{m}-\ell| \end{vmatrix} \mathbf{q}_{m\ell}^{S} - \mathbf{\Sigma} \mathbf{q}_{m\ell}^{S} \\ \mathbf{s}=|\mathbf{m}-\ell| \end{vmatrix} \leq \mathbf{B}_{m\ell} .$$
(3.79)

Table:	Coefficients	q ^r mℓ	for	ł	=	15,	m	=	16	and	17	and	r	=	٥,	1,	2,	•••,	299	•
--------	--------------	-------------------	-----	---	---	-----	---	---	----	-----	----	-----	---	---	----	----	----	------	-----	---

H =	≖16 L	-15									
R	0		1	2	3	4	5	6	7	8	9
0 10 30 30 50 50 50 50 50 50 50 50 50 5		۵	221 + 00 221 + 00 2201 + 00 2201 + 00 201		2,77366-02 -5,0367-020-02 -5,0367-020-02 -5,0367-020-02 -1,00199-1,00 -1,0019-1,00		-2.9588-00 -2.9588-00 -2.9588-00 -2.9588-00 -2.9588-00 -7.75994-00 -7.79948-00 -7.79948-00 -7.79948-00 -7.71146708-00 -7.71466708-00 -7.71466708-00 -7.71466708-00 -7.71466708-00 -7.71466708-00 -7.71466708-00 -7.71466708-00 -7.71466708-00 -7.7146778-00 -7.714778-00 -7.714778-00 -7.714778-00 -7.714778-00 -7.714778		1.5058-043 5.5599-0400 1.50599-0400 1.50599-0400 1.50599-0400 1.50599-0400 1.50599-0400 1.50599-0400 1.5059-04000 1.5059-04000 1.5059-04000 1.5059-04000 1.5059-04		
H =	• 17 L	=15	-								
R	0		1	2	3	4	5	6	7	8	9
0 10 30 30 50 70 90 110 130 140 140 140 140 140 220 220 220 220 220 220 220 220 220 2	0. 4.9818E+ 1.4561E+ 1.450E+ 3.7215E+ 1.4412E+ 3.7215E+ 3.8936E+ 2.40092E+ 1.5912E+ 3.8936E+ 3.8936E+ 3.7817E+	0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.		2.9900±01 3.2801±041 3.2801±041 3.2801±041 3.2801±041 3.2801±041 3.2801±041 3.2801±041 3.2804±042 4.2845±042 4.2845±044 3.6196±0443.6196±044 3.6196±0443.6196±044 3.6196±0443.6196±044 3.6196±0443.6196±044 3.6196±0443.6196±044 3.6196±0443.6196±0443.6196±0400000000000000		-6.7346E+02 4.7327E+04 1.0908E+01 4.3860E+01 2.4606E+02 2.4606E+02 3.1766E+03 2.0214E+03 3.1766E+03 3.1776E+03 3.1776E+03 3.1776E+03 3.17776E+03 3.17776E+03 3.17776E+03 3.17776E+03 3.17776E+03 3.17776E+03 3.17776E+03 3.17776E+03 3.177776E+03 3.177776E+03 3.177776E+03 3.177776E+03 3.177776E+03 3.177777777777777777777777777777777777	0.000.000.00000000000000000000000000000				

The infinite sum

 $\sum_{s=|m-\ell|}^{\infty} q_{m\ell}^{s}$

can be computed exactly using (3.56) and (3.57) or their equivalent representation (3.74a).

3.5.4 Annex to Section 3.5: Details of the numerical calculation.

3.5.4.1 THE COMPUTATION OF THE PRECISION MATRICES $s_{m\ell}$ of $T_{m\ell}^{-1}(\gamma)$.

Following very similar considerations as those for the determination of the precision matrices of $T_{\ell m}(\gamma)$ (see in 3.3.4.2) the basic relation for the check of the accuracy of the $T_{m\ell}^{-1}(\gamma)$ is

$$\begin{vmatrix} & & \\ \Sigma & q_{m\ell}^{S} \gamma^{S} - \sum_{s=|m-\ell|}^{S} q_{m\ell}^{S} \gamma^{S} \end{vmatrix} \xrightarrow{\infty} \left(\sum_{s=|m-\ell|}^{\infty} q_{m\ell}^{S} \gamma^{S} \right) \xrightarrow{\infty} \left(\sum_{s=|m-\ell|}^{\infty} q_{m\ell}^{S} \gamma^{S} \right) \xrightarrow{\infty} \left(3.80 \right)$$

$$\simeq \left| \begin{array}{c} \sum \\ \Sigma \\ s=S+1 \end{array} q_{m,\ell}^{S} \gamma^{S} \right| \left| \begin{array}{c} S \\ \Sigma \\ s=|m-\ell| \end{array} q_{m,\ell}^{S} \gamma^{S} \right| \leq B_{m,\ell} \gamma^{S+1} \left| \begin{array}{c} \sum \\ \Sigma \\ s=|m-\ell| \end{array} q_{m,\ell}^{S} \gamma^{S} \leq \epsilon \\ = |m-\ell| \end{array} \right|$$

where ϵ denotes the relative error which is constant for all $\mathbb{T}_{m\,\ell}^{-1}(\gamma)$ computed.

In order to satisfy (3.80) the power series has to be summed up to a certain S and, as this is true for any $T_{m\ell}^{-1}(\gamma)$, we obtain matrices $S_{m\ell}$, which we call **precision** matrices S. Such matrices for some typical values of γ are given in Table 3.6.

Table 3.6: Precision matrices $S_{m\ell}$ of the functions $T_{m\ell}^{-1}$ for $\gamma = 0.01, 0.1, 0.5, 0.9$ and a relative error $\epsilon \leq 10^{-4}$. The left side column is the number of non-vanishing terms taken into account, whereas the right side column is equal to $S_{m\ell}$.

MAT	RIX S	GAMMA = .010	EPS = 1.000E-04	PIMAX -	140				
H L	0	1	2 3	4	5	6	7		9
0 12 3 4 5 6 7 8 9 10 11 12 13 15 16 7 18 19 20	1 0 1 2 1 4 1 4 1 6 1 6 1 8 9 1 10 1 12 1 4 5 1 6 7 1 8 9 1 10 1 12 1 14 5 1 16 7 1 12 1 14 5 1 16 7 1 11 1 16 7 1 16 1 16 7 1 16 1 16	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0023234567890112344567890011234456789001123445678900112344567890011234456789001123445678	06543234567890111234561	0001343234556789910112234456789910112234455678991011223445567899101122344556789910112234455678991011223445567899101122344556789910112234455678991011223445567899101122344556789910112234455678991011223456789910112234567899101122345567899101122345567899101122345567899101122345567899101122345567899101122345567899101122345567899101122345567899100000000000000000000000000000000000	0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0000454323456789011123	0009876543234567890111213
ML	20	11	12 13	14	15	16	17	18	19
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 7 18 19 20	0 0 0 0 0 0 0 5 6 5 4 3 2 3 4 5 6 7 8 9 10 11 12 12	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 165 0 165 0 165 111 109 87 65 43 23 45 67 89 10	000000078765432345678	03333222222222222222222222222222222222	000000008987654343456	0 0 3 20 3 18 3 18 3 16 12 2 2 10 2 2 8 7 6 5 4 3 2 3 4 5 5	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 3 221 3 3 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1
MATE	RIX S	GAMMA = .100	EPS = 1.000E-04	PINAX =	140				
HL	0	1	2 3	4	5	6	7	8	9
0123456789011121345167 111213451671890	01234567890112344567	0 2 2 3 6 7 8 9 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{c} 0 & 0 \\ 1 & 2 \\ 2 & 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 9 \\ 10 \\ 3 \\ 11 \\ 12 \\ 3 \\ 14 \\ 14 \\ 14 \\ 3 \\ 16 \\ 16 \\ 3 \\ 17 \\ 18 \\ 3 \\ 19 \\ 10 \\ 3 \\ 12 \\ 14 \\ 14 \\ 14 \\ 3 \\ 16 \\ 16 \\ 3 \\ 17 \\ 18 \\ 3 \\ 20 \\ 3 \\ 21 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10$	0 0 2 2 3 4 5 6 7 8 9 0 1 1 2 3 3 3 3 4 5 6 7 8 9 10 1 1 2 3 3 3 14 5 16 7 18 9 10 11 3 3 3 14 5 16 7 18 9 3 3 16 7 18 9 3 3 10 16 7 18 9 3 3 10 16 7 18 9 3 3 10 16 7 18 9 3 3 10 16 7 18 9 3 3 10 16 7 18 9 3 3 10 16 7 18 9 3 3 10 16 7 18 9 3 3 10 16 7 18 9 3 3 10 16 7 18 9 10 16 7 18 10 10 10 10 10 10 10 10 10 10 10 10 10	087654567890111213456789101121341567189	0003456567890112345678	0 0 0 0 0 0 0 9 8 7 6 5 6 7 6 7 8 9 0 11 2 3 3 3 3 4 4 5 6 7 6 5 6 7 7 8 7 8 7 6 5 6 7 6 5 6 7 6 5 6 7 6 5 6 7 7 8 7 6 5 6 7 6 7 6 7 6 5 6 7 7 8 7 6 5 6 7 6 7 6 7 6 7 8 7 8 7 8 7 6 5 6 7 6 7 8 7 8 9 0 0 11 12 12 12 12 12 12 12 12 12	000045656789109111213445	04433334444444444444333
NL	10	11	12 13	14	15	16	17	18	19
0 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 1 1 1 2 3 4 5 6 7 8 9 1 1 2 3 4 5 6 7 8 9 1 1 2 3 4 5 6 7 8 9 1 1 1 2 3 4 5 6 7 8 9 1 1 2 3 4 5 6 7 8 9 1 1 1 2 3 4 5 6 7 8 9 1 1 2 3 4 5 1 1 2 3 4 5 1 1 2 3 4 5 1 1 2 3 4 5 1 1 2 3 4 5 1 1 2 3 4 5 1 1 2 3 4 5 1 1 2 3 1 1 2 3 1 1 2 3 1 1 2 3 1 1 2 3 1 1 2 3 1 1 2 3 1 1 2 3 1 1 2 3 1 1 2 3 1 1 2 3 1 1 2 3 1 1 2 3 1 1 1 2 3 1 1 2 3 1 1 2 1 1 1 2 3 1 1 1 2 3 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 4 \\ 15 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16$	00000078989878989011	0444444333334445555444	00000008909098989090	0423229871632110909898900	000000000000000000000000000000000000000	02554321918714321101109090

MAT	RIX S	GANNA = .500	EPS = 1.000E-04	PIMAX = 140				
HL	0	1	2 3	4	5 6	7	8	9
0 123345 667899 101112 13415 166717 1819 1920	1 0 1 12 1 23 1 4 1 5 1 6 1 7 8 1 9 1 12 1 13 1 14 1 15 1 16 1 12 1 13 1 14 1 15 1 16 1 12 1 13 1 14 1 12 1 14 1 15 1 16 1 12 1 14 1 12 1 14 1 12 1 14 1 12 1 14 1 12 1 14 1 15 1 16 1 12 1 12 1 14 1 12 1 14 1 12 1 12 1 14 1 12 1 16 1 16 1 16 1 17 1 18 1 19 1 12 1 16 1 17 1 18 1 19 1 19 1 18 1 19 1 19 1 18 1 18 1 19 1 18 1 19 1 18 1 18 1 19 1 19 1 18 1 18 1 19 1 19 1 19 1 19 1 19 1 18 1 19 1 1	0 6 6 9 0 111 111 113 6 6 118 6 6 118 6 6 221 6 6 224 6 6 224 6 6 224 6 6 224 6 6 224 6 6 224 6 6 228 8 9 0 11 12 12 12 12 12 12 12 12 12	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0 0 0 7 0 0 0 7 6 12 6 6 8 8 3 3 5 6 8 3 3 5 6 8 3 1 1 6 6 3 112 6 6 3 3 112 6 6 6 3 112 6 6 6 3 112 6 6 6 3 112 6 6 6 3 112 6 6 6 3 112 6 6 6 3 117 6 6 6 3 19 6 6 6	0 0 113 12 121 12 121 14 145 4 145 4 145 4 147 14 148 4 120 4 121 12 122 14 145 4 167 4 189 4 201 4 221 4 221 4 221 4 221 4 221 4 221 4 221 4 221 4 221 4 221 4 223 4	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	000004567890111214 112145555555555555555555555555555	0 0 9 223 20 20 7 17 6 14 7 14 6 13 7 14 6 13 9 16 9 18 10 8 18 8 19 8 20 9 18 10 7 21 7 20 7 20 7 20 7 20 7 20 20 7 7 20 7 20
ML	10	11	12 13	14	15 16	17	18	19
0123456789011234567891011234516718190	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 10 28 10 27 9 23 7 15 6 15 14 9 17 16 9 19 9 19 9 19 9 21 9 22 10 18 9 23 9 23 10 18 9 23 9 24 9 24 8 22 8 2 8	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0 0 12 0 0 12 0 0 11 0 0 11 0 0 11 0 0 11 0 0 12 0 0 11 0 0 9 1 7 8 4 10 6 5 11 7 8 145 11 8 16 11 8 18 12 11 8 19 11 8 12 11	0 33552318 22522176 156 2118 22522176 156 2118 19 0 212254 25 25 25 25 25 25 25 25 25 25 25 25 25	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	00000000000000000000000000000000000000	0 0 14 41 13 40 12 36 12 36 11 32 11 32 11 32 11 32 11 32 11 32 11 32 12 35 11 32 12 35 12 35 11 32 12 35 12 35 11 32 12 35 11 32 12 35 11 32 12 35 11 32 12 35 11 32 12 35 12 35 11 32 12 35 12 35 13 32 13 32 13 35 13 3
HATE	aix s	GANNA = .900	EPS = 1.000E-04	PIMAX = 140]			
H L	0	<u>1</u>	2 3	<u> </u>	<u> </u>	7	<u> </u>	9
5123456789011213456789101121345678901112134567890		1768992589125567.0012256670 17198992589125567.001225666871	$\begin{array}{c} 1 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\$	95552343433434343435555788824 2022794567899111171456788924 1011217145678992111171456978924	600123444 5007549 5007549 7761770 7723 7747 7781 884 884 880 99	-0 C 3 4 5 6 4 16 13 12 5 6 4 5 8 8 9 0 11 12 13 14 5 6 7 8 9 0 11 12 13 14 5 6 7 8 9 0 11 12 13 14 5 6 7 8 9 0 11 12 13 14 5 6 7 8 9 0 11 12 13 14 5 6 7 8 9 0 11 12 13 14 5 6 7 8 9 0 0 11 12 13 14 5 6 7 8 9 0 0 10 11 12 13 14 5 6 7 8 9 0 0 10 11 12 13 14 5 6 7 8 9 0 0 10 10 10 10 10 10 10 10 10 10 10 10	00004567890112345667890	4937313953448389401488881 4937313953448389401488881 10961782574778038881 10961949909 4439909999 4439909999 4439909999 4439909999999999
HL	10	11	12 13	14	15 16	17	18	19
012345678901123454	000005678910112345666666	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0 0 0 552 552 0 0 0 552 0 0 0 0 0 0 473 7 8 342 9 0 38 9 0 38 9 6 112 49 8 14 49 8 14	0 0 115 0 115 0 107 0 102 0 93 0 69 1 90 2 79 3 80 4 59 6 97 7	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	00000000000000000000000000000000000000	0 0 600 136 599 1323 597 1327 557 1224 551 1122 551 1122 551 1122 551 1122 551 1122 551 1122 551 1122 551 1122 551 1122 553 881 864 333 881 814 845 501 103

From this table one can immediately read off the speed of convergence and an indication of the computation time dependent on the variable γ used and for various m, ℓ . One can, for example, see that the computation time for the element m=2, ℓ =5 is roughly eight times greater for $\gamma = 0.9$ than for $\gamma = 0.1$.

3.5.4.2 THE COMPUTATION OF
$$T_{m,\ell}^{-1}(\gamma=1^-, \mu \in [0,1])$$
.

For the calculation of these matrix elements we have formulae (3.74a) and (3.76) and their equivalent sum free representations (3.56) and (3.57) at our disposal. Method A and Method B (see (3.76) and in 3.2.4.2.1) are complementary as can be seen from the following **Table:**

Table: The difference between Method A and Method B.

	0	1	2	3	4	5	6	7	8	9	10
0	1= 1	1- 2	- 3- 1=	1= 4~	1= 5~	1= 6~	1= 7~	1= 8~	9~ 1=	1= 10~	1= 11~
1	2= 1	- 2	3~	4.	5~	6.	7~	8~	9-	10~	11~
2	2~	2= 1	= 2~ 2=	2= 3-	2= 4~	2= 5-	2= 6~	2= 7~	2= 8~	2= 9~	2= ^{10~}
3	2~ 14	1- 2	• 3	-	5~	6	7~	8~	9-	10~	11~
4	3.	3~	3= 1=	3= 2~	3= 3~	3= 4~	3= 5-	3= 6~	3= ⁷ ~	3 = 8∼	3= ^{9~}
5	3~ 1'	2~ 2	• 3= 1=	-	5~	6.	7~	8~	9-	10~	11~
6	4~	*	4	4= 1=	4= 2~	4= 3-	4 ⁴	4= ⁵ ~	4= 6~	4= 7~	4- ⁸ ~
7	4~ ¹	· 3~ 2	2~ 3=	1= 4=	5-	\$	7~	8~	9-	10~	11~
8	5.	5-	5.	5.	5= ¹⁼		3~ 5=	5= 4	5- 5=	5= 6~	5= ⁷ ~
9	5~ ¹	4 ²	3-3-	2~ 4=	5= 1=	6.	7~	8~	9~	10~	11~
10	6~	6.	6~	6~	6-	1= 6=	6= ² ~	6= ³ -	6= 4~	6= 5-	6= 6~

To explain the data given above we take the box m = 10, $\ell = 6$:



Data given below the diagonal concern Method A and those given above the diagonal concern Method B. 6= means that six terms have been used in the series and the sign of all terms is equal. 2~ means that two terms of the series have been used and the sign of the terms changes. No data means that the method is not applicable for that case.

3.6 THE MATRICES T AND T-1.

3.6.1 Properties of the matrices T,T⁻¹.

• The transformation matrices have some interesting properties. One is the upper limit of the value of their elements. For them the following inequalities are valid

$$\left| \mathbf{T}_{\mathcal{M}}(\boldsymbol{\gamma}) \right| \leq 1$$
 and $\left| \mathbf{T}_{\mathcal{M}}^{-1}(\boldsymbol{\gamma}) \right| \leq 1$ (3.81)

Proof: Let us start with the defintion of $\mathbb{T}_{\mathbf{M}}(\gamma)$

$$T_{\mathcal{M}}(\gamma) = \frac{2m+1}{2} \int_{-1}^{+1} P_{\mathcal{A}}(\mu) P_{m}(\bar{\mu}) d\bar{\mu} =$$
$$= \frac{2m+1}{2} \int_{-1}^{+1} P_{\mathcal{A}}(\mu) (a+b\bar{\mu})^{1/2} P_{m}(\bar{\mu}) (a+b\bar{\mu})^{-1/2} d\bar{\mu} ,$$

where

$$a + b\bar{\mu} = 1 + 2\gamma\bar{\mu} + \gamma^{2} ,$$

$$T_{\ell m}(\gamma) = \frac{2m+1}{2} f_{\ell}(c_{\ell}) \int_{-1}^{+1} P_{m}(\bar{\mu}) (a+b\bar{\mu})^{-1/2} d\bar{\mu} \qquad c_{\ell} \in [-1,1]$$

With the aid of the well known relation [GR65,p.1027]

$$(1+2\gamma\mu+\mu^2)^{-1/2} = (-1)^n \sum_{n=0}^{\infty} \gamma^n P_n(\mu)$$

and the orthogonality property of the Legendre polynomials, we obtain

$$\begin{bmatrix} +1 \\ P_{m}(\bar{\mu}) & (a+b\bar{\mu})^{-1/2} d\mu = \frac{2}{2m+1} (-1)^{m} \gamma^{m} \end{bmatrix}$$

Hence,

$$T_{\ell m}(\gamma) = \frac{2m+1}{2} f_{\ell}(c_{\ell}) \frac{2}{2m+1} (-1)^{m} \gamma^{m} = (-1)^{m} f_{\ell}(c_{\ell}) \gamma^{m}$$

As $\gamma \in [0,1]$, it follows that

$$\left| \mathbb{T}_{\ell m}(\gamma) \right| \leq f_{\ell}(c_{\ell})$$

Now

$$f_{\ell}(C_{\ell}) \sim \int_{-1}^{+1} P_{\ell}(\mu) (a+b\overline{\mu})^{1/2} d\overline{\mu}$$

Since $T_{00}(\gamma) = 1$ we have to show that

$$f_{\ell+1}(c_{\ell+1}) \leq f_{\ell}(c_{\ell})$$

According to the inequality of SCHWARZ we have

$$f_{\ell}(c_{\ell}) \sim \int_{-1}^{+1} P_{\ell}(\mu) (a+b\bar{\mu})^{1/2} d\bar{\mu} \leq \\ \leq \left[\int_{-1}^{+1} P_{\ell}^{2}(\mu) d\bar{\mu} \right]^{1/2} \cdot \left[\int_{-1}^{+1} (a+b\bar{\mu}) d\bar{\mu} \right]^{1/2} \sim \left(\frac{h}{2\ell+1}\right)^{1/2}$$

where A is a constant which is independent of $\boldsymbol{\mathcal{X}}$.

f, thus decreases with increasing <code>l</code>. This completes the proof.

Note that

 $\left| P_{\ell}(\mu) (a+b\bar{\mu})^{1/2} \right| \leq 2$.

A similar proof can be made for $T_{m\ell}^{-1}(\gamma)$.

• Figures 6 to 8 illustrate the integrant $P_1(\mu)P_2(\bar{\mu})$ as a function of μ and $\bar{\mu}$, respectively, for various values of γ . From them one can approximately gauge the value of the corresponding integrals. They also demonstrate the smooth change of the integrants with the variation of the value of γ .

• Another interesting property of the matrices $T(\gamma)$ and $T^{-1}(\gamma)$ is their behaviour if γ approaches the boundary value equal to 1. In this case the following relations hold

$$T_{\ell m}(\gamma=1^{-}) = T_{\ell m}(\gamma=1)$$
 , $T_{m\ell}^{-1}(\gamma=1^{-}) \neq T_{m\ell}^{-1}(\gamma=1)$, (3.82)

where 1- indicates the left side of the boundary $\gamma = 1$. This results ipso facto from **Figure 5** on page 76 where the function $\bar{\mu}[\mu(\gamma)]$ is represented. The following **Figure 8** on page 98 is an additional demonstration of (3.82).

• Another interesting aspect of the functions $T_{\ell m}(\gamma)$ and $T_{m\ell}^{-1}(\gamma)$ is the variation caused by their dependence on γ . We did not investigate this in detail. Figures 9 to 14, however, give some idea of their behaviour. We have plotted there $T_{\ell m}(\gamma)/\gamma^{|\ell-m|}$ instead of $T_{\ell m}(\gamma)$ to enhance the variation (idem for $T_{m\ell}^{-1}(\gamma)$).

The following general **remarks** can be made on **these figures**:



Figure 6. The integrant $P_1(\mu)P_2(\bar{\mu})$ as a function of μ .

- The functions $T_{\ell m}(\gamma)/\gamma |\ell m|$ and $T_{m\ell}^{-1}(\gamma)/\gamma |m \ell|$ given there change smoothly with γ .
- The functions T_3 , and T_1 , have zeros. It would be of particular interest to study this item of the functions $T_{\ell m}(\gamma)$ and $T_{m\ell}^{-1}(\gamma)$ in more detail.

3.6.2 Some fundamental considerations.

As already stated in **CHAPTER 2**, the matrix T transforms \bar{a}_m into a_d and the matrix T^{-1} performs the inverse transformation.



Figure 7. The integrant $P_1(\mu)P_2(\bar{\mu})$ as a function of $\bar{\mu}$.

$$a_{\ell} = \sum_{m=0}^{\infty} T_{\ell m} \bar{a}_{m}, \quad \bar{a}_{m} = \sum_{\ell=0}^{\infty} T_{m\ell}^{-1} a_{\ell}.$$
 (3.83)

In matrix symbols, this reads

$$A = T.\overline{A} , \quad \overline{A} = T^{-1}.A . \quad (3.84)$$

In fact we have here to deal with infinite matrices which do not necessarily have the same properties as finite matrices [C055].

Formally it follows from (3.84) that

$$A = T.T^{-1}.A = I.A$$
, (3.85)


Figure 8. An example of the validity of (3.82): $T_{12}(\gamma=1^{-}) = T_{12}(\gamma=1);$ $T_{21}^{-1}(\gamma=1^{-}) \neq T_{21}^{-1}(\gamma=1).$

where I is the unit matrix.

Relation (3.85) is only valid if $T.(T^{-1}.A) = (T.T^{-1}).A$.

Note, however, that the product of infinite matrices is, in general, not associative.

From (3.84) it follows further that
$$\overline{A} = T^{-1} \cdot T \cdot \overline{A} = I \cdot \overline{A}$$
.

(3.86)



This relation is again only valid if

$$T^{-1}.(T.\bar{A}) = (T^{-1}.T).\bar{A}$$

and

 $T^{-1}.T = T.T^{-1}$

i.e., if the product of the matrices involved is associative **and** commutative. However, **infinite matrices are**, **in general**, **not commutative**.

Assuming that (3.85) holds, we have

$$I_{ij} = \sum_{k=0}^{\infty} T_{ik} T_{kj}^{-1} = \sum_{k=0}^{K} T_{ik} T_{kj}^{-1} + \sum_{k=K+1}^{\infty} T_{ik} T_{kj}^{-1}$$
(3.87)
i, j = 0, 1, 2,

In practice only the first summation term on the right-hand side is computed. The infinite matrices are thus truncated. Supposing that (3.87) is valid and the matrix elements of T, T⁻¹ are computed exactly, we immediately obtain the error due to the truncation of the matrices



 $\sum_{\substack{k=K+1}}^{\infty} T_{ik} T_{kj}^{-1} = I_{ij} - \sum_{\substack{k=0\\k=K}}^{K} T_{ik} T_{kj}^{-1} . \qquad (3.88)$

In reality the matrix elements of T and T^{-1} are, in general, not computed exactly. They can, however, be computed with a sufficiently high accuracy in order to perform a matrix truncation error check by using (3.88).

The inversion of the matrices T or T^{-1} by means of classical inversion techniques, i.e., starting from a well known matrix (using the code **EISPACK** for example), is not advisable in our case since the accuracy of the elements of the inverted matrix would then be influenced by three effects:



- the inaccuracy of the elements of the matrix to be inverted;
- the uncertainty caused by the truncation of this matrix,
- and of course the algorithm used.

We will now turn to the discussion of the products T^{-1} . T and $T.T^{-1}$ which have a certain importance for checking the numerical quality of the transformation.

3.6.3 The matrix products T⁻¹.T and T.T⁻¹.



3.6.3.1 THE PRODUCT T-1.T.

According to the definition of these matrices the product explicitly reads

$$(\mathbf{T}^{-1} \cdot \mathbf{T})_{ij} = \sum_{k=0}^{\infty} \mathbf{T}_{ik}^{-1} \mathbf{T}_{kj} = \mathbf{I}$$
, (3.89)

where i, $j = 0, 1, 2, \ldots$ and I is the unit matrix.



However, in practice one has to confine oneself to finite matrices. We thus have to deal with matrices of the size (L,M) for T and (M,L) for T⁻¹. Equ.(3.89) therefore reads

$$(\mathbf{T}^{-1} \cdot \mathbf{T})_{ij} = (\mathbf{T}^{-1} \cdot \mathbf{T})_{ij,1} + (\mathbf{T}^{-1} \cdot \mathbf{T})_{ij,2} =$$

= $\sum_{k=0}^{K} \mathbf{T}_{ik}^{-1} \mathbf{T}_{kj} + \sum_{k=K+1}^{\infty} \mathbf{T}_{ik}^{-1} \mathbf{T}_{kj} = \mathbf{I}_{1} + \mathbf{I}_{2} = \mathbf{I}$ (3.90)

It can be shown that the following relation holds

$$\sum_{k=K+1}^{\infty} T_{ik}^{-1} T_{kj} = 0$$
for K > 2j+1 and any i.
$$(3.91)$$

This is demonstrated in the following **Table**, where we give the explicit numerical results of the matrix product T^{-1} . T for $\gamma = 0.5$ and K = 20.

We can immediately see from this table that (3.91) is satisfied at least for $j \leq 9$.



From (3.90) and (3.91) one immediately obtains

 $(T^{-1}.T)_{ij} = I_{1} = (T^{-1}.T)_{ij,1}$ (3.92) for K \leq 2j+1 and any i,

Table: Explicit numerical results of the products $(T^{-1}.T)_{1j}$, $(T^{-1}.T)_{2j}$ and $(T^{-1}.T)_{3i}$; $\gamma = 0.5$; K = 20; $\epsilon_{me} \leq 10^{-4}$. N is the total number of non-vanishing terms.

I	J	N	(T-1.T) IJ	K-TH TERM WITH SIGN	
111111111111111111111122	01234567890112345678901	33456789011111111111111144	6.3955142E-06 1.0000177E+00 6.00747055-06 2.6600998E-06 -1.2554676E-06 6.0831822E-07 -2.9860973E-07 -3.4769768E-07 -3.4631062E-08 -1.8325499E-08 -1.8325499E-08 -1.86325499E-08 -1.86735E-10 -2.964268E-11 -3.52263E-11 -3.52735E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E-10 -3.52755E	Lotteriteriteriteriteriteriteriteriteriter	
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	1234567890112345678900	4567890112222222222222222	6.0222444=0 1.0000055:+00 2.8686337E=06 3.653951E=06 2.4497261E=06 -3.62299E=07 -3.9028299E=07 -3.901416E=07 -5.977413E=07 -7.5475362E=08 3.6451549E=08 -1.6937209E=08 -1.6937209E=08 -3.5005166E=10 5.905166E=10 5.905166E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054136E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.9054156E=11 5.90540	$ \begin{array}{c} c = -1 \\ c = $	
ຑຓຓຓຓຓຓຓຓຓຓຓຓຓຓຨຬຎຓ	1234567890111234567890111234567890111234567890111234567890111234567890111234567890	56789011233333333333333333333333333333333333	-1.32634625-08 2.26812685-06 9.99998225-01 1.66933435-06 -1.27492975-06 -1.27492975-06 -1.2469736185-06 -1.246973615-06 -1.246973615-06 -1.246973615-08 -1.246973615-08 -1.2244375-08 -2.25422775-08 -2.25422775-08 -2.2542775-08 -2.46138965-08 -1.41474675-08 8.06388505-09	น้ำนา่านา่านา่านา่านา่านา่านา่านา่า นั่นหนึ่งหนึ่งหนึ่งหนึ่งหนึ่งหนึ่งหนึ่ง นั่นชื่อยน้อยน้อยน้อยน้อยน้อยน้อย ************************************	19 19 19 19 -19 -19 19 -19 19 19 19

i.e., in spite of dealing with the truncated matrices T⁻¹, T we always get a submatrix of  $(T^{-1},T)_{ij}$  which is a unit matrix, assuming of course that the elements of  $T^{-1}$ , T have been computed exactly.

In the **Table 3.7** we give  $(T^{-1},T)_{ij} - I$  for i = 0, 1, ..., 20; j = 0, 1, ..., 19;K = 20.

**Table 3.7:**  $(T^{-1},T)_{jj} - I$  for  $i = 0, 1, ..., 20; j = 0, 1, ..., 19; K = 20; \gamma = 0.01,$ 0.1, 0.5 and 0.9;  $\epsilon_{\rm me} \leq 10^{-4}$ .

L	1 1	0	1	2	3	4	5	6	7	8	9
	0123456789011234567890112345678901123456789011234567890112345678901123456789001123456789001123456789001123456789001123456789001123456789001123456789001123456789001123456789001123456789001123456789001123456789001123456789001123456789001123456789001123456789001123456789000000000000000000000000000000000000	$\begin{array}{c} 0,\\ 1.9047[E-12]\\ -4.76(19E-14)\\ -7.1739E-16\\ -2.4895[E-18]\\ -5.4116E-21\\ -4.1607E-22\\ -4.1607E-22\\ -4.1607E-22\\ -2.4415E-28\\ -2.4415E-28\\ -2.4415E-28\\ -2.2415E-28\\ -2.2415E-28\\ -2.2415E-28\\ -2.2976E-49\\ -3.0107E-39\\ -2.2976E-49\\ -1.795E-46\\ -1.7955E-46\\ -1.7955E-46\\ -1.7955E-46\\ -1.665E-49\\ -1.665E-49\\ -1.665E-49\\ \end{array}$	0. 2.8572E-10 3.3494E-16 -6.7563E-13 2.4981E-15 -1.1575E-17 2.10579E-21 1.18321E-23 -7.7087E-26 -5.2487E-32 -4.5537E-34 4.7330E-28 -5.2487E-32 -4.5537E-34 -5.5955E-38 -5.5955E-38 -1.1844E-41 1.9510E-43 -3.2059E-43 -3.2059E-47 -5.1557E-47	$\begin{array}{c} 0, \\ -3.0477E-11, \\ +2.850L-09, \\ -9.1721E-11, \\ +1.426E-12, \\ -3.3337E-15, \\ -1.3719E-16, \\ -1.3719E-16, \\ -1.37950E-18, \\ -1.3935E-20, \\ -1.3422E-24, \\ -1.397E-30, \\ -1.397E-30, \\ -1.397E-36, \\ -1.4937E-30, \\ -1.4937E-30, \\ -1.4937E-30, \\ -1.534E-34, \\ -1.5717E-36, \\ -1.534E-34, \\ -1.5717E-36, \\ -1.532E-34, \\ -1.5$	0. -6.3664E-14 -1.7576E-10 -2.9327E-08 -3.9522E-10 -1.7864E-11 -3.9230E-14 -3.9230E-14 -3.9230E-14 -3.9230E-14 -3.9230E-14 -1.1545E-23 -1.3601E-25 -1.3601E-27 -1.5856E-20 -1.5856E-21 -1.4735E-27 -1.5856E-21 -1.4735E-27 -1.5856E-21 -1.949E-37 -1.8021E-35 -1.9070E-39 2.0713E-41	0. 1.6430E-15 1.5859E-12 5.5575E-10 7.794E-08 -1.0702E-09 5.8902E-11 -1.5125E-13 3.2434E-17 -4.8650E-19 5.8187E-27 -4.8650E-19 5.8187E-27 -8.6856E-23 7.6658E-23 -1.2308E-34 -1.2308E-34 -1.4559E-36 -1.4559E-38	0. -4.7850E-18 2.6001E-15 -9.8295E-12 -1.3777E-09 -2.3371E-09 -2.3371E-09 -2.3371E-09 -2.3371E-02 -2.3371E-02 -2.3371E-20 -2.3371E-20 -2.4092E-132 2.4092E-132 5.6098E-30 -5.6098E-30 -5.6098E-30 -7.2626E-34 8.1669E-36	0. 6.1962E-21 5.7136E-18 7.8752E-15 7.874E-11 -2.8441E-09 4.9304E-07 -4.4648E-09 -1.037E-12 -3.7474E-10 -1.037E-12 -3.7477E-10 -1.037E-12 -1.6295E-23 -1.6622E-25 -1.6622E-25 -1.6622E-25 -1.6622E-25 -2.7623E-31 -3.2214E-33	0. 3.2775E-22 3.2775E-19 -3.0088E-16 -5.8196E-14 -1.1230E-10 -5.2464E-09 -9.0174E-07 -7.7720E-09 -7.97074E-10 -7.97074E-10 -7.97074E-10 -2.1055E-12 -1.6016E-13 -2.1555E-16 -2.1555E-17 -3.3429E-21 -3.3429E-21 -4.755E-25 -4.755E-25 -4.4150E-29 -1.0212E-30	0. 4.5823E-24 4.5823E-24 5.6211E-21 3.5897E-18 2.3064E-15 -2.0553E-13 -2.7930E-10 -2.7930E-10 -1.5185E-06 -1.5350E-09 -1.5350E-09 -1.5350E-09 -1.5350E-09 -1.5497E-15 -6.1050E-19 -5.4704E-17 -6.1050E-19 -1.2400E-22 -1.6387E-24 -2.1150E-24 -2.1630E-28	0. -1.7443E-26 2.4538E-23 -3.2457E-20 -3.2457E-20 -3.2457E-20 -3.5509E-13 -5.5509E-13 -5.5509E-13 -5.5509E-13 -1.4524E-08 -2.4022E-06 -1.9450E-08 -2.7679E-09 -7.2291E-12 -7.9109E-13 9.725E-15 -1.3775E-16 -1.3775E-16 -1.24427E-20 3.2490E-224 -2.4297E-20 3.2490E-224 -5.9770E-26
E	ΙJ	10	11	12	13	14	15	16	17	18	19
	0123456789011234567890112341567890	0. 5.0412E-29 2.0127E-25 3.3095E-22 2.0721E-19 6.8503E-17 -1.2676E-12 -1.2277E-11 -1.2277E-12 -3.48676E-14 -1.2277E-12 -3.6230E-06 -2.8708E-08 -3.6230E-06 -2.8708E-08 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.6230E-06 -3.738E-18 -3.738E-18 -5.7931E-22 -1.735E-23	0. -6.6284E-31 -2.1341E-27 -3.5992E-24 2.4171E-21 -9.7904E-19 2.0300E-16 -9.7889E-14 -2.5886E-12 -2.5886E-12 -7.8833E-09 -7.8833E-01 -9.40921E-08 -7.8833E-01 -1.9941E-11 -2.9555E-12 -1.9555E-14 -6.4604E-16 6.5562E-19 -5.9506E-21	0. 5.1404E-33 2.0946E-29 3.7921E-26 7.7000E-23 1.1730E-20 3.6968E-18 5.1958E-16 5.1958E-16 5.1958E-16 7.3735E-06 -5.6656E-08 -3.1198E-11 4.0013E-09 -4.402E-08 -3.1198E-11 5.2933E-12 -5.2933E-12 -1.2473E-08 -3.1198E-11 -1.2667E-17 -1.2667E-17 -4.3004E-18	0. -9.0924E-36 1.9327E-31 1.9327E-31 2.9555E-25 -1.3579E-22 4.3953E-20 -1.1801E-17 -5.3707E-25 -5.3707E-13 -6.6809E-09 -1.0075E-05 -7.6533E-08 -1.9098E-08 -1.9098E-08 -7.6533E-08 -1.9098E-08 -7.6533E-08 -1.9098E-08 -1.9098E-08 -7.6533E-08 -1.9098E-08 -1.2508E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 -1.2681E-15 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\hbox{\tt E-08}\\ -1.0122 \hbox{\tt E-08}\\ -3.9995 \hbox{\tt E-08}\\ -1.0122 \hbox{\tt E-08}\\ -1.01$	$\begin{array}{c} 0.\\ -8.1804E-40\\ 1.9181E-35\\ -4.2666E-32\\ 3.5041E-29\\ -1.7797E-26\\ 6.4645E-24\\ -1.7962E-21\\ 3.7793E-26\\ 3.7793E-21\\ -2.1482E-12\\ -2.3118E-11\\ -1.6550E-08\\ -1.3145E-07\\	0. 4.0973E-41 2.0312E-37 4.4655E-34 4.4655E-34 2.0950E-28 5.3069E-21 9.3603E-19 9.3603E-19 9.3603E-19 9.3603E-19 9.2648E-15 -3.9448E-15 -3.9448E-15 -3.9448E-15 -2.4912E-08 -1.4015E-07 -2.495E-10 -3.3285E-10 -4.1039E-09	0. -1.1100E-42 -2.2817E-39 -4.7032E-36 4.0538E-33 -2.2385E-30 -2.7582E-25 -3.7582E-25 -3.7582E-25 -3.452E-25 -3.245E-16 -4.2345E-16 -4.2345E-16 -4.648E-08 -1.7839E-07 -2.8732E-05 -3.5713E-08 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 -3.0030E-07 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Г	MATR	IX T-1+T - 1	GAMMA	= .100	EPS = 1.000	E04 P1	MAX = 140				
F	MATR	IX T-1*T - 1 0	GAMMA 1	= .100 2	EPS = 1.000	E04 P) 4	IMAX = 140 5	6	7	8	9
	MATR I J 0 1 2 3 4 5 6 7 8 9 10 11 12 14 15 16 17 19 20	1X T-1*T - 1 0 0. 1.9111E-07 -3.8277E-08 2.8851E-11 -3.5337E-12 2.8851E-11 -3.5337E-12 -4.0054E-13 -4.0054E-13 -7.6901E-16 -7.6901E-16 -7.6901E-16 -4.8131E-18 2.6365E-20 -4.3263E-21 2.6365E-20 -3.3074E-26	GANMA 1 2.8877E-06 -3.9019E-09 -3.9019E-09 -3.8204E-08 1.3448E-08 -1.7374E-09 2.1056E-10 -7.4383E-11 2.7434E-12 -3.7433E-12 -4.973E-17 -5.2504E-129 -6.0706E-20 -7.8142E-23 8.5123E-24	<ul> <li>.100</li> <li>2</li> <li>0.</li> <li>-1.94426-07</li> <li>-3.4246-08</li> <li>-1.95986-08</li> <li>-2.49871-10</li> <li>-2.59216-12</li> <li>-2.59216-12</li> <li>-2.59216-13</li> <li>-3.49036-14</li> <li>-5.58211-15</li> <li>8.34822-16</li> <li>8.34822-16</li> <li>-1.65236-19</li> <li>-2.34711-20</li> <li>-3.24021-21</li> <li>-3.24021-21</li> <li>-3.7456-23</li> </ul>	EPS = 1.000 3 0. 1.7524E-08 9.3496E-09 9.3496E-09 -1.8733E-07 1.2423E-08 -9.385E-08 -1.1490E-08 -9.3656E-17 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.4905E-08 -1.	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E-04 P) 4 0. -1.6709E-09 7.5913E-09 2.5337E-07 4.52016E-07 4.52016E-07 4.52016E-07 4.52016E-07 4.5276E-08 1.2349E-08 2.2276E-09 3.7854E-10 5.9708E-11 1.9209E-13 -2.7684E-14 5.9708E-14 1.9209E-13 -2.7684E-14 5.9728E-16 5.9728E-16 5.9728E-16 5.9728E-16 5.9728E-16 5.9728E-16 5.9728E-16 5.9728E-16 5.9728E-16 5.9729E-12 1.9209E-13 5.9129E-18 8.0748E-19 14	IMAX = 140 5 0. 1.5224E-10 2.0927E-10 6.1820E-08 1.6279E-06 7.2639E-06 -3.0876E-07 4.9305E-08 9.3304E-09 1.33947E-09 9.3304E-09 1.33947E-09 7.2035E-08 1.3878E-13 -1.8843E-14 2.5025E-15 4.9853E-16 -6.6883E-17 15	6 0. -1.4479E-11 -9.9917E-09 -1.8756E-07 -1.6447E-06 9.8832E-07 -8.7196E-07 -1.6992E-07 -9.2284E-08 1.4095E-08 -0.2954E-07 -9.2284E-08 1.4095E-08 -0.2954E-07 -1.6992E-07 -9.2284E-08 1.4095E-08 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.731E-12 -1.731E-15 -1.7731E-15 -1.6992E-07 -1.6992E-07 -1.7731E-15 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.7731E-15 -1.6992E-07 -1.6992E-07 -1.7731E-15 -1.6992E-07 -1.6992E-07 -1.7731E-15 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.7731E-15 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.7731E-15 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.7731E-15 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6992E-07 -1.6	7 0. 1.3728E-12 4.2855E-12 -1.0197E-09 5.9664E-08 6.7023E-07 4.3011E-06 3.4777E-06 -7.0824E-07 -7.0824E-07 -7.0824E-07 -7.0824E-07 -7.0824E-07 -7.0824E-07 -7.9845E-09 -1.7902E-10 2.4305E-13 -2.431E-12 -1.2734E-13 -1.7099E-14 17	8 0. -1.2919E-13 1.2779E-12 -1.6643E-10 9.3009E-09 9.3009E-09 9.3009E-09 -9.8271E-07 -3.8933E-07 -3.8933E-07 -3.8933E-07 -3.8933E-07 -3.8231E-08 -9.8271E-09 -1.6647E-09 -1.6647E-09 -2.3387E-10 -3.6360E-11 4.3098E-15 -3.4509E-14 3.0086E-15 -18	9 D. 1.2030E-14 1.25594E-13 2.5594E-14 1.25594E-14 1.25594E-14 1.25594E-14 1.25594E-14 1.25594E-14 1.25594E-14 1.25594E-14 1.25594E-14 1.25594E-14 1.25594E-14 1.25594E-14 1.25594E-14 1.25595E-14 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10 1.25575E-10

MATRIX T-1*T - I

GANNA = .010

EPS = 1.000E-04

PIMAX = 140

## TABLE 3.7

MAT	RIX T-1=T - 3	I GAMMA	= .500	EPS = 1.00	DE-04 P	MAX = 140				<u> </u>
IJ	0	1	2	3	4	5	6	7	8	9
01234567890112314567890 1112314567890	0. 35575 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.3577 1.35777 1.3577 1.3577 1.3577 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.35777 1.357777 1.357777 1.357777 1.357777 1.357777 1.357777 1.357777 1.357777 1.3577777 1.3577777 1.35777777 1.35777777777777777777777777777777777777	0. 7052-1-078 7052-1-078 7052-1-078 7052-1-078 7052-1-078 7052-1-078 7052-1-078 7052-1-078 7052-1-078 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MATE	IX T-1*T - I	E GANMA	900	EPS = 1.00	)E-04 P1	IMAX = 140				
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-2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.2477E-04 -2.	0. 2.1479E-06 -1.0824E-06 4.9715E-07 1.7421E-06 2.5594E-06 2.5594E-06 1.939E-06 1.939E-06 2.4739E-06 9.0565E-06 8.0312E-04 -7.9903E-04 8.0312E-04 -7.9903E-04 8.0312E-04 -7.9903E-04 8.0312E-04 -7.9903E-04 8.0312E-04 -7.9903E-04 8.0312E-04 -7.9903E-04 8.0312E-04 -7.9903E-04 8.0312E-04 -7.9903E-04 8.0312E-04 -7.9903E-04 8.0312E-04 -7.9903E-04 -7.9903E-04 -7.9903E-04 -7.9903E-04 -7.9903E-04 -8.0312E-04 -7.9903E-04 -8.0312E-04 -7.9903E-04 -8.0312E-04 -7.9903E-04 -8.0312E-04 -7.9903E-04 -8.0312E-04 -7.9903E-04 -8.0312E-04 -1.683E-03 -1.683E-03 -1.683E-03 -1.683E-03 -1.683E-03 -1.683E-03 -1.683E-03 -1.683E-03 -1.683E-03 -1.683E-03 -1.683E-04 -1.683E-03 -1.683E-04 -1.683E-03 -1.683E-04 -1.683E-03 -1.683E-04 -1.683E-03 -1.683E-04 -1.683E-03 -1.683E-04 -1.683E-03 -1.683E-04 -1.683E-03 -1.683E-04 -1.683E-03 -1.683E-04 -1.683E-03 -1.683E-04 -1.683E-03 -1.683E-04 -1.683E-04 -1.683E-04 -1.683E-04 -1.683E-04 -1.683E-04 -1.683E-04 -1.683E-04 -1.683E-04 -1.683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1683E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-04 -1.1682E-0
LI	10	11	12	13	14	15	16	17	18	19
012345675	0. -1.5367E-06 -7.0430E-07 4.4449E-06 -1.0428E-05 2.2643E-05	0. 2.6684E-06 -3.8211E-06 8.1814E-06 -2.0835E-05 5.1758E-05	0. -1.1100E-06 -6.8531E-07 2.7529E-06 -5.8163E-06 1.2904E-05	0. 6.2768E-07 2.0778E-06 -5.7531E-06 1.2745E-05 -2.9449E-05	0, -6.8379E-07 -1.5190E-06 3.7710E-06 -7.9996E-06 1.8082E-05 -4.3260E-05	0. 8.7842E-07 3.5282E-07 -6.3750E-07 7.4674E-07 -1.2385E-06	0. -1.0046E~06 5.1261E~07 -1.5866E~06 4.5620E~06 -1.0832E~05 2.7063E~05	0. 1.0041E-06 -9.3420E-07 2.4973E-06 -6.6752E-06 1.5391E-05 -3.7594E-05	0. -8.9609E-07 9.0581E-07 -2.4483E-06 5.9800E-06 -1.3674E-05 3.3359E-05	0. 7.2686E-07 -5.4726E-07 1.6010E-06 -3.8260E-06 8.4971E-06 -2.0803E-05

According to (3.92), the submatrix i = 0, 1, ..., 20; j = 0, 1, ..., 9 does not contain any error due to truncation of the size of the matrix but only contains the uncertainty due to the error of the matrix elements of T and T⁻¹. Note that the matrix elements of T⁻¹ and T have only been calculated to a relative error of  $\epsilon_{me} \leq 10^{-4}$ . This submatrix is, therefore, not equal to zero as it should be. Consequently, the smaller this relative error becomes, the more the values of this submatrix should approach the value 0. This is demonstrated in the following Table. Note, this is a numerical proof of the correctness of the error estimation formalism which is discussed in Subsections 3.3.3 and 3.5.3. For j > 9 there is, with increasing j, an increasing influence of the error due to truncation and also an increasing influence of the matrix elements as i increases, since the number of summation terms of the matrix product grows with i. These two influences appear clearly in Table 3.7.

**Table:** Demonstration of the convergence of the submatrix  $(T^{-1}.T)_{ij}$  for some elements and various relative accuracies  $\epsilon_{me}$  of the matrix elements of the matrices T,  $T^{-1}$ ;  $\gamma = 0.5$ .

i	j\ [€] me	10-3	10-4	10- <del>5</del>	10-6
1	0	5.52E-05	6.40E~06	1.14E-07	2.16E-08
1	1	1.50E-04	1.77E-05	5.11E-07	6.07E-08
4	0	-5.37E-06	-8.07E-07	-4.68E-08	-4.08E-09
4	4	-9.87E-05	-7.06E-06	-3.70E-07	-6.71E-08
9	0	3.56E-07	2.04E-08	3.45E-09	1.13E-10
9	9	6.07E-06	-1.81E-06	-3.65E-07	-1.39E-08

3.6.3.2 THE PRODUCT T.T-1.

This product reads more explicitly

$$(T.T^{-1})_{ij} = \sum_{k=0}^{\infty} T_{ik} T_{kj}^{-1} = I$$
, (3.93)

where i, j = 0, 1, 2, ... and I is the unit matrix.

For practical applications, as already seen above, one is dealing with finite matrices. However, no analogous relation to (3.91) holds. This is demonstrated in the following **Table**, where we give the product (3.93¹ explicitly for j = 0, 1, ..., 20; i = 1, 2, 3; K = 20;  $\gamma = 0.5$  and  $\epsilon_{me} \leq 10^{-4}$ .

**Table:** Explicit numerical results of the products  $(T.T^{-1})_{j1}$ ,  $(T.T^{-1})_{j2}$  and  $(T.T^{-1})_{j3}$ ;  $\gamma = 0.5$ ; j = 0, 1, ..., 20; i = 1, 2, 3; K = 20;  $\epsilon_{me} \leq 10^{-4}$ . N is the total number of non-vanishing terms.

J	I	N	(T.T-1) IJ	K-TH TERM NITH SIGN
ן 123456789901123456789001234567-89011234567890012345678901123456789011234567	1 1111111111111111111111111110000000000	222212012012121212012120112222219218217216215214213212011222221921821706025242330	1.1-1-1) 1.00001800+0.0 9.294907945-06 2.481407445-06 2.49902054495-08 2.49902054495-08 2.49902054495-08 2.49902054495-08 2.49902054495-08 1.240532445-07 2.240532445-07 2.24532445-07 2.24532445-07 2.24532445-07 2.24532445-07 2.24532445-07 2.24532445-07 2.24532445-07 2.24532445-07 2.2453245-08 4.1555695-08 8.53472365-08 8.53472365-09 9.69524705-08 8.53472365-09 9.69524705-08 8.53472365-09 1.21344285-09 2.55141785-08 8.53472365-09 1.21344285-07 1.553233145-00 2.5534735-06 8.53472365-07 1.553233145-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307335-06 2.36307355-06 3.3731735-01 1.60732535-06 3.37325335-06 2.36307335-06 3.37325335-06 2.36307335-06 2.3630735-06 3.3732535-06 3.37325335-06 3.37325335-06 3.37325335-06 3.37325335-06 3.37325355-06 3.37325355-06 3.37325355-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.373255335-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.37325535-06 3.373255555555-06 3.37325555555555555555555555555555555555	$\begin{array}{c} 1 & 2 & 3 & 4 & 5 & 6 & 7 & 8 & 9 & 10 & 11 & 12 & 13 & 14 & 15 & 16 & 17 & 18 & 19 & 20 \\ 1 & -2 & -3 & -4 & -5 & 6 & -7 & -8 & -9 & 10 & 11 & 12 & 13 & 14 & 15 & 16 & 17 & 18 & 19 & 20 \\ 1 & -2 & -3 & -4 & -5 & 6 & -7 & -8 & -9 & 10 & 11 & 12 & 13 & 14 & 15 & 16 & 17 & 18 & 19 & 20 \\ -1 & -2 & -3 & -4 & -5 & 6 & -7 & -8 & -9 & 10 & 11 & 12 & 13 & 14 & 15 & 16 & 17 & 18 & 19 & 20 \\ -1 & -2 & -3 & -4 & -5 & 6 & -7 & -8 & -9 & 10 & 11 & 12 & 13 & 14 & 15 & 16 & 17 & 18 & 19 & 20 \\ -1 & -2 & -3 & -4 & -5 & 6 & -7 & -8 & -9 & 10 & 11 & 12 & 13 & 14 & 15 & 16 & 17 & 18 & 19 & 20 \\ 1 & 1 & 2 & 3 & -4 & -5 & 6 & -7 & -8 & -9 & 10 & 11 & 12 & 13 & 14 & 15 & 16 & 17 & 18 & 19 & 20 \\ 1 & -2 & -3 & -4 & -5 & 6 & -7 & -8 & -9 & 10 & -11 & -12 & -13 & -14 & -15 & -16 & -17 & 18 & 19 & 20 \\ 1 & -2 & -7 & -8 & -9 & 10 & -11 & -12 & -13 & -14 & -15 & -16 & -17 & 18 & 19 & 20 \\ -1 & -2 & -7 & -8 & -9 & 10 & -11 & -12 & -13 & 14 & -15 & -16 & -17 & 18 & 19 & 20 \\ 1 & -7 & -8 & -9 & 10 & 11 & 12 & 13 & -14 & -15 & -16 & -17 & 18 & 19 & 20 \\ 1 & -7 & -8 & -9 & 10 & 11 & 12 & -13 & -16 & 17 & 18 & 19 & 20 \\ 1 & -7 & -8 & -9 & 10 & -11 & -12 & -13 & 14 & 15 & 16 & 17 & -18 & -19 & 20 \\ 1 & -7 & -8 & -9 & -10 & 11 & 12 & -13 & -14 & -15 & -16 & -17 & 18 & 19 & 20 \\ 1 & -12 & -3 & -4 & -5 & -6 & -7 & -8 & -9 & -100 & -11 & -12 & -13 & -14 & -15 & 16 & 17 & -18 & -19 & -20 \\ 1 & -12 & -13 & -14 & 15 & 16 & -17 & -18 & -19 & 20 & 11 & -12 & -13 & -14 & -15 & -16 & -17 & -18 & -19 & -20 \\ 1 & -12 & -13 & -14 & 15 & 16 & -17 & -18 & -19 & -20 & 11 & -12 & -13 & -14 & -15 & -16 & -17 & -18 & -19 & -20 \\ 1 & -12 & -13 & -14 & -15 & -6 & -7 & -8 & -9 & -100 & -11 & -12 & -13 & -14 & -15 & -16 & -17 & -18 & -19 & -20 \\ 1 & -12 & -13 & -14 & 15 & 16 & -17 & -18 & -19 & -20 & -11 & -12 & -13 & -14 & -15 & -16 & -17 & -18 & -19 & -20 \\ 1 & -12 & -13 & -14 & 15 & 16 & 17 & -18 & -19 & -20 & -11 & -12 & -13 & -14 & 15 & 16 & 17 & -18 & -19 & -20 \\ 1 & -12 & -7 & -3 & -4 & -5 & -6 & -7 & -8 & -9 & -10 & -11 & -12 & -13 & -14 & -15 & -16 & -$
19 20	33	20 11	-6.9427333E-06 -3.7918975E-06	1 -2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 -10 11 -12 13 -14 15 16 17 -18 -19 20

We see from this **Table** that non-vanishing terms of (3.93) start at  $k = k_1$ . The values for  $k_1$  are given in the subsequent **Table**.

Table: Values for k1.

i /j	even = 2j'	ođđ = 2j'+1
even =2i'	i'	j' .i ≤ j-3 i' .i > j-3
odd =2i'+1	1	j' + δ _{j1}

In analogy to (3.90), we have

$$(\mathbf{T}.\mathbf{T}^{-1})_{ij} = (\mathbf{T}.\mathbf{T}^{-1})_{ij,1} + (\mathbf{T}.\mathbf{T}^{-1})_{ij,2} = \\ = \sum_{k=0}^{K} \mathbf{T}_{ik} \mathbf{T}_{kj}^{-1} + \sum_{k=K+1}^{\infty} \mathbf{T}_{ik} \mathbf{T}_{kj}^{-1} = \mathbf{I}_{1} + \mathbf{I}_{2} = \mathbf{I} \quad .$$
(3.94)

As  $1_2$  never vanishes, no submatrix of  $(T.T^{-1})_{ij,1}$  exists which is a unit matrix as was the case for  $(T^{-1}.T)_{ij}$ . All elements of the matrix  $(T.T^{-1})_{ij} - I$  are thus influenced by both the error due to the truncation of the matrices and, for numerical reasons, by the error of the matrix elements. In **Table 3.8** we give the matrix  $(T.T^{-1})_{ij} - I$  for i = 0, 1, ..., 20; j = 0, 1, ..., 19; K = 20.

**Table 3.8:** The matrix  $(T.T^{-1})_{ij} - I$  for  $i = 0, 1, ..., 20; j = 0, 1, ..., 19; K = 20; <math>\gamma = 0.01, 0.1, 0.5$  and  $0.9; \epsilon_{me} \le 10^{-4}$ .

TABLE 3.8	
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	RIX  * -1 -	I GAMMA	= .010	EP2 = 1.000	DE-04 P.	IHAX = 140		-		
IJ	0	1	2	3	4	5	6	7	8	9
0 12334567890 1112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 112314567 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 11231457 1123147 1123147 1123147 1123147 1123147 11231457 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 1123147 11231	0. 92602 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9262 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9275 9	0. 254846311145 2572511145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 257251145 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HATE I J 0 12 34 45 67 89 10 111 123 134 15 16 17 18 19 20	IX         T+T-1 >           0         -           -3.8726E-08         -           -6.7116E-18         -           8.582E-11         -           -7.5081E-13         -           -2.2840E-13         -           -1.4192E-12         -           7.5081E-13         -           -2.2840E-13         -           -1.4192E-12         -           7.5081E-13         -           -2.2840E-13         -           -3.7002E-19         -           -3.7002E-19         -           -3.7002E-19         -           -2.2100E-21         -           -8.8541E-23         -           -8.8541E-23         -           -2.2100E-213         -           -3.7002E-19         -           -2.2100E-23         -           -3.86541E-23         -           -2.2102E-21         -           -3.7010E-23         -           -2.29234E-22         -	GAMMA           1           0.           2.8874E-06           3.5978E-07           -7.7576E-08           -8.724E-09           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 -4.3127E-08         -2.6249E-12           -6.2649E-12         -6.2649E-12           -6.21596E-13         -1.3786E-14           -3.5376E-13         -3.4444E-16           -5.977C-15         -2.9466E-16           -3.4444E-16         -6.7847E-16	H4X = 140 5 0. 1.8495E-10 4.9276E-09 7.4250E-08 7.4250E-08 4.5879E-07 9.3608E-06 4.5879E-07 1.1839E-08 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 8.1885E-09 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-2.923E-19           -1.0164E-18           -2.923E-19           1.0164E-18           -2.923E-19           1.0164E-18           -2.923E-19           11	100 2 0. 3.3730E-16 3.6159E-08 -7.5724E-16 3.4315E-08 3.4315E-08 3.4315E-08 3.4315E-08 3.4315E-08 3.4315E-08 -7.0282E-10 5.0630E-14 2.5983E-13 3.6055E-14 2.5983E-13 3.6055E-14 2.5983E-13 5.6756E-16 -7.0297E-17 9.3744E-18 -3.0977E-17 9.3744E-18 -1.2618E-19 3.1240E-19 -7.4256E-19 -7.4256E-19 12	EFS = 1.000 3 0. -1.5309E-09 2.8053E-08 -1.8737E-07 2.45518E-07 7.4379E-09 -7.1933E-09 0.4195E-10 4.9536E-12 4.4540E-13 3.7655E-14 1.1652E-14 1.1652E-14 1.1652E-14 -2.3013E-16 -9.9307E-18 -1.1474E-17 2.4520E-17 13	DE-04         PI           4         0.           1.5837E-18         7.0066E-12           1.2503E-15         1.2926E-06           -1.2326E-06         -3.237E-08           -3.6236E-06         -3.6236E-08           -3.6236E-08         -1.5770E-09           -3.6236E-08         -1.5770E-09           -1.570E-09         -1.5766E-13           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MAT!	RIX T=T-1 -	I GAMMA	= .500	EPS = 1.000	)E-04 P)	IMAX = 140				
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-3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -3.7549E-03 -	7 0. 1.5907E-02 -4.3742E-02 6.0612E-02 -2.1611E-02 -7.0482E-01 3.1631E-01 -7.075E-02 8.7579E-02 8.7579E-02 8.7579E-02 8.7579E-02 1.9901E-02 -7.0769E-02 4.3259E-03 5.7203E-02 4.3259E-03 5.7203E-02 4.3259E-03 5.7203E-02 4.3259E-03 5.7203E-02 4.3259E-03 5.7203E-02 4.3259E-03 5.7203E-02 4.2034E-02 -1.8729E-02	8 0. -1.1161E-02 3.5950E-02 -6.6845E-02 -1.5499E-02 -1.2462E-01 2.9207E-01 2.9207E-01 2.9725E-01 -3.7590E-02 -3.7590E-02 -7.6154E-02 7.6154E-02 7.6154E-02 7.6154E-02 -1.2214E-02 -2.8350E-02 2.2247E-02 18	9 0. -4.3903E-03 8.3534E-03 -1.0744E-03 -2.5155E-02 -3.0447E-02 -3.0447E-02 -3.0447E-02 -3.0447E-02 -3.0472E-02 8.7638E-01 -9.1425E-02 8.7110E-02 8.7110E-02 8.74978E-02 -7.4979E-02 6.4728E-02 -4.4263E-03 19

The influence of both the uncertainty due to the error in the matrix elements and that due to the truncation of the matrices is clearly reflected in **Table 3.8** for  $\gamma = 0.9$ , because the elements of the submatrix  $(T.T^{-1} - I)_{ij}$  (i = 0, 1, ..., 20; j = 0, 1, ..., 9) are about a thousand times higher than the corresponding values in **Table 3.7**, where only the uncertainty due to the error of the matrix elements is reflected.

# 3.6.4 Tables of the matrices $T_{fm}$ and $T_{mf}^{-1}$ .

For the sake of completeness we give here the matrices  $T_{\ell m}$  and  $T_{m\ell}^{-1}$  for some typical  $\gamma$ -values. The relative error  $\epsilon_{me}$  is the same for all elements:  $\epsilon_{me} \leq 10^{-4}$ .

Note that such tables have been published in extenso in [LA59] for  $\gamma = 0.01(0.01)0.99$ ;  $\ell$ , m = 0, 1, ..., 10. However, they are very inaccurate and should therefore be used with precaution.

HATE	UX T G	MMA = .010	EPS = 1	.000E-04	PIMAX = 14	10		TEMPS = .01	1 \$	
LH	0	1	2	3	4	5	6	7	8	9
0 1 2 3 4 5 6 7 8 9 10 1 12 3 4 5 16 7 8 9 10 1 12 3 4 5 6 7 8 9 10 1 12 3 4 5 6 7 8 9 10 112 13 4 5 16 7 8 9 10 112 13 4 5 16 7 8 9 10 112 11 112 11 112 11 112 11 112 11 112 11 11	1.0000E+00 6.6667E-03 2.0000E-05 0.5874E-10 0.3312E-15 0.4.1141E-20 0.7.9400E-25 0.7.9400E-25 0.34049E-34 0.3559E-39 0.6190E-43 0.6147E-48	0,9994E-01 1.2000F-02 6.8571E-05 1.9048E-07 0,1948E-07 1.9748E-17 0,748E-17 0,748E-17 0,4028E-22 0,4627E-27 0,4627E-27 0,4627E-27 0,3000E-31 0,7160E-36 0,58282E-41 0,2758E-45	0 -6.6661E-03 9.9984E-01 1.7142E-02 1.4285E-04 6.9264E-07 1.7483E-09 0.1519E-14 0.1519E-14 0.25388E-24 0.25388E-24 0.46944E-29 0.2588E-34 0.9053E-38 0.398E-43	0 5 9994E-05 -1 1998E-02 9 9969E-01 2 2219E-02 2 4240E-04 1.6316E-06 6 9619E-09 1.6126E-11 0.6126E-11 0.1847E-21 0.1847E-21 0.1847E-21 0.3605E-31 0.4662E-36 0.13051E-40	0. -5.7137E-07. 1.3712E-04. 9.9349E-01. 2.7266E-02. 3.6708E-04. 3.1326E-06. 3.8140E-08. 4.8140E-08. 4.8345E-11. 1.5004E-13. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24. 0.2941E-24.	0.55550E-09 -1.5236E-06 2.3304E-04 -2.2214E-02 9.9324E-01 3.2295E-02 5.3205E-06 3.8406E-08 1.9804E-10 6.9979E-13 1.4073E-15 0. -6.8153E-21 0. -1.135E-26 0. -1.0668E-30 0. 1.7748E-35	0. -5.4540E-11 1.6621E-08 3.6351E-04 -3.0296E-06 3.6351E-04 -2.7288E-02 9.8894E-01 3.7314E-02 9.8894E-01 3.7314E-02 -1.1506E-08 4.5482E-10 2.1342E-12 7.0063E-15 1.3289E-15 0.0035E-15 0.60095E-28 0.60095E-28 0.82399E-33	0.381E-13 -1.7899E-10 3.6705E-08 -5.2198E-06 -5.2198E-06 -5.2198E-06 -5.2198E-06 -5.2198E-06 -5.2198E-07 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E-02 -3.2285E	0.3328E-15 -5.3328E-15 1.9093E-12 6.9998E-08 6.9998E-08 6.8883E-04 -3.7300E-02 9.9819E-01 4.7326E-02 1.1159E-03 1.7253E-05 1.9432E-07 1.6751E-09 1.2933E-11 5.9631E-14 2.4132E-16 7.0222E-19 1.2039E-21 0. -4.5520E-27	0.2936E-17 -17-0216-14 -4.9401-12 -0216-14 -4.9401-12 -1.2156E-05 -8.8876E-04 -4.2305E-02 -9.9774-01 -1.3565E-03 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3436E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 -2.3456E-05 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9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9234E-01 9.9244E-01 9.9244E-01 9.9244E-01 9.9244E-01 9.9244E-0	0. -5.1423E-35 2.8392E-32 -1.0595E-29 -7.5353E-22 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 -2.7598E-20 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MATR	IX T G	MMA = .100	EPS = 1	.000E-04	PIMAX = 14	10		TEMPS = .0:	L7 S	<u> </u>
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MATF L M 0 1 2 3 4 5 5 6 7 8 9 10 11 11 12 13 14 15 16 17 18 19 20 L M	IIX         T         GJ           0         0         0           1.0000E+00         6.0000E-01         0           0.19669E-02         -         1.295E-03           -1.0809E-03         0         3.1529E-04           0.3.1529E-04         -         9.8033E-05           0.3.1786E-05         -         1.0614E-05           0.6228E-06         -         -           0.12573E-06         10         -	HHA = .900 1 0.51400E-01 7.7874E-01 5.5543E-01 1.9216E-01 0.215654 4.8125E-03 0. 1.2934E-03 0. 1.2934E-03 0. 3.8377E-04 0. 1.3275E-05 0. 4.5541E-06 11	EPS = 1 2 0. -1.8343E-01 6.8954E-02 5.7086E-01 5.0494E-01 0. -1.8647E-02 0. 4.0282E-03 0. -1.0717E-03 0. 3.1587E-04 0. -1.0806E-05 0. -1.0806E-05	1.000E-04 3 0. 1.2150E-01 7.6828E-02 -1.9168E-01 1.5090E-01 6.1779E-01 1.5090E-01 4.5677E-01 1.4719E-01 0. -1.5465E-02 0. 3.2464E-03 0. -2.4630E-04 0. 2.4630E-04 0. 2.4676E-05 13	PIMAX = 14 4 0.4486E-02 8.0734E-02 1.0213E-01 -1.4303E-01 -2.3220E-01 6.5157E-01 1.2799E-01 0.26057E-03 0.26057E-03 0.26057E-03 0.26057E-03 0.26057E-03 0.56544E-04 0.19035E-04 0.5.8261E-05 14	5 0. 7.8339E-02 -5.5542E-02 1.2991E-02 -1.2991E-02 1.2991E-02 1.2991E-02 1.2991E-01 5.2477E-02 1.31015E-01 6.5376E-01 3.1015E-01 6.5376E-01 3.1015E-01 0. -1.0631E-02 0. 0. -2.0962E-03 0. -5.2338E-04 0. 1.4717E-04 15	6 0. -6.6994E-02 2.4995E-02 -1.1407E-04 1.4932E-01 -8.0413E-03 3.7925E-02 3.7925E-02 3.7925E-01 6.8453E-02 3.7925E-03 0.4535E-04 9.7167E-02 0.1672-01 1.6925E-03 0. -4.1305E-04 16	TEMPS = .11 7 0. 5.8266E-02 7.9779E-02 -3.0430E-03 9.7119E-02 -3.8566E-02 -3.8566E-02 -3.8566E-02 1.4335E-01 -6.9518E-02 .4335E-01 -5.9656E-03 .43944E-01 6.8679E-01 3.0202E-01 3.6202E-01 3.0202E-01 3.0202E-01 1.3720E-03 1.3720E-03 17	80 5 8 0. -5.1186E-02 7.7200E-02 -1.3351E-02 5.8045E-02 5.8045E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -8.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.057E-02 -9.	9 0.5253E-02 7.4058E-02 2.5758E-02 2.5758E-02 4.3552E-02 6.3562E-02 6.3562E-02 6.3562E-02 6.3562E-02 1.45559E-02 2.8068E-02 -1.1355-01 1.2619E-01 5.3268E-02 -1.7353E-01 6.5049E-02 19

MAT	RIX T GA	MMA = 1.0								
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0 1 2 3 4 5 6 7 8 9 10 11 12 13 4 5 6 7 8 9 10 11 2 13 14 5 6 7 8 9 10 11 2 3 4 5 6 7 8 9 10 11 2 3 4 5 6 7 8 9 10 11 2 11 2 3 4 5 6 7 8 9 10 11 11 2 3 4 5 6 7 8 9 10 11 11 11 11 11 11 11 11 11 11 11 11	1.0000E+00 6.6667E-01 2.5000E-01 0.15625E-02 0.5573E-03 0.5573E-03 0.5573E-03 0.29297E-03 0.0142E-03 0.14547E-03 0.4547E-03 0.4547E-03 0.4547E-03 0.4547E-03 0.4547E-03 0.4547E-03	0.0000E-01 7.5000E-01 6.8571E-01 0.1250E-01 0.5250E-02 0.5215E-02 0.5215E-03 0.5215E-03 0.5215E-03 0.5554E-03 0.5554E-03 0.5554E-03 0.3.3920E-03 0.2.6035E-03	0 	0. 4.4444E-02 9.6970E-02 9.7296E-01 9.3296E-01 9.33916E-01 0.33916E-01 0.35916E-02 0.5970E-02 0.5909E-02 0.5965E-03 0.5965E-03 0.5965E-03 0.5965E-03 0.5965E-03 0.5965E-03	0. -2.5974E-02 0.7952E-02 0.5904E-02 0.6857E-01 0.33915E-01 0.33915E-01 0.79882E-02 0.7686E-02 0.22196E-02 0.4688E-02 0.4688E-02 01.0437E-02	0. 1.7094E-02 2.9304E-02 4.8265E-02 5.4837E-02 5.6580E-01 3.6580E-01 3.979E-01 5.4172E-01 5.4172E-01 5.4172E-02 5.8755E-02 0.23082E-02 0.5413E-02	0. -1.2121E-02 0.9964E-02 6.0022E-02 4.8035E-02 4.395E-02 5.6389E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7.450E-01 7	0, 9.0498E-03 1.4549E-02 2.0784E-02 3.0122E-02 9.3306E-02 9.3306E-02 9.3306E-02 9.3306E-01 7.1344E-01 7.0161E-01 3.4483E-01 8.3224E-02 4.0152E-02	0. 7.0175E-02 0.1195E-02 0.1056E-02 0.1029E-02 0.1029E-02 0.7404E-02 0.7404E-02 0.6144E-01 7.0222E-01 3.4584E-01 0.83826E-02	0.6022E-03 5.6022E-03 0.8787E-03 0.1872E-02 0.1072E-02 0.1072E-02 0.1072E-02 0.1072E-02 0.7128E-02 0.233E-02 0.233E-02 0.233E-02 0.233E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-02 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.202E-01 0.
LH	10	11	12	13	14	15	16	17	18	19
0 1 2 3 4 5 6 7 8 9 10 112 13 4 5 6 7 8 9 10 112 13 4 5 16 7 12 3 4 5 6 7 8 9 10 112 13 4 5 6 7 8 9 10 112 13 4 5 6 7 8 9 10 112 13 4 5 6 7 8 9 10 112 112 112 115 115 115 115 115 115 115	0. -4.5767E-03 0. 7.1073E-03 0. -9.4764E-03 0. 1.2199E-02 0. 1.5777E-02 0. 2.1036E-02 0. -2.9765E-02 0. 4.6889E-02 0. -9.1974E-02 0. 3.5992E-01 7.1154E-01	0.8095E-03 0.814E-03 0.7543E-03 0.7543E-03 0.2343E-02 0.2343E-02 0.2343E-02 0.25798E-02 0.25798E-02 0.25798E-02 0.25970E-02 0.46682E-02 0.46682E-02 0.1674E-02	0.2206E-03 4.9499E-03 6.4710E-03 0.743E-03 0.743E-03 0.2399E-02 7.5780E-02 0.2993E-02 7.9500E-02 4.6502E-02 0.4502E-02	0. 2.7586E-03 4.2250E-03 5.4870E-03 6.7769E-03 6.7769E-03 0. 2.422E-03 0. 1.2411E-02 0. 1.2411E-02 0. 2.0816E-02 0. 2.9385E-02	0.2.3895E-03 0.4.494E-03 0.7147E-03 0.7766E-03 0.766E-03 0.312E-03 0.312E-03 0.12400E-02 0.12400E-02 0.15698E-02 0.2.0741E-02 0.2.0741E-02	0.20899E-03 2.0899E-03 0.40969E-03 0.40969E-03 0.40969E-03 0.409875E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03 0.4018E-03	0. -1.8433E-03 0.036E-03 -3.5944E-03 0.4.3530E-03 0.4.3530E-03 0.4.242E-03 0.0423E-03 0.0423E-03 0.33964E-03 0.33964E-03 0.2349E-02 1.2349E-02	0. 1.6380E-03 2.4875E-03 3.1800E-03 3.8346E-03 4.5095E-03 5.2495E-03 6.1015E-03 6.1015E-03 0. 7.1242E-03 8.4012E-03 0. 1.0061E-02	0. -1.4652E-03 0. 2.2222E-03 0. -2.8340E-03 0. -3.9847E-03 0. -3.9847E-03 0. -3.91947E-03 0. -3.119E-03 0. -3.1319E-03 0. -3.1373E-03 0. -3.373E-03 0. -3.3968E-03	0.3184E-03 0.973E-03 0.5420E-03 0.6451E-03 0.6451E-03 0.6451E-03 0.6421E-03 0.6726E-03 0.6726E-03 0.61553E-03 0.7,1406E-03

HATE	RIX T-1	GAMMA = .0	10 EPS -	= 1.000E-04	PINAX =	140		TEMPS = .	010 S	
ML	0	11	2	3	4	5	6	77	8	9
0 12 3 4 5 6 7 8 9 0 11 12 3 4 5 6 7 8 9 0 11 12 3 4 5 6 7 8 9 0 11 12 3 4 5 6 7 8 9 0 11 12 3 4 5 6 7 8 9 0 11 12 3 4 5 6 7 8 9 0 11 12 3 4 5 6 7 8 9 0 11 12 3 4 5 6 7 8 9 0 11 12 3 4 5 6 7 8 9 0 11 12 3 4 5 8 9 0 11 12 12 1 12 1 1 12 1 12 1 12 1 1 12 1 1 12 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.0005-0005-0005-0005-0005-0005-0005-000	0. 9.9998E-01 -1.2704E-02 -1.2714E-02 -1.27238E-08 -1.77021E-02 -2.2238E-08 -1.79021E-02 -2.2218E-14 -2.2228E-14 -2.2228E-14 -2.2228E-14 -2.2228E-14 -2.2228E-14 -2.2228E-14 -2.228E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 -2.4195E-22 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ſ	NL	10	11	12	13	14	15	16	17	18	19
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#### The following general comments can be made about these tables:

- $T_{\mu}(\gamma) = 0$  for  $\ell$ -odd,  $m = 0, 1, 2, ..., (\ell-3)/2; \gamma \in [0,1].$
- $T_{\ell_m}(\gamma=1) = 0$  for  $\ell$ -even,  $m \ge \ell/2+1$  and for  $\ell$ -odd,  $m \le (\ell-3)/2$ .
- $T_{m\ell}^{-1}(\gamma) = 0$  for  $\ell$ -even,  $m = 0, 1, 2, ..., \ell/2-1; \gamma \in [0, 1^-].$
- $|T_{\eta}(\gamma)| \leq 1; \gamma \in [0,1].$
- $\left|\mathbb{T}_{m\ell}^{-1}(\gamma)\right| \leq 1; \gamma \in [0,1^{-}].$

#### 3.7 APPLICATIONS IN PHYSICS.

The present numerical analysis of the Taylor series expansion method for transforming angular distribution cross sections from the laboratory to the center-or-mass frame of reference and the inverse has essentially been performed with a view to application in physics. The **applicability** of the method can be judged by the **following criteria**:

- 1. Can it be applied to a large variety of physical cases ?
- 2. Does it permit an accuracy control of the transformation ?
- 3. Is the computing time reasonable ?

The first of these criteria concerns **physics** which is mainly characterized by the variable  $\gamma$ . We have seen above that the transformation from the center-of-mass to the laboratory system can be carried out by means of the present method for all  $\gamma \in [0,1]$ , and the inverse transformation can be performed for all  $\gamma \in [0,1^-]$ . This covers a large variety of physical cases; in particular it covers all but exotic cases of the Evaluated Neutron Data Files.

Let us now have a look at the **second criterion**. In fact our efforts were focused on the error analysis. The **main accuracy-control of the transformation is twofold**. Firstly, we control the accuracy of the elements of the transformation matrix; secondly, we control the accuracy of the transformed angular distributions which depend mainly on the size of the transformation matrix. The former has already been described in Subsection 3.3.3, the latter is carried out in the following way.

Using the so-called kinematic equation:

$$\frac{d\sigma}{d\omega}(\mu, E) = \frac{(1+2\gamma\overline{\mu}+\gamma^2)^{3/2}}{|1+\gamma\overline{\mu}|} \frac{d\overline{\sigma}}{d\overline{\omega}}(\overline{\mu}, \overline{E}) , \qquad (3.95)$$

an exact point-by-point transformation from one reference system to the other can be made (in our case 101 angles of equidistant cosine between -1 and +1). It can be used to check the transformation which has been performed with the aid of the transformation matrix. The number of rows of this matrix is increased until the required accuracy is reached. We define the transformation accuracy  $\epsilon_{tr}$ 

$$(\sigma_{k} - \sigma_{tr}) / \sigma_{k} = \epsilon_{tr}$$

where  $\sigma_k$  denotes the cross-section obtained by means of the kinematic formula, and  $\sigma_{tr}$  denotes the cross-section obtained by means of the transformation matrix. This generally results in a rectangular transformation matrix.

In addition to these accuracy checks we test, prior to and after the transformation, whether there are any angular distributions which have negative values. For this test we use a program based on the **algorithm by IRVING** et al.[IR66]. Such a test prior to the transformation is necessary, as there seem to be Legendre fits in the literature and hence in data files which show up this deficiency.

Finally, the quality of the transformation is checked by the inversion of the transformation. In **Table 3.10a** we demonstrate these transformation procedures for isotropic angular distributions and several values of  $\gamma$ .

**Table 3.10a:** Transformation procedures for isotropic angular distributions and  $\gamma = 0.01$ , 0.1, 0.5 and 0.9. Error limit of matrix elements:  $|\epsilon_{\rm me}| = 10^{-4}$  (rel-tive error); error limit of transformed cross section:  $|\epsilon_{\rm tr}| = 10^{-2}$ .

TRANSFORMATION: CENTER OF MASS ----> LABORATORY

GAMMA = .010

ERROR LIMIT = 1.000E-02

LEGENDRE COEF. A(M) = A IN CH SYSTEM

м	<b>А</b> (М)
0	1.00000E+00

	ACCURACY CHECK ANALYSIS OF THE TRANSFORMATION IN DEPENDENCE OF THE SIZE OF THE MATRIX T										
L	MAX.DEVIAT	ION AT MU	NB.POINTS ABOVE ERROR LIMIT	NEGAT FROM MU1	TO MU2	PROB.					
0	0 2.03 -1.000 51										

RESUL	TS	
M/L	Ā	A = T * A  A = T  -1  -1  -1  -1  -1  -1  -1
0 1	1.00000E+00 0.	1.00000E+00 1.00000E+00 6.66667E-03 -1.33333E-07

TRANSFORMATION: LABORATORY ---> CENTER OF MASS

GAMMA = .010 ERROR LIMIT = 1.000E-02

L	A(L)
0	1.00000E+00

	ACCURACY CHECK ANALYSIS OF THE TRANSFORMATION IN DEPENDENCE OF THE SIZE OF THE MATRIX T++(-1)										
м	M MAX.DEVIATION AT HU NB.POINTS ABOVE ERROR LIMIT FROM MU1 TO MU2 PROB.										
0	2.01	1.000	51								

RESUL	rs		
L/M	A	$\bar{A} = T^{-1} * A$	$\Lambda = T * \{T^{-1} \\ * A\}$
0 1	1.000COE+00 0.	1.00000E+00 -6.66667E-03	1.00000E+00 4.00000E-07

GANMA = .100

ERROR LIMIT = 1.000E-02

LEGENDRE COEF.  $\widetilde{A}(K) = \widetilde{A}$  IN CH SYSTEM

н	Ā(M)
0	1.00000E+00

		ACCURACY CH IN DEPEND	ECK ANALYSIS OF THE ENCE OF THE SIZE OF	TRANSFORMAT THE MATRIX	TON	
L	MAX.DEVIA	TION AT MU	NB.POINTS ABOVE ERROR LIMIT	NEGAT FROM MU1	IVE PROBABI	PROB.
0 1	23.46 1.23	-1.000 -1.000	96 3			

RESUL	TS		
H/L	Ā	A = T*A	1 - A ≠ T ≠(T*A)
0 1 2	1.00000E+00 0. 0.	1.00000E+00 6.66657E-02 2.00287E-03	1.00000E+00 1.9111JE-07 -2.73333E-08

TRANSFORMATION: LABORATORY ---> CENTER OF MASS

GANNA - .100

ERROR LIMIT = 1.000E-02

L	A(L)	
0	1.00000E+00	

	ACCURACY CHECK ANALYSIS OF THE TRANSFORMATION IN DEPENDENCE OF THE SIZE OF THE MATRIX $T\text{w}\text{=}(-1)$					
M	MAX.DEVIAT	ION AT HU	NB.POINTS ABOVE ERROR LIMIT	NEGAT	TO HU2	PROB.
0 1	21.00 3.20	1.000 1.000	96 59			

RESULT	rs		
L/M	A	$\overline{A} = \overline{T} = \overline{A}$	A = T = (T = A)
0 1 2	1.00000E+00 0. 0.	1.00000E+00 -6.66667E-02 6.00000E-03	1.00000E+00 3.42857E-06 -6.83048E-05

TRANSFORMATION: CENTER OF MASS -> LABORATORY

GANNA = .500 ERROR LINIT = 1.000E-02

LEGENDRE COEF.  $\overline{A}(M) = \overline{A}$  IN CH SYSTEM

M	Ã(H)
0	1.00000E+00

	ACCURACY CHECK ANALYSIS OF THE TRANSFORMATION IN DEPENDENCE OF THE SIZE OF THE MATRIX T							
L	MAX.DEVIA	TION AT HU	NB.POINTS ABOVE ERROR LIMIT	NEGAT FROM MU1	IVE PROBABI TO MU2	LITY PROB.		
0 1 2 3	300.00 100.00 3.91 3.91	-1.000 -1.000 -1.000 -1.000	100 95 5 5					

RESULTS					
M/L	Ā	A = T#A	$\bar{A} = T^{-1} + (T + \bar{A})$		
0 1 2 3	1.00000E+00 0. 0. 0.	1.00000E+00 3.33333E-01 5.19537E-02 0. -1.25050E-03	1.00000E+00 6.39551E-06 -1.35573E-06 -2.99655E-06 -2.14909E-05		

TRANSFORMATION: LABORATORY ---> CENTER OF MASS

GANMA = .500

ERROR LIMIT = 1.000E-02

L	A(L)
0	1.00000E+00

	ACCURACY CHECK ANALYSIS OF THE TRANSFORMATION IN DEPENDENCE OF THE SIZE OF THE MATRIX T++(-1)					
M	HAX.DEVIAT	ION AT HU	NB.POINTS ABOVE ERROR LIMIT	NEGAT FROM MU1	TVE PROBABI	PROB.
0123456789	125.00 100.00 68.75 43.75 26.56 15.62 8.98 5.08 2.83 1.56	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	100 100 99 97 92 84 69 25 3 1			

RESULT	S	
L/M	•	$\tilde{A} = T + A  A = T + (T + A)$
01234567890	1.00000E+0 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	0 1.0000E+00 1.0000E+00 -3.33333E-01 1.30316E-07 -7.14286E-02 4.58300E-06 -7.14286E-02 4.58300E-06 -7.14286E-02 4.17314E-05 -1.70455E-02 4.17314E-05 -1.16467E-03 1.08222E-04 -4.16667E-03 1.08222E-04 -4.16667E-03 -2.64870E-05 5.11533E-04 8.9537FE-05

# TRANSFORMATION: CENTER OF MASS -> LABORATORY

GANNA = .900

ERROR LIMIT = 1.000E-02

H	Ā(H)
0	1.00000E+00

	ACCURACY CHECK ANALYSIS OF THE TRANSFORMATION IN DEPENDENCE OF THE SIZE OF THE MATRIX T					
L	MAX.DEVIA	TION AT HU	NB.POINTS ABOVE ERROR LIMIT	NEGA" FROM HUI	TIVE PROBAB	ILITY PROB.
0 1	9900.00 8100.00	-1.000 -1.000	101 98	-E ##45-01	-1.0005+00	8 8865-02
2	1368.58	-1.000	83	-4.582E-01	MEG.PROB.	5.117E-03
3	1368.58	-1.000	83	TOTAL	NEG. PROB. 4	5.117E-03
*	401.66	-1.000	27	TOTAL	NEG. PROB	= 5.117E-03
5	401.66	-1.000	27	TOTAL	NEG.PROB1.000E+00	3.492E-04 3.492E-04
678910 11112 131415 1617	135.17 135.17 48.58 48.58 17.63 6.88 6.88 2.34 2.34 1.17 1.17	-1.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000	772211111111111111111111111111111111111	TOTAL	NEG. <b>PROB</b> .	<b>- 3.492</b> E-04

RESULT	S	
M/L	Ā	$A = T * \overline{A} = T^{-1} * (T * \overline{A})$
0 1234567 890 111 12345 167 18	1.00000E+00 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	1.00000E+00 1.00000E+00 6.00000E+01 1.529195-05 0.83972E+01 -1.26164E+05 0.12950E+02 -1.21638E+05 0.12950E+03 -1.217912E+05 0.12950E+03 -1.09730E+05 0.3822460E+05 -1.08091E+03 -8.22460E+06 0.315288E+04 -6.95069E+06 0.315288E+04 -6.95069E+06 0.317858E+05 -5.46392E+06 0.317858E+05 -5.46392E+06 0.317858E+05 -5.46392E+06 0.317858E+05 -5.46392E+06 0.317858E+05 -5.46392E+06 0.317858E+05 -5.46392E+06 0.317858E+05 -5.46392E+06 0.317858E+05 -5.46392E+06 0.362275E+06 -4.52970E+06

TRANSFORMATION: LABORATORY -> CENTER OF MASS

GAMMA = .900 ERROR LINIT = 1.000E-02

L	A(L)
0	1.00000E+00

	ACCURACY CHECK ANALYSIS OF THE TRANSFORMATION IN DEPENDENCE OF THE SIZE OF THE MATRIX TOP(-1)					
				NEGATIVE PROBABILITY		
M	MAX.DEVIAT	TON AT MU	ERROR LINIT	FROM MU1 TO MU2 PROB.		
0 1	261.00 388.80	1.000	101 101			
				1.000E+00 5.556E-01 8.889E-02 TOTAL NEG.PROB. = 8.889E-02		
2	488.43	1.000	101	5.933E-01 -9.943E-02 1.010E-01		
3	564.25	1.000	100	1.000E+00 8.677E-01 3.929E-02		
				7.651E-02 -4.442E-01 9.022E-02 TOTAL NEG.PROB. = 3.929E-02		
4	620.01	1.000	101	8.5498-01 5.2888-01 5.1698-02		
5	658.99	1.000	101	TOTAL NEG.PROB 5.169E-02		
_				1.000E+00 9.381E-01 2.174E-02 5.473E-01 2.135E-01 4.405E-02		
4	683 86	1 000	100	TOTAL NEG.PROB. = 2.174E-02		
v	003.70	1.000	100	9.266E-01 7.463E-01 3.073E-02 2.620E-01 -3.237E-02 3.687E-02		
-	<i></i>			-5.893E-01 -7.938E-01 5.654E-02 TOTAL NEG.PROB. = 3.073E-02		
	697.36	1.000	100	1.000E+00 2.645E-01 1.322E-02		
				3.109E-02 -2.170E-01 3.057E-02 -4.15E-01 -8.257E-01 -5.257E-02		
8	701.23	1.000	101	TOTAL NEG. PROB 1.322E-02		
				9.556E-01 8.435E-01 1.922E-02 5.253E-01 3.206E-01 2.067E-02		
				-1.500E-01 -3.557E-01 2.496E-02 -7.473E-01 -8.652E-01 3.467E-02 TOTAL NEC DEDE = 1.922E-02		
9	697.36	1.000	100	1.000E+00 9.772E-01 8.460E-03		
				8.282E-01 6.876E-01 1.594E-02 3.250E-01 1.632E-01 1.611E-02		
				-7.968-01 -4.610-01 1.992-02 -7.960-01 -8.859E-01 2.510E-02		
10	687.25	1.000	101	9.700E-01 8.947E-01 1.232E-02		
				6.708E-01 5.274E-01 1.216E-02 1.547E-01 -5.897E-03 1.223E-02		
				-4.039E-01 - 5.421E-01 1.539E-02 -8.332E-01 -9.010E-01 1.673E-02		
11	672.18	1.000	101	1.000E+00 9.843E-01 5.585E-03		
				8.786E-01 7.807E-01 9.927E-03 5.103E-01 3.767E-01 8.812E-03		
				6.202E-03 -1.299E-01 8.953E-03 -4.935E-01 -6.054E-01 1.137E-02		
12	<u> </u>	1 000	99	TOTAL NEG.PROB. = 5.585E-03		
	0,3.20	1.000	,,	9.782E-01 9.249E-01 7.979E-03 7.581E-01 6.559E-01 7.138E-03		
				3.583E-01 2.407E-01 6.030E-03 -1.202E-01 -2.327E-01 6.200E-03		
				-5.662E-01 -6.554E-01 7.864E-03 -8.866E-01 -9.199E-01 4.226E-03		
13	631.40	1.000	100	1.000E+00 9.886E-01 3.758E-03		
				9.092E-01 8.389E-01 6.137E-03 6.274E-01 5.318E-01 4.685E-03		
				2.193E-01 1.207E-01 3.784E-03 -2.279E-01 -3.180E-01 3.926E-03		
				-9.081E-01 -9.239E-01 6.261E-04 TOTAL NEG.PROR. = 3.758E-03		
14	607.38	1.000	100	9.833E-01 9.442E-01 5.17DE-03		
				8.139E-01 7.405E-01 4.047E-03 4.967E-01 4.145E-01 2.708E-03		
				9.3031-02 1.625E-02 2.035E-03 -3.204E-01 -3.887E-01 2.112E-03 -5.766E-01 -7.268E-01 2.412E-03		
				TOTAL NEG.PROB. = 5.170E-03		

ACCURACY CHECK ANALYSIS OF THE TRANSFORMATION IN DEPENDENCE OF THE SIZE OF THE MATRIX T						
			NEGATIVE PROBABILITY			
L	MAA.DEVIAI	TOH AT HU	ERROR LIMIT	FROM MU1	TO MU2	PROB.
15	581.85	1.000	99	1.000E+00 9.290E-01 7.059E-01 3.707E-01 1.932E-02 -4.010E-01 -7.205E-01	9.915E-01 8.776E-01 6.390E-01 3.070E-01 -7.319E-02 -4.467E-01 -7.513E-01	2.558E-03 3.699E-03 2.263E-03 1.224E-03 7.668E-04 7.725E-04 7.414E-04
16	555.35	1.000	100	9.866E-01 8.515E-01 5.928E-01 2.499E-01 -1.257E-01 -4.767E-01 TOTAL	9.572E-01 7.991E-01 5.404E-01 2.124E-01 -1.450E-01 NEG.PROB.	2.998E-03 2.125E-03 9.208E-04 2.560E-04 4.014E-05 1.928E-05 3.316E-03
17	528.33	1.000	101	1.000E+00 9.425E-01 7,601E-01 4.765E-01 TOTAL	9.935E-01 9.046E-01 7.163E-01 4.505E-01 NEG.PR08.	1.751E-03 2.122E-03 8.672E-04 1.026E-04 1.751E-03
18	501.17	1.000	99	9.889E-01 8.775E-01 6.587E-01 TOTAL	9.665E-01 8.415E-01 6.367E-01 NEG.PROB.	2.081E-03 9.520E-04 8.808E-05 2.081E-03
19	4/4.15	1.000	99	1.000E+00 9.519E-01 7.975E-01 TOTAL	9.949E-01 9.244E-01 7.752E-01 NEG.PROB.	1.199E-03 1.111E-03 1.496E-04 1.199E-03
20	447.52	1.000	100	9.905E-01 8.957E-01 TOTAL	9.734E-01 8.738E-01 NEG.PROB.	1.255E-03 2.838E-04 1.255E-03

RESULT	rs		
L/M	A	$\ddot{A} = T^{-1} * A$	$A = T*(T^{-1}*A)$
01234567890112345678910112345678910112345678910112345678910112345678910112345678910112345678910011234567891001123456789100112345678910011234567891001123456789100112345678910011234567891001123456789100112345678910011234567891001123456789100112345678910011234567891001123456789100112345678910011234567891000000000000000000000000000000000000	1.00000E+00 D. O. O. D. D. D. D. D. D. D. D. D. D. D. D. D.	1.000000000000000000000000000000000000	1.000000000000000000000000000000000000

**Table 3.10b:** The dimension of the transformation matrices in dependence on  $\gamma$  supposing that only  $a_0 = 1 = \bar{a}_0$  exists (isotropic angular distributuion) in the original frame of reference. Therefore, only the submatrices  $T_{\ell,m=0}$  and  $T_{m,\ell=0}^{-1}$  operate in the transformations  $a = T.\bar{a}$  and  $\bar{a} = T^{-1}.a$ , respectively.  $\epsilon_m \leq 10^{-4}$ ;  $\epsilon_{tr} \leq 10^{-2}$ .

γ	0.001	0.05	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
a	0	1	2	2	2	4	4	6	6	10	18
ā	0	1	2	3	5	7	10	15	19	> 19	> 19

We emphasize once more that the dimension of the transformation matrix is mainly dictated by the accuracy  $\epsilon_{+r}$ .

From these tables we can formulate the following conclusions:

- A quadratic transformation matrix is not sufficient even for very small γ, say γ > 0.02.
- The size of the transformation matrix increases with increasing γ.
- One needs a larger matrix for the transformation from the laboratory to the center-of-mass system than for the inverse transformation and this difference is enhanced with increasing γ.
- The transformation becomes more and more laborious as γ is increasing.
- For the extreme case  $\gamma = 1^-$  (elastic scattering of identical particles), the transformation via transformation matrices is defined and numerically possible, but is generally not recommended as the size of the transformation matrix becomes rather large (see **Figure 15** on page 128 and Subsection 3.8.4 (Outlook)).

To demonstrate once more the importance of the size of the transformation matrix T(L,M), we illustrate by **Figure 16** on page 129 the scattering probabilities in the laboratory system resulting from the transformation using the L-values: L = 4 = M, L = 5 and 10.

This figure renders apparent that for L = 4 there are negative scattering probabilities and at least L = 10 is required to reach an accuracy of  $\epsilon_{++} = 1$ %.

The **third important criterion** for the applicability of the present method is the **computing time**. It depends on the variable  $\gamma$ , on the accuracies imposed and on the angular distribution considered. The **total computing time**  $\tau$  can be decomposed as follows

$$\tau(\gamma, \epsilon_{\text{me}}, \epsilon_{\text{tr}}, p) = \tau_0 + \tau_1 + \tau_2$$
(3.96)



Figure 15. Influence of the size of the transformation matrix: demonstration of the influence of the size of the transformation matrix on the transformed angular distribution and the requirement of relatively large transformation matrices for the extreme case  $\gamma = 1^-$ . Transformation of an isotropic angular distribution from the center-of-mass to the laboratory system.



matrices: Transformation of the angular distribution ( $\bar{a}_0 = 1$ ,  $\bar{a}_1 = 0.2$ ,  $\bar{a}_2 = 0.125$ ,  $\bar{a}_3 = 0.125$ ,  $\bar{a}_4 = 0.05$ ;  $\gamma = 0.5$ ) to the laboratory system using transformation matrices T(L = 4, 5, 10, M = 4).

where  $\gamma$  is the well known variable,  $\epsilon_{me}$  and  $\epsilon_{tr}$  are the relative errors of the matrix elements and the <u>transformed</u> function respectively (for definition see above), p indicates the angular distribution considered;

- $\tau_{o}$  denotes the computing time needed for the calculation of the Taylor series coefficients,
- $\tau_1$  indicates the computing time for the calculation and the accuracy check of the transformation matrix elements,
- τ₂ denotes the computing time of the transformation procedure, i.e., transformation, negative probability check, accuracy check and inverse transformation.

Values of these computing times are given in **Table 3.11** for some typical values of  $\gamma$ .

Transformation from the center-of-mass to the laboratory system					
γ	$\tau_1(sec)$ $\tau_2(sec)$ $\tau(sec)$				
0.1	< 0.001	0.020	~ 0.02		
0.2	< 0.001	0.020	~ 0.02		
0.3	< 0.001	0.021	~ 0.02		
0.4	~ 0.002	0.025	~ 0.03		
0.5	~ 0.002	0.025	~ 0.03		
0.6	~ 0.003	0.031	~ 0.03		
0.7	~ 0.004	0.031	~ 0.03		
0.8	~ 0.02	0.045	~ 0.07		
0.9	~ 0.10	0.090	~ 0.20		

Table 3.11: Computing times. Computer: CDC-7600.

Transformation from the laboratory to the center-of-mass system						
γ	$\tau_1(sec)$	$\tau_2(sec)$	$\tau(sec)$			
0.1	< 0.001	0.020	~ 0.02			
0.2	< 0.001	0.023	~ 0.02			
0.3	~ 0.002	0.028	~ 0.03			
0.4	~ 0.002	0.033	~ 0.04			
0.5	~ 0.005	0.042	~ 0.05			
0.6	~ 0.01	0.067	~ 0.08			
0.7	~ 0.04	0.095	~ 0.14			
0.8	~ 0.08	0.108	~ 0.20			
0.9	~ 0.20	~ 0.5	~ 0.70			

### Concerning the computing time the following can be concluded:

•  $r_{o}$  is predominant, but small. Note that for a sequence of transformations the Taylor series coefficients  $b_{\ell m}^{r}$  and  $q_{m,\ell}^{r}$  have only to be calculated once and then kept on permanent file. Total computation time is, therefore, practically not affected.

- $\tau_1$  is very small.
- τ₂ is also small despite the multiple accuracy checks.
- The total computing time (CDC-7600) amounts to:
  - $\tau \leq 0.05$  seconds for  $\gamma \in [0, 0.5]$ ,
  - $\tau \leq 0.2$  seconds for  $\gamma \in [0.5, 0.8]$ ,
  - $-\tau \sim 1$  second for  $\gamma = 0.9$ .
- The transformation method investigated here, taken as a whole, is a surprisingly economical tool.

3.8 BRIEF ACCOUNT AND CONCLUDING REMARKS ON THE TAYLOR SERIES EXPANSION METH-OD.

#### 3.8.1 Numerical analysis.

The representation of the functions  $T_{\ell m}(\gamma)$  and  $T_{m\ell}^{-1}(\gamma)$  by means of the Taylor series permits separation of the computation into a constant part, i.e., the coefficients  $b_{\ell m}^{r}$  and  $q_{m\ell}^{r}$ , and a variable dependent part, i.e., the summation of the series. This results obviously in saving computing time.

It came to light that all elements  $T_{\chi m}(\gamma)$  for *i*-odd and  $T_{m\ell}^{-1}(\gamma)$  for *i*-even are polynomials. They can thus be calculated exactly. For all other indices, these functions are represented by infinite series which have to be cut off for numerical computation. We are able to give a close-knit estimate of the remainder. Surprisingly, we could not find any publication where the remainder in question had been treated. It is not crucial as long as the variable  $\gamma$  remains very small, because a Taylor series generally converges very fast in the vicinity of the point of expansion.

We could further show that the **Taylor series are convergent for**  $\gamma \in [0,1]$  for the functions  $T_{\ell m}(\gamma)$ , and for  $\gamma \in [0,1-\epsilon]$ ,  $\epsilon$  positive and arbitrarily small, for  $T_{m\ell}^{-1}(\gamma)$ . For  $\gamma = 1$ ,  $T_{m\ell}^{-1}(\gamma)$  show up discontinuities. This is, as far as we know,

also a new result. Physically,  $\gamma = 1$  comprises, among other nuclear reactions, elastic scattering of identical particles, i.e., proton-proton reactions etc.. For the two boundary cases  $T_{\ell m}(\gamma=1)$  and  $T_{m\ell}^{-1}(\gamma=1^{-})$  simple sum-free formulae were derived, which naturally permit a very fast and exact computation of these functions.

It results that for a given accuracy of the transformation, the matrix  $T_{\ell m}$  as well as the matrix  $T_{m\ell}^{-1}$  are not in general quadratic, but rectangular and the matrix  $T_{m\ell}^{-1}$ usually contains more rows than the matrix  $T_{\ell m}$ . The more  $\gamma$  increases, the more this becomes apparent.

We are thus able to keep the computation of the transformation matrices as well as the transformation itself under accuracy-control. A natural application of this accuracy-controllable transformation procedure is a verification of the transformation matrices which are given in the Evaluated Neutron Data File. **ENDF.** Such a verification has been carried out in our laboratory for all nuclei with A < 60. We did not verify beyond this A-limit as  $\gamma$  becomes sufficiently small for such A-values to guarantee a satisfactory accuracy of the transformation matrices even if one applies, for their computation, a low order approximation as that which seems to have been used for the calculation of the transformation matrices given in **ENDF.** The results of this systematic verification are presented in **Annex-1.** Here we just give an example which demonstrates the importance of such a check.

**Example:** Verification of the transformation matrix for  $T(\gamma=0.5)$  given in **ENDF/B4** (elastic scattering of neutrons by deuterium).

1. Comparison of the matrix as given in **ENDF/B4** with the matrix computed by means of the Taylor series expansion method, **Figure 17** on page 133.

From this graph one can directly see that deviations become considerable when  $\ell$ , m increase.

2. Graphical comparison, **Figure 18** on page 134, of the angular distributions in the laboratory system as obtained using the transformation matrix given in **ENDF/B4** (--- line) and with the aid of the corresponding matrix calculated by us (--- line),  $\gamma = 0.5$  (elastic scattering of 20 MeV neutrons by deuterium).



Figure 17. Comparison of T matrices: Comparison of the transformation matrix  $T(\gamma=0.5)$  as given in ENDF/B4 with the matrix computed by means of the Taylor series expansion method (BRC).

A glance at this figure shows that the deviation is far outside the possible experimental error limit and that moreover the "ENDF"-distribution becomes negative between 90 and 125 degrees. The latter distribution must be rejected.

Obviously one expects that these deviations would also become apparent in results of neutron transport calculations. We have performed such a comparative calculation for a deuterium-sphere. Details of it are given in **Annex-2**.


Figure 18. Comparison of angular distributions: Elastic scattering of 20 MeV neutrons by deuterium, using the transformation matrix from ENDF/B4 and the matrix calculated by us (BRC).

# 3.8.2 Suitability of the Taylor series expansion method.

The present method is economical, permits the numerical computation to be kept under accuracy-control and covers all physical cases for which  $\gamma \in [0,1]$ , with the exception of  $T^{-1}(\gamma=1)$  for which the transformation is not defined in the present form.

The Taylor series expansion method is **economical**, as the computing time remains, for one complete transformation, below half a second (CDC-7600) in most of the cases, and even for more extreme cases, i.e., for  $\gamma \approx 0.9$ , is about one second.

The **accuracy-control** of the transformation procedure is rather tight and therefore avoids waste of computing time.

To transform angular distribution data from one of the two reference systems to the other, the method proposed in this section is **applicable to a large variety of cases** in physics and, in particular, covers practically all of those which appear in the **Evaluated Neutron Data Files**.

## 3.8.3 Interesting mathematical relations derived in this chapter.

• From (3.1), (3.9) and (3.10) it follows that:

$$\frac{2m+1}{2} \int_{-1}^{+1} P_{\ell} [(\gamma + \bar{\mu})(1 + 2\gamma \bar{\mu} + \gamma^2)^{-1/2}] P_{m}(\bar{\mu}) d\bar{\mu} = \gamma \in [0, 1]$$

$$= \sum_{r=|\ell-m|}^{\infty} b_{\ell m}^{r} \gamma^{r} \quad \text{for } \ell \text{-even},$$

$$= \sum_{r=|\ell-m|}^{m+1} b_{\ell m}^{r} \gamma^{r} \quad \text{for } \ell \text{-odd}, \quad (3.97)$$

where the  $b_{\ell m}^{r}$  can be calculated by means of the recurrence formula  $b_{\ell m}^{r+1} = \frac{(m+1)(m+2-r)}{(r+1)(2m+3)} b_{\ell,m+1}^{r} - \frac{m(m+r-1)}{(r+1)(2m-1)} b_{\ell,m-1}^{r}$  $b_{\ell m}^{0} = \delta_{\ell m}$ .

• From (3.43), (3.48) and (3.49) it follows that:

$$\frac{2\ell+1}{2}\int_{-1}^{+1} P_{\mathfrak{m}}[\gamma(\mu^{2}-1)+\mu(\gamma^{2}(\mu^{2}-1)+1)^{1/2}] P_{\ell}(\mu) d\mu = \gamma \in [0,1]$$

$$= \sum_{\substack{r=|m-\ell|}}^{\infty} q_{m\ell}^{r} \gamma^{r} \quad \text{for } \ell \text{-odd},$$
$$= \sum_{\substack{r=|m-\ell|}}^{\ell} q_{m\ell}^{r} \gamma^{r} \quad \text{for } \ell \text{-even}, \quad (3.98)$$

where

$$\begin{aligned} q_{m\ell}^{r+1} &= \frac{m(m+1-r)}{(2m+1)(r+1)} q_{m+1,\ell}^r - \frac{(m+1)(m+r)}{(2m+1)(r+1)} q_{m-1,\ell}^r \\ \text{with} \quad q_{m\ell}^0 &= \delta_{m\ell} \\ \text{which permits calculation of the coefficients } q_{m\ell}^r. \end{aligned}$$

• From (3.20) and (3.21) it follows that:

$$\frac{2m+1}{2} \int_{-1}^{+1} P_{\ell} \left[ \left( \frac{1+\bar{\mu}}{2} \right)^{1/2} \right] P_{m}(\bar{\mu}) d\bar{\mu} =$$

$$= (-1)^{n+m+1} \frac{2^{n+1}}{n!} (2n+1)!! \frac{(2m-2n-3)!!}{(2m+2n+3)!!} (2m+1) \frac{(m+n)!}{(m-n)!}$$
for  $\ell = 2n+1$ ,  $n = 0$ ,  $1$ ,  $2$ , ...
$$= (-1)^{n+m-1} \frac{(2m+1)}{2^{n}} \frac{n!}{(n-m)!} \frac{(2n+2m-1)!!}{(2n-1)!!} \frac{(2n-2m-3)!!}{(n+m+1)!}$$
for  $\ell = 2n$ ,  $n = 0$ ,  $1$ ,  $2$ , ...

• From (3.56) and (3.57) it follows that:

$$\frac{2\ell+1}{2} \int_{-1}^{+1} P_{m}(2\mu^{2}-1) P_{\ell}(\mu) d\mu =$$

$$= \frac{(-1)^{m+n}}{2} \frac{2^{n}(2n-1)!!}{n!} (4n+1) \frac{(2m-2n-1)!!}{(2m+2n+1)!!} \frac{(m+n)!}{(m-n)!}$$
for  $\ell = 2n$ ,
$$= \frac{(-1)^{m+n}}{2^{n+2}} \frac{n!}{(n-m)!} (4n+3) \frac{(2n-2m-1)!!}{(2n+1)!!} \frac{(2n+2m+1)!!}{(n+m+1)!} +$$

$$+ (-1)^{m+\ell+n} \frac{2\ell+1}{2} \frac{(2n-1)!!}{2^{n+1}(n+1)!}$$
for  $\ell = 2n+1$ .

• From (3.60) and (3.61) it follows that:

$$\int_{-1}^{+1} (1-\mu^2)^r \frac{d^r P_{\ell}(\mu)}{d\mu^r} P_m(\mu) d\mu = \frac{2}{2m+1} a_{\ell m}^r$$
 (3.101)  
for  $r = 0, 1, 2, ...,$   
 $\ell, m = 0, 1, 2, ...,$ 

where the  $a_{\pounds m}^r$  are given by the recurrence formula

$$a_{\ell m}^{r+1} = \frac{(m+1)(m+2+2r)}{2m+3} a_{\ell,m+1}^{r} - \frac{m(m-1-2r)}{2m-1} a_{\ell,m-1}^{r}$$
  
and  $a_{\ell m}^{0} = \delta_{\ell m}$ .

Using either the relation [GR65,p.1031]

$$C_{m-r}^{r+1/2}(\mu) = \frac{1}{(2r-1)!!} \frac{d^{L}P_{m}(\mu)}{d\mu^{r}}$$
, where  $C_{m-r}^{r+1/2}(\mu)$ 

denotes Gegenbauer polynomials, or the relation [GR65,p.1031]

$$\frac{d^{L}P_{\ell}(\mu)}{d\mu^{r}} = (-1)^{r} (1-\mu^{2})^{r/2} P_{n}^{r}(\mu) ,$$

one obtains the equivalent representation of (3.101)

$$\int_{-1}^{+1} (1-\mu^2)^r c_{\ell-r}^{r+1/2}(\mu) c_m^{1/2}(\mu) d\mu = \frac{2}{(2m+1)(2r-1)!!} a_{\ell m}^r$$

anđ

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$$\int_{-1}^{+1} (1-\mu^2)^{\frac{3r}{2}} P_{\ell}^{r}(\mu) P_{m}(\mu) d\mu = (-1)^{r} \frac{2}{2m+1} a_{\ell m}^{r}$$

respectively.

Explicit values for the matrices  $a_{\ell m}^r$  are given in **Table 3.12**.

R	- 1								
			1	2	3	4	5	6	7
		3	Ŭ	-2 3	0	0	0	0	0
2		0	5	0	-65	0	0	0	0
3		0	0	12 7	0	- <u>12</u> 7	0	0	0
•		0	0	0	20 9	0	-20 9	0	0
5		0	0	0	0	30 11	0	- <b>30</b> 11	0
•		0	0	0	0	0	42 13	0	-42 13
7		0	0	0	0	0	0	56 15	0
	·						······		
		0	1	2	3			6	7
1		0			<u> </u>	0	0	0	0
2		8	-3 0	-192	5	24	0	0	0
	1	5	24	35	_002	7	40	•	•
		v	-7	v	105	v	Ť	Ũ	Ŭ
4		0	0	40 7	0	-10000 693	0	280 33	0
5		0	0	0	280 33	0	-2920 143	0	1680 143
6		0	0	0	0	1680 143	0	-3920 143	0
7		0	0	0	0	0	1008 65	0	-117376 3315
						·····			
R	- 3								
	<b> </b>	-16		4528	3	-32		<u>0</u>	
		ĨĴ		315				-	•
2		0	-544 25	0	5856 175	0	-320 21	0	0
З		48 7	0	-10736 245	0	73648 1155	0	-2160 77	0
4		0	16	0	-54256 693	0	8692720 81081	0	-19600 429
5		0	0	320 11	0	-598160 4719	0	261168 1573	0
6		0	0	•	6720 143	0	-1067360 5577	0	38314976 158015
7		0	0	0	0	10080 143	0	-50031968 182325	0
	·								
	• • <u> </u>		1	2	3			6	
1		0	14656		-157952	0	320	0	0
2		-4352	175 0	900224	1575 0	-3438976	9	640	0
3		75	-243648	3675 0	17267648	13475 0	-155200	7	25920
	}	128	1225	-663296	33075	2054910464		-25452800 0	- 143
			1152	1617	-2931774	2081079	72217216	27027	-542074844
		~	~~ĩi	20000	3861	-26288280	42471	1888303103	347633
•		v	Ū	143		-20207280 20449	U	2370225	U
7	[	0	0	0	4450 13	0	-12 <b>3563936</b> 60775	012	2239329324375

One can show that  $a_{\ell m}^r \neq 0$  only for  $|\ell-m| \leq r$  and then only for  $\ell+m$ -even and r-even, or for  $\ell+m$ -odd and r-odd.

The integral (3.101) thus vanishes in many cases.

The **identity** (3.69) which allows the evaluation of some interesting **integrals** and shows up a connection with **number theory** is also worthy of note.

#### 3.8.4 Outlook.

In the present study a set of  $b_{\ell m}^{r}$  and  $q_{m\ell}^{r}$  matrices have been derived. Some of the properties of these matrices have already been treated here. It would obviously be of interest to investigate them more profoundly. We can compute the Taylor series coefficients  $b_{\ell m}^{r}$  and  $q_{m\ell}^{r}$  with recurrence relations. One is naturally tempted to look for analytical expressions of these coefficients. An **algebraic program** would certainly be a powerful tool in solving this problem.

The functions  $T_{\ell m}(\gamma)$  and  $T_{m\ell}^{-1}(\gamma)$  in general, and the polynomials  $T_{\ell m}(\gamma)$  (for  $\ell$ -odd) and  $T_{m\ell}^{-1}(\gamma)$  (for  $\ell$ -even) in particular, would be an interesting subject for further investigation.

The calculation of the transformation matrices in the present case was confined to values of  $\gamma \in [0,1]$ . It would be quite natural to search for its **extension to the range**  $\gamma > 1$ . However, a very preliminary treatment of this problem indicates that the transformation matrices would have to be redefined to cover such an extended range of  $\gamma$ -values.

# 4.0 PERFORMANCE-COMPARISON OF THE VARIOUS METHODS AVAILABLE FOR THE COMPUTA-TION OF THE TRANSFORMATION MATRICES.

In **CHAPTER 3** the mathematical analysis of the **Taylor series method** together with its numerical exploration were presented. This method turned out to be **most satis**-factory in its overall performance.

In order to judge its **efficiency relative to other methods** available for calculating the transformation matrices T and T⁻¹, **comparative computations were carried out**.

In this chapter we intend, therefore, to compare the **three methods available for** evaluating such matrices, which is to say, the Taylor series method which serves as a standard will be compared with the following two methods:

- the method which permits computation of the matrix elements recursively, and
- the method which represents the matrix elements as a four-fold product of finite sums.

We only perform an efficiency comparison for the matrix T as the essential conclusions to be drawn from it are equally valid for its inverse, T⁻¹.

## 4.1 RECURRENCE FORMULA IN TERMS OF MATRIX ELEMENTS.

This formula has assumed a prominent position in evaluating the transformation matrices. Closer examination shows, however, that it is not recommendable.

#### 4.1.1 Brief recapitulation of the formula.

The recurrence formula concerned reads [BE65,p.23]

$$T_{\ell+1,m} = \frac{2\ell+1}{\ell+1} \begin{bmatrix} \sum_{n=0}^{\infty} T_{1n} & \sum_{k=|n-m|}^{n+m} C^2(n,k,m) T_{\ell k} \end{bmatrix} - \frac{\ell}{\ell+1} T_{\ell-1,m}$$
(4.1)

with the initial values

$$T_{Om} = \delta_{Om}$$
 (4.2)  
and

 $T_{1m} = \frac{m}{2m-1} (-\gamma)^{m-1} - \frac{m+2}{2m+3} (-\gamma)^{m+1} \qquad m = 0, 1, ..., M \qquad (4.3)$ 

C denote the particular CLEBSCH-GORDON coefficients <n 0 k 0 m 0>.

Note that the formula (4.1) contains an infinite sum. For use in numerical calculations it has thus to be cut off at a certain term, say at n = N. The computational process for this case is schematically represented in Figure 19 on page 143. Curtailing the infinite series in (4.1) evidently requires an estimation of the remainder of the series and an error propagation analysis. Only then can the computational process be kept under accuracy-control. No such analysis exists in the relevant literature.

Besides the uncertainty due to the cut-off of the infinite sum, the round-off error might also play a significant role.

For an efficiency comparison we did not need to deal analytically with these problems because the Taylor series method, as presented in **CHAPTER 3**, permits an accuracy-controlled evaluation of the matrix elements. It can thus serve as a standard method.

#### 4.1.2 Comparison with the Taylor series method.

Firstly, the matrix elements  $T_{m}$  are calculated, by means of the Taylor series method presented in **CHAPTER 3**, to within a given relative accuracy  $\epsilon_{M1}$ . These matrix elements are then compared with those computed with the aid of the recurrence relation (4.1).

To be more precise, the comparison is centered on three items:

- The dependency of the accuracy on the remainder of the infinite sum in (4.1),
- the round-off stability of (4.1), and
- the computation time.



Figure 19. Schematic representation of the computational process of (4.1): Dimension of the matrix: (L,M). All elements below the diagonal have to be calculated for the unique purpose of obtaining the actual matrix T_{/m}.

4.1.2.1 THE DEPENDENCE OF THE ACCURACY ON THE REMAINDER OF THE INFINITE SUM APPEARING IN (4.1).

To this end, calculations of the matrix elements  $T_{\ell m}$  were carried out by means of formula (4.1) for different remainders of the infinite sum. The corresponding numerical results are given in **Table 4.1**. In this table each matrix T is followed by the corresponding **accuracy matrix A**, the elements of which are defined as follows

 $A_{\ell m} = \frac{T_{\ell m, M2} - T_{\ell m, M1}}{T_{\ell m, M1}} \quad \text{for } T_{\ell m, M1} \neq 0 \qquad (4.4)$ =  $T_{\ell m, M2} \qquad \text{for } T_{\ell m, M1} = 0$ .

Here, the subscripts M1 and M2 denote the use of the Taylor series method and the relationship (4.1), respectively. In our case the elements  $T_{\ell m, M1}$  were computed to within a relative error of  $\epsilon_{M1} \leq 10^{-4}$ .

**Table 4.1:** The matrix T computed using (4.1) in **single precision** and the accuracy matrix A, (4.4), for various  $\gamma$ -values. Computer: CDC-7600. Cases treated:  $\gamma = 0.01$ , N = 5, 10, 15, 25;  $\gamma = 0.1$ , N = 10, 25, 35;  $\gamma = 0.4$ , N = 10, 25, 35;  $\gamma = 0.5$ , N = 10, 25, 50;  $\gamma = 0.7$ , N = 10, 25;  $\gamma = 0.9$ , N = 10, 25.

HAT	ATRIX T GAMMA = .010 N MAX = 5			TIME = .439 5			SINGLE PRECISI			
LM	0	1	2	3	4	5	6	7	8	9
0 12 3 4 5 6 7 8 9 0 111 112 13 4 15 16 18 19 0 20	1.000E+00 6.6667E-03 2.000E-05 -6.338E-16 -1.5876E-10 9.9493E-15 -1.0460E-12 4.6725E-11 3.9221E-13 5.2267E-11 3.9221E-13 5.3324E-11 5.7503E-13 5.3761E-11 5.0405E-13 5.4214E-11 6.9176E-13	0. 9.9994E-01 1.2000E-02 6.8571E-05 1.9048E-07 -1.1301E-12 6.1535E-11 -1.5745E-12 1.4896E-12 1.4896E-12 1.4896E-12 1.6465E-12 1.645E-12 1.625E-10 1.625E-10 1.625E-10 2.0128E-12 1.625E-10	0. -6.6661E-03 9.9984E-01 1.7142E-02 1.4285E-04 6.9271E-07 1.4057E-10 2.485E-12 2.5420E-10 2.3779E-12 2.6570E-10 2.7328E-12 2.7328E-12 2.7328E-12 2.7356E-10 3.0735E-12 2.7104E-10 3.2082E-12	0. 5.9994E-05 5.9994E-01 9.9996E-01 2.2219E-02 2.2219E-02 2.2219E-02 2.2219E-02 2.2219E-02 2.2219E-02 2.2219E-02 2.2219E-02 2.2219E-02 2.2219E-02 2.2219E-02 3.6066E-10 3.4468E-12 3.798E-10 4.1998E-12 3.7966E-10	0. -7.7137E-07 -1.3712E-04 -1.7138E-02 9.9949E-01 2.7266E-02 3.6708E-04 3.1328E-06 3.6708E-04 3.1328E-06 3.6708E-04 3.6708E-04 3.6708E-04 3.6708E-04 3.6708E-04 3.6708E-04 3.6708E-04 5.0757E-12 4.8673E-10 5.5127E-12 4.8673E-10 5.5127E-12 4.8773E-10 5.3007E-12	0. 5.5550E-09 -1.5235E-06 2.3804E-04 -2.2214E-02 3.3204E-04 5.3207E-06 3.2295E-02 5.1660E-04 5.3207E-06 3.2495E-03 5.8205E-10 5.4205E-10 5.4205E-10 5.4205E-10 5.4205E-12 5.9353E-10 6.6028E-12 5.9353E-10 6.5053E-12 5.943E-10 5.943E-10 5.943E-10 5.943E-10 5.943E-10 5.943E-10 5.943E-10 5.943E-10 5.943E-10 5.943E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-10 5.944E-1	0. -5.4540E-11 -5.4541E-08 -3.0295E-06 3.6351E-04 -2.7298E-02 3.6351E-04 -2.7298E-02 3.6351E-04 8.9153E-04 8.3205E-06 6.9153E-04 8.3205E-06 9.2144E-10 -3.9605E-12 -3.9605E-12 -3.9605E-12 -7.0401E-10 7.6401E-10 7.8315E-12	0. 5.3841E-13 -1.3494E-10 3.6705E-08 -5.2137E-06 5.1375E-04 -3.2285E-02 9.9859E-01 4.2323E-02 8.9124E-04 1.2257E-05 1.2181E-07 1.4642E-09 -2.1240E-12 1.4642E-09 -2.1240E-12 8.0682E-10 8.5841E-12 8.1077E-10	0. -5.3328E-15 -1.2436E-12 -3.5237E-10 6.9595C-08 -8.2202E-06 6.8883E-04 -3.7300E-02 9.9819E-01 4.7326E-02 9.9819E-01 1.7554E-35 1.9432E-07 1.9432E-10 9.9242E-10 9.9552E-12 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 9.1542E-10 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LM	10	11	12	13	14	15	16	17	18	19
0123455678990111213445567899001112134455678990011121334455678990011121334455678990011121334556789900000000000000000000000000000000000	0. -5.2626E-19 -3.1555E-16 8.0919E-12 -1.5005E-07 -1.7153E-03 -1.7153E-03 -1.7153E-03 -4.7303E-07 -3.7312E-02 9.9725E-01 5.7312E-02 9.9725E-01 5.7312E-02 9.9725E-01 5.4.2920E-07 5.4.2920E-07 5.4.2920E-07 5.4.2920E-01 1.1159E-09 1.1328E-09 1.318E-11 .318E-11 .318E-11	0. 5.2376E-21 -1.1146E-18 2.94312-14 4.021246E-18 2.94312-14 -2.950129 2.9202E-07 -2.3334E-05 1.3632E-03 3.9856-0297E-02 1.9332E-03 3.9856-0297E-02 1.9332E-03 3.9856-0297E-02 1.9332E-03 3.9856-0297E-02 1.9332E-03 3.9856-0297E-02 1.9332E-03 3.9856-0297E-02 1.9332E-03 3.9856-0297E-02 1.9332E-03 3.9856-0297E-02 1.9332E-03 3.9856-0297E-02 1.9332E-03 3.9856-0297E-02 1.9332E-03 1.2244E-09 1.2244E-09 1.2244E-09 1.2244E-09 1.2244E-09 1.2244E-09	0. 5.2169E-23 1.0927E-20 2.707FE-18 7.7748E-16 1.8555E-11 3.3289E-11 4.2613E-07 -3.0824E-05 1.6376E-03 -5.7279E-02 9.9610E-01 6.7276E-02 2.2634E-03 5.0340E-05 8.2793E-07 1.1641E-08 8.2793E-07 1.4541E-08 9.3466E-11 1.3322E-09 1.4581E-11	0. 5.1995E-25. 2.5850E-22. 2.5850E-22. 2.5850E-22. 2.5850E-22. 2.5850E-12. 5.9534E-13. 5.9534E-10. 6.8729E-01. 7.2249E-01. 7.2249E-01. 7.2249E-01. 7.2249E-01. 7.2249E-01. 7.2249E-01. 7.2249E-01. 1.424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 1.4424E-09. 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3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08 3.0445E-08	0. 0. 1.1618E-08 2.5361E-08 2.5361E-08 2.5361E-08 2.5361E-08 2.53298E-08 1.2471E-08 1.2471E-06 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-07 1.2471E-0
LH	10	11	12	13	14	15	16	17	18	19
012345	0. 2.3422E-14	0. 1.3789E-14	0. 2.8842E-14	0. 2.2608E-14	0. 3.0998E-14 3.1189E-09	0. 4.1617E-14 1.4458E-05	0. 3.8014E-14 4.2990E-07	0. 5. <b>5259E-14</b> 1.4447E-01	0. 5.3223E-14 2.1218E-01	0. 7.8081E-14 2.5998E-01

LM

LH

MATR LM

HAT	NIX T GA	MMA = .010	N MAX -	25		TIME =25.	.504 S		SIN	GLE PRECISION
LM	0	1	2	3	4	5	6	7	8	9
0123456789011234567890	1.0000E+00 6.6667E-03 2.0000E+05 -1.5876E-10 -1.5876E-10 -1.2807E-15 -9.3563E-16 2.7516E-15 2.7516E-15 2.7566E-14 1.9944E-17 5.1498E-15 -6.6001E-14 5.1498E-15 -1.3647E-14 8.3006E-14 1.39647E-14 8.3006E-13	0.99994E-01 1.2000E-02 6.8571E-05 1.9048&-07 -3.8159E-14 -4.1294E-14 -4.9815E-15 -6.429E-15 -6.429E-15 -6.429E-15 -7.9810E-14 -1.1842E-14 3.2106E-14 -2.6674E-14 3.2106E-14 -2.6674E-15	0. -6.6661E-03 9.9984E-01 1.7142E-02 1.4285E-04 6.9264E-07 1.7483E-09 -2.6090E-15 2.6031E-14 -3.7161E-15 2.6031E-14 -3.7161E-15 2.6031E-14 -1.7552E-14 1.7653E-13 -1.3340E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-13 -1.466E-15 -1.466E-15 -1.466E-15 -1.466E-15 -1.466E-15 -1.466E-	0. 5.9994E-05 7.1998E-02 9.9969E-01 1.6316E-06 6.9618E-09 1.6114E-11 2.7033E-14 6.7634E-15 4.6008E-14 7.608E-14 4.6008E-13 1.8368E-13 1.8368E-13 1.8368E-13 3.5947E-13 8.7224E-15 8.7224E-15 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7224E-14 8.7	0.7137E-07 -3.7137E-04 -1.7138E-02 9.9949E-01 2.7266E-02 3.6708E-04 3.1326E-06 4.8140E-08 1.8140E-08 4.9825E-11 9.8225E-11 9.8225E-11 9.8225E-14 1.22846E-13 3.5945E-15 2.7716E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 3.4413E-13 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0.000E-05\\ - 0.000E-05\\ - 0.00E-05\\ -$	$\begin{array}{c} 0,\\ 1,0843E-14\\ 4,1421E-09\\ 1,9703E-08\\ 3,9027E-09\\ 2,3135E-10\\ 2,3135E-10\\ 2,3135E-10\\ 2,3135E-10\\ 2,3135E-10\\ 2,3135E-10\\ 2,3135E-10\\ 2,3135E-10\\ 2,3135E-10\\ 2,3125E-10\\ 3,1445E+12\\ 1,5874E-13\\ 1,58445E+12\\ 1,5874E-13\\ 1,58445E+12\\ 1,5874E-13\\ 1,58445E+12\\ 1,5874E-13\\ 1,58445E+12\\ 1,5874E-13\\ 1,58445E+12\\ 1,5874E-13\\ 1,58445E+12\\ 1,5874E-13\\ 1,4849E+26\\ 1,2325E+13\\ 1,4941E+26\\ 1,2355E+13\\ 1,2355E+12\\ 1$	0. 5.9298E-15 4.0566E-09 1.5779E-08 1.4927E-08 3.4173E-09 4.2246E-09 3.0375E-07 4.2246E-09 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 3.0375E-07 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HATE	IX T GA	MMA = .100	N MAX -	- 25		TIME =25.	516 S		SIN	GLE PRECISION
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MATR	IX A (M2-H)	L)/M1 G/	<b>UHA =400</b>	7						
MATR L M	IX A (H2-H) 0	L)/H1 G/ 1	<b>UHA = .400</b> 2	]3	<u> </u>	3	6	7	8	9
HATR L M 0 1 2 3 4 5 6 7 8 9 9 0 11 112 15 16 17 18 19 20	0 0. 6.6613E-15 8.2523E-06 3.4939E-09 7.958IE-05 2.3039E-07 9.5239E-02 3.7428E-06 2.768IE-01 1.7138E-05 1.7113E+03 1.3395E-05 1.2819E+06 -4.5136E-06 7.0365E+07 -1.8196E-05 5.4179E+10	1)/M1 G/ 1 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	VH4A = .400           2           0.           2.0730E-06           7.77201E-15           2.0730E-06           7.7746E-08           1.3383E-05           2.0012E-03           2.0012E-03           2.0021E-03           2.0021E-03           2.0021E-03           2.0021E-03           2.0021E-03           2.0021E-03           3.0078E-05           3.0459E-01           3.0950E-05           1.0004E+05           3.6099E+06           -4.2482E+05           3.6099E+06           -4.3482E-05           4.1138E+09	3 0. 5.4304E-15 2.0480E-06 2.4047E-07 3.6447E-07 1.7057E-05 2.0039E-04 2.5756E-03 3.9382E-02 -6.8249E-05 4.5882E-00 -1.3591E-04 4.5882E+00 -1.3591E-04 3.0281E+02 -1.5559E-04 4.7530E+06 -2.8041E-04 2.6635E+08	4 0. 0. 1.9151E-06 8.7054E-07 1.8522E-03 3.787E-05 3.787E-05 3.787E-05 3.787E-05 3.787E-05 3.787E-05 3.787E-05 3.787E-05 3.787E-05 3.757E-05 3.4022E-01 3.9502E-05 3.4022E-01 3.9502E-05 3.4022E-01 3.4022E-01 5.6737E-05 6.5849E-05 1.0402E-08	3 0. 4.6195E-15 1.1454E-06 4.1375E-06 2.5415E-04 2.6259E-05 2.5415E-04 8.2627E-05 1.2263E-04 1.237E-05 1.2263E-04 2.0228E-04 1.7311E-03 2.5668E-01 -2.7504E-04 1.5507E-02 -3.3741E-04 -3.7941E-04 -3.4043E-04 2.3667E+06	6 0. 0. 2.1571E-05 5.8240E-05 1.2886E-04 6.8663E-04 9.7461E-05 2.4417E-04 9.7461E-05 2.4417E-04 9.7461E-05 5.2707E-03 3.6538E-02 5.2707E-03 3.6538E-02 5.2707E-03 3.6538E-02 5.2707E-03 5.5377E-03 9.8452E-06 4.5566E-02 -1.9766E-05 2.9978E-04 -5.1517E-05 1.2337E+06	7 0. 7.4669E-15 4.0424E-05 1.1776E-04 1.8905E-04 1.8905E-04 1.8905E-04 4.005E-04 6.6734E-05 3.4010E-05 5.4606E-04 6.6734E-05 1.3422E-03 8.6476E-01 1.1744E-01 -4.0300E-04 1.1745E-04 1.5563E-04	8 0. 4.7149E-15 3.1236E-04 6.6101E-04 6.0725E-04 5.5179E-05 5.7016E-04 8.0871E-05 5.7016E-04 8.0871E-05 1.2086E-03 5.0015E-04 1.2147E-02 6.4793E-03 5.0015E-04 1.2147E-02 6.4793E-03 3.082% 01 8.8280E-02 3.4558E+01 -2.2089E-05 5.7231E+03	9 0. 5.9402E-15 2.5797E-03 3.7790E-03 9.2371E-05 6.0016E-04 9.3913E-06 6.0573E-04 6.6573E-04 6.6573E-04 6.9560E-04 6.7562E-05 1.1220E-03 3.7780E-04 8.0158E-03 1.3552E-01 1.3552E-01 4.0504E-02 7.2623E+00 4.4665E+00
HATR L M 0 1 2 3 4 5 6 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 L M	IX         A         (H2-H)           0         6.6613E-15         8.2523E-06           8.2523E-06         9.2523E-06         9.2523E-02           7.958IE-05         2.3039E-07         9.5239E-02           7.738E-05         1.7113E+03         1.1396E-05           1.3689E+04         1.3889E+04         1.9892E-05           1.2819E-05         1.2819E-05         1.2819E-05           1.0         10         10	1//M1 G/ 1 0. 0. 0.2931E-06 6.2931E-06 6.2931E-06 1.4755E-05 -9.0824E-07 -7.4350E+00 -7.4350E+00 -7.4350E+00 -7.4350E+00 -8.2573E+05 -8.2573E+05 -8.2573E+05 -1.2316E-04 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 -1.3521E-049 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	11A I 0	APPIA = .4UU	N MAX ·	- 25		TIME =25.	.505 S			GLE PRECISIO
LM	0	1	2	3	4	5	6	7	8	9
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3.9257E-10 1.0257E-10 1.0257E-10	0. -3.0986E-02 1.6752E-01 -4.3308E-01 3.3211E-01 6.9143E-01 1.7220E-01 1.7220E-01 1.7220E-01 4.3337E-02 7.1511E-03 6.5346E-04 2.1921E-13 6.5346E-04 2.1921E-13 6.5346E-04 2.1921E-13 6.5346E-04 7.3789E-12 1.2794E-01 3.6056E-11 -3.4671E-09 8.6968E-11 -1.6139E-12 1.1067E-12 1.1067E-12	0. 1.2017E-02 7.4546E-02 2.4978E-01 1.0410E-01 5.4445E-01 5.4445E-01 5.4445E-01 1.63280E-01 5.4445E-01 1.8871E-02 2.8646E-03 2.4591E-04 -1.4384E-11 -2.1384E-11 -2.1384E-11 -2.1384E-11 -1.4384E-11 -1.4384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 -1.1384E-11 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1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 1.7426E-01 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LH	10	11	12	13	14	15	16	17	18	19
0 1 3 3 4 5 6 7 8 9 10 111 13 14 5 16 7 18 19 20	0. -1.1609E-04 1.0694E-03 -6.2660E-03 2.6725-02 -8.5116E-02 1.9786E-01 -3.0694E-01 1.22664E-01 1.4001E-01 -3.3787E-01 -3.3787E-01 -3.3694E-03 3.3480E-01 2.4095E-01 2.4095E-01 2.6398E-03 1.6398E-03 2.5815E-04	0. 4.6201E-05 4.4829E-04 2.7984E-03 1.2920E-02 4.5638E-02 1.2261E-01 2.3959E-01 1.2457E-01 2.3728E-01 2.3728E-01 2.3728E-01 2.3728E-01 1.5152E-01 1.4572E-01 1.51340E-02 1.5703E-02 3.7453E-03	0. -1:8404E-05 1.8717E-04 -1:2399E-03 6.1111E-03 -2:3532E-02 -1:6307E-01 2:6863E-01 -2:6863E-01 -2:6863E-01 -2:6865E-01 1:1686E-02 2:9028E-01 -3:4995E-01 -3:4995E-01 -3:4995E-01 -3:4995E-01 -3:4995E-02 -2:7928E-02	0. 7.3357E-06 7.7879E-05 5.4073E-04 2.8411E-03 1.1780E-02 3.8962E-02 1.0170E-01 2.7885E-01 2.7885E-01 2.9334E-02 2.9389E-01 2.9389E-01 3.0877E-01 5.1509E-01 1.2310E-01	0. -2.9255E-06 3.2312E-05 -3.2312E-05 -3.2312E-05 -3.2312E-05 -3.2312E-05 -3.2312E-01 -3.2312E-01 -3.2312E-01 -2.3416E-01 -2.8453E-01 -2.8453E-01 -2.8453E-01 -2.8453E-01 -2.8452E-01 -2.8452E-01 -3.2935E-01	0. 1.1672E-06 -1.3373E-05 1.0143E-04 2.7650E-03 -1.6610E-02 3.3420E-02 -1.6610E-02 3.3420E-02 -1.7170E-01 -2.5410E-01 -1.5213E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5233E-02 -2.4100E-01 -1.5235E-02 -2.4100E-01 -1.5235E-02 -2.4100E-01 -1.5235E-02 -2.4100E-01 -1.5235E-02 -2.4100E-01 -1.5235E-02 -2.4100E-01 -1.5235E-02 -2.4100E-01 -1.5235E-02 -2.4100E-01 -1.5235E-02 -2.5400E-01 -1.5235E-02 -2.5400E-01 -1.5235E-02 -2.5400E-01 -3.1555E-02 -3.8968E-01 -4.9712E-01 -5.535E-02 -5.535E-02 -5.535E-02 -5.535E-02 -5.535E-02 -5.535E-02 -5.535E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02 -5.555E-02	0. -4.6584E-07 5.5226E-06 -4.3542E-05 5.5226E-03 -3.385E-03 -1.8068E-02 -1.1511E-01 -2.0396E-03 -1.8068E-02 -1.1511E-01 -2.0396E-01 -2.0396E-01 -2.0396E-01 -2.0396E-01 -2.5726E-01 -2.674E-02 -7.5419E-02 -3.3030E-01 -1.1227E-01 -3.4040E-01	0. 8977E-07 -2.2763E-06 -2.2763E-06 -1.1791E-04 6.0937E-04 -2.6243E-03 9.4926E-03 -2.8785E-02 -2.8785E-02 -2.8785E-02 -2.46085E-01 -2.46085E-01 -2.46085E-01 -2.4656E-02 -2.4779E-01 -2.2143E-01	0. -7.4257E-08 9.3667E-07 -7.9171E-06 5.2106E-05 -2.8107E-04 1.2715E-03 -4.8714E-03 1.5822E-02 -4.3263E-02 -4.3263E-02 -1.7777E-01 -2.0376E-01 -1.7822E-01 -2.3497E-01 -2.3291E-01	0. 2.9657E-08 3.3668E-06 7.2882E-05 1.2840E-04 6.0754E-04 2.4512E-03 2.4884E-02 2.4884E-02 2.4884E-02 2.4884E-02 2.4884E-02 2.4884E-02 2.4884E-02 2.489E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3297E-01 2.3301E-01 2.3301E-01
MATR	IX A (H2-H)	L)/M1 GA	MMA = .400	]						
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5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	-5.3291E-14 1.1304E-06 -7.2249E-14 5.2599E-06 -5.9255E-17 2.447E-06 -6.7190E-14 1.6288E-06 -2.2542E-14 1.6288E-06 -2.2542E-14 1.6288E-06 2.9753E-02 3.9794E-12 8.1503E+00 8.6829E-12 2.3369E+10 2.3369E+10 10	6.294/E-06 1.1819E-12 3.2310E-06 1.6331E-13 3.2586E-06 1.6736E-13 1.6509E-06 1.6736E-13 1.6509E-06 1.0464E-13 2.0572E-06 9.9320E-13 1.77272E-02 2.8030E+00 2.6639E-11 1.21684E+02 7.5534E+01 7.5534E+01 7.5534E+01 11	1.30186-13 1.439E-05 6.0759E-12 6.0759E-12 6.2151E-02 5.2151E-02 6.2776E-13 2.2227E-06 -2.9795E-13 2.2227E-06 -2.9795E-13 2.2235E-05 1.7316E-12 2.2435E-05 1.7316E-12 2.2435E-05 1.7316E-12 6.58844E-01 4.6530E-11 1.5523E+03 1.2 12	4.4428E-14 2.0060E-06 5.7205E-13 1.4085E-06 1.5411E-11 6.6075E-06 6.6075E-06 6.6075E-06 8.8688E-07 -4.3764E-12 2.6815E-06 -4.3764E-12 2.6815E-06 -4.3764E-12 2.6815E-06 -1.2092E-01 1.2092E-01 1.2092E-01 2.4568E+02 13	3.6915:-14 2.1306:-06 1.0790:-13 1.8827E-06 2.67718:-12 1.6070E-06 7.1005:-11 9.7001E-07 2.1921E-13 1.5614E-06 7.3789:-12 1.4525E-04 1.6556:-11 1.8272E-02 8.6968E-11 1.0156:+00 1.1067E-10 3.5418E+01 	6.7562E-14 1.0239E-05 4.4367E-13 9.9539E-06 3.5237E-13 1.8270E-06 5.4499E-12 1.7795E-06 7.4109E-10 1.1472E-06 -1.4384E-11 1.2432E-05 -1.0511E-01 -1.1857E-10 1.0511E-01 -1.1857E-10 1.0511E-01 -1.1857E-10	2.7431E-14 6.9893E-06 3.3198E-14 2.7788E-06 2.0730E-13 8.6564E-13 1.8033E-06 7.4414E-11 9.306E-06 1.9762E-08 7.7330E-07 7.4092E-11 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1.3580E-04 1	1.0498E-13 5.5683E-06 6.6130E-14 7.4373E-06 6.9351E-13 7.3372E-06 6.6082E-13 5.3549E-06 3.5123E-11 7.913E-06 2.0892E-09 2.0388E-06 2.0892E-09 2.0388E-06 2.0892E-09 2.0388E-06 4.4935E-06 -1.1161E-10 4.5937E-04 -1.5636E-10 4.5937E-04 17	3.3309:-14 7787:-06 7.2464:-15 3.0481:-06 4.4360:-13 4.5027:-06 6.6554:-12 2.9966:-06 2.3372:-11 4.6050:-06 4.7348:-10 1.7812:-06 1.7812:-06 1.7812:-03 1.7773:-10 1.9682:-03 18	2.527/E-13 2.657/8-13 1.8932-05 5.6728-13 1.8952E-13 5.6728-13 5.6728-12 5.8506-12 5.8506-10 1.8591E-06 2.1031E-10 1.8591E-06 3.5262E-08 3.5262E-08 3.5594E-05 3.5594E-05 3.5594E-05

MATI	RIX T G/	AMMA = .400	N MAX -	35		TIME -65.	848 S		SIN	GLE PRECISION
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-7.7928E-13 -7.7928E-13 -7.484E-14 -7.7928E-13 -7.7928E-13 -7.484E-14 -7.7928E-13 -7.7928E-13 -7.484E-14 -7.7928E-13 -7.7928E-13 -7.484E-14 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 -7.7928E-13 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2.4594E-08 -1.1708E-13 2.9741E-11	0. 3.2560E-02 1.2951E-02 1.2951E-02 1.2951E-02 1.2951E-02 1.2951E-02 1.2951E-02 1.2951E-02 1.2951E-02 1.2951E-02 1.2455E-02 1.4455E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4452E-02 1.4552E-02 1.4552E-02 1.4552E-02 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3.5207E-01 3.5207E-02 1.8322E-02 1.8322E-02 1.8322E-02 1.8322E-02 3.5405E-03 4.5981E-04 3.5435E-05 -3.7467E-14 4.5027E-09 -3.5407E-14 4.5027E-09 -3.5407E-14 4.5027E-09 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 -3.5407E-14 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1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03 1.4645E-03	$\begin{array}{c} 0.\\ 2.9203E-04\\ -2.5390E-03\\ -3.5390E-04\\ -3.5390E-02\\ -5.3719E-01\\ -2.8719E-01\\ -3.8719E-01\\ -3.8719E-01\\ -3.7426E-01\\ -3.7426E-01\\ -3.7426E-01\\ -3.7426E-01\\ -3.7118E-01\\ -3.7118E-01\\ -3.7103E-03\\ -5.5498E-02\\ -3.7103E-03\\ -5.5498E-02\\ -7.3684E-05\\ -7.3684E$
LM	10	11	12	13	14	15	16	17	18	19
01234567891011213445 167891011213445 1671819920	0. -1.1609E-04 1.0694E-03 -6.2660E-03 2.672E-02 -8.5116E-02 1.9786E-01 -3.0694E-01 1.22664E-01 1.4001E-01 -3.3787E-01 -3.3787E-01 -3.3787E-01 -3.4095E-01 2.4095E-01 2.4095E-02 8.0752E-03 1.6396E-03 2.5815E-04	0. 4.6201E-05 4.4829E-04 2.7984E-03 1.2920E-02 4.5638E-02 1.2261E-01 2.3959E-01 1.2457E-01 2.3728E-01 2.3728E-01 2.3728E-01 1.2457E-01 3.1231E-01 3.1231E-01 1.4572E-01 5.3140E-02 1.4572E-01 3.7453E-03 3.7453E-03	0. -1.8404E-05 1.8717E-04 -1.2359E-03 -2.3532E-02 -6.1111E-03 -2.3532E-02 -2.6863E-01 -2.6865E-01 -2.6865E-01 -1.2955E-01 -1.2955E-01 -3.4095E-01 -3.4095E-01 -3.4095E-01 2.3022-02 -3.8156E-01 2.3022-02 2.7928E-02 2.7928E-02	0. 7.3357E-06 7.7879E-05 5.4093E-04 2.8411E-03 1.1780E-02 2.8411E-03 1.1780E-02 2.842E-02 1.0170E-01 2.7885E-01 2.9339E-01 2.9339E-01 2.6534E-03 -3.413E-01 3.0877E-01 2.6498E-01 1.2300E-01 1.2300E-01	0. -2.9255E-06 3.2312E-05 -2.3497E-04 1.3025E-03 -5.7611E-03 -2.6616E-02 -2.3416E-01 -2.3416E-01 -2.4616E-01 -2.456E-01 -2.456E-01 -2.456E-01 -2.456E-01 -2.456E-01 -2.456E-01 -2.456E-01 -2.456E-01 -2.456E-01 -2.456E-01 3.2935E-01 3.2935E-01	0. 1.1672E-06 1.3373E-05 1.0143E-04 2.7650E-03 3.3420E-02 2.5410E-01 2.5932E-01 1.7170E-01 1.5213E-02 -2.5410E-01 1.6999E-01 2.1836E-01 -3.1254E-01 2.3836E-01 -3.1254E-01 2.3836E-01 -3.1254E-01 2.3896E-01 -3.1254E-01 2.3896E-01 -3.1254E-01 2.3896E-01 -3.1254E-01 2.3896E-01 -3.1254E-01 2.3896E-01 -3.1254E-01 2.3896E-01 -3.1254E-01 2.3896E-01 -3.1254E-01 2.3896E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 -3.1254E-01 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MATH	IX A (M2-M1	L)/M1 GA	MMA = .400							
LM	0	1	2	3	4	5	6	7	8	9
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MATE	IX A (M2-H1	)/M1 G/	UHA = .500	٦						
LM	0	1	2	3	4	5	6	7	8	9
0 1 2 3 4 5 6 7 8 9 10 11 2 13 14 15 16 17 18 190 20	0. 5.3291E-15 7.6166E-06 2.0103E-07 7.5279E-06 6.5623E-05 4.8830E+01 1.3994E-04 4.9638E+02 3.6951E-05 1.1974E+04 4.8129E+04 4.8129E+04 4.8129E+04 4.8129E+04 4.8129E+04 4.8738E-04 3.1828E+09	0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	0. 6.7825E-15 3.3752E-06 2.7010E-06 6.4516E-04 1.4026E-02 3.5277E-04 5.19524E-04 5.1116E+01 5.2817E-04 5.1116E+01 5.2817E-04 3.373EE-04 3.373EE-04 7.5545E+05 -2.2603E-04 7.5545E+05 -2.2603E-04 3.7772E+08	0. 7.7047E-15 2.8038E-06 1.2031E-05 2.2323E-04 1.5250E-03 1.1405E-02 1.0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01 .0747E-01	0. 0. 2.6720E-07 2.6420E-05 7.5261E-04 3.0302E-04 1.9043E-03 3.6425E-02 3.4425E-02 3.4425E-02 3.4212E-01 5.3002E-04 1.202E-03 3.1502E-04 4.55016E-04 6.5978E+05 -4.9895E-04 1.3874E+07	0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	0. 8.6206E-15 5.8343E-05 2.3487E-04 6.4917E-04 2.8355E-03 1.8564E-03 1.9541E-03 7.7928E-04 6.4242E-03 4.3976E-03 3.2147E-02 3.2147E-02 3.2354E-04 3.4386E+02 -2.6433E-04 -7.9976E-04 3.3440E+05	0. 8.7482E-15 2.7489E-04 8.1233E-04 8.1233E-04 4.3796E-02 3.2320E-03 3.6012E-02 3.6580E-03 3.6012E-02 3.6580E-03 4.3837E-02 5.1355E-04 9.9982E-01 1.1134E+00 -3.2158E-03 9.1544E+03	0. 1.7686E-14 1.3103E-03 2.8898E-03 5.1936E-04 5.8210E-03 7.9423E-04 5.4421E-03 1.0426E-03 2.764457E-03 6.6416E-04 4.2578E-03 3.8313E-01 2.8171E+01 5.9110E-04 2.4019E+03	0. 8.9161E-15 6.85156-03 1.0556-02 4.2559E-04 4.2559E-04 4.2559E-04 4.2559E-04 4.2559E-04 4.2559E-04 4.2559E-04 1.4087E-04 2.4732E-02 3.3829E-04 1.1924E-02 7.0118E-04 2.9091E-02 8.5989E-04 6.2747E-03 1.927E-04 1.927E-02 4.1879E-03 1.8552E-01 8.3477E-02 6.0710E+00 1.2323E+01
LM	10	11	12	13	14	15	16	17	18	19
012345	0. 3.5897E-14	0. 3.6086E-14	0. 5.4363E-14	0. 4.5467E-14	0. 6.3851E-14	0. 7.3166E-14 3.6041E-01	0. 6.4169E-14 3.9453E-01	0. 1.0104E-13 4.2316E-01	0. 9.2020E-14 4.4775E-01	0. 1.1982E-13 4.6923E-01

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HATE	IX T GA	MHA = .500	N HAX	- 25		TIME =25.	534 S		SIN	GLE PRECISIO
LH	0	1	2	3	4	5	6	7	6	9
0 123456789 10 112134 15 167 18 190	1.0000E+00 3.3333=01 5.1954&02 -6.6613E-14 4.7863E-05 4.1107E-13 -2.4064&-06 9.2265E-12 -3264&-07 9.9595E-11 -3264&-07 9.9595E-11 -2.4064&-06 -2.482E-10 8.028E-07 9.32747E-09 -3.7259E-09 -3.7259E-09 -1.8363E-09	0. 8.5000E-31 5.5517E-01 1.7143E-01 2.5551E-02 2.5551E-02 2.5551E-02 2.5551E-02 2.5551E-02 2.5551E-02 2.5551E-02 2.5551E-02 2.5551E-02 2.2139E-05 -3.2107E-11 1.0979E-06 -3.2900E-10 6.0838E-08 -1.9760E-09 -1.1338E-08 1.0756E-10 -6.0740E-09 -1.1338E-08 1.0756E-09 6.1394E-09 6.1394E-09	0. -2.6190E-01 6.3520E-01 6.3520E-01 8.6580E-02 3.2479E-01 8.6580E-02 3.5223E-12 1.1892E-02 3.5223E-12 1.1892E-02 3.5223E-11 8.8290E-06 6.5151E-10 8.8290E-06 6.5151E-10 1.5675E-08 1.5675E-08 1.3918E-08 -1.2085E-08	0. 1:1528E-01 3:5644E-01 3:5644E-01 4:7786E-01 4:7786E-01 4:3512E-02 5:5320E-03 -1:2994E-10 9:542E-05 -1:1469E-09 3:5170E-06 -5:742E-09 3:5170E-06 2:1792E-08 2:246E-08 2:1194E-08 1:9926E-08	0. -5.4383E-02 2.1950E-01 -3.9298E-01 5.9334E-01 3.0522E-01 1.0128E-01 2.1823E-02 2.5907E-03 1.9086E-09 2.5907E-03 1.9096E-06 1.9997E-08 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4606E-09 4.1282E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-0582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582E-05 8.4582	0. 2.6309E-02 -1.2221E-01 2.9315E-01 -3.0982E-01 -3.0982E-01 -3.0982E-01 -3.0982E-01 -3.0982E-01 -3.0982E-02 -0.0934E-02 -0.0934E-02 -1.7994E-08 -1.7994E-08 -2.7632E-08 -2.36408E-08 -2.7632E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -3.5093E-08 -5	0. -1.2879E-02 6.6764E-02 -1.9203E-01 -1.6234E-01 -1.6234E-01 -1.6234E-01 -2.2534E-01 -3.1113E-01 2.2534E-01 5.3374E-01 2.8975E-03 1.0945E-01 2.9765E-08 2.9745E-08 2.9745E-08 2.9745E-08 2.0172E-07 4.2004E-08 5.1110E-08	0. 34545-03 -3.59945-02 -3.59945-02 -3.59945-02 -2.49285-01 -2.49285-01 -2.49285-01 -3.57135-01 -5.94045-03 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.88705-01 -5.48705-01 -5.48705-01 -5.48705-01 -5.48705-01 -5.48705-01 -5.48705-01 -5.48705-01 -5.48705-01 -5.48705-01 -5.48705-01 -5.48705-01 -5.48705-01 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HAT	RIX T G	AMMA = .700	N MAX	= 10		TIME ≈ 2.	224 S		SIN	GLE PRECISION
LM	0	1	2	3	4	5	6	7	8	9
0 12 34 56 67 89 90 111 112 113 145 167 18 190 20	1.0000E+00 4.6667E-01 1.032E-01 1.032E-01 5.5210E-03 7.7240E-03 7.7240E-04 1.6315E-03 7.6895E-03 1.5205E-04 1.22503E-04 1.3255E-03 1.5165E-03 1.5165E-03 1.5165E-03 -4.6383E-03 -5.1514E-03	0. 7.0640E-01 7.1054E-01 3.3580E-01 7.7695E-02 3.5232E-04 -4.5226E-03 3.5232E-04 -4.5226E-03 3.2153E-03 -3.7345E-04 1.5914E-03 -3.039E-03 1.6616E-03 2.0997E-03 1.6616E-03 2.0997E-03 -8.4611E-04 -1.0807E-03 -8.4611E-04 -1.0807E-03 -9.5739E-03 -1.3843E-02	0. -2.7067E-01 -3.4365E-01 7.4306E-01 5.66115E-01 2.4158E-01 5.66115E-01 2.4158E-01 7.0843E-03 2.3567E-03 2.3577E-03 -3.6232E-03 -3.6232E-03 -3.6232E-03 -3.6232E-03 -3.6232E-03 -3.6232E-03 -3.6232E-03 -3.464E-02 -1.4674E-02	0. 1.6061E-01 -2.9202E-01 5.5507E-01 6.8964E-01 1.5882E-01 1.5882E-01 1.5882E-01 1.5882E-01 -5.0274E-03 3.9411E-02 -5.0274E-03 -7.5938E-03 -1.0221E-02 -1.6221E-02 -1.8241E-02 -1.8231E-02 -1.8231E-02	$\begin{array}{c} 0, \\ -1, 0432 {\mbox{-}01} \\ 2, 3534 {\mbox{-}01} \\ -2, 3534 {\mbox{-}01} \\ -2, 3534 {\mbox{-}01} \\ -2, 3632 {\mbox{-}01} \\ 6, 34532 {\mbox{-}01} \\ 6, 34532 {\mbox{-}01} \\ 3, 2384 {\mbox{-}01} \\ 3, 2384 {\mbox{-}01} \\ 1, 2767 {\mbox{-}01} \\ 1, 2767 {\mbox{-}01} \\ -1, 2561 {\mbox{-}02} \\ -1, 526 {\mbox{-}02} \\ -1, 5226 {\mbox{-}02} \\ -1, 5226 {\mbox{-}02} \\ -2, 5254 {\mbox{-}02} \\ -2, 5374 {\mbox{-}02} \\ $	0. 7.0039E-02 -1.8394E-01 1.9078E-01 6.8049E-02 -7.9463E-02 4.1775E-01 5.0068E-01 5.0068E-01 5.0068E-01 -2.5556E-01 6.8408E-03 -2.0321E-02 -1.3337E-02 -1.3337E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 -2.3676E-02 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-3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02 -3.3121E-02	0. -2.2684E-02 -7.8862E-02 -1.4798E-01 -1.4798E-01 -2.2870E-03 -2.0277E-01 -1.045E-01 1.6407E-01 -1.3703E-01 -3.2775E-01 -4.8888E-03 -3.2775E-01 -4.4868E-01 2.4037E-01 -7.3299E-03 -7.3299E-03 -2.8993E-02 -3.5362E-02 -3.5362E-02 -3.5774E-02	0. 1.5723E-02 5.7295-02 1.8822E-01 -1.6658E-01 5.5271E-02 1.1667E-01 1.167E-01 1.167E-01 1.22.0440-01 2.0440-02 1.8028E-01 5.56027E-02 -2.9889E-01 5.56027E-02 5.6089F-01 5.3623E-01 1.738E-01 1.738E-01 1.738E-02 -3.7984E-02 -3.7984E-02
LM	10	11	12	13	14	15	16	17	18	19
01234567890111234567890	$\begin{array}{c} 0.\\ -1.0922E-02\\ 3.8040E-02\\ -1.0316E-02\\ 1.3592E-01\\ -1.1747E-01\\ 1.3592E-01\\ -1.6614E-01\\ -1.6644E-01\\ -1.6682E-02\\ 1.8925E-01\\ -3.2559E-01\\ -3.2559E-02\\ -3.2559E-01\\ -3.2559E-02\\ -3.2559E-02\\ -3.2559E-01\\ -3.2559E-02\\ -3.2559E-02$	0. 7.5989E-03 -3.2420E-02 6.9024E-02 -1.3741E-01 1.1418E-01 1.3401E-02 -1.5822E-01 1.3402E-02 -1.5822E-01 1.3402E-02 -1.8471E-01 -2.9856E-01 4.5365E-02 4.5365E-02 4.5365E-02 2.2617E-01 2.2617E-01	0. -5.2926E-03 1.8971E-02 -6.1906E-02 1.0087E-01 -1.4189E-01 4.8853E-02 6.7226E-02 -1.9013E-01 3.4485E-02 1.0477E-01 -1.0247E-01 1.0477E-01 -1.18397E-01 1.8493E-01 4.6177E-01 5.0175E-01	0. 3.6894E-03 1.2418E-02 4.2683E-02 9.3484E-02 1.1677E-01 1.3228E-01 -1.4619E-01 1.3228E-01 -1.4419E-01 1.3228E-01 -2.2589E-01 2.5143E-02 1.6618E-01 8.6742E-02 2.3463E-01 -6.2429E-02 2.9467E-01	0. -2:5735E-03 8:3397E-03 -2:9321E-02 -1:1487E-01 1:0260E-01 -3:3220E-02 -1:2691E-01 -1:2691E-01 -1:2691E-01 -1:2491E-01 -2:2171E-02 -2:2171E-02 -2:2171E-02 -3:228E-01 -2:5759E-01	0. 1.7941E-03 5.6675E-03 2.0082E-02 1.0168E-01 1.1270E-01 5.3423E-02 -1.4270E-01 5.3423E-02 -1.4270E-01 5.3423E-02 -1.3291E-01 -9.2099E-02 1.3493E-01 -1.5259E-01 1.1336E-01 -1.9308E-01	0. -1.2540E-03 .8783E-03 -1.3707E-02 -4.0696E-02 -8.4446E-02 -8.4446E-02 -1.1306E-01 -7.9147E-02 1.2244E-01 -1.4911E-01 -1.4911E-01 -1.4945E-02 -1.326E-02 -1.326E-02 -1.326E-02 1.8519E-01 1.8519E-01	U. 8.7579E-04. 9.3366E-03 9.3366E-03 9.3366E-03 9.3366E-03 6.7337E-02 1.0467E-01 9.6828E-02 1.0467E-01 9.6828E-02 1.7337E-02 -7.6613E-02 -7.6613E-02 -7.6613E-02 -7.6613E-02 -7.662E-01 1.4645E-01 -7.462E-01 -7.462E-01 -7.2396E-01 -7.4527E-02 -1.393E-01 -1.3193E-01 -1.3193E-01	0. -6.1183E-04 1.8386E-03 -6.3379E-03 -7.1952E-02 -7.1952E-02 -7.1952E-02 -1.0366E-01 -1.0366E-01 -1.3346E-01 1.5488E-02 -1.3346E-01 1.5488E-02 -1.1589E-01 -1.1588E-01 -1.1588E-01 -1.1588E-01 -1.1588E-02 -1.120E-01 -1.1588E-02 -1.120E-01 -1.1588E-02 -1.120E-01 -1.2667E-01	0. 4.2752E-04 4.2727E-03 4.3227E-03 3.9226E-02 7.6653E-02 1.0233E-01 1.0525E-02 1.0552E-02 1.0552E-02 4.5244E-02 8.4497E-02 7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3338E-02 -7.3340E-02 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03 -7.5407E-03
MATE L N	RIX A (H2-H	1)/M1 G/ 1	A <b>HH</b> A = .700 2	3	4	5	6	7	8	9
01234567890112345678901112314567890	0. 7.6130E-15 5.3562E-05 6.3045E-02 7.7240E-04 1.6315E-02 7.7240E-04 1.6315E-02 7.7250E-00 1.5836E-01 1.5836E-01 1.5836E-01 1.5836E-01 1.5836E-01 1.5836E-02 7.7353E-02 7.7353E-04 1.00394E-00 7.7353E-03 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 1.2113E+07 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7.9591E+00 -3.7344E-04 3.9460E+01 -3.3049E-03 4.3688E+03 2.9642E+03 4.3688E+03 2.9642E+03 4.3648E+03 2.9642E+04 1.0990E+04 -2.6442E+03 6.7197E+06	0. 6.5629E-15 1.0884E-04 5.0702E-04 2.7633E-03 1.6864E-02 2.7633E-03 1.6845E-02 1.2940E-01 7.0843E-03 1.458E+01 4.533E-03 3.3577E-03 3.3577E-03 3.3377E-03 2.330E+05 1.7421E+05 -1.1957E-02 1.3937E+06	0. 2.2120E-14 2.4088E-04 2.1185E-03 8.2339E-03 1.9717E-02 4.9877E-02 4.9877E-02 1.8248E-01 -5.0274E-03 1.8248E-01 -5.0274E-03 5.0371E-03 5.0371E-03 6.4329E-03 8.8251E-04 1.5052E-02 8.8251E-04 -1.6323E-02 6.4542E+05	0. 4.2568E-15 5.2265E-04 7.2028E-03 1.3652E-02 1.3652E-02 1.5333E-02 1.5333E-02 1.5333E-02 1.5333E-02 1.5333E-02 2.4362E-02 2.4362E-02 2.9300E-04 1.3671E+01 -5.0548E-02 2.22568E-02 2.22568E-02 2.22568E-02 2.2142E+04 2.2142E+04 2.2142E+04 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 2.1120E+05 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6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.3090E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.300E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 6.3.200E-06 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-4,9031\pm05\\ \end{array}$	$\begin{array}{c} 0,\\ -0.039E-02\\ -1.8414E-01\\ 1.9235E-01\\ 6.3013E-02\\ -2.9265E-01\\ -8.9587E-02\\ -4.2700E-01\\ 5.1333E-01\\ -5.5726E-01\\ 5.1333E-01\\ -5.5726E-01\\ -5.5732E-02\\ -4.7062E-04\\ -5.5719E-05\\ -5.4063E-05\\ -5.4063E-05\\ -5.638E-05\\ -5.638E-$	0. -4.7752E-02 1.4121E-01 -1.9597E-01 4.60292E-02 2.0341E-01 -1.5503E-01 -2.7843E-01 -1.968E-01 -2.7843E-01 -2.787E-05 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 -3.9228E-04 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20	3.10030-01	4.33572-01								
20 MATR	IX A (H2-H	1)/H1 G	UMA = .900	7						
20 HATR L. M	IX A (H2-H	1)/H1 G/	MMA = .900 2	3	4	5	6	7	8	9
20 HATR L M 0 1 2 3 4 5 6 7 8 9 10 11 12 13 4 5 6 7 8 9 10 11 12 13 14 15 6 7 18 19 20	3.1063E-01 IX A (H2-H 0 0. 1.72251-03 1.7257E-03 1.3597E-03 1.3597E-03 1.3597E-03 1.3597E-03 1.3597E-03 1.2544E-03 5.7438E-01 2.5695E-03 3.1417E+00 2.7657E-03 1.9600E-02 2.0755E+03 1.9600E+02 2.0755E+03 1.9600E+02 2.0755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 1.9755E+03 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1.4432E+01 1.1676E-01 1.6300E-01 3.3541E-01 1.2222E+00 -9.4413E-02 1.1148E+01 7.0803E+01 7.0803E+01	8 0. 6.5070E-14 1.3001E-01 2.1302E-01 2.4599E-01 8.2700E-01 8.2700E-01 6.1437E-01 6.2188E-01 6.2188E-01 2.4728E-01 2.4728E-01 1.6728E-01 1.6728E-01 1.6728E+00 1.6403E+01	9 0. 1.9795E-13 1.9292E-01 1.3052E-00 2.0021E-01 7.6235E-01 1.5097E+00 4.8021E-01 7.6393E-01 1.5256E+00 1.5256E+00 2.5469E-01 1.5464E+00 2.54612E-01 2.6612E-01 2.6642E-01 1.9659E+00
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1.5559E-03 1	4.3037L 01 1)/M1 G/ 0. 0. 1.2610E-03 7.0404E-03 3.4762E-02 -2.5225E-03 1.0635E-02 2.3705E-01 1.0635E-02 2.3705E-01 1.0635E-02 2.3705E-01 1.0635E-02 2.3705E-01 1.0635E-02 2.5040E+01 4.8093E+00 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 2.5040E+01 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2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.0555E-02 2.	0. 1.4546E-02 5.9495E-02 2.8878E-01 2.8878E-01 1.4414E-01 1.4417E-01 1.4417E-01 1.4417E-01 1.4583E-01 1.5956E-01 7.8786E-02 9.7150E-02 9.7150E-02 9.7150E-02 3.5425E-01	0. 5.3849E-14 1.8671E-02 6.8747E-02 2.5332E-01 1.3974E-01 3.6650E-01 1.3974E-01 3.6650E-01 1.3938E-01 1.28538E-02 6.8538E-02 6.8538E-02 6.26747E-01 1.5648E-01 1.5648E-01 1.5648E-01	0. 3.7496E-15 2.4129E-02 7.9926E-02 2.3160E-01 1.4071E-01 2.9867E-01 3.7032E-01 1.0857E-01 1.6299E+00 1.7755E-02 2.6019E-01 2.9684E-01 4.2102E-01 3.2159E-01

The main result of these calculations is that, for small  $\gamma$ -values, despite the increase in N, i.e., a more accurate computation of the infinite sum in (4.1), the accuracy of certain elements does not improve. This phenomenon is once more clearly illustrated in Table 4.2.

**Table 4.2:** Limitation of accuracy improvement, when using (4.1) with single precision arithmetic on a CDC-7600, demonstrated by the matrix element  $T_{60}$  and for  $\gamma = 0.01$ .  $A_{60}$  is the accuracy defined in (4.4) and N is the upper summation index in (4.1).

N	5	10	15	25
A., 0	449.69	1.6136	1.6134	1.6134

The results given in this table suggest that a **double precision calculation** is necessary.

4.1.2.2 ON THE ROUND-OFF STABILITY OF THE RECURRENCE RELATION IN TERMS OF MATRIX ELEMENTS, (4.1).

To investigate the round-off stability of (4.1) we have repeated calculations given in **Table 4.1** applying **double precision arithmetic.** The corresponding results are given in **Table 4.3**.

**Table 4.3:** The matrix T calculated using (4.1) and **double precision arithmetic** plus the accuracy matrix A, (4.4), for various  $\gamma$ -values. Computer: CDC-7600. Cases treated:  $\gamma = 0.01$ , N = 5, 10, 15, 25;  $\gamma = 0.1$ , N = 10, 25, 35;  $\gamma = 0.4$ , N = 10, 25, 35;  $\gamma = 0.5$ , N = 10, 25;  $\gamma = 0.7$ , N = 10, 25;  $\gamma = 0.9$ , N = 10, 25.

MAT	RIX T G	.010 - AMMA	N MAX -	- 5		TIME =	.848 S		DOL	BLE PRECISION
LH	0	1	2	3	4	5	6	7	8	9
0123456789101111345617819120	$\begin{array}{c} 1.0000 E + 00\\ 6.6667 E - 03\\ 2.0000 E - 05\\ -5.4165 E - 10\\ 1.0685 E - 14\\ 4.6725 E - 10\\ -1.0488 E - 12\\ 4.6725 E - 11\\ 3.9686 E - 13\\ 5.3288 E - 13\\ 5.3288 E - 13\\ 5.3288 E - 13\\ 5.3760 E - 13\\ 5.3280 E - 13\\ 5.3760 E - 13\\ 5.3290 E - 13\\ 5.3280 E - 13\\ 5.3417 E - 13\\ 5.3681 E - 1$	0. 9.9994E-01 1.2000E-02 6.8571E-05 1.9048E-07 -1.1048E-12 6.1534E-11 -1.5654E-11 1.4896E-10 1.5554E-12 1.6066E-10 1.6060E-12 1.6068E-12 1.6252E-10 1.6068E-12 1.6252E-10	0. -6.6661E-03 9.9984E-01 1.7142E-02 1.4225E-04 6.9271E-07 1.4265E-04 6.9271E-07 1.44057E-10 2.3319E-12 2.6370E-10 2.6392E-10 2.6392E-10 2.6392E-12 2.6735E-10 2.6853E-12	0. 5.9994E-05 9.9945E-01 2.2219E-02 2.2219E-02 2.2219E-02 2.2219E-02 2.2219E-02 2.2219E-02 2.2219E-02 2.2219E-02 2.2217E-12 3.6066E-10 3.3306E-12 3.7347E-10 3.7625E-12 3.7820E-10 3.7525E-12 3.7968E-10	0. -5.7137E-07 1.3712E-04 -1.7138E-02 9.9949E-01 2.7266E-02 3.6708E-04 3.1328E-06 3.6708E-04 3.1328E-06 4.8139E-08 3.7173E-10 4.2986E-12 4.8772E-10 4.8328E-12 4.8772E-10 4.8258E-12	0. 5.5550E-09 -1.5235E-06 2.3304E-04 2.3304E-04 2.2214E-02 9.9924E-01 5.1600E-04 5.3207E-06 5.3207E-06 5.3207E-06 5.3255E-10 5.3255E-10 5.7528E-12 5.7528E-12 5.7558E-12 5.7558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5.9558E-12 5	C 	0. 5.3841E-13 5.3841E-13 5.3841E-10 3.6705E-08 5.2197E-06 5.1375E-04 7.3725E-02 9.9859E-01 4.2323E-02 8.9124E-04 4.2323E-02 8.9124E-04 1.2257E-05 1.2181E-07 7.9106E-10 7.9106E-10 8.0681E-10 8.0164E-12 8.1277E-10	0. 5.3328E-15 1.2436E-12 1.2436E-12 1.2436E-12 1.2436E-12 1.2436E-12 6.9598E-08 6.9598E-08 6.9598E-08 6.9598E-08 6.9883E-04 6.9883E-04 6.9883E-04 6.9883E-04 6.9883E-04 6.9883E-04 1.1559E-03 1.7254E-05 1.9431E-07 2.3080E-09 1.1055E-12 9.0853E-12 9.0853E-12	0. 5.2936E-17 1.1835E-14 3.3509E-12 1.1948E-05 8.8876E-04 1.2156E-05 8.8876E-04 4.2305E-02 9.9774E-01 5.2322E-02 1.3655E-03 2.9463E-07 2.9463E-07 2.9463E-07 9.96415E-12 1.0075E-09 9.6415E-12 1.0075E-09 9.24119E-12 1.0039E-11 1.0283E-09
LH	10	11	12	13	14	15	16	17	18	19
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0 12334567890 111123144517 11819 20	0. -5.2626E-19 2.1279E-16 -5.5716E-11 -1.6378E-09 -1.9195E-07 -1.7153E-05 -1.1135E-03 -4.7303E-02 9.9725E-01 5.7312E-02 9.9725E-01 5.7312E-02 9.9725E-01 5.7312E-02 9.9725E-01 1.6399E-02 3.0929E-05 4.2900E-07 4.6251E-09 3.9795E-11 2.7793E-13 2.4863E-16 -1.7096E-13	0. 5.2376E-21 5.2376E-21 6.2005E-13 2.1477E-11 2.8154E-09 2.9202E-07 -3.334E-05 -3.334E-05 -3.334E-05 -3.334E-05 -3.234E-02 9.9670E-01 1.9332E-03 9.9670E-01 1.9332E-03 9.9670E-01 -3.9855E-05 6.0428E-07 -1.1552E-09 6.8163E-11 1.5576E-16	0. -5.2169E-23 -5.2169E-23 -5.264E-15 -5.264E-15 -2.7176E-13 -3.9171E-11 -4.5624E-05 -3.9271E-02 -3.0224E-05 -5.7276E-02 -5.7276E-02 -5.7276E-02 -5.7276E-02 -5.7276E-02 -5.7276E-02 -5.7276E-02 -5.7376E-03 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 -5.0340E-05 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-3.727E$	$\begin{array}{c} 0.\\ 1346E-37\\ -1.5642E-34\\ 5.9032E-342\\ -2.1880E-29\\ -6.6574E-27\\ -3.2566E-24\\ -3.2566E-24\\ -3.2566E-24\\ -3.2566E-24\\ -3.2566E-24\\ -7.8657E-18\\ -7.8657E-18\\ -7.8657E-18\\ -7.8957E-18\\ -7.8957E-18\\ -7.99713E-06\\ -9.9713E-06\\ -1.3030E-04\\ -4.2517E-03\\ -9.9952E-01\\ -1.0195E-01\\ -1.0195E-$
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11 12 13 14 15 16 17 18 19 20	4.5074E-16 3.0650E+09 4.4276E-16 4.3126E+16 7.0196E+18 7.3113T-16 7.3113T-16 1.7982E+24 -1.4256E-16 8.2395E+28 -2.9939E-16 3.3453E+33	1.9656E-14 3.8834E+06 7.4213E-15 1.0280E+10 1.3767E-14 3.0081E+15 3.3818E+20 -3.9850E-14 1.1301E+25 -3.8099E-14 8.4110E+29	1.8075-106 4.8114E-16 4.9514E+04 6.7084E-16 3.6922E+09 1.6336E-15 8.8679E+14 -2.1566E-16 5.1104E+19 7.2999E-16 3.3602E+24 -1.4044E-15 1.4384E+29	5.2946E-06 2.5079F-15 7.7237E+00 8.5979E-15 2.1254E+06 -3.9498E-14 5.9175E+10 -6.6687E-14 2.5814E+15 -6.8481E-14 4.6222E+19 -8.3030E-14 9.8335E+24	6.7333E-07 1.9175E-05 1.7387E-02 9.3363E-16 3.0387E+04 1.9047E-15 6.9204E+09 6.2564E-16 6.2564E-16 6.2836E+14 3.4840E+19 8.2730E-16 2.3575E+24	3.6218E-09 3.3385E-07 1.8316E-06 5.1388E-02 7.2585E-02 -4.9466E-14 2.0574E+05 -8.4823E-14 2.2494E+08 -1.0375E-13 1.2866E+15 -1.0690E-13 1.5344E+19	1,303E-08 3,154E-08 1,2599E-08 7,9603E-07 1,8214E-06 2,9928E-02 1,3724E-01 5,2222E+03 8,0548E-16 1,6759E+09 5,7032E-16 2,1064E+14 -2,2349E-15 1,5060E+19	4.7748E-07 1.4713E-07 6.2290E-08 2.8305E-08 7.1028E-07 1.9681E-06 1.6207E-02 8.2585E+03 1.1379E+04 1.1379E+04 2.0391E+18 4.0291E+14	2.4974E=07 7.9442E=07 2.4929E=07 1.0999E=07 5.3868E=08 5.4367E=07 1.6677E=06 8.6638E=03 2.5445E=02 4.3096E+02 1.1153E+03 3.1296E=16 3.7296E=16 3.6604E+13	1.0202-07 3.9668E-07 1.2471E-06 3.9618E-07 9.2233E-08 3.71968E-07 8.4929E-07 8.4929E-07 1.8202E-02 1.7844E+02 5.2152E+02 2.2706E+07 6.3884E+07
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MAT	RIX T G	AMMA = .010	N MAX	= 15		TIME =12.	.978 S		DOL	BLE PRECISION
LM	0	1	2	3	4	5	6	7	8	9
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 5 16 7 18 19 20	$\begin{array}{c} 1.00005+000\\ 6.6667E-003\\ 2.0000E-05\\ -5.4397E-17\\ -1.58775-10\\ -2.9738E-16\\ 3.7650E-15\\ -3.7744E-16\\ 4.5074E-16\\ -3.7650E-15\\ -3.377E-16\\ -3.337E-16\\ -3.337E-16\\ -3.337E-16\\ -3.337E-16\\ -1.3227E-14\\ -1.42256E-16\\ -1.3339E-14\\ -1.42256E-16\\ -1.3339E-14\\ -2.9939E-16\\ -1.2092E-14\\ \end{array}$	0. 9.9994E-01 1.2000E-02 6.8571E-05 1.9048E-07 -6.3753E-15 1.9326E-14 6.6181E-17 1.9656E-14 6.6181E-17 -7.4213E-15 6.6433E-17 -1.3767E-14 3.9106E-14 9.1851E-16 9.1851E-16 -3.9806E-14 9.1851E-16 -3.9806E-14 -3.9806E-14 -3.9806E-14 -3.9806E-14 -3.9806E-14 -3.9806E-14 -3.9806E-14 -3.9806E-14 -3.9806E-14 -3.9806E-14 -3.9806E-14 -3.9806E-14 -3.9806E-14 -3.9806E-14 -1.0731E-15	0. -6.6661E-03 9.9984E-01 1.7142E-02 1.4225E-04 6.9224E-07 1.428E-09 -2.8844E-16 1.428E-09 -2.8844E-16 -1.428E-09 -9.9228E-15 -7.5887E-15 -7.5887E-15 -7.5887E-15 -7.2999E-16 -4.4022E-14 -1.4022E-14 -1.4022E-14 -5.8109E-14	0. 9.9994E-05 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1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8687E-08 1.8647E-08 1.8647E-08 1.8647E-08 1.8647E-08 1.8647E-08 1.8647E-08 1.8647E-08 1.8647E-08 1.8647E-08 1.8647E-08 1.8646E-08 1.8646E-08 1.8646E-08 1.8646E-08 1.8646E-08 1.8646E-08 1.8646E-08 1.8646E-08 1.8646E-08 1.8646E-08 1.8646E-08 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.32 9.8395E .32 9.8395E .32 9.8395E .32 1.8413E .24 3.4249E .27 7.8460E .18 5.5560E .20 7.8869E .16 1.0592E .13 9.9171E .12 7.9472E .10 2.9713E .06 2.9713E .06 2.9712E .0712E .071
MATE	IX A (M2-M1	.)/M1 G/	AMMA = .010	7						
LM	0	1	2	3	4	5	6	7	8	9
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-3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 -3.9850E-14 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1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1.9047E-15 1	0. 9.9994E-15 4.0007E-09 1.3572E-08 3.8387E-08 3.8387E-08 3.8387E-08 3.8395E-02 3.8395E-02 4.9466E-14 5.1388E-09 5.1388E-02 5.1388E-02 7.2585E-02 -4.9466E-14 5.1388E-02 2.0474E+05 -8.4623E-14 2.2493E+08 -1.0375E-13 1.5344E+19	0. 9:9985E-15 3:9615E-09 1.2737E-08 7.9999E-08 1.887E-08 7.9999E-08 1.5545E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 1.2559E-08 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		AMMA = .100	N HAX	= 10		TIME = 4	.454 S		DOU	BLE PRECISION
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JHMA = .100           2           0.           9.2572E-15           2.8219E-08           9.2572E-15           2.8219E-08           9.5287E-08           6.1755E-13           7.50247E-10           2.8246E-11           3.7467E-11           4.7451E-12           2.6584E+00           -2.6584E+00           -2.6582E-11           1.3008E+12           -2.5522E-11           6.1254E+14           12	3 0. 9.3458E-17 7.2888E-08 2.4676E-15 6.8445E-08 3.2861E-08 3.2861E-08 6.2104E-08 6.2104E-08 6.2104E-08 6.2104E-08 6.2104E-08 1.9270E-02 1.9270E-02 1.8919E+01 -2.3505E+04 -3.2565E-10 2.2252E+09 -3.5665E-10 2.6450E+12 13	4 0. 2 4277E-15 7 1298E-08 2 9593E-14 2 9593E-14 9 7575E-03 6 5654E-08 7 8584E-07 7 22758E-03 1.0657E-03 1.0657E-03 1.0532E-11 2.8571E+00 2.4526E-11 9.8375E+11 9.8355E+11 9.8355E+11 9.8355E+11 9.8355E+11 9.8355E+11 9.8355E+11	5 0. 9.9:41E-15 9.9:41E-15 9.9:41E-15 1.8694E-13 8.4325E-06 8.3232E-07 8.3232E-07 9.7325E-08 4.2818E-07 5.2431E-07 3.3652E-04 4.2838E-07 3.9355E+00 -4.0677E-10 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	RIX T	GAMMA = .100	N MAX	= 25		TIME -53.	796 S		DOL	BLE PRECISIO
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1.7237E-0237E-024\\ 1.62237E-024\\ 6.7237E-024\\ 1.62245E-024\\ 6.7245E-024\\ 1.62245E-024\\ 1.62256E-13\\ 1.62256E-13\\ 1.62256E-13\\ 1.62256E-14\\ 1.62356E-14\\ 1.62356E-1$	0. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9	$\begin{array}{c} 0,\\ -5,6597E-04,\\ -3,503E-02\\ -1,6793E-01\\ -3,693E-01\\ -3,659E-02\\ -3,1052E-03\\ -3,1052E-03\\ -3,1052E-03\\ -3,1052E-03\\ -3,057E-05\\ -8,057E-05\\ $	$\begin{array}{c} 0.\\ 5.5017E-05\\ 5.5017E-07\\ 7.52049E-07\\ 7.52049E-07\\ 7.52049E-07\\ 7.52049E-07\\ 7.52049E-07\\ 7.52049E-07\\ 7.52049E-07\\ 7.52049E-07\\ 7.722E-07\\ 7.4722E-07\\ 7.472E-07\\ 7.472$	0. 4012E-06 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 4012E-07 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MATR	IX A (H2-H	1)/M1 G/	AMMA = .100	]	·····	E				
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2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2372E-05 2	NMMA         - ,400           2         -           0.         -           1.1192E-14         -           2.3333E-053         -           2.6525E-051         -           0.6225E-052         -           2.6525E-055         -           2.6525E-051         -           2.00724E-052         -           2.00724E-053         -           2.00724E-053         -           1.009054E-055         -           2.00724E-055         -           1.009054E-055         -           2.00724E-056         -           1.009054E-057         -           3.60952E-058         -           3.100952E-059         -           3.13052E-059         -           3.14945E-059         -           4.1138E+09         -	3 0. 1.7391E-15 20.480E-06 2.4047E-07 3.6447E-07 4.5882E-05 4.5882E-05 4.5882E-05 4.5882E-05 4.5882E-05 4.5882E-05 4.5882E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.0528E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 5.058E-05 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-7,4257\pm-08\\ -7,4257\pm-08\\ -7,4257\pm-07\\ -7,9171\pm-07\\ -5,2106\pm-07\\ -5,2106\pm-07\\ -5,2106\pm-07\\ -5,2106\pm-07\\ -1,2715\pm-07\\ -1,2715\pm-0,2725\pm-07\\ -1,2715\pm-0,2725\pm-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,2725+-0,272$	0. 2.9657E-08 3.9568E-06 -2.2882E-05 3.3568E-06 -2.2882E-05 -2.2882E-05 -2.2882E-05 -2.4512E-03 -2.4512E-03 -8.4596E-03 -2.4592E-03 -2.4592E-03 -2.4592E-03 -2.4592E-03 -2.4592E-01 -2.4592E-01 -2.3010E-01 1.5830E-01 2.3010E-01
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LH	10	11	12	13	14	15	16	17	18	19
01234567890112	0. 4.2890E-14 1.9285E-06 3.2945E-14 3.39295E-06 3.3510E-14 1.3827E-06 8.9944E-16 2.2356E-06 8.6331E-13 2.0744E-06 2.2719E-13	0. 3.9512E-14 1.9162E-06 7.9380E-15 3.6753E-06 2.1491E-14 2.2717E-05 1.0685E-13 2.0177E-05 1.0245E-12 1.7811E-06 8.4551E-14	0. 5.6625E-14 1.9053E-06 9.5715E-15 3.4811E-06 2.8536E-14 1.9347E-05 1.1767E-13 1.2148E-05 4.3634E-13 2.1066E-05 8.9194E-13	0. 5.2208E-14 1.8957E-06 2.1702E-14 3.3280E-06 2.6015E-14 1.7045E-05 5.4588E-14 8.5357E-06 1.2728E-13 1.7018E-05 7.6066F-13	0. 6.8349E-14 1.8872E-06 3.4201E-14 3.2042E-06 2.7907E-14 1.5380E-05 9.0933E-14 6.5582E-06 6.5795E-14 7.09678E-06 7.9961E-13	0. 8.2801E-14 1.8796E-06 2.6266E-14 3.1020E-06 3.8079E-14 1.4124E-05 5.2451E-14 5.3161E-06 1.9267E-13 4.0779E-06 5.4212E-13	0. 7.8900E-14 1.8728E-06 4.1373E-14 3.0163E-06 5.7431E-15 1.3145E-05 4.1809E-14 4.4889E-06 2.2687E-13 2.7393E-06 5.7336E-14	0. 1.0390E-13 1.8667E-06 5.3497E-14 2.943E-06 6.0570E-15 1.7368E-15 3.9006E-06 6.6578E-14 2.0135E-06 1.7943E-13	0. 9.8637E-14 1.8611E-06 1.2468E-13 2.8805E-06 3.5193E-15 1.1719E-05 4.3508E-14 3.4636E-06 8.3905E-14 1.5713E-06 1.9220E-13	0. 1.769E-13 1.8561E-06 6.4087E-14 2.8258E-06 4.5013E-05 1.1186E-05 7.9353E-14 3.1280E-06 1.4618E-13 1.2797E-06 9.4112E-14

MAT	RIX T G	AMMA = .500	N MAX	= 10		TIME = 4	.452 S		DOL	BLE PRECISION
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012345678901112341567189011123415167189020	1.000E+00 3.3333E-01 5.1954E-02 2.0103E-07 7.5279E-00 2.1886E-05 6.5623E-05 1.1991E-04 1.3994E-04 1.3994E-04 4.1085E-05 4.2462E-05 1.6596E-04 4.2462E-05 1.3768E-04 4.3768E-04 -3.5438E-04 -3.5438E-04 -3.7114E-04	0. 5.5517E-01 1.7143E-01 2.5657E-02 2.5657E-02 2.5657E-02 2.5657E-02 2.5657E-02 2.5657E-02 2.5657E-02 2.5652E-02 3.6248E-04 -3.7855E-04 2.6462E-04 -3.0814E-04 2.1322E-05 2.1322E-05 2.1325E-04 -4.4285E-04 -4.4285E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 -5.6427E-04 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LM	10	11	12	13	14	15	16	17	18	19
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2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.1054E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 2.503E-02 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2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02 2.8454E-02

# TABLE 4.3

17.5	

_	11 1 0	AMMA = .500	N MAX =	- 25			770 S		DOL	BLE PRECISION
LM	0	1	2	3	4	5	6	7	8	9
D123456789011111314516678190	1.0006-00 3.3335-01 3.3335-01 -2.8410-15 -2.8410-15 -2.8410-15 -2.8410-15 -2.8410-15 -2.8404-06 -3146-12 1.3264-07 9.9685-11 -7.99155-09 -8.24785-10 -8.02785-10 -8.02785-10 -8.02785-10 -8.02785-10 -9.3.91016-09 -3.72295-09 -3.72295-09 -3.72295-09 -3.5205-09 -1.83635-09	0. 5.55717E-01 1.7143E-01 2.5651E-02 5.8015E-14 -5.4419E-04 -5.4419E-04 -5.4419E-04 -5.305E-12 -1.7830E-12 -1.7830E-12 -1.9795E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 9.7897E-09 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5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-022 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6293E-020 5.6295E-02005E-020 5.6295E-020 5.6295E-020 5.6295E-020 5.6295E-020 5	a 5314-1-15 5424-1-103 5424-1-103 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5424-1-10-12 5444-1-10-12 5444-1-10-12 5444-1-10-12 5444-1-10-12 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3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-01 3.097E-0	2 5162E-15 3 4888E-02 6 6126E-02 2 6213E-01 8 6165E-03 1.7793E-01 1.7806E-02 1.7413E-01 8.5599E-02 1.3792E-01 8.8711E-02 1.7641E-01 4.7193E-02 1.66519E-02 1.66519E-02 1.6451E-01 1.9479E+01 1.3775E+01
	1.2113E+07	6.7197E+06	1.9397E+06	6.45425705	2.11202-09		1,101/2.04	2.03572-03		
LM	1.2113E+07 10	6.7197E+06	1.9397E+06	13	14	15	16	17	18	19

# TABLE 4.3

7	E
1	Э

		GAMMA = .700	N MAX -	- 25		TIME =53.	.750 S		DOL	BLE PRECISION
LM	0	1	2	3	4	5	6	7	8	9
0 12 3 * 5 6 7 8 90 111 112 145 166 17 18 19 20	$\begin{array}{c} 1.0000 \pm 00\\ 4.66671 \pm 00\\ 4.66671 \pm 00\\ 9.5817 \pm 10\\ 9.5817 \pm 10\\ 3.6301 \pm 00\\ 3.6301 \pm 00\\ 4.3204 \pm 00\\ -5.84581 \pm 00\\ 3.630541 \pm 00\\ -8.38921 \pm 00\\ 4.3204 \pm 00\\ -8.38921 \pm 00\\ -7.52311 \pm 00\\ 5.7174 \pm 00\\ -7.52311 \pm 00\\ -7.5311 \pm 0$	0 0. 7.0600E-01 7.1052E-01 3.34600E-01 3.74620E-07 3.77452E-07 4.3.77452E-07 4.3.77452E-07 5.3.6238E-04 5.3.6238E-04 7.1372E-06 5.3.6238E-05 7.1372E-06 9.7181E-05 9.7181E-05 9.7461E-05 9.7181E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 9.7191E-05 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9.4191E-03 9.4191E-03 9.4191E-03 -7.1372E-06 3.0462E-01 -1.8432E-05 4.1757E+00 -2.0581E-05 1.5407E+03 -1.807E+05 5.1428E+03	JHHA = .700           2           0.           1.5431E-14           1.7352E-05           7.7258E-07           1.9616E-05           8.7672E-07           9.4438E-06           2.3593E-06           2.3593E-05           3.0312E-05           1.5176E+00           1.7624E-05           2.8534E-05           2.8534E-05           2.8514E-05           2.86648E+03	3 0. 8.3051E-15 1.7934E-05 3.2145E-07 1.8752E-05 2.1453E-05 2.1453E-05 2.1453E-05 2.1453E-05 2.1453E-05 2.1453E-05 2.1453E-05 2.1453E-05 2.1453E-05 2.1453E-05 2.1453E-05 2.648E+00 -7.755E-05 2.648E+00 -7.755E-05 2.648E+00 -7.755E-05 2.648E+00 -7.755E-05 2.648E+00 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 -7.755E-05 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67 89 10 11 13 145 16 17 18 19 20	1)2344E-03 5,7438E-01 -2,5898E-03 6,0772E-01 4,5489E-03 3,1417E+04 2,7617E+01 -8,7211E-04 2,7617E+01 1,960E+02 2,0785E+02 2,0785E+02 2,0785E+02 2,0785E+02 2,0785E+02 2,3707E+03	1. 4762E-02 -2. 5225E-03 2. 3705E-03 2. 3705E-03 1. 0636E-02 4. 8093E-00 1. 4581E-02 4. 5040E+01 4. 5273E-02 2. 5040E+01 4. 5273E+02 2. 5340E+01 4. 5273E+02 2. 33425E+02 2. 34425E+02 2. 34425E+0205E+0205E+0205E+0205E+0205E+020	1.4121E-02 9.8010E-03 6.6145E-02 -1.2152E-02 -1.2152E-02 1.4961E+00 -6.2602E-04 2.602E-04 2.602E-04 2.0256E+02 9.2475E-03 1.8409E+02 -1.8847E-02 1.9509E+03	9, (294:-02 8, 3420:-03 1, 8497:-02 4, 1994:-02 4, 6076:-02 -9, 3281:-03 4, 7508:-01 1, 7733:-02 7, 8199:+00 2, 3972:-02 1, 2886:+01 1, 1244:-03 7, 0046:+01 -2, 6592:E-02 1, 9477:+02 1, 0891:+03	3:3488E-02 7:8074E-02 5:802E-03 3:8064E-02 3:8064E-02 8:064E-02 8:064E-02 8:064E-02 8:064E-02 8:064E-02 8:064E-02 8:064E-02 1:006E+01 1:006E+01 1:006E+01 1:006E+01 2:5249E+02 2:5249E+02 4:5529E+02 4:5529E+02	6:00/12:00 9:3493E-02 9:3493E-02 7:7170E-03 1:7416E-02 7:4472E-02 4:2189E-02 7:4472E-02 4:2189E-02 4:2189E-02 4:2189E-02 5:0866E-02 3:0071E+01 5:2556E-02 4:3757E+02	1.35522 1.3422E-01 1.4422E-01 1.4422E-01 3.4582E-012 3.4582E-012 3.4582E-012 3.4582E-012 3.4582E-012 3.4582E-012 7.15545E-01 7.15545E-02 7.65588E+00 7.5711E-02 5.2068E+01 1.2705E+02 1.2705E+02	2.2225E-01 .6495E-01 .0038E-01 4.2062E-01 1.8902E-01 1.8902E-01 1.432E+02 1.8502E-01 1.4576E-01 1.1676E-01 1.2232E+00 -9.4413E-02 .1148E+01 .2232E+00 -9.4413E-02 .1148E+01 .2232E+00 -9.4413E-02 .1148E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+01 .2003E+0	2.1102E-01 2.4599E-01 4.4191E-01 8.2700E-01 5.7425E-01 9.1447E-01 6.2138E-01 2.0470E-00 2.2878E-01 1.6779E-01 2.1780E-01 2.1780E-01 1.6798E-00 1.6403E+01 1.6403E+01	2.0221E-01 1.5097E+00 4.8021E-01 3.4770E+00 7.6393E-01 2.1923E+00 8.5814E-01 1.5256E+00 2.5407E-01 0.24407E-01 2.0355E-01 2.6612E-01 1.9659E+00
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LM	0	1	2	3	4	5	6	7	8	9
0123456789011113145167 111113145167 118190	1.0000E+00 6.0000E+01 1.8937E+01 4.1971E+05 1.9810E+02 3.1011E+04 3.69022+03 4.1671E+04 5.3270E+04 5.3270E+04 5.3270E+04 5.3270E+04 4.6238E+04 -2.1824E+04 4.6238E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 2.26134E+04 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5.7696E-04 4.6686E-03 5.7696E-04 4.6686E-03 5.7696E-04 4.6686E-03 5.7696E-04 4.6686E-03 5.7696E-04 4.6686E-03 5.7696E-04 4.6686E-03 5.7696E-04 4.6686E-03 5.7696E-04 4.6686E-03 5.7696E-04 4.6686E-03 5.7696E-04 4.6686E-03 5.7696E-04 4.6686E-03 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5.7696E-04 5	0. -9.4486E-02 8.0674E-02 1.0273E-01 -1.4434E-01 -1.4430E-01 -2.2932E-01 6.5505E-01 4.1141E-01 1.2942E-01 -5.6954E-03 -1.27028E-04 -1.3770E-02 -5.6954E-03 -1.2725E-04 -2.2525E-04 -2.4023E-03 -2.4023E-03 -2.4023E-03 -2.4023E-03 -2.4023E-03 -2.4023E-03 -2.4023E-03 -2.4023E-04 -1.1940E-03	0. 8.339E-02 -5.6044E-02 -5.6044E-02 -1.3155E-01 4.9091E-02 -1.8700E-01 -1.2795E-01 3.1170E-01 3.1170E-01 3.1170E-01 3.1170E-01 3.1170E-01 3.1170E-02 -2.5784E-03 3.6604E-03 3.6604E-03 3.6604E-03 3.6604E-03 3.6604E-03 3.6604E-03 3.6604E-03 3.6604E-03 3.6604E-03 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-1.222E-03 -6.4655E-03 -1.222E-03 -6.4655E-03 -1.222E-03 -6.4655E-03 -1.222E-03 -6.4655E-03 -1.222E-03 -6.4655E-03 -1.222E-03 -6.4655E-03 -1.222E-03 -6.4655E-03 -1.222E-03 -6.4655E-03 -1.222E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 -6.4655E-03 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5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512E-01 5.4512	0. 4.5253E-G? -3889E-02 2.4716E-02 6.6642E-02 -7.4310E-02 -3.4663E-02 -3.4663E-02 -3.4663E-02 -3.4674E-02 -1.4772E-01 -3.4474E-02 -1.4748E-01 -2.0746E-01 -1.2748E-01 -5.3113E-01 -6.7472E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 -5.3113E-01 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LM	10	11	12	13	14	15	16	17	18	19
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MATE				-						
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2.0352E-03           3.6302E-02           3.736E-04           1.756E-03           1.7395E-04           1.7395E-04           3.733E-04           1.7395E-04           9.6196E-04           9.6197E-03           3.866E+01           9.0473E+01           9.0473E+01	3 0. 3.0000E-14 5.8969E-04 1.5675E-03 6.7435E-03 3.4818E-03 4.2385E-03 7.2032E-03 7.2032E-03 7.2032E-03 9.8411E-04 6.4754E-02 9.8411E-04 6.456E-04 7.665E+00 2.3037E-03 5.8252E+00 6.8207E+01 6.8907E+01 13	4 0. 2.3066E-14 7.4833E-04 3.8957E-03 9.2181E-03 1.6620E-02 1.6649E-02 5.3449E-03 1.7848E-03 2.3244E-03 1.7848E-03 2.3244E-03 1.75288E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 5.7028E-02 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From Table 4.3 we can draw the following essential conclusions:

Firstly, (4.1) is single precision round-off unstable for small  $\gamma$ -values; that is for some typical cases demonstrated in Table 4.4.

**Table 4.4:** Single precision round-off instability of (4.1) demonstrated with the aid of some typical cases; A is the accuracy matrix defined in (4.4). N = 25 (N is the upper summation index of (4.1)). CDC-7600.

Precision	$\gamma = 0.01 ; A_{s,s}$	$\gamma = 0.1$ ; A ₁₉ ,
single	7.3888E-04	3.0984
double	5.2946E-06	0.3127

**Secondly**, any attempt to improve the accuracy of certain matrix elements is doomed to failure, meaning that, despite an increase in N and a double precision calculation, the accuracy is not improved. That is demonstrated in **Table 4.5** for  $t_{1,\varphi}$  element  $T_{3,\varphi}$  and for  $\gamma = 0.01$ . The smaller  $\gamma$  is, the more apparent this phenomenon becomes.

**Table 4.5:** Example of failure of accuracy improvement when applying (4.1). A is the accuracy matrix defined in (4.4). N is the upper summation index of (4.1).

	$\gamma = 0.01 ; A_{*0}$						
Precision	5	10	15	25			
single	9.5333E+06	6.6883E+04	6.6883E+04	6.6883E+04			
double	9.6463E+06	2.7058E+05	2.7058E+05	2.7058E+05			

Thirdly, in order to reach a given relative accuracy (if at all possible) of the matrix elements, the computational parameters N and word-length to be used depend on the  $\gamma$ -value. That is summarized in Table 4.6.

Turning from the accuracy comparison, we next consider the execution times of the two methods concerned.

**Table 4.6:** Computational parameters, N (upper summation index of (4.1)) and word-length, needed when calculating the matrix elements to a given relative accuracy.

	Dimension of matrix T: (21,21); CDC-7600. Relative error of matrix elements = 10 ⁻⁴								
γ	0.01	0.1	0.4	0.5	0.7	0.9			
N	15 1)	35 1)	35	50	50	50			
Precision	double	double	double	single	single	single			

¹⁾ Any attempt to reach the accuracy desired for this  $\gamma$ -value is **doomed to failure.** 

### 4.1.2.3 COMPARISON OF THE COMPUTATIONAL TIME.

A reasonable comparison of the computational times of the two methods concerned must, of course, be based on a comparable accuracy of calculations. In our case we have fixed the relative accuracy of the matrix elements to the value 10⁻⁴, which is sufficient for current applications.

The computational parameters needed to reach such an accuracy using (4.1) are presented in **Table 4.6**. In applying them, we have compared the computational time required when using the recurrence formula (4.1) with that needed when using the Taylor series method. The results of this comparison are summarized in **Table 4.7**.

From this table we can draw the following conclusions:

- Equ.(4.1) fails for small γ-values.
- $\tau_{M2}$  depends only slightly on  $\gamma$ , whereas  $\tau_{M1}$  depends strongly on  $\gamma$ . The Taylor series method thus takes advantage of its adaptability-property and avoids wasteful computation.
- The Taylor series method is much superior in regard to execution efficiency.

**Table 4.7:** Computational times:  $\tau_{M2}$ ,  $\tau_{M1}$  for several  $\gamma$ -values.  $\tau_{M1}$  and  $\tau_{M2}$  designate CPU-time of the Taylor series method and the recurrence relation (4.1), respectively. Relative accuracy of the matrix elements is approximatively 10⁻⁴. Dimension of matrix (21,21). CDC-7600.

Quantity $\gamma$	0.01	0.1	0.4	0.5	0.7	0.9
τ _{M1} (sec)	0.014	0.023	0.040	0.045	0.070	0.220
τ _{M2} (sec)	Equ.(4.1) fails	Equ.(4.1) fails	140	184	184	184
$\tau_{M2}/\tau_{M1}$			3500	4100	2600	840

Finally, we present in **Figure 20** on page 181, for the sake of completeness, the execution time in dependence of N, i.e., the upper summation bound of (4.1).

From this figure one immediately sees that the computational time increases rapidly with increasing N.

We now turn our attention to comparing the Taylor series method with the method which in principle permits an exact evaluation of the matrix elements  $T_{\ell m}$ . In the following section we shall proceed along similar lines as in this section.

### 4.2 CLOSED-FORM REPRESENTATION OF THE ELEMENTS OF THE MATRIX T.

## 4.2.1 Short recapitulation of the formula.

The matrix elements in this representation [GE63,p.5] read:

$$T_{\ell m}(U) = \frac{2m+1}{1-e^{-U}} \sum_{\substack{j=0 \ k=0}}^{\lfloor \ell/2 \rfloor} \sum_{\substack{\ell=2j \ j=0 \ k=0}}^{\lfloor m/2 \rfloor} \sum_{\substack{j=0 \ k=0}}^{m-2i} \sum_{\substack{j=0 \ k=0}}^{\lfloor m/2 \rfloor} \sum_{\substack{\ell=0 \ k'=0}}^{\lfloor m-2i-k'} \sum_{\substack{j=0 \ k'=0}}^{\lfloor m-2i-k'} \sum_{\substack{j=0 \ k'=0}}^{\lfloor m-2i-k'} \sum_{\substack{\ell=0 \ \ell-2j-k/2 \ (1+e^{-U})k' \ \ell-2j \ (1-e^{-U})^{m-2i}}}^{\lfloor m-2i-k'} \frac{1-e^{-\nu U}}{\nu}$$
  
with  $\nu = 1 + \ell/2 - j - k + m - 2i - k'$ 



Figure 20. Execution time in dependence on N: Execution time in dependence on N (n = 0, 1, 2, ..., N) when using (4.1) for comptutation of the matrix elements T_{lm}; l, m = 0, 1, 2, ..., 20; CDC-7600, single precision.

$$P_{\ell}(\mu) = \sum_{j=0}^{\lfloor \ell/2 \rfloor} q_{\ell j} \mu^{\ell-2j} , \quad q_{\ell j} = \frac{(-1)^{j} (2\ell-2j)!}{2^{\ell} (\ell-j)! (\ell-2j)! j!} , \quad (4.6)$$

$$v = -\log \left(1 - \frac{2\gamma}{(1+\gamma)^2} \left(1 - \overline{\mu}\right)\right) , \quad U = 2 \log \left(\frac{1+\gamma}{1-\gamma}\right) = v_{\text{max}} , \quad (4.7)$$

$$\overline{\mu} = 1 - \frac{(1+\gamma)^2}{2\gamma} \left(1 - e^{-\nu}\right) , \quad \mu = \frac{1+\gamma}{2\gamma} e^{-\nu/2} - \frac{1-\gamma}{2\gamma} e^{\nu/2} ,$$

$$\overline{\mu} = \frac{2e^{-\nu} - 1 - e^{-U}}{1 - e^{-U}} , \quad \mu = \frac{e^{U/2} e^{-\nu/2} - e^{\nu/2}}{e^{U/2} - 1} .$$

Expression (4.5) does not contain any infinite sum and thus formally permits an exact evaluation of the matrix elements. However, (4.5) might be round-off unstable.

#### 4.2.2 Comparison with the Taylor series method.

Quite analogously to Subsection 4.1.2 all comparisons are made relative to the Taylor series method. **Our attention is here centered on:** 

- the round-off stability, and
- the execution time.

#### 4.2.2.1 ON THE ROUND-OFF STABILITY OF THE CLOSED FORM EXPRESSION, (4.5).

To study the round-off stability of (4.5) we carried out single and double precision runs for several  $\gamma$ -values. The results of this computations are given in **Table 4.8**. There, the matrix B (not dependent on  $\gamma$ ) gives the total number of summation terms involved and precedes the matrix  $T(\gamma)$  calculated with the aid of (4.5) and the accuracy-matrix  $A(\gamma)$  which is defined in a similar fashion to (4.4), i.e.,

$$A_{\ell m} = \frac{T_{\ell m, M3} - T_{\ell m, M1}}{T_{\ell m, M1}} \quad \text{for } T_{\ell m, M1} \neq 0 \qquad (4.8)$$
  
=  $T_{\ell m, M_3} \qquad \text{for } T_{\ell m, M1} = 0$ .

The subscripts M1 and M3 denote the Taylor series method and the method expressed by (4.5), respectively.

**Table 4.8:** The matrix B (not dependent on  $\gamma$ ) followed by the matrix T( $\gamma$ ) calculated with the aid of (4.5) using **single and double precision arithmetic** and the accuracy matrix A( $\gamma$ ), (4.8). Computer: CDC-7600. Cases trated:  $\gamma = 0.01, 0.1, 0.4, 0.5, 0.7$  and 0.9.

HAT	RIX B		TOTAL	NUMBER OF S	UNHATION TER	MS OF (4.5)				
LM	0	1	2	3	4	5	6	7	8	9
0 1 2 7 4 5 6 7 8 9 0 1 1 2 7 4 5 6 7 8 9 0 1 1 2 7 1 4 5 6 7 8 9 0 1 1 2 7 1 4 5 6 7 8 9 0 1 1 2 7 1 8 9 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 2 4 6 9 1260553362 429 564 281 9000 110 121	2 4 8 112 4 2 4 2 12 4 400 6 7 2 4 9 8 112 8 111	4 8 16 24 36 44 45 45 45 10 1224 45 8 10 224 2324 2324 2324 2356 2324 2356 2324 2356 2324 2356 2400 244 244 244 244 244 244 244 244 24	6 124 364 1254 1250 1250 1250 1250 1250 1250 1250 1250	9 136 55 1004 18250 18250 2724 3741 576 8 100 9999 9909 9909	12 24 70 1442 2400 3622 4504 556 567 568 5768 56720 10800 13252	16 324 944 1926 33200 4576 7896 4576 7896 4576 7896 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11	20 400 1200 2420 4000 7200 8400 7200 8400 11280 14420 18000 18000 22000 22000	25500 11525000 11525000 10525000 10525000 10525000 10525000 111111 1111222000 10525000 10525000 10525000 1111111111	30 600 1200 2700 3480 6750 1080 12470 1080 14470 19200 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 214800 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 21480 214800 214800 214800 2100000000000000000
LH	10	11	12	13	14	15	16	17	18	19
0123456789101123415678910112341567891011234	36 72 144 216 324 576 720 900 1080 1295 1512 1764 2016 2304 2592 2916 3240 3600 3960 4356	42 84 168 252 376 672 840 1050 1260 1512 1764 2058 2352 2352 2352 2352 2352 2352 2352 23	49 98 196 294 441 588 784 980 1225 1470 1470 1470 1470 1470 1470 2058 2401 2744 2058 3520 3522 4410 5390 5529	56 112 224 336 672 896 1120 1400 2016 2352 2744 31584 4032 4536 5640 6160 6160 6160	64 128 256 384 576 1024 1280 1600 1920 2304 2688 3135 3534 4096 4608 5184 5760 6400 7040	72 144 288 648 864 1152 1440 2160 2160 2160 2592 3024 4032 4608 5184 5184 5184 5184 5184 5184 5184 518	81 162 324 486 729 972 1296 1620 2025 2430 2916 3402 2916 3402 2916 35184 55184 55184 55184 55184 55184 55184 5519 7290 89100 89100	90 180 360 540 810 1080 1440 1800 2250 2700 3240 3780 4410 5040 5760 6480 7290 8100 9900 9900 10890	100 200 400 900 1200 2500 3000 4200 4200 4900 5600 6400 7200 8100 9000 11000 11000	110 220 440 660 990 1320 2750 2750 33960 4620 5390 6160 7040 7920 8910 9900 11000 12100

# TOTAL NUMBER OF SUMMATION TERMS OF (4.5)

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	<u>HJA I G</u>					TIME =23	.719 5		511	GLE PRECISION
LM	0	1	2	3	4	5	6	7	8	9
0 1 2 3 4 5 6 7 8 9 0 11 1 2 3 4 5 6 7 8 9 0 11 12 3 4 5 6 7 8 9 0 11 2 3 4 5 6 7 8 9 0 11 2 3 4 5 6 7 8 9 0 11 2 3 4 5 6 7 8 9 0 11 2 3 4 5 6 7 8 9 0 11 12 3 4 5 6 7 8 9 0 11 12 3 4 5 6 7 8 9 0 11 12 3 4 5 6 7 8 9 0 11 12 3 4 5 6 7 8 9 0 11 12 3 14 5 6 7 8 9 0 11 12 3 14 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.0000E+00 6.6667E-03 2.0001E-05 1.3131E-08 2.2801E-04 3.1581E-01 -3.7468E+00 -1.1037E+04 -5.7132E+05 3.1315E+08 -1.1117E+10 -1.1696E+13 8.6376E+14 3.9436E+14 -1.3791E+19 -1.6144E+22 1.0493E+24 4.2841E+26 -9.84430E+27 -1.6467E+31	2.1745E-12 9.9994E-01 1.2000E-02 5.9405E-05 2.4879E-03 1.7155E-01 -3.9882E+03 2.6704E+06 -1.2048E+07 -9.5511E+10 -9.5511E+10 -1.5587E+12 3.2559E+15 2.2379E+16 -1.4503E+21 4.4417E+24 4.4417E+24 -1.4670E+29 2.0770E+30 5.0950E+33	-1.0107E-09 -6.6662E-03 9.9986E-01 2.0001E-02 -6.1837E-01 -6.0565E+01 1.8701E+04 1.5242E+06 -6.4990E+08 -4.9753E+10 2.3094E+13 -7.4569E+17 -7.4569E+17 -7.55254E+19 2.5577E+22 B.8405E+23 -9.3146E+26 -4.5747E+28 3.2397E+31 -5.5337E+32 -1.3331E+36	2.8055E-07 8.9097E-05 1.5506E-02 3.4089E-01 1.1177E+02 1.6393E+04 -5.3563E+08 -3.7328E+06 -5.3563E+08 1.3358E+11 1.4749E+13 -4.2260E+17 1.61021E+20 1.6109E+22 -5.9842E+24 1.6109E+22 -5.9842E+24 1.1878E+29 1.1924E+31 -8.0022E+33 -8.6709E+35 2.5950E+38	-5.2662E-05 -6.0762E-03 7.4289E-01 1.2319E-02 -1.9077E+04 -4.0061E+06 6.9241E+08 1.1063E+11 -3.3436E+15 8.8274E+17 1.1683E+20 -3.1076E+22 -3.6395E+24 1.06773E+27 -3.6395E+24 1.0373E+27 -3.6395E+24 1.0373E+27 -3.6395E+24 1.32732E+27 -3.8431E+31 1.5246E+36 -5.3820E+40	8.8272E-03 1.2180E+00 -1.3270E+02 -2.6588E+04 9.2117E+08 4.5525E+16 4.5525E+17 -1.7535E+20 -2.5800E+22 5.55541E+24 9.3724E+25 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724E+26 9.3724	-9.3140E-01 -2.1281E-02 2.2656E+04 5.5105E+06 -5.8305E+08 -1.63312E+11 1.6337E+13 1.6337E+13 -1.6347E+13 -1.6347E+13 -3.8478E+22 2.8248E+22 2.8248E+22 2.8248E+22 -1.9295E+29 3.6278E+31 -1.9295E+29 3.6278E+31 -1.8174E+38 5.4995E+40 -1.8174E+38 5.4995E+40 -1.8174E+38 5.4995E+40 -1.8174E+38	$\begin{array}{c} 1.4487E+02\\ 3.7366E+04\\ -2.9649E+06\\ -8.696E+08\\ -8.696E+08\\ -3.3499E+15\\ -8.2983E+17\\ 1.2708E+20\\ 3.0395E+22\\ -4.8663E+24\\ -1.0110E+27\\ 1.7615E+29\\ -3.6449E+31\\ -7.2193E+33\\ .6449E+31\\ -7.2193E+33\\ .6448E+32\\ .6448E+$	-2.0896E+04 -6.4456E+06 3.2277E+08 5.5806E+11 -1.2419E+13 -5.2447E+15 5.9390E+17 -2.3595E+22 -5.7472E+24 -3.0535E+31 1.0557E+36 -3.25057E+38 -4.2888E+40 -6.464E+42 1.8017E+45 -2.9554E+47 -6.3614E+49	$\begin{array}{c} 3.0843 \pm 06 \\ 1.0546 \pm 09 \\ -6.8133 \pm 10 \\ -2.6477 \pm 13 \\ 1.2460 \pm 15 \\ 7.3034 \pm 17 \\ -2.4404 \pm 12 \\ 2.4435 \pm 12 \\ -2.4035 \pm 12 \\ 4.3340 \pm 12 \\ -2.9329 \pm 13 \\ 1.0757 \pm 34 \\ 1.0757 \pm 34 \\ 1.0757 \pm 34 \\ 1.0757 \pm 34 \\ -1.7692 \pm 433 \\ 1.0757 \pm 34 \\ -1.7692 \pm 433 \\ 1.0757 \pm 34 \\ -1.7692 \pm 433 \\ 1.0757 \pm 34 \\ -1.7692 \pm 440 \\ -3.3759 \pm 440 \\ 5.9626 \pm 422 \\ -1.9362 \pm 445 \\ -1.936 \pm 445 \\ -1.9362 \pm 445 \\ -1.936 \pm 445 \\ -1.936 \pm 445 \\ -1.936 \pm 445 \\ -1.936 \pm 44$
LM	10	11	12	13	14	15	16	17	18	19
0 1 2 3 4 5 6 7 8 9 10 11 12 3 4 5 6 7 8 9 10 11 2 3 4 5 6 7 8 9 10 11 2 3 4 5 6 7 8 9 10 11 2 3 4 5 6 7 8 9 10 11 2 3 4 5 6 6 7 8 9 10 11 12 3 4 5 6 6 7 8 9 10 11 12 3 13 4 5 6 6 7 8 9 10 11 11 12 3 11 11 11 11 11 11 11 11 11 11 11 11 1	9.3023E+08 -1.4224E+11 3.065E+12 3.0165E+12 3.0165E+22 4.1376E+24 4.1376E+24 4.1376E+24 4.2540E+30 5.8653E+30 5.8653E+35 5.7702E+32 6.91466E+457 -2.7241E+40 6.91466E+457 -2.7241E+40 6.91466E+457 -2.7241E+40 6.91466E+457 -2.7241E+40 6.91466E+457 -2.7241E+40 6.91466E+457 -2.7241E+40 1.00084E+54	$\begin{array}{c} 3.04431 \\ -1.38784 \\ -1.37884 \\ -1.37884 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ -2.437941 \\ 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7-6.357E+288 86.974E+288 86.974E+288 86.974E+287 7-1.35454E+447 7-1.55634E+447 7-1.55634E+447 7-1.55634E+447 7-1.55634E+447 7-2.57737E+514 86.9774E+317 8.5564E+447 7-2.57737E+514 8.55634E+447 7-2.57737E+514 8.55634E+447 7-2.57737E+514 8.55634E+450 8.57737E+514 8.57632E+50 8.77737E+514 8.57632E+50 8.77737E+514 8.57632E+50 8.77737E+514 8.57632E+50 8.77737E+514 8.57632E+50 8.77737E+514 8.57632E+50 8.77737E+514 8.57632E+50 8.77737E+514 8.57632E+50 8.77737E+514 8.57632E+50 8.77737E+514 8.57632E+50 8.77737E+514 8.57632E+50 8.77737E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 8.5774E+514 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-2.8826E+190 6.8966E490 2.0688E426 4.7339E426 3.3256E430 1.8836E+325 1.8836E+325 1.8836E+325 1.8836E+45 1.8836E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 1.8856E+45 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MATR L M 0 1 2 3 4 5 6 7 8 9 10 112 13 14 5 16 7 112 13 14 5 16 7 112 13 14 5 16 7 12 3 4 5 6 7 8 9 10 112 112 112 112 112 112 112 112 112	IIX         A         (M3-H1           0         4.2633E-140         3.0392E-100           1.3270E-058         6.69738+04         2.2801E-04           2.3131E-08         6.69738+04         2.2801E-04           2.32801E-04         7.468E+020         3.9440E+32           3.9440E+32         -1.1117E+100         7.23932+41           8.6376E+14         -1.3791E+13         9.1947E+60           -1.3791E+13         2.1947E+60         1.0493E+24           -2.5556E+78         4.5556E+78           10         10	1/M1 GA 1 2.1745E-12 7.66772E-10 6.4106E-06 1.3367E-01 1.3060E+04 1.7159E-01 1.3050E+04 1.7159E-01 1.3522E+23 -1.2048E+07 2.8068E+32 -2.2048E+07 -2.2379E+16 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.0381E+12 5.	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MATI	RIX A (M3-M	L)/M1 G/	UMMA = .010	<u> </u>						
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# TABLE 4.8

	MATE	IX T G	AMMA = .100				TIME =59.	024 5		DOU	BLE PRECISIO
	LM	0	1	2	3	4	5	6	7	8	9
	0 1 2 3 4 5 6 7 8 9 10 112 13 4 5 6 7 8 9 10 112 13 4 5 6 7 8 9 10 112 3 4 5 6 7 8 9 10 112 13 4 5 6 7 8 9 10 112 13 14 5 6 7 8 9 10 112 13 14 5 6 7 8 9 10 112 13 14 5 6 7 8 9 10 112 112 112 112 112 112 112 112 112	1.0000E+00 6.6667E-02 2.0029E-03 -3.9708E-26 2.55411E-24 2.3545E-09 -1.0984E-21 6.0489E-19 8.0535E-15 -2.2889E-16 1.5122E-14 1.5122E-14 1.5222E-14 1.5222E-14 1.5525E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2532E-09 -1.2552E-09 -1.2552E-09 -1.2552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 -1.552E-09 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6.955E-03 6.9619E-05 1.6180E-06 -1.9409E-14 -2.2991E-09 1.00952E-07 -1.1617E-05 -7.648E-04 -2.795E-07 -1.1617E-05 -7.648E-04 -2.785E-07 -1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 1.2486E-03 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MAT	RIX T G	AMPLA = .400				TIME =23.	.139 S		SI	GLE PRECISIO
LM	0	11	2	3	4	5	6	7	8	9
0123456	1.0000E+00 2.6667E-01 3.2774E-02 1.1315E-13 -4.4545E-04 7.3115E-13 1.1306E-05	2.6112E-14 9.0400E-01 4.5744E-01 1.0971E-01 1.2766E-01 1.0758E-11 -1.6399E-04	-1.3056E-13 -2.3010E-01 7.5986E-01 6.0038E-01 2.1559E-01 4.4329E-02 4.7153E-03	-8.5301E-13 8.1778E-02 -3.6577E-01 5.5976E-01 6.8082E-01 3.3537E-01 9.7858E-02	-8.6367E-12 -3.0986E-02 1.6752E-01 -4.3308E-01 3.3211E-01 6.9143E-01 4.5101E-01	5.0937E-11 1.2017E-02 -7.4546E-02 2.4978E-01 -4.3399E-01 1.0410E-01 6.3280E-01	-8.3915E-10 -4.7116E-03 3.2560E-02 -1.2951E-01 3.1446E-01 -3.7455E-01 -9.8301E-02	-1.8093E-09 1.8586E-03 -1.4036E-02 6.3454E-02 -1.8938E-01 3.4920E-01 -2.6777E-01	2.2884E-09 -7.3587E-04 5.9921E-03 -2.9998E-02 1.0381E-01 -2.4514E-01 3.4631E-01	1.4044E-07 2.9215E-04 -2.5402E-03 1.3833E-02 -5.3703E-02 1.5047E-01 -2.8744E-01
7 8 9 10 11 12 13	-1.6407E-11 -3.4612E-07 3.2176E-10 1.3800E-08 -6.5072E-11 -4.5518E-08 5.0232E-08	-6.5542E-11 4.0438E-06 1.3234E-09 -1.2818E-07 5.0134E-08 2.6837E-08 3.1431E-07	8.2074E-10 -5.4735E-05 -2.9206E-08 1.3613E-06 3.1224E-07 -3.1934E-06 -1.7907E-05	1.7823E-02 1.7488E-03 3.3151E-08 -1.8707E-05 -3.9441E-06 2.4934E-05 2.8652E-05	1.7220E-01 4.3337E-02 7.1496E-03 6.6437E-04 1.5636E-05 -2.9561E-04 -1.9180E-04	5.4445E-01 2.6175E-01 8.4091E-02 1.8801E-02 2.8630E-03 1.9690E-03 1.8639E-03	5.1414E-01 6.0014E-01 3.5705E-01 1.4118E-01 4.3182E-02 -4.3069E-03 -4.5332E-02	-2.5360E-01 3.5219E-01 6.0812E-01 4.4317E-01 1.9828E-01 1.4920E-01 3.6001E-01	-1.3193E-01 -3.4829E-01 1.6248E-01 5.9978E-01 6.5345E-01 -7.5969E-01 -4.9331E-01	3.0052E-01 1.4668E-02 -3.6285E-01 -1.5032E-01 3.8390E-01 6.0547E+00 9.2202E+00
14 15 16 17 18 19 20	1.7346E-06 -3.5847E-06 -2.6391E-05 8.7137E-06 8.1243E-04 9.4277E-04 -1.5607E-02	-1.3381E-05 -8.1615E-06 2.9507E-04 3.4172E-04 -5.6745E-03 -1.4578E-02 1.2469E-01	2.7745E-05 7.2421E-05 -1.1509E-03 -4.4468E-03 4.3627E-02 1.7143E-01 -1.2004E+00	-6.8514E-04 -2.1200E-03 1.4325E-02 6.1681E-02 -2.7950E-01 -1.4757E+00 1.0330E+01	5.2307E-03 1.0019E-02 -1.6122E-01 -4.6244E-01 3.0273E+00 5.5619E+00 -8.7264E+01	-2.6621E-02 -2.6701E-01 6.6213E-01 2.9578E+00 -2.4093E+01 -9.0066E+01 4.6166E+02	2.9439E-01 3.4413E-01 -3.9180E+01 -1.3310E+01 1.4808E+02 4.8033E+02 -3.6570E+03	-1.0287E+00 -6.5892E+00 7.6634E+00 1.5901E+02 -1.0723E+03 -5.2845E+03 3.4884E+04	1,9366E+01 -2.5640E+00 -9.2020E+01 -1,9423E+02 2.8430E+03 2.6734E+04 -2.4561E+05	-1.5074E+02 -1.6033E+02 3.7335E+03 8.4322E+03 -7.2085E+04 -1.4853E+05 1.7849E+06
LH	10	11	12	13	14	15	16	17	18	19
0112345	-1.2495E-07 -1.1867E-04 1.0765E-03 -6.2129E-03 2.6622E-02 -8.5633E-02	5.8204E-06 5.3646E-05 -4.9160E-04 2.9852E-03 -1.2612E-02 4.8954E-02	-3.7712E-05 -1.0851E-04 4.8616E-04 -1.6591E-04 -4.2509E-03 -7.5500E-02	6.3207E-05 -1.8222E-04 1.6086E-03 -1.2969E-02 7.3458E-02 2.9219E-01	-3.2782E-03 2.4847E-03 2.7658E-02 -1.8410E-02 -3.9143E-02 1.1873E-02	3.2193E-02 1.1984E-02 -2.5715E-01 3.6045E-01 3.8187E+00 -1.0784E+00	-1.8327E-01 -2.2621E-01 4.4693E-01 1.4746E+00 -1.0097E+01 1.1312E+02	6.1269E-01 -1.9853E-01 4.7180E+00 -1.9770E+01 -1.4344E+01 -2.1304E+02	-4.3353E+00 -2.1501E+01 :6.6517E-01 1.5109E+02 -3.1532E+02 6.9399E+03	-2.4777E+01 2.0949E+01 1.2388E+01 1.0201E+03 -8.4883E+02 -4.4028E+04
67 89 10 11 12	2.0217E-01 -2.9932E-01 1.8843E-01 -1.5257E-02 3.4890E-01 1.9072E+00 -4.7516E+01	-1.2165E-01 3.2396E-01 3.5726E-01 7.1711E-01 -6.8025E+00 2.1460E+00 2.6698E+02	2.9465E-01 -5.1153E-02 -3.4258E+00 -1.0403E+01 5.5699E+01 -8.1674E+01 -4.6428E+02	-5.3412E-01 2.0592E+00 1.8127E+01 -6.9568E+01 -5.1368E+02 1.8954E+03 8.7647E+03	3.1767E+00 -1.2170E+01 -1.3552E+02 -1.6184E+0? 3.2141E+03 -1.5140E+04 -6.6646E+04	-8.8934E+01 8.9215E+01 1.6064E+03 -1.3302E+03 -8.0870E+03 5.9623E+04 3.2242E+05	2.5605E+02 -2.5435E+03 -1.0025E+04 4.3030E+04 1.5185E+05 -1.1977E+06 -6.3871E+06	-2.20?1E+03 -8.0404E+03 8.2558E+05 1.8807E+05 -6.1849E+03 -3.4473E+05 1.0280E+07	3.54976+03 -1.3005E+05 2.1423E+05 1.6453E+06 8.7486E+06 -1.7394E+07 -2.0960E+08	1.5214E+04 2.1006E+05 -1.3466E+05 -4.3567E+06 -5.2399E+07 6.7146E+08 1.6286E+09
13 14 15 16 17 18 19	-3.4655E+01 6.6238E+02 1.8416E+03 -2.1532E+04 1.3513E+04 3.5384E+05 7.7364E+05	9.4880E+01 -4.3001E+03 -6.33999E+03 2.6351E+04 9.7467E+04 -1.1291E+06 7.6935E+06	1.6957E+03 -7.6649E+03 1.0397E+04 -7.6534E+05 1.1631E+06 1.2400E+07 -3.0752E+06	-4.6720E+03 -1.5723E+05 -1.2989E+05 4.1555E+06 -9.8274E+06 -4.5045E+07 2.0459E+08	3.7788E+05 2.9377E+06 ~2.9619E+06 -6.4556E+07 5.5432E+07 1.4413E+09 ~2.1472E+09	3.2716E+04 -4.1530E+06 3.7561E+07 1.7374E+08 -1.7882E+09 -7.3731E+09 2.1729E+10	1.4688E+07 3.7120E+07 -3.4105E+08 2.9181E+06 9.9623E+09 1.9156E+10 -1.4920E+11	-6.2653E+07 -3.1363E+07 9.2824E+08 1.1993E+10 -8.9688E+10 -3.1341E+10 2.2907E+12	1.7791E+09 2.0391E+09 -2.5986E+10 1.7193E+10 8.1990E+11 1.9456E+12 -2.0542E+13	-1.3699E+10 -3.6382E+10 1.9516E+11 9.6686E+10 -2.4182E+12 -1.5354E+13 1.2073E+14
20	-1.3255E+07	7.085555+07	-3.09921708	9.07812+08	~1.03802+10	2.29092+11	-1.2032E+12	1.07562+13	-0.87/62+13	3.89032+14
MATE	IX A (M3-H1	.)/M1 GA	MHA = .400	<u> </u>						<u></u>
LM	0	1	2	3	4	5	6	7	8	9
01234	7.1054E~15 2.6645E~14 8.2573E~06 1.1315E~13 1.1303E~06	2.6112E-14 3.5370E-14 6.2947E-06 2.2262E-12 3.2311E-06	-1.3056E-13 2.6248E-13 2.0761E-06 1.8285E-12 1.1439E-05	-8.5301E-13 1.7122E-11 2.0680E-06 3.6863E-11 2.0061E-06	-8.6367E-12 2.0545E-10 2.0462E-06 5.3420E-11 2.1344E-06	5.0937E-11 2.7471E-10 2.0285E-06 6.3132E-09 1.0298E-05	-8.3915E-10 1.4783E-07 2.1073E-06 3.3135E-08 7.2050E-06	~1.8093E-09 1.4342E-06 3.0688E-06 1.4037E-06 7.3700E-06	2.2884E-09 4.3217E-05 2.3547E-05 2.6687E-05 2.5749E-05	1.4044E-07 4.0364E-04 4.9336E-04 2.1815E-04 3.1294E-04
5 6 7 8 9	7.3115E-13 5.6320E-06 -1.6407E-11 3.4369E-04 3.2176E-10	1.0758E-11 3.2681E-06 -6.5542E-11 5.6150E-05 1.3234E-09	4.7573E-10 5.3047E-06 8.2074E-10 1.4847E-04 -2.9206E-08	1.8739E-09 1.4231E-06 1.0327E-07 2.7642E-05 3.3151E-08	2.0390E-09 1.9436E-06 1.845BE-07 8.8508E-06 2.0990E-04	7.1709E-08 1.0175E-05 1.0615E-06 1.2215E-05 2.6953E-05	4.5321E-07 1.1795E-05 7.6536E-06 3.2396E-05 2.9497E-05	2.1780E-06 3.5586E-05 8.6104E-05 3.4156E-04 1.0082E-03	2.1786E-07 1.6096E-04 1.6589E-03 2.5860E-03 3.5226E-02	5.7538E-04 1.0149E-03 1.1085E-02 3.5079E-01 3.0473E-02
10 11 12 13	1.8984E-01 -6.5072E-11 1.0993E+02 5.0232E-08 1.1532E+05	5.4290E-02 5.0134E-08 5.6632E+00 3.1431E-07 9.4713E+04	6.7378E-02 3.1224E-07 8.5331E+01 -1.7907E-05 2.3217E+04	2.0257E-02 -3.9441E-06 6.1077E+01 2.8652E-05 6.1321E+04	1.6694E-02 1.5636E-05 4.6524E+01 -1.9180E-04 6.0878E+04	3.7376E-03 1.1731E-03 7.0068E+00 1.8639E-03 1.2446E+04	2.7671E-03 8.7097E-02 1.5305E+00 4.0480E+01 3.1608E+03	6.5128E-03 6.1870E-02 1.0707E+00 1.8649E+01 2.9829E+02	6.6393E-02 2.6658E-01 3.6131E+00 5.2137E+00 5.4306E+02	1.0617E+01 1.7997E-01 9.9097E+00 2.3840E+01 8.6604E+02
15 16 17 18 19	-3.5847E-06 4.6669E+07 8.7137E-06 3.7502E+10 9.4277E-04	-8.1615E-06 5.7343E+07 3.4172E-04 2.9482E+10 -1.4578E-02	7.2421E-05 2.7970E+07 -4.4468E-03 2.9524E+10 1.7143E-01	-2.1200E-03 4.0902E+07 6.1681E-02 2.3711E+10 -1.4757E+00	1.0019E-02 4.7348E+07 -4.6244E-01 2.9317E+10 5.5619E+00	-2.6701E-01 1.6011E+07 2.9578E+00 2.2907E+10 -9.0066E+01	3.4413E-01 5.2626E+06 -1.3310E+01 1.0922E+10 4.8033E+02	1.4331E+C+ 2.1626E+05 1.5901E+02 4.0927E+09 -5.2845E+03	3.0984E+02 6.2834E+04 1.0551E+06 2.0990E+08 2.6734E+04	2.5916E+03 2.1797E+05 2.2727E+06 1.1697E+08 2.0158E+09
20	1.00346+13	11	12	13	14	1.49622913	1.10992+13	17	18	19
0	-1.2495E-07	5.8204E-06	-3.7712E-05	6.3207E-05	-3.2782E-03	3.2193E-02	-1.8327E-01	6.1289E-01	-4.3353E+00	-2.4777E+01
1 2 3 4 5	2.2209E-02 6.5587E-03 8.4844E-03 3.8604E-03 6.0723E-03	1.6113E-01 9.6613E-02 6.6777E-02 2.3828E-02 7.2662E-02	4.8959E+00 1.5975E+00 8.6576E-01 1.6956E+00 2.2083E+00	2.5840E+01 2.1655E+01 2.4976E+01 2.6855E+01 2.3804E+01	8.5033E+02 8.5497E+02 7.7350E+01 3.1051E+01 3.0609F+00	1.0267E+04 1.9228E+04 3.5528E+03 6.4702E+03 3.9102E+02	4.8559E+05 8.0926E+04 3.3868E+04 3.8115E+04 8.6584E+04	1.06/5E+06 2.0726E+06 1.0626E+06 1.2164E+05 3.4960E+05	2.8954E+08 7.1015E+05 1.9084E+07 6.0514E+06 2.4691E+07	7.0640E+08 3.2191E+07 3.0388E+08 3.7096E+07 3.4290E+08
6 7 9	2.1802E-02 2.4832E-02 1.6858E-01 1.1090E+00	7.8402E-03 3.5215E-01 2.1957E+00 4.7564E+00	3.1582E+00 6.8632E-01 1.3753E+01 3.8882E+01	1.2709E+01 1.9248E+01 9.0727E+01 2.5048E+02	1.5296E+02 2.0303E+02 9.9515E+02 6.9015E+02	8.3810E+03 2.6685E+03 1.8815E+04 7.7484E+03	4.8051E+04 1.4077E+05 1.9799E+05 3.7382E+05	8.3911E+05 8.4702E+05 2.8681E+05 2.6001E+06	2.7917E+06 2.6696E+07 1.3540E+07 3.8029E+07	2.5043E+07 8.5696E+07 1.5918E+07 1.7508E+08
11 12 13 14	2.032/E+00 1.2261E+01 1.4292E+02 6.3467E+01 1.4934E+03	9.5758E+00 9.4590E+02 5.3204E+02 8.4072E+03	4.70552+03 2.8236E+02 3.5828E+03 4.9745E+03 4.5921E+05	1.9676E+04 2.9823E+04 1.7568E+06 4.6092E+05	1.3703E+05 3.6118E+05 1.5077E+06 2.3538E+07	2.6001E+02 2.1193E+07 1.3575E+05 2.4430E+07	4.6556E+06 3.7469E+07 1.8853E+08 1.4348E+08	1.5075E+06 4.2708E+07 6.5901E+08 2.0018E+08	9.7845E+07 8.6767E+08 8.7311E+09 1.7995E+11	5.3194E+08 5.3194E+09 7.9680E+09 5.7293E+10 2.4499E+11
15	7 6418F+03	7 7881F+04	2 4344E+N4	1.0022E+06	1.0285E+07	1.7201E+08	5.1153E+09	3.9247E+09	1.2334E+11	2.7534F+12

MATI	RIX T G	AMMA = .400				TIME =59.	.1 <b>12</b> S		DOL	BLE PRECISION
LM	C	1	2	3	4	5	6	7	8	9
0 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 6 7 8 9 0 1 1 2 3 4 5 6 6 7 8 9 0 1 1 2 3 4 5 6 6 7 8 9 0 1 1 2 3 4 5 6 6 7 8 9 0 1 1 1 2 3 4 5 6 7 8 9 0 1 1 1 2 3 4 5 1 1 1 1 2 3 4 5 1 1 1 1 1 2 3 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.0000E+00 2.6667E-01 3.2774E-02 1.8554E-26 1.1306E-05 -2.2883E-25 -2.2883E-25 -2.2883E-25 -3.4600E-07 8.4514E-25 -3.4600E-07 8.4514E-25 1.1598E-08 4.4277E-23 -4.1032E-10 1.50482E-11 -5.0982E-21 1.50482E-11 -5.0982E-21 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.65550E-13 -5.6550E-13 -5.6550E-13 -5.6550E-13 -5.6550E-13 -5.6550E-13 -5.6550E-13 -5.6550E-13 -5.6550E-13 -5.6550E-13 -5.6550E-13 -5.6550E-13 -5.6550E-13 -5.6550E-13 -5.6550E-13 -5.6550E-13 -5.6550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13 -5.550E-13	1.85546-28 9.0400E-01 1.0971E-01 1.2766E-02 -5.1209E-26 1.6399E-04 1.6676E-24 4.0436E-06 -2.6109E-24 4.0436E-06 -2.6109E-24 4.0476E-09 1.1608E-20 -1.4127E-10 -2.1049E-19 5.1456E-12 1.7467E-19 5.1456E-12 1.950E-13 1.2012E-16 8.5390E-15	-3.5562E-27 -2.3010E-01 6.0038E-01 6.0038E-01 2.1559E-01 4.4329E-02 7.2598E-02 4.4329E-02 7.2508E-24 7.5524E-24 1.5151E-21 1.2754E-06 1.5151E-21 1.2754E-06 1.5151E-21 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.2754E-06 1.27	1.0823E-26 8.1778E-02 3.6577E-01 5.5976E-01 3.3537E-01 3.3537E-01 1.7488E-03 6.0264E-22 1.7488E-03 6.0264E-22 -3.0262E-20 -3.0262E-20 -3.0262E-20 -3.0382E-16 -3.0325E-05 -3.0262E-20 -1.1337E-05 -3.0325E-05 -3.0262E-20 -3.0325E-05 -3.0262E-20 -3.0325E-05 -3.0262E-20 -3.0325E-05 -3.0262E-20 -3.0325E-05 -3.0262E-20 -3.0325E-05 -3.0262E-20 -3.0325E-05 -3.0262E-20 -3.0325E-05 -3.0262E-20 -3.0325E-05 -3.0262E-20 -3.0325E-05 -3.0262E-20 -3.0262E-20 -3.0325E-05 -3.0262E-20 -3.0262E-20 -3.0325E-05 -3.0262E-20 -3.0262E-20 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MATR	NIX A (M3-M)	.)/M1 GA	MMA = .400	<u> </u>						
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1.1376E-05	2.3241E-17 2.6209E-10 1.8798E-06 2.4775E-12 3.1020E-06 3.1020E-06 3.1020E-01 1.4124E-05 2.3660E-11 4.124E-05 2.3660E-11 4.0785E-06 3.0598E-07 1.8427E-08 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 1.5374E-05 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1.8552E+04 1.0359E+04 1.0359E+04 4.2135E+05 5.8564E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 5.2692E+06 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9.7406{\rm E}{\rm -02}\\ -3.1312{\rm F}{\rm -01}\\ 3.14952{\rm E}{\rm -01}\\ 3.7436{\rm E}{\rm -01}\\ 1.8409{\rm E}{\rm -01}\\ 1.8409{\rm E}{\rm -01}\\ 1.9896{\rm E}{\rm -02}\\ 4.3688{\rm E}{\rm -02}\\ 4.3688{\rm E}{\rm -02}\\ 4.3684{\rm E}{\rm -02}\\ 6.8623{\rm E}{\rm -04}\\ 6.83313{\rm E}{\rm -05}\\ \end{array}$
L h -	10	11	12	13	14	15	16	17	18	19
0 1 2 3 4 5 6 7 8 9 0 11 12 14 5 16 7 18 9 20	2.135E-22 -7.7321E-04 -3.619E-03 -2.3315E-02 -2.3315E-02 -2.3315E-02 -2.3315E-02 -2.3315E-02 -2.3315E-02 -1.6220E-01 -1.9384E-01 -3.3667E-01 -3.3667E-01 -9.9256E-02 -3.5160E-01 1.1783E-01 1.6742E-01 1.1783E-01 2.6742E-01 1.0784E-02 2.2859E-03	5:3242E-21 3:8456E-04 2:8102E-03 1:3047E-02 4:4097E-02 1:1110E-01 2:787E-01 2:20260E-01 2:787E-01 2:2057E-01 1:2048E-01 2:2957E-01 1:2048E-01 2:453E-01 2:453E-01 3:5540E-01 1:8240E-01 7:3362E-02 2:3537E-02	-5.3814E-20 -1.9146E-04 1.4669E-03 -7.2165E-03 2.6231E-02 -7.2730E-02 2.6231E-02 -7.2730E-02 1.5214E-01 -2.2595E-01 1.2711E-02 -2.3242E-01 1.2615E-01 -1.4845E-01 -1.4845E-01 -1.4845E-01 -1.4845E-01 -1.4845E-01 -1.4845E-01 -1.4845E-01 -1.5274E-01 5.2974E-01 2.5397E-01 1.2009E-01	-8.2568E-19 9.5383E-05 7.6308E-04 3.9542E-03 7.5317E-02 4.6042E-02 7.0741E-01 1.1825E-01 1.1525E-01 7.2391E-01 1.1526E-01 7.2395E-03 7.3174E-02 7.1994E-01 7.1994E-01 7.8995E-01 4.8875E-01 4.8875E-01 4.8875E-01	-2.9346E-18 -4.7545E-05 3.9581E-04 -7.1499E-03 3.9581E-04 -7.2499E-03 -2.8402E-02 -1.4406E-01 -1.9998E-01 2.83910E-02 -1.8765E-01 1.4078E-01 -2.28659E-01 1.4078E-01 1.4078E-01 -2.2903E-01 -2.29559E-01 -2.29559E-01 -2.3931E-01 5.0938E-01	1.8720E-18 2.3709E-05 -2.0479E-04 1.1613E-03 5.0074E-03 1.7163E-02 -4.7329E-02 1.0411E-01 2.1164E-01 -7.15518E-02 2.1406E-01 -7.4518E-02 2.3199E-01 -9.8296E-02 2.3199E-01 -1.2060E-01 2.5547E-01	-1.3390E-16 -1.1827E-05 1.0573E-04 -6.2375E-04 -6.2375E-04 -7.2039E-02 1.3738E-01 -1.0978E-02 1.3738E-01 -1.9799E-01 1.8716E-01 -4.9210E-02 2.4845E-01 1.8716E-01 1.8715E-02 2.5771E-01 1.0515E-02 2.5771E-01 1.0515E-02 2.5771E-01 -2.439E-01	-1.2753E-15 5.99017E-06 5.4481E-05 3.3342E-04 7.5706E-03 5.9749E-03 7.8693E-02 4.8193E-02 -1.8193E-02 -1.0114E-01 1.6725E-01 1.3745E-01 1.3145E-01 1.3145E-01 1.3139E-01 1.3139E-01 1.3139E-01 1.6767E-01 -1.758E-01	-4.3836E-15 -2:9456E-05 2:8025E-05 -1:7748E-04 8:6926E-04 -3:4593E-03 -1:1413E-02 -3:1378E-02 -1:3172E-01 -1:8771E-01 -1:8771E-01 -1:8771E-01 -1:924E-01 2:7319E-02 1:9258E-01 -1:9229E-01 1:9229E-01 2:3966E-01	-4.6718E-14 1.4704E-06 9.4122E-05 9.4122E-05 4.7797E-64 1.9825E-03 1.9979E-02 9.8481E-02 9.8481E-02 9.8481E-02 -1.5942E-01 1.9292E-01 1.9292E-01 1.4127E-01 -1.4127E-01 -1.4127E-01 -1.4127E-01 -1.4127E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01 -1.427E-01
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MATR L M	IX A (M3-M1 0	)/M1 GA 1	HHA = .500 2	3	4	5	6	7	8	9
MATR L M 011233455 6677890101123145 1111231441551718190200	IX A (H3-H1 0 0. 1.0000E-14 7.8572E-06 2.5559E-28 3.1573E-06 -7.0997E-28 3.14313E-26 2.3542E-06 -1.2757E-25 3.14313E-24 9.3959E-07 -5.3267E-23 5.4603E-07 -3.1731E-23 1.2140E-06 8.7127E-21 6.2377E-07 -7.6456E-21 1.6935E-06	1//H1 GA 1 0. 1.4449E-28 5.8325E-06 8.3333E-15 5.5484E-06 1.4554E-26 1.9132E-06 -2.0004E-25 1.9132E-06 -2.468E-24 1.9132E-06 -2.468E-24 1.9132E-06 -2.468E-24 1.9132E-06 -2.468E-24 1.9132E-06 -2.468E-24 1.9132E-06 -2.468E-24 1.9132E-06 -2.468E-24 1.9132E-06 -2.468E-24 1.9132E-06 -2.468E-24 1.9432E-21 1.9498E-06 -3.305E-07 7.5563E-07 7.5563E-07	HHA         .500           2           8.5197E-28           1.2045E-14           3.5726E-46           4.3103E-15           1.8581E-05           1.8581E-06           3.1639E-16           -1.631E-02           2.7234E-23           2.7324E-23           2.7325E-23           3.8675E-23           3.0216E-21           1.1795E-06           6.9517E-07           3.3827E-20           6.3312E-26           7.3582E-20           6.337E-07           7.3582E-20           6.337E-07           7.3582E-20           6.337E-07           7.3582E-20           6.337E-07           7.3582E-20	3 6.3614E-27 3.0120E-15 3.600E-06 3.4532E-14 3.5626E-06 2.5169E-06 2.5169E-06 2.4320E-14 2.5169E-06 2.4320E-23 4.2149E-01 4.6208E-00 2.44817E-06 2.2187E-19 1.5416E-06 5.2187E-19 1.5515E-07 5.1258E-07	4 -1.9808E-26 3.5975E-05 3.5607E-05 3.5607E-05 3.5607E-06 3.5507E-05 3.5607E-06 2.9565E-15 2.9565E-15 2.9565E-15 2.9565E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 2.9555E-15 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0 1 2 3 4 5 6 6 7 8 9 10 1 12 13 4 15 16 7 18 19 20	1.0000E+00 4.6667E-01 1.0632E-01 1.1001E-14 4.9707E-04 5.2491E-03 -3.6669E-14 4.9707E-04 5.4270E-13 -7.356E-05 -1.5401E-13 7.2868E-06 1.2974E-11 -9.7993E-07 -2.3810E-08 1.9562E-08 1.9562E-08 1.4758E-07	0. 7.0600E-01 7.1052E-01 3.3600E-01 7.6820E-02 8.1405E-13 3.5900E-04 1.6448E-11 3.5900E-04 1.6448E-11 4.1378E-05 -1.431E-09 -7.670E-07 7.6611E-09 -7.0670E-07 7.6611E-09 -4.5933E-08 5.913E-08 -1.1931E-07 -1.5438E-07	-5.5004E-14 -2.7067E-01 3.4370E-01 7.4267E-01 2.3758E-01 2.3758E-01 2.3758E-01 2.303E-02 -7.9339E-12 2.303E-03 1.0240E-10 2.0240E-10 2.0240E-10 2.0240E-10 2.0240E-10 2.0240E-10 2.0240E-10 1.0225E-05 1.0225E-05 1.0225E-05 1.713E-05 1.713E-05 2.4225E-07 1.7867E-07 -1.7049E-06 -5.9043E-07 2.8323E-06	$\begin{array}{c} 1.0267E{-}13\\ 1.6061E{-}01\\ -2.9742E{-}02\\ 5.5262E{-}01\\ 6.9537E{-}01\\ 3.3329E{-}02\\ -2.8009E{-}10\\ 3.3329E{-}02\\ -2.8009E{-}10\\ 1.2065E{-}04\\ -4.9285E{-}08\\ -3.3325E{-}07\\ -3.3325E{-}07\\ -3.3325E{-}07\\ -3.33525E{-}07\\ -4.3465E{-}06\\ -3.1132E{-}07\\ -3.1132E{-}07\\ -4.3465E{-}06\\ 8.4241E{-}06\\ 8.4241E{-}06\\ 4.4609E{-}05\\ -3.409E{-}05\\ -3.409E{-}05\\ -3.409E{-}05\\ -3.409E{-}05\\ -3.1132E{-}07\\ -4.3465E{-}06\\ -4.4609E{-}05\\ -3.409E{-}05\\ -3.409E$	$\begin{array}{c} -2.4752E{-}13\\ -1.0433E{-}01\\ -2.3548E{-}01\\ -2.3548E{-}01\\ -2.3548E{-}01\\ -2.3548E{-}01\\ -2.3545E{-}01\\ -2.6245E{-}01\\ -2.6245E{-}01\\ -3.3807E{-}01\\ -1.737E{-}01\\ -1.737E{-}01\\ -1.737E{-}01\\ -2.2050E{-}02\\ -1.827E{-}08\\ -8.5612E{-}04\\ -8.8892E{-}06\\ -8.8892E{-}06\\ -8.8892E{-}06\\ -8.8892E{-}06\\ -8.8892E{-}06\\ -8.8892E{-}06\\ -8.82797E{-}05\\ -1.357E{-}06\\ -1.$	1.4924E-11 7.0039E-02 -1.8416E-01 1.9235E-01 6.3013E-02 -2.9265E-01 6.59224E-01 5.1336E-02 4.2701E-01 8.2330E-02 5.5316E-01 8.2330E-02 5.5776E-04 4.3256E-05 5.4418E-05 5.54418E-05 5.54418E-05 5.54418E-05	5.3938-11 -4.7752E-02 1.4121E-01 -1.9597E-01 1.5502E-01 -2.7844E-01 1.970E-01 5.4942E-01 1.970E-01 5.7732E-03 -5.4942E-01 1.970E-01 5.7732E-03 -5.4937E-06 -2.8224E-04 -1.990E-04 -2.8224E-04 -1.4935E-04 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E-06 -2.4937E	-4.224.3E-11 3.2830E-02 1.7664E-01 1.7668E-01 1.76645E-02 2.1519E-01 4.6643E-02 2.1519E-01 4.6643E-02 3.0668E-01 6.0434E-01 1.4165E-01 3.0655E-02 3.7890E-02 3.7890E-02	-4.2862E-09 -2.2684E-02 -7.9337E-02 -1.5358E-01 1.5663E-01 -6.2039E-03 -1.8144E-01 1.9531E-01 -1.8745E-01 1.9531E-01 -2.9436E-01 1.6727E-02 4.4591E-01 4.8231E-01 -1.0212E-01 1.0212E-01 1.0212E-01 -1.7953E-01 -1.7953E-01	-2.3468E-08 1.67/23E-02 -5.9371E-02 1.27724E-01 -1.6172E-01 7.4907E-02 1.1072E-01 -1.7013E-01 -2.4830E-01 2.1830E-01 2.2669E-01 1.9156E-01 2.0687E-01 2.0687E-01 -4.45194E+00 4.5194E+00
LM	10	11	12	13	14	15	16	17	18	19
0 1 2 3 4 5 6 7 8 9 0 11 12 14 15 16 17 18 9 20	2.2608E-08 -1.0922E-02 4.3823E-02 -1.0278E-01 1.5283E-01 -1.1695E-02 1.6621E-01 -3.5152E-02 -1.6553E-01 -1.0278E-02 -1.6553E-01 -1.0221E-01 -3.0736E-01 -1.0221E-01 -3.0736E-01 3.3126E-10 -2.9499E+01 -2.9499E+01	1.8635E-07 7.5989E-03 3.2185E-02 8.1491E-02 8.1491E-02 -1.3679E-01 1.3751E-01 1.3751E-01 1.3505E-01 1.3505E-01 1.3505E-01 1.3505E-01 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 -3.2494E-02 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-8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 -8.5079E+00 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2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-02 2.8177E-	1.3864E-04 1.4029-03 2.7010-02 2.7010-02 2.7010-02 1.0742E-01 1.3803E-01 1.3803E-01 1.3803E-01 2.1987E-01 -2.8016E-01 -3.2097E-02 -3.2003E-01 -3.2003E-01 -3.2032E+02 -3.2514E+02 6.2334E+02 -1.1671E+04 6.2334E+02 -1.671E+04 -5.2627E+04 -5.2627E+04	-6.1341E-04 -1.8528E-03 -3.3826E-03 -3.3202E-02 2.4808E-02 1.0624E-01 -1.2429E+00 1.3575E+01 -3.2833E+00 -3.2833E+00 -3.2833E+00 -3.2755E+03 -3.2755E+03 -2.5755E+03 -2.5755E+03 -2.8935E+05 -2.8935E+05 -2.8935E+05 -2.8935E+05	-1.6688E-02 2.9344E-02 7.0001E-02 -3.0937E-02 1.0347E-01 6.1054E-02 7.2493E-01 9.5225E+00 1.9248E+01 -6.3241E+01 1.9248E+02 8.3366E+02 -1.7454E+03 -2.8679E+04 -9.1262E+04 -9.1262E+04 -9.1262E+04 -9.1262E+04 -9.1262E+04 -9.1262E+04 -9.1262E+04 -9.1381E+06 1.1341E+06	5.4797E-02 9.6568E-02 -3.2575E-01 -5.7760E-01 -3.9992E+00 -3.9992E+00 -1.3491E+01 5.3588E+00 2.4761E+05 -7.3722E+02 -7.3722E+02 -7.3722E+02 -7.3722E+02 -7.3722E+02 -1.4470E+05 -7.52E+06 -8.8494E+05 -7.652E+06 -8.8494E+05 -7.652E+06	5.5096E-01 -1.2770E400 3.9094E400 -1.728E400 -1.728E400 -1.728E400 -1.728E400 -1.728E400 -1.4592E402 -1.4592E402 -1.4592E402 -2.4197E403 -2.4197E403 -1.2848E404 -1.2314E404 -1.2314E404 -1.2314E404 -1.2314E404 -1.2314E404 -1.2314E404 -1.337E404 -1.337E404 -1.337E404 -1.3396E408
MATI	RIX A (N3-H1	.)/H1 G/	VIMA = .700	]						
LM	0	1	2	3	4	5	6	7	8	9
0 12 3 4 5 6 7 8 9 10 11 12 3 4 5 6 7 8 9 10 11 12 3 4 5 6 7 8 9 10 11 2 3 4 5 6 7 8 9 10 11 2 3 4 5 6 7 8 9 10 11 2 3 4 5 6 7 8 9 10 11 2 3 4 5 6 7 8 9 10 11 2 3 4 5 6 7 8 9 10 11 2 3 4 5 6 7 8 9 10 11 11 2 3 4 5 6 7 8 9 10 11 11 2 3 4 5 6 7 8 9 10 11 11 2 3 4 5 11 11 11 11 11 11 11 11 11 11 11 11 1	1.4211E-14 1.5226E-14 1.5226E-14 1.5714E-05 1.10011E-14 8.9206E-06 4.2510E-06 5.4270E-13 5.8079E-06 -1.5401E-13 5.8079E-06 1.2974E-11 7.6082E-05 7.0595E-11 8.2024E-04 -2.3810E-09 1.9562E-08 5.0450E+00 -5.7727E-08 3.4800E+02	0. 5.0322E-15 5.0322E-15 5.0322E-15 5.0324E-05 7.4126E-06 8.1405E-13 1.2124E-05 -5.5444E-12 1.2124E-05 -5.5444E-12 1.2124E-05 -5.5444E-12 1.2424E-05 -1.431E-06 7.7611E-09 1.2522E-01 1.5229E-03 7.7611E-09 1.2522E-01 1.5233E-08 1.5233E-08 1.3533E-06 1.1931E-07 7.5943E+01	-5.5004E-14 6.2347E-13 1.2533E-05 1.2533E-12 1.9542E-05 6.9971E-06 6.9971E-06 1.0240E-10 9.4729E-06 1.0240E-10 1.4146E-05 1.4146E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05 1.4446E-05	1.0267E-13 1.7724E-12 1.7736E-05 1.5801E-11 1.8628E-05 1.2052E-11 1.0584E-05 6.6441E-10 6.7392E-06 8.7392E-06 8.7392E-06 6.1915E-06 2.3204E-09 3.0660E-05 -4.9285E-08 3.0660E-05 -4.9285E-08 1.5331E-01 -3.1132E-07 8.4241E-06 1.558E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 1.556E+03 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1.6442E-05 6.4308E-06 6.4308E-06 6.2395E-05 1.6877E-05 6.2859E-08 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 1.4555E-05 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1.4087E-01 -1.07964E-04 1.4697E-03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 2.0921E+03 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3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938E-04 3.5938	-2.3468E-08 2.6102E-07 1.7036E-05 6.4002E-06 8.1032E-06 8.1032E-06 1.4774E-05 6.4002E-06 8.1032E-06 1.4774E-05 2.4301E-04 1.0202E-06 1.4774E-03 3.5008E-03 1.3408E-02 1.225E-01 1.7194E-03 3.5008E-03 1.3408E-02 1.3258E-01 1.7194E-05 2.4375E+01 1.5190E+03
LM	10	11	12	13	14	15	16	17	18	19
0 1 2 3 4 5 6 7 8 9 10 11 2 3 4 5 10 11 2 3 4 5 10 11 2 3 4 5 10 11 2 3 11 2 3 11 2 11 2 11 2 11 2 11	2.2608E-08 4.4852E-06 1.8359E-05 5.9102E-06 1.5137E-05 2.7881E-06 9.9539E-05 3.4341E-04 1.7358E-04 6.7014E-04 8.8349E-03 3.8887E-03 3.8887E-03 3.2481E-02	1.8635E-07 9.0232E-06 1.9627E-05 1.8461E-05 2.7974E-05 2.8600E-03 1.7485E-04 4.3916E-03 4.7650E-04 1.77650E-04 1.5645E-01 1.4571E-01 1.4571E-01	-7.0314E-07 3.6309E-04 1.6137E-04 2.3717E-04 2.3717E-04 2.943E-04 5.1662E-04 2.9053E-03 9.1520E-03 8.4788E-03 1.1911E-02 4.2692E-02 3.6315E-01 3.8738E+00	-1.8471E-05 1.7383E-03 6.6710E-04 2.1360E-03 2.4249E-03 9.5719E-03 4.0812E-01 1.0994E-01 3.4163E-01 1.0116E-01 1.2302E+00 1.2392E+01 1.6492E+01	5.6777E-05 1.3484E-02 2.3668E-02 1.9049E-03 2.0868E-03 6.6781E-03 8.5508E-02 6.2625E-01 9.9079E-02 1.1393E+00 7.3554E+00 1.8734E+00 1.8734E+00 1.8734E+00 1.8734E+00	1.3864E-04 2.1892E-01 2.3573E-01 5.7941E-02 1.6396E-03 3.5130E-02 1.3802E-01 8.02900E-01 4.1722E+00 1.1593E+00 2.3236E+00 1.7429E+01 5.4501E+01 5.4501E+01	-6.1341E-04 4.7756E-01 6.3483E-01 5.3312E-01 5.2876E-01 2.1071E+00 2.6026E+00 1.1256E+01 8.3333E+02 1.2780E+02 2.2517E+02 4.0333E+03 1.3835E+C4	-1,6688E-02 3,2529E+01 1,5564E+00 3,4884E+00 2,4636E+00 8,1645E+00 8,1645E+01 4,4104E+02 9,2181E+02 9,2181E+02 1,1793E+03 2,1369E+04 1,7021E+04 5,56417E+04	5.4797E-02 1.5884E+02 9.6903E+01 4.6481E+01 1.1799E+02 5.8477E+01 1.2800E+02 4.5639E+01 1.9420E+03 9.0101E+03 9.0101E+03 7.5464E+03 2.7459E+05 1.8197E+05	5.50966-01 2.9880E-03 8.8403E+02 4.3058E+02 1.0338E+02 2.6653E+02 2.6653E+02 1.0338E+02 2.6653E+03 1.2491E+05 4.8839E+04 1.3024E+06

# TABLE 4.8

HATE	RIX T	GAMMA = .700	]			TIME =59.	.044 S		DOL	BLE PRECISIO
LH	0	1	2	3	4	5	6	77	8	9
0 12 34 5 67 8 9 10 11 12 13 14 15 16 11 15 16 19 20	1.0000E+ 4.6667E- 1.0605E- 5.2491E- -8.3376E- -7.3846E- 7.2868E- 7.2868E- 7.2868E- 2.3814E- -7.986E- -8.1932E- 1.3678E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E- -2.6257E-	00 0. 01 7.0600E-01 01 7.1052E-01 01 7.1052E-01 03 7.6420E-02 03 7.6420E-02 03 7.6420E-02 03 7.6420E-02 04 -3.7494E-03 07 -1.2585E-26 05 3.5500E-04 05 3.5500E-04 06 -4.1378E-05 06 -4.1378E-05 06 -4.1378E-05 06 -4.1378E-05 06 -4.1378E-05 07 -7.052518E-06 05 -4.1378E-05 06 -4.1378E-05 07 -7.05628E-03 08 9.8431E-08 09 -1.4100E-08 09 -1.4100E-08 02 -8.2170E-22 00 2.0600E-09 00 -000E-09 00 -000E-000E-09 00 -000E-00E-09 00 -000E-00E-00E-00E-00E-00E-00E-00E-00	7.8165F-28 -2.7067E-80 -2.7067E-80 -2.7067E-80 -2.707E-01 7.4267E-01 2.3758E-01 2.3758E-01 2.3758E-01 2.3758E-01 -2.308E-03 -2.308E-03 -2.308E-03 -2.308E-03 -2.304E-04 -2.346E-05 -1.9697E-23 2.0894E-04 -2.346E-05 -1.9697E-23 2.0894E-04 -2.346E-05 -1.9697E-23 2.0894E-04 -2.346E-05 -1.9697E-23 2.0874E-02 -1.5572E-22 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28 5.3270E-28	-2.1886E-27 1.6061E-01 -2.92105-01 -2.9742E-02 5.5262E-01 6.9537E-01 1.6716E-01 3.3329E-02 1.1275E-24 1.2064E-04 1.2064E-04 1.2064E-04 1.2064E-04 1.2064E-04 1.2064E-04 1.2064E-04 1.2064E-04 1.5891E-06 -2.9039E-20 -2.0669E-20 2.8116E-08 2.8016E-20 2.8116E-08 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9039E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-20 -2.9049E-2	3 3122E-26 -1.0433E-01 -2.35&8E-01 -1.4494E-01 -2.25&8E-01 -2.62&5E-01 -2.62&5E-01 -2.62&5E-01 -2.62&5E-01 -2.62&5E-01 -2.62&5E-02 -3.3807E-01 1.1737E-01 -3.3807E-02 -7.0319E-02 -7.0319E-02 -7.339E-06 -9.2318E-20 8.683&2-07 -1.8163E-18 -1.1067E-07 -1.8163E-18 -1.1067E-07	2.1323-25 7.0039E-02 7.0039E-02 7.0039E-02 6.3013E-02 7.29265E-01 8.9589E-02 4.2701E-01 5.1336E-01 5.1336E-01 5.45924E-01 5.45924E-01 5.45924E-01 7.457E-02 5.6964E-21 1.4657E-02 5.6964E-21 1.4657E-02 5.6964E-21 4.1130E-05 4.1142E-21 4.1142E-21 4.1785E-07 4.1142E-21 4.1785E-07	-9.6195E-25 -4.7755E-02 1.4122E-01 1.4122E-01 1.4122E-01 2.0341E-01 1.5502E-01 -1.5502E-01 -1.5502E-01 -2.7844E-01 1.970E-01 5.4942E-01 1.970FE-01 5.4942E-01 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.7847E-03 9.775E-03 9.775E-03 9.7847E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 9.775E-03 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-4.2463E-17 4.3552E-16 1.4552E-16 1.4552E-16	-2.3420E-25 -2.2604E-02 -7.5937E-02 -1.5358E-01 1.5663E-01 -6.2039E-03 -1.8144E-01 1.0725E-01 1.9531E-01 -1.3700E-01 1.6700E-02 4.4558E-01 6.0788E-01 1.6435E-01 2.6506E-01 1.0435E-01 2.6506E-01 1.0435E-01 2.4407E-01 2.6307E-02 -1.3010E-04	-2.4852E-22 -5.9371E-02 -5.9371E-02 -1.2724E-01 -1.6172E-01 -1.6172E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.012E-01 -1.02E-01 -1.02E-01 -2.1259E-01 -2.1259E-01 -2.1259E-01 -2.1259E-01 -2.1259E-01 -2.1259E-01 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LM	10	11	12	13	14	15	16	17	18	19
0 1234567890 11123145 167189 20	-1.6859E-08 -4.0178E-08 -3.5136E-02 -3.5136E-02 -4.7984E-02 -7.2629E-02 -1.4886E-02 -8.9577E-02 -1.0252E-02 -1.0252E-02 -1.02532E-02 -1.6112E-02 1.6112E-02 1.6411E-01 -1.7782E-01 -2.5327E-01 -5.9327E-01 -5.93242E-01 -3.984E-01 1.7717E-01	-2.07595-07 3.57785-02 6.68511-02 4.21335-02 3.36222-02 -7.22971-02 3.36222-02 -7.7.22971-02 -7.7.22971-02 -7.7.32955-02 -7.7.97135-02 5.78095-02 5.78095-02 6.80795-02 -1.19085-01 5.20916-02 2.08605-01 6.43495-02 -5.36655-01 8.90822-01 2.38195-00	1.3847E-06 -3.1928E-02 -3.1928E-02 -4.7226E-02 -4.7226E-02 -2.0590E-02 -6.3823E-02 -7.3750E-02 -6.3862E-02 -5.390E-02 -5.390E-02 -7.4371E-02 -7.4371E-02 -7.4371E-02 -7.4371E-02 -7.5539E-02 -2.7225E-01 1.7225E-01 1.7225E-01 1.753E+01 -1.7153E+01	-3.0318E-06 2.8535E-02 5.0202E-02 5.0202E-02 5.0202E-02 5.0202E-02 5.0202E-02 5.0202E-02 5.0202E-02 4.8193E-02 -3.2291E-02 2.7394E-02 2.7394E-02 2.7394E-02 2.7394E-02 2.7394E-02 2.7394E-02 2.7395E-00 -2.3710E+00 7.2113E+01	5 0845E-05 2 5395E-02 5 5455E-02 5 5455E-02 5 5455E-02 5 54354E-04 5 7196E-02 3 1442E-02 4 3798E-02 3 1442E-02 4 3331E-02 4 7405E-01 1 0050E+00 1 7745E-01 1 7745E-01 1 7745E-01 1 7755E-01 1 7753E-02 2 7533E-02 2 7532E-02 2 7552E-02 2 7552E-02 2 7552E-02 2 7552E-02 2 7552E-02 2 7552E-02 2 755	1.1823E-04 2.2379E-02 5.1830E-02 5.1830E-02 5.2378E-02 7.1104E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.2318E-02 7.23578E-01 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.23578E-02 7.25578E-02 7.25578E-02 7.25578E-02 7.25578E-02 7.25578E-02 7.25578E	-1.9256-03 -1.9121E-02 4.9342E-02 -6.0294E-02 5.1883E-02 7.1883E-02 7.1852E-01 1.0102E-01 7.1862E-01 1.9379E+00 -2.2042E+00 9.6487E-01 3.3227E+01 3.3227E+01 -3.7166E+01 2.4027E+02 1.3060E+02 1.5473E+04	6.8901E-03 1.9656E-02 -4.6288E-02 9.0683E-02 9.0683E-02 1.9493E-01 2.5900E-01 -1.9493E-01 2.0527E-01 -3.7358E+00 -3.6350E+01 -4.5570E+02 1.9557E+01 5.8976E+02 1.9774E+03 6.9440E+03 -3.639E+04 -3.639E+04	2.2252E-04 -3.9084E-02 1.6294E-01 -5.3419E-02 -5.458E-01 7.8255E-01 3.6416E+00 -1.5903E-01 9.7397E-01 -1.6529E+01 1.2306E+02 -1.338E+02 -2.255E+03 4.6035E+03 2.2255E+03 4.6035E+03 1.3922E+05 -1.37560E+05	-5.4624E-01 -3.2865E-01 -3.2865E-02 -2.4716E-02 -2.4716E-02 -2.4716E-02 -2.4716E-02 -2.6373E+01 1.7239E+01 5.6471E+02 1.4454E+03 -1.4454E+03 -2.0513E+04 -2.7443E+04 -2.7443E+04 -2.6836E+05 -3.6915E+05 -1.9836E+06
MATE	IX A (M3-M1	.)/H1 G/	UMA = .900							
LM	0	1	2	3	4	5	6	7	8	9
0 1 2 3 4 5 6 7 8 9 10 112 13 14 5 6 7 8 9 10 112 3 4 5 6 7 8 9 10 112 3 4 5 6 7 8 9 10 112 3 4 5 6 7 8 9 10 112 13 4 5 6 7 8 9 10 112 13 14 5 6 7 8 9 10 112 13 14 5 6 7 8 9 10 112 112 112 112 112 112 112 112 112	7.1054E-15 5.9212E-15 2.3771E-05 -3.5626E-15 1.9164E-05 -3.5626E-15 1.7609E-05 -4.3642E-14 1.2285E-05 3.0816E-13 1.2695E-05 -1.5141E-13 7.5562E-06 1.1372E-11 7.6370E-06 1.1372E-11 7.6370E-06 -7.3927E-10 5.4560E-03	-2.1375E-14 6.9119E-15 2.9836E-05 2.3973E-05 -1.2024E-13 1.5323E-05 -1.2024E-13 1.2465E-05 -2.1095E-12 2.4902E-12 1.033E-05 -2.3214E-11 8.4951E-36 -2.3214E-11 1.033E-05 -2.3214E-11 1.033E-05 -2.3214E-11 2.8303E-09 -2.5705E-10 2.8303E-09 -2.637E-04 -7.5709E-09 5.7038E-03	-1.2469E-13 7.2631E-14 2.2886E-05 6.5346E-13 2.3317E-05 7.8803E-13 1.6657E-05 -4.2372E-12 2.4598E-05 2.5504E-11 1.1080E-05 -5.0121E-11 1.1080E-05 -5.0121E-11 2.1806E-05 6.5322E-04 6.5322E-04 6.5322E-04 7.5048E-08 2.4542E-02	8.4789E-13 3.6551E-15 5.1711E-12 2.0787E-05 1.0541E-11 1.5979E-05 9.1248E-11 1.3639E-05 9.1248E-11 1.3639E-05 -5.6710E-10 1.0488E-05 1.0488E-05 1.1078E-09 2.8688E-09 1.1915E-04 2.1412E-08 2.1412E-08 5.1163E-02	-4.4889E-13 1.7773E-11 1.9095E-05 5.3177E-12 1.8090E-05 1.4144E-10 1.6805E-05 1.7100E-05 2.1595E-09 1.7216E-05 4.7573E-09 1.8666E-06 -2.2182E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 8.6643E-08 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GAMMA = .900

MATRIX T

# TABLE 4.8

TIME -58.914 S

0	0	1	2	3	4	5	6	7	8	9
1 2 3 4 5 6 7 8 9 101 112 13 4 15 16 7 18 9 10 112 13 4 15 16 7 18 19 0 20	$\begin{array}{c} 1.0000 \pm 00\\ 6.0000 \pm 00\\ 1.8738 \pm 01\\ 1.2340 \pm 0.23\\ 1.2340 \pm 0.23\\ 1.2340 \pm 0.23\\ 1.1929 \pm 0.27\\ 1.0809 \pm 0.3\\ 1.9998 \pm 0.27\\ 3.1529 \pm 0.4\\ 6.2018 \pm 0.2\\ 3.1786 \pm 0.5\\ 1.061 \pm 0.5\\ 3.3490 \pm 0.2\\ 3.3490 \pm$	3.0376±-28 5.1400E-01 5.5543E-01 7.7872E-01 7.3093E-28 -2.1903E-28 -2.1903E-28 -2.1903E-20 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 -4.8126E-03 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2.4995E-02 2.4995E-02 1.493E-01 -5.0942E-03 1.493E-01 -8.0413E-03 7.493E-01 -8.0413E-03 7.725E-01 6.8545E-02 -4.1042E-20 -8.554E-19 1.6925E-19 1.6925E-19 1.6925E-04	-4,2322E-24 5,8266E-02 -3,0430E-03 9,7120E-02 -3,8506E-02 -3,8506E-02 -3,8506E-02 -3,8506E-02 -3,8506E-02 -3,8506E-02 -4,9548E-01 -5,9656E-03 -5,9656E-03 -5,9656E-03 -5,9656E-03 -7,4008E-19 -7,4008E-19 -7,4008E-18 1,3720E-03	2.4317E-23 1186E-02 1136E-02 13351E-02 13351E-02 80558E-02 80558E-02 80558E-02 80558E-02 1351E-02 	$\begin{array}{c} 2.1400 {\rm fc} -22\\ 4.525 {\rm gc} -02\\ 7.4059 {\rm fc} -02\\ 2.575 {\rm gc} -02\\ 6.3543 {\rm c} -02\\ {\rm fc} -8.491 {\rm fc} -02\\ {\rm fc} -8.455 {\rm fc} -01\\ {\rm fc} -3.451 {\rm fc} -02\\ {\rm fc} -1.755 {\rm fc} -01\\ {\rm fc} -3.451 {\rm fc} -02\\ {\rm fc} -1.755 {\rm fc} -01\\ {\rm fc} -3.254 {\rm fc} -01\\ {\rm fc} -3.550 {\rm fc} -02\\ {\rm fc} -0.550 {\rm fc} -0.5\\ {\rm f$
LM	10	11	12	13	14	15	16	17	18	19
0123456789011113145167 111113145167 11111111111111111111111111111111111	-2.0405E-22 -4.0178E-02 -3.5136E-02 -4.7983E-02 -4.7983E-02 -4.7983E-02 -1.4886E-02 -8.9574E-02 1.0321E-01 1.0321E-01 1.6323E-02 -2.2888E-02 -1.6272E-01 1.6323E-02 -2.1028E-01 -1.7555E-01 6.5676E-01 6.5676E-01 4.7258E-01	9.1260E-21 3.5778E-02 4.2132E-02 7.2295E-02 7.2295E-02 7.8248E-02 7.9519E-02 5.8011E-02 8.8077E-02 5.8011E-02 8.8077E-02 6.9554E-02 -1.1302E-01 6.5545E-01 -2.3525E-01 -1.3547E-01 5.9147E-01 5.9147E-01	3.1951E-20 -3.1927E-02 6.3048E-02 -4.7224E-02 -2.0587E-02 6.8809E-02 -2.3790E-02 -2.3790E-02 -5.4765E-02 5.4765E-02 5.4765E-02 5.4765E-02 -4.7940E-02 -4.7940E-02 -1.0547E-02 -1.0547E-02 -1.0547E-02 -1.0547E-02 -1.0547E-02 -1.0547E-02 -1.4519E-01 -7.2429E-02 -7.2429E-02 -7.2429E-02 -7.2429E-02 -7.2429E-02	-3.2558E-21 2.8535E-02 5.0776E-02 5.0776E-02 8.9259E-03 -6.3144E-02 4.7261E-02 -4.7261E-02 -4.7261E-02 -3.6625E-02 -1.27361E-02 -3.4649E-02 -3.4649E-02 -3.4649E-02 -1.27361E-02 1.4296E-01 -1.2193E-01 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-3.95728E-02 -3.9575E-02 4.775848E-02 -7.75848E-02 -4.9466E-02	$\begin{array}{c} -3,7314 \pm -15\\ 1.4405 \pm -02\\ -3.8531 \pm -02\\ -3.8531 \pm -02\\ -3.8531 \pm -02\\ -5.2796 \pm -02\\ -3.4534 \pm -02\\ -3.4534 \pm -02\\ -3.0255 \pm -02\\ -3.0255 \pm -02\\ -3.0255 \pm -02\\ -3.1474 \pm -02\\ -5.3705 \pm -02\\ $
MATE	IX A (MJ-HI	L)/H1 G/	MHA = .900							
LM	0	1	2	3	4	5	6	7	8	9
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DOUBLE PRECISION

### From these tables we observe:

- Equ.(4.5) is round-off unstable when using single precision arithmetic.
- For small  $\gamma$ -values (say  $\gamma < 0.2$ ) even a double precision computation (on a CDC-7600) is not sufficient to reach a relative accuracy of the matrix elements of the order of  $10^{-4}$ .

In **Table 4.9** we demonstrate this numerical phenomena once more for the matrix element  $T_{12,0}$ .

**Table 4.9:** Round-off instability of (4.5) demonstrated for the matrix element  $T_{12,0}$  for several  $\gamma$ -values. A is the accuracy matrix as defined in (4.8). Relative error of  $T_{12,0}$  is 10⁻⁴.

Precision CDC-7600	sing	gle	double		
$\gamma$ matrix element	T1210	A _{12/0}	T12/0	A1210	
0.01 0.1 0.4 0.5 0.7 0.9	-1.1696E+13 -7.5678E-01 -4.5518E-08 -9.1245E-09 -9.7993E-07 -9.8034E-05	7.2393E+41 4.5716E+16 1.0993E+02 1.8125E-01 7.6082E-05 9.2018E-06	-3.7576E-01 1.5122E-14 -4.1032E-10 -7.7244E-09 -9.7986E-07 -9.8034E-05	2.3257E+28 9.1446E+02 3.4034E-07 9.3959E-07 4.5058E-06 9.2417E-06	

The question regarding the round-off stability of (4.5) having been clarified, we are now in a position to compare the execution times of the two methods concerned.

#### 4.2.2.2 COMPARISON OF COMPUTATION TIME.

For this comparison we have fixed the accuracy of the matrix elements so as to lie below the bound  $\epsilon_{M1} = 10^{-4}$ . It follows from **Table 4.8** that to reach this accuracy, **double precision** arithmetic is at least required when using (4.5) and this method fails for small  $\gamma$ -values. The results of this comparison are presented on **Table** 4.10. **Table 4.10:** Execution times:  $\tau_{M1}$ ,  $\tau_{M3}$  for several  $\gamma$ -values.  $\tau_{M1}$  and  $\tau_{M3}$  designate the CPU-time of the Taylor series and the method formulated by (4.5), respectively. Dimension of matrix: (21,21). Relative accuracy of the matrix elements is approximately 10⁻⁴.

	$\tau_{M3} = 59$ sec; double precision; CDC-7600								
γ	0.01	0.1	0.4	0.5	0.7	0.9			
$\tau_{\rm M1}$ (sec)	0.014	0.023	0.040	0.045	0.070	0.220			
$\tau_{\rm M3}^{\prime}/\tau_{\rm M1}^{\prime}$	Equ.(4.5) fails	Equ.(4.5) fails	1500	1300	840	270			

- the closed form expression, (4.5), fails for small γ-values;
- $\tau_{M3}$  does not depend on  $\gamma$ , whereas  $\tau_{M1}$  is a function of  $\gamma$  and thus reflects more closely the computation expanditure really needed;
- the Taylor series method is manifestly superior as regards execution time and round-off stability.

### 4.3 CONCLUDING REMARKS.

The foregoing comparisons can be summarized as follows:

- The Taylor series method takes advantage of its adaptability-property and thus avoids wasteful computation. Consequently, the smaller  $\gamma$  is, the more superior this method is, when compared with the other two methods.
- The Taylor series method is single precision stable for the whole γ-range ([0,1]) considered, whereas the Recurrence Relation method, (4.1), fails for small γ-values and requires for certain γ-values double precision arithmetic. The use of the closed form representation, (4.5), implies at least a double precision arithmetic and even then it fails for small γ-values.

• The Taylor series method is thus the most superior with regard to round-off stability and execution time. This is once more exhibited in Table 4.11.

**Table 4.11:** Summary of execution time comparison: The subscripts M1, M2 and M3 denote as usual the use of Taylor series method, (4.1) and (4.5), respectively. Dimension of matrix: (21,21). Relative accuracy of the matrix elements: 10⁻⁴.

	Taylor series	Equ.(4.1)	Equ.(4.5)
Precision CDC-7600	Single	Double for $\gamma=0.4$ Single otherwise	Double
$\gamma$ Ex.time	τ _{M1} (sec)	τ _{M2} /τ _{M1}	τ _{M3} /τ _{M1}
0.01	0.014	Equ.(4.1) fails	Equ.(4.5) fails
0.1	0.023	Equ.(4.1) fails	Equ.(4.5) fails
0.4	0.040	3500	1500
0.5	0.045	4100	1300
0.7	0.070	2600	840
0.9	0.220	840	270

### 5.0 SUMMARY AND CONCLUSIONS.

An **inventory** of the methods so far available for the calculation of the transformation matrices T,  $T^{-1}$  (see **Table 1.1**) has shown that **none** was **satisfactory**, either as far as mathematical analysis was concerned or their numerical exploration.

This situation has prompted the present work the central object of which was the elaboration and testing of a reliable and efficient algorithm to calculate these matrices and, quite generally speaking, to establish a mathematical basis which permits the entire transformation procedure to be kept under accuracy-control.

For reasons which we outlined in **CHAPTER 1** we centered **our study** on the **Taylor series method**. It has proved to be most satisfactory both in the analytical as well as the numerical aspect.

### 5.1 RESULTS OF NUMERICAL EXPLORATION.

Indeed, the **Taylor series method** has the outstanding merit of possessing a **natural adaptability-property** to any specific case considered. That is expressed by the **dependency** of the **computer time** on **two quantities** which characterize a given problem:

- the variable γ which reflects the physical aspect, and
- the accuracy of the computed matrix elements.

The remaining two methods: the one which uses a recurrence relation in terms of matrix elements (4.1) and the one which expresses the matrix elements as a four-fold product of finite sums (4.5) do not have this faculty, but the former implicitly reveals such a dependency on accuracy.

However, the former method (4.1) does not enable computation of all matrix elements to the same accuracy i.e., elements with smaller subscripts have to be computed with greater accuracy than those with larger subscripts in order to ensure a fixed tolerance of the whole matrix. In other words, the accuracy of the matrix elements degrades with increasing subscripts due to error propagation inherent in the recurrence formula in terms of matrix elements (4.1). This unavoidably results in wasteful computation which becomes more important as the size of the matrix increases.

In conclusion, we thus **observe** that, when using the **Taylor series method**, **wasteful computation** is reduced to a **minimum**.

Furthermore, the **Taylor series method** permits **reliable** computation **with single precision** arithmetic, whereas neither the method using recurrence relation in terms of matrix elements (4.1) nor the Expression (4.5) which enables an exact computation of the matrix elements are single precision stable. These two last-mentioned methods require at least double precision arithmetic on a CDC-7600 computer in order to guarantee an acceptable round-off stability.

Consequently, for our purpose, the **Taylor series method** proved to be the **most efficient** of all those so far available for computing the transformation matrices. That is mainly due to its adaptability-faculty and its higher round-off stability.

These features are once more clearly exhibited in Table 5.1.

The data in **Table 5.1** are relative to the Taylor series method as this is, at present, the only one which is really reliable (see **CHAPTER 3**).

No error analysis at present exists for the method using the recurrence relation in terms of matrix elements (4.1). It should, however, be stressed that such an analysis would **not change the results** given in **Table 5.1**.

As for the method expressing the matrix elements in form of finite sums (4.5), this is obviously the most elegant from the analytical point of view. However, its single precision instability (one word on CDC-7600) and its low efficiency makes (4.5) less practical.

Unfortunately, we had to omit a thorough numerical exploration of these two methods, i.e., of (4.1) and (4.5), owing to lack of time. **Table 5.1:** Comparison of essential computational features of the various methods available for calculating the transformation matrices T,  $T^{-1}$ .

Method Item	Taylor series	Recurrence relation in terms of matrix elements Equ.(4.1)	Four-fold product of finite sums Equ.(4.5)
Computation wasteful?	NO, since adapted to $\gamma$ and tolerance	YES, since only partly adapted to tolerance, but no adaptation to $\gamma$	YES, since neither adapted to $\gamma$ nor to tolerance
Round-off stability requirements? (word-length on CDC-7600)	single	at least double	at least double
Efficiency (speed of computation)	high	very low	low

However, as we have observed in **Table 5.1**, the overall numerical comparison of these methods relative to the Taylor series method had already yielded quite instructive and conclusive information. In particular, it became apparent that the Taylor series method is, for our aim, the most superior of the three methods so far available.

# 5.2 RESULTS OF THE MATHEMATICAL ANALYSIS.

Besides the basic numerical results which we mentioned in the foregoing paragraph, we obtained a series of mathematical conclusions which might be worthy of enumeration.

### 5.2.1 Conclusions concerning the matrices T and T⁻¹.

• The transformation matrix elements of T⁻¹ are discontinuous at  $\gamma = 1$ .

- The elements  $T_{\ell m}$  of the matrix T are polynomials in  $\gamma$  for  $\ell$ -odd and infinite power series in  $\gamma$  otherwise.
- The elements  $T_{m\ell}^{-1}$  of the matrix  $T^{-1}$  are polynomials in  $\gamma$  for  $\ell$ -even and infinite power series in  $\gamma$  otherwise.
- The absolute value of the elements of the matrices T, T⁻¹ is smaller or equal to 1.
- The elements  $T_{\ell m}$  vanish for  $\ell$ -odd,  $m > (\ell-1)/2$ , and the elements  $T_{m\ell}^{-1}$  vanish for  $\ell$ -even,  $m < \ell/2$  and for  $\ell > 1$ , m = 0.

#### 5.2.2 Various results.

- A recurrence relation for the coefficients of the Taylor series representation of the matrix elements of T⁻¹ has been derived. The corresponding relation for the matrix T was already obtained much earlier by AMSTER [AM58]. In both cases one has a three-term homogeneous recurrence relation.
- Properties of the coefficients of the Taylor series representing the matrix elements of T and T⁻¹ were investigated. This turned out to be more than a mere academic exercise and resulted in an appreciable reduction of storage space for these data plus leading the way to a deeper insight into the properties of the power series.
- New relations for integrals have been found.
- Ramification to other mathematical disciplines emerged: Partition functions, Polya numbers.

### 5.3 SURVEY OF PRODUCTION USING THE TAYLOR SERIES METHOD.

After having shown that the Taylor series method is for calculating the transformation matrices reliable and efficient, we have applied it for **production**:

- As a first application we have calculated extensive tables of the transformation matrices of which some are given in Table 3.9 (CHAPTER 3). They have been compared with those which existed already [LA59]. It turns out that these latter tables have to be discarded, as they are too erroneous.
- As a second application we have verified the transformation matrices as given in ENDF. We found that they are also seriously incorrect for light elements.
- As an ultimate application we have treated a neutron transport problem using once the transformation matrices computed with the aid of the Taylor series method and then repeating the same computer runs applying the matrices as given in ENDF-B4. To be more precise, we have computed the neutron transport across a deuterium-sphere having at its centre a neutron point-source. Spheres with different dimensions have been studied. Again, we observe quite substantial discrepancies between the results of the two types of computer runs. Clearly, the transformation matrix for deuterium as it is given in ENDF has to be discarded. It is much too incorrect.

#### 5.4 UPDATED STATUS OF THE METHODS FOR CALCULATING T, T-1.

We have seen from **Table 1.1** (**CHAPTER 1**) that the situation concerning the methods available for calculating the transformation matrices was surprisingly unsatisfactory prior to this work. Our study was aimed to improve this situation.

In **Table 5.2** we present an updated version of **Table 1.1** taking account of the results of our investigation. We see from there that this domain is still not explored completely. However, we emphasize once more that the situation is now quite satisfactory at least what concerns current applications.

### 5.5 PROPOSAL FOR FUTURE INVESTIGATIONS.

In the course of the present work we have touched domains which we did not further explore either because they are beyond the scope of the present subject or because of lack of time. **Table 5.2:** Updated status of the methods available for calculating the transformation matrices (update from **Table 1.1** (**Chapter 1**)). Remarks preceded by a bold point "•" are new results.

Method Item	Recurrence relation in terms of matrix elements Equ.(4.1)	Finite sum expression Equ.(4.5)	Taylor series expansion
Error analysis?	ло	по —	
Validity range (γ-range) defined?	no	no	• yes $\gamma \ \epsilon \ [0,1]$
Convergence investigated?	no	no	• yes $\gamma \leq 1$
Reliability tested (round-off stability)?	● yes	● yes	• yes
Matrices treated?	T, T-2	Т	T, • T ⁻¹
Numerically explored?	partly	partly	• fully
Efficiency studied?	• yes relative to Taylor series	• yes relative to Taylor series	• yes
Used for production?	yes ENDF	partly	<ul> <li>●Tables</li> <li>●Verification <ul> <li>→ ENDF</li> <li>→ Tables[LA59]</li> </ul> </li> <li>●Neutron transport <ul> <li>Deuterium-sphere</li> </ul> </li> </ul>

One of these items is the **extension of the study to a**  $\gamma$ -range:  $\gamma > 1$ . From **Figure 21** on page 206 where we have represented the function  $f(\bar{\mu}) = \mu$  for  $\gamma > 1$  and  $\bar{\mu} \in [-1,1]$ , one can immediately read off the following:

- $\mu \in [\mu_0, 1], \mu_0 \ge 0$ , where  $\mu_0 = \cos[\operatorname{Arc} \sin(1/\gamma)]$ .
- $\mu_0(\gamma_1) > \mu_0(\gamma_2)$  for  $\gamma_1 > \gamma_2$ .
- $\lim_{\gamma \to \infty} \mu_0(\gamma) = 1.$
- $f(\bar{\mu}) = \mu$  is a two valued function.

This means that the situation for  $\gamma \in [1,\infty]$  is different from that for  $\gamma \in [0,1]$ , a range which we have investigated in the present work.

For example, a straightforward extension of the Taylor series method to the range  $\gamma > 1$  is not feasible for two reasons:

- There is a **discontinuity at**  $\gamma = 1$  which does prohibit an analytical continuation, i.e., a series expansion at subsequent points covering the range  $\gamma \in [0, \infty]$ .
- The definition of the matrices T and T⁻¹ has presumably to be revised because:
  - The variable  $\mu$  does not anymore cover the whole possible range [-1,1] as it was the case for  $\gamma \in [0,1^{-}]$ .
  - $f(\bar{\mu}) = \mu$  is a double valued function.

### 5.6 FINAL REMARKS.

We wish to emphasize that the considerable success of the Taylor series method for calculating the transformation matrices was not at all evident a priori, as this method is not a panacea in numerical analysis. It is of course also not necessarily the most optimal possible method for evaluating these matrices.



**Figure 21.** The function  $f(\bar{\mu}) = \mu$  for  $\gamma > 1$ .
### ANNEX 1. SYSTEMATIC VERIFICATION OF THE TRANSFORMATION MATRICES GIVEN IN ENDF/B4.

In Subsections 3.3.3 and 3.5.3 we have shown that the calculation of the transformation matrices can be kept under accuracy-control when using the Taylor series method. Furthermore, in Subsection 3.8.1 (Figure 17 on page 133) we found that there are, for deuterium, serious discrepancies between the transformation matrix T as calculated by means of the Taylor series method and the corresponding matrix given in ENDF/B4. This has led us to verify the transformation matrices which are given in ENDF/B4 also for heavier nuclei.

More precisely, we have checked these matrices for elastic scattering for nuclei listed in the following **Table**.

Table: List of nuclei verified.

1- D- 2	5- B-10	8- 0-16	13-A1-27	23- V-nat	27-Co-59
2-He- 4	6- C-nat	9- F-19	14-Si-nat	24-Cr-nat	28-Ni-nat
3-Li- 6	6- C-12	11-Na-23	20-Ca-nat	25-Mn-55	29-Cu-nat
3-Li- 7	7- N-14	12-Mg-nat	22-Ti-nat	26-Fe-nat	

This **verification** was in fact twofold for each nucleus and each incident energy for which the coefficients  $\bar{a}_m(E)$  are presented in **ENDF/B4**:

• The calculation of the transformation matrix elements  $T_{\ell m}$  within the **relative** error  $\epsilon_m \leq 10^{-4}$  by means of the Taylor series method and an iterative determination of the size ( $\ell = L$ ) of this matrix to guarantee a transformation

,

$$a_{\ell}(E) = \sum_{m=0}^{\infty} T_{\ell m} \bar{a}_{m}(\bar{E})$$

within the accuracy required  $\epsilon_{\rm tr}$ . This includes a test of non-negative probabilities for each  $\ell$ -value (algorithm by IRVING et al.[IR66]).

 Comparing these results with those obtained by the help of the corresponding data from ENDF/B4. As an example, we give in the following **Table** detailed results of this verification for elastic scattering of neutrons by deuterium for incident energies lying in the range from 3.5 to 18 MeV (note that in Subsection 3.8.1, **Figure 18** on page 134, we presented such results for an incident energy of E = 20 MeV).

**Table:** Comparison of scattering probabilities which are obtained by the Taylor series method (indicated by BRC) with those obtained by the help of data from ENDF/B4. Nucleus: Deuterium. Nuclear reaction: Elastic scattering of neutrons.

ENERGY (EV)	MMAX ENDFB4	LMAX BRC	LMAX ENDFB4	COEFF ACCEP	FROM M	NEGA U1	TIVE PROBABI	LITY PROB	DEVIATION FROM MU1	> .01 TO MU2	MAXINUM DEVIATION	RANGE
3.46000E+06	6	9	6	6					1:829E+80 -7.458E-01	8.138E-9 -7:403E-8 -1.000E+0	$1 - \frac{31}{71} \cdot \frac{15}{92}$ 0 129.72	99.28
4.02000E+06	6	9	6	6					1.000E+00 8.088E-01 -7.453E-01	8.107E-0 -7.407E-0 -1.000E+0	1 -30.48 1 77.52 0 139.42	99.68
4.44000E+06	6	9	6	6					1.000E+00 8.151E-01 1.044E-01 -7.449E-01	8.212E-0 1.048E-0 -7.411E-0 -1.000E+0	1 -30.24 1 81.57 1 -86.23 0 146.78	99.49
4.91000E+06	6	9	6	6					1.000E+00 8.150E-01 -7.448E-01	8.237E-0 -7.412E-0 -1.000E+0	1 -30.21 1 -97.43 0 153.44	
5.43000E+06	6	9	6	6	-1.281E-	-01	-3.967E-01	3.786E-03	1.000E+00 9.172E-01 1.209E-01 -7.452E-01	8.231E-0 1.228E-0 -7.410E-0 -1.000E+0	1 -30.11 1 89.16 1 -111.71 0 160.29	99.40
6.30000E+06	6	9	6	6	-5.294E-	-02	-4.645E-01	1.412E-02	-1:228E=89	=7:6655==8	1 - <del>1</del> 28:98	99.92
6.97000E+06	6	9	6	6	-2.800E-	-02	-4.868E-01	2.013E-02	1.000E+00 8.265E-01	8.299E-0 -1.000E+0	1 ~30.07 0 172.52	99.83
8.10000E+06	6	9	6	6	-7.771E-	-03	-5.099E-01	2.637E-02	1.000E+00 8.258E-01	8.310E-0 -1.000E+0	1 -30.28 0 175.52	99.74
8.95000E+06	6	9	6	6	-1.837E-	-03	-5.188E-01	2.892E-02	1.000E+00 8.255E-01	8.319E-0 -1.000E+0	1 -30.40 0 176.58	99.68
1.04000E+07	6	9	6	6	3.940E-	-03	- <b>5.31</b> 7E-01	3.228E-02	1.000E+00 8.254E-01 1.562E-01 -7.554E-01	8.326E-0 1.568E-0 -7.539E-0 -1.000E+0	1 -30.23 1 94.28 1 -190.42 0 177.54	99.53
1.27000E+07	6	10	6	5	8.462E-	-03	-5.457E-01	3.620E-02	1.000E+00 8.254E-01	8.329E-0	1 -29.92 0 -212.17	99.63
1.47500E+07	6	10	6	5	9.422E-	-03	-5.533E-01	3.828E-02	1.000E+00 8.255E-01	8.329E-0	1 -29.71 0 -227.08	99.63
1.80000E+07	6	10	6	5	1.248E-	-02	-5.616E-01	4.111E-02	1.000E+00 8.256E-01	8.329E-03 -1.000E+00	1 -29.53 0 -249.35	99.63

Z = 1 A = 2 ENDFB4 MAT = 1120 MF = 4 MT = 2 GAMMA = .50075

To summarize the results of our systematic verification in a compact and illustrative form we have introduced, as measure of the deviation, the quantity F which is the fraction of the interval [-1,+1] for which the angular distributions deviate more than  $\epsilon_{tr}$  from the correct values. This variable depends on the target nucleus, the incident neutron energy E and the precision  $\epsilon_{tr}$  of the transformation itself. This fraction F is represented in **Figure 22** on page 209.

All nuclei (A < 60) which do not appear in the Figure 22 on page 209, but for which we have verified the data in ENDF/B4, have correct transformation data in ENDF/B4.



values, in dependence on the incident neutron energy E(MeV).

Concerning the deuterium, this nucleus represents a particular case, as the deviations are considerable practically for all incident particle enrgies.

For the other nuclei the deviations become significant only for higher incident particle energies (> 13 MeV).

In conclusion, the examples given above exhibit the high sensitivity of the results of a transformation with respect to both the accuracy and the size of the transformation matrix.

#### ANNEX 2. CALCULATION OF NEUTRON TRANSPORT ACROSS A DEUTERIUM-SPHERE.

#### 2.1 GENERAL REMARKS.

In Annex-1 we have verified angular distribution data which are given in ENDF/B4. We found that they are seriously incorrect for several light nuclei, in particular for deuterium. That has led us to study also the influence of such incorrect data on results of neutron transport calculations. As an example we consider the neutron transport across deuterium-spheres having different radii. These spheres are supposed to be isotropic with respect to neutron transport, which is to say, no direction is privileged.

#### 2.2 MICROSCOPIC DATA PROCESSING.

Firstly, the basic data of the angular distribution of neutrons elastically scattered by deuterium, i.e., the coefficients  $\bar{a}_{m}(E)$ , have been retrieved from ENDF/B4.

**Secondly**, these coefficients have been transformed into the laboratory system for further usage applying:

- the transformation matrix T_{ENDE} as given in ENDF/B4,
- the transformation matrix T_{BRC} which has been calculated by means of the Taylor series method developed in our laboratory, (<u>Br</u>uyères-le-<u>C</u>hatel).

Two sets of cross section have thus been established: the set (ENDF) and the set (BRC).

Note, for our facility, which will be described below, we have confined ourselves, for reason of simplicity, to energies below 3 MeV as, in this energy range, only elastic scattering and capture interactions are possible. Moreover, the capture cross section is negligible (10* times lower) compared to the elastic scattering cross section.

For neutron transport calculation these data have to be put into the so-called group cross sections, i.e., cross sections averaged over energy intervals.

The choice of the number of groups results from the following considerations:

- If the cross sections vary slowly with the incident neutron energy (which is our case), the energy intervals for the groups do not need to be narrow.
- However, for the description of the energy loss per collision one needs narrow energy intervals. In fact, the energy of a neutron after collision  $E_{out}$  can be very different from the incident energy  $E_{inc}$ , especially for neutrons backscattered by light nuclei like deuterium. For example,  $E_{out} = E_{inc}/9$  at 180°.

Rather narrow energy intervals have hence to be chosen in our case in the energy range from 0.8 to 3 MeV, as, on the one hand, the outgoing particle energy depends strongly on the scattering angle and, on the other hand, the two data sets reveal serious discrepancies in this energy range.

These energy bounds are for each group, which we have used, given in the following **Table** (where the lethargy corresponds to the maximal energy of a group).

The methods applied for generating the group cross sections require in general a flux weight, which we have assumed to be constant taking into consideration the fact that deuterium has no neutron reaction resonances and that the cross sections vary slowly with energy.

Moreover, the cross sections which have been used for generating the group cross sections have been computed up to the Legendre polynomial series term of **order** L = 8. This relatively high order approximation was needed in order to represent the angular distribution data correctly (see Section 3.7).

Emax	Emin	Lethargy	Emax	Emin	Lethargy
(eV)	(eV)	max	(eV)	(eV)	max
2.725+05 2.350+05 2.019+06 1.643+06 1.353+06 1.108+06 9.072+05 7.427+05 6.081+05 4.979+05 4.076+05 3.337+05 2.732+05	2.350+06 2.019+06 1.643+06 1.353+06 1.108+06 9.072+05 7.427+05 6.081+05 4.979+05 4.076+05 3.337+05 2.732+05 2.237+05	1.30 1.45 1.60 1.81 2.00 2.20 2.40 2.60 2.80 3.00 3.20 3.40 3.60	1.499+05 1.228+05 8.651+04 5.247+04 5.000+04 1.700+04 3.000+03 5.500+02 1.000+02 3.000+01 1.000+01 3.000+00	1.228+05 8.651+04 5.247+04 5.000+04 1.700+04 3.000+03 5.500+02 1.000+02 3.000+01 1.000+01 3.000+00 1.000+00 4.000-01	4.20 4.40 4.75 5.25 5.30 6.38 8.11 9.81 11.50 12.70 13.80 15.00 16.10
2.237+05	1.831+05	3.80	4.000-01	1.000-01	17.00
1.831+05	1.499+05	4.00	1.000-01		18.40

Table: Energy bounds for the groups used.

#### 2.3 DESCRIPTION OF THE FACILITY.

The facility investigated has the following characteristics:

- A neutron point-source covering the neutron energy range from 2.35 to 2.725 MeV (i.e., the group n°1) with an intensity equal to 1.
- This source is placed at the centre of the deuterium-sphere, which has a density = 0.3 g/cm³ (N = 0.09 cm⁻¹). The spheres considered have the radii: r = 5 and 50 cm, which approximately correspond to 1 and 10 mean free paths, respectively, of the neutrons in question.

In all cases, the meshes in radial direction, i.e., dr = r/n, where n indicates the number of meshes, has been chosen sufficiently fine, in order to avoid negative fluxes [SO70]. Note that the semi-empirical inequality dr <  $2/\Sigma_{t}$  = 10 cm should be satisfied.

#### 2.4 COMPUTER CODES USED.

The common neutron transport codes used for solving the BOLTZMANN equation are based on the so-called  $S_N - P_r$  methods.

We have carried out a first trial calculation with the code AMPX-2 [GR76] on a IBM-370/145 computer. It turned out that this code is not suitable for solving our problem. The reasons for it are the following:

- The code AMPX-2 is not adequate for treating problems having discontinuities, which are present when using point-sources.
- The available precision of the IBM-370/145 does not permit a sufficiently accurate computation of the Legendre polynomials of high order.

The results obtained by means of the code AMPX-2 reveal oscillations and negative fluxes in spite of using fine meshes in radial direction.

We have thus applied a more performing code to treat our problem. The code **GRPHEE** [VE81], implemented on a CDC-7600, was found to be quite appropriate for our purpose. This code has been developped on basis of the so-called first collision density technique in the view of treating neutron transport in a facility having a point-source. Furthermore, this code uses highly stable and efficient numerical interpolation methods. Finally, the computation is accurate for an approximation up to the order L = 10.

#### 2.5 RESULTS OF THE CALCULATIONS.

All calculations carried out imply **17 integration directions** (S16). The **neutron fluxes** which are obtained by integration over space and directions **are**:

The flux outgoing from the sphere

$$4 \pi R^2 \int_0^1 \phi(R,\mu) \mu \, d\mu$$

• The 'capture flux'

.

$$\int_{V} \Sigma_{t}(E) \phi(\vec{r}, E, \vec{\Omega}) a^{3}r a^{2}\Omega$$

which corresponds to an average flux inside the sphere.

• The flux of the source which is in fact the sum of the two fluxes mentionned above, which in turn are principally reflecting differences of the anisotropy

$$\int_{V} \Sigma_{\text{prod}}(E) \phi(\vec{r}, E, \vec{\Omega}) a^{3} r a^{2} \Omega .$$

#### 2.5.1 The outgoing flux.

The outgoing flux which has been calculated using the data set (BRC) is represented in **Figure 23** on page 217. There the flux is expressed as number of neutrons per group. The radius r of the deuterium-sphere is equal to 5 cm (dr = 2.5 mm). The energy range covered is 100 keV to 3 MeV (17 first groups), as the majority of the outgoing neutrons have an energy lying in this range. In fact, the outgoing flux corresponding to no collision amounts to 0.36 neutrons [exp( $-\Sigma_t$ r)] (not included in **Figure 23** on page 217), and the sum of the first 17 groups amounts to 0.48. This makes a total of 0.84 neutrons.

The outgoing flux distribution in dependence on the groups which is represented in **Figure 23** on page 217 (not including the flux corresponding to no collision) shows:

- the energy loss of neutrons from the source due to one collision. This corresponds essentially to a moderation of neutrons down to the minimum energy of about 300 keV (E/9).
- A lower energy part corresponding to neutrons having undergone several collisions.

In **Figure 23** on page 217 we give also the outgoing flux which has been obtained by the help of the data set (ENDF). This flux considerably deviates from that computed using the correct data set (BRC). In particular, the peak at high energies of the former is larger and shifted down to lower energies.

In order to exhibit still more clearly the difference between the results obtained by means of the two different data sets we represent the ratio R =outgoing flux (ENDF) / outgoing flux (BRC) in **Figure 24** on page 218.

From Figure 24 on page 218 one can see that the deviations vary between 0.78 and 1.42 depending on the group considered (0.1 - 3 MeV). However, in the energy range from 0 to 100 keV (not given in Figure 24 on page 218) the deviations do not exceed 1 %.

The peak at 1.5 MeV reflects the fact that the angular distribution (ENDF) favours more the scattering at large angles and backscattering, for which the outgoing energy is very different from the incident energy. This results in turn in an accumulation of neutrons having energies which are clearly downward shifted relative to the energies of the corresponding source-neutrons. Hence, the neutron spectrum of the outgoing flux (ENDF) is thus more soft already after one collision.

We have verified this qualitative interpretation. For this purpose we supposed that one collision only occurs (which is a reasonable assumption as the mean free path is equal to the radius in the case r = 5 cm). The probability that one neutron of a given group leaves the sphere reads then

,

$$\frac{1}{\Sigma_{t}} \left(1 - e^{-\Sigma_{t} X}\right) \int_{\mu_{1}}^{\mu_{2}} \sigma(E,\mu) d\mu$$

where  $\mu_1$  and  $\mu_{\pm}$  correspond, according to kinematics, to the energy limits of the group g and E denotes the energy of the source. The ratio of probabilities which has been obtained in this way using the data set (ENDF) and the data set (BRC) is represented in **Figure 25** on page 219, where we compare this ratio with that of the fluxes as given in **Figure 24** on page 218.

Figure 25 on page 219 renders apparent a quite similar behaviour of both ratios. The deviations between them are due to neutrons having undergone more than one collision.

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Figure 23. Outgoing flux for the d-sphere r = 5 cm: Outgoing flux (number of neutrons per group) from the deuterium-sphere with a radius r = 5 cm. (....) results from the data set (ENDF), (_____) results from the data set (BRC). The outgoing flux of neutrons without collisions (=0.36) is not included.

It is clear that this simple approach, i.e., supposing only one collision, has its limit, as in practice, particularly because of the negligible capture cross section, any neutron from the source would in this case leave the sphere, which would in turn lead to a compensation between the groups.

In case of a deuterium-sphere with a radius r = 50 cm (around 10 mean free paths), the great number of collisions which neutrons undergo when crossing the sphere leads to a considerable reduction of the number of neutrons leaving the sphere with an energy between 0.1 and 3 MeV. Actually, the outgoing neutron flux is in this case about 10⁻³. Almost the entire neutron spectrum lies below 100 keV, i.e., in a range where the differences of anisotropy between the data set (ENDF) and the data set (ERC) are negligible.



Figure 24. Ratio F of the outgoing fluxes: Ratio F = outgoing flux (ENDF) / outgoing flux (BRC). Deuterium-sphere, radius = 5 cm.

Figure 26 on page 220 shows the outgoing neutron flux from a deuterium-sphere with a radius r = 50 cm, in the energy range 0.1 - 3 MeV. The neutron flux is there expressed as number of neutrons per group. Results which have been obtained with the data set (ENDF) as well as the data set (ERC) are given.

The ratio F of these fluxes, i.e.,  $F \approx flux$  (ENDF) / flux (BRC) is shown in Figure 27 on page 221.

This ratio (Figure 27 on page 221) has a quite different behaviour than that for a deuterium-sphere with a radius r = 5 cm (Figure 24). Furthermore, the deviations appearing in Figure 26 on page 220 between the flux (ENDF) and the flux (BRC) are considerable. They even reach 40 %. However, at low energies one observes only deviations of not more than 4 %. An interpretation of the results which are represented in Figure 26 on page 220, in the way as we did this for those given in



Figure 24, is not feasable, since neutrons undergo in the former case in general more than one collision.



Figure 26. Outgoing flux for a d-sphere with r = 50 cm: The outgoing neutron flux from a deuterium-sphere with a radius = 50 cm. The flux per group is given. The flux of neutrons having undergone no collision is not included.

#### 2.5.2 The flux of captured neutrons.

The ratio  $F_{C}$  of the fluxes corresponding to captured neutrons:  $F_{C}$  = capture flux (ENDF) / capture flux (BRC) are for the deuterium-spheres with a radius r = 5 cm and a radius r = 50 cm represented in **Figure 28** on page 222 and **Figure 29** on page 223, respectively. These figures show that these ratios have for both spheres a similar behaviour.



#### 2.6 CONCLUDING REMARKS.

The present study of the sensivity of the transformation matrices with respect to results of neutron transport calculations have clearly shown that incorrect transformation matrices have serious repercussions on the values of the neutron fluxes. This influence was demonstrated by calculating the neutron transport across deuterium-spheres of a radius r = 5 cm and 50 cm, respectively. The code **ORPHEE** which is particularly appropriate for treating point-sources has been used. For the deuterium-sphere with a radius r = 5 cm we have verified the results which yielded the code ORPHEE by means of simplified calculations based on a one collision approach.

In conclusion, the neutron transport calculations have shown that precise transformation matrices have to be used. One has thus to be particularly careful when using codes like **AMPX**, which apply the transformation matrices as they are given in **ENDF/B4**.



Unfortunately, we could not, because of lack of time, make similar calculations for the nuclei like He, Li, Fe, ... for which we have also detected erroneous transformation matrices in **ENDF/B4** (see **Figure 22** on page 209 in **Annex-1**). Repercussions of these erroneous transformations matrices may thus become particularly apparent in safety problems of nuclear fusion reactors.



Figure 29. Ratios of "capture" fluxes: Ratios  $F_c$  = capture flux (ENDF) / capture flux (BRC) for a deuterium-sphere of a radius r = 50 cm.

#### ACKNOWLEDGEMENTS.

We are very grateful to D.VERWAERDE for the neutron transport calculations using the code ORPHEE.



#### ANNEX 3. DESCRIPTION OF PROGRAMS AND DETAILS ON NUMERICS.

3.1 STORAGE OF THE  $b_{/m}^r$  AND  $q_{m/}^r$  COEFFICIENTS.

#### 3.1.1 General considerations.

According to the definition of the functions  $T_{M}(\gamma)$  (see (3.9)) the indices  $\ell$ , m, r should theoretically run from zero to infinity. For evident numerical reasons the maximum value of these subscripts, denoted by L, M and R respectively, have to be finite (see also **CHAPTER 2** Subsection 2.2.2). L and M are generally fixed by the considered angular distribution (e.g., the ENDF upper limit is L = M = 20), whereas R depends on the desired accuracy for the T_{em}( $\gamma$ ) functions.

As we have seen in Subsection 3.2.1 the  $b_{\ell m}^r$  coefficients are defined by the recurrence relation

$$b_{\ell,m}^{r+1} = \frac{(m+1)(m+2-r)}{(r+1)(2m+3)} b_{\ell,m+1}^{r} - \frac{m(m+r-1)}{(r+1)(2m-1)} b_{\ell,m-1}^{r}$$

This recurrence formula relates only to m and r indexes, thus there is such a relation for each  $\ell$ -value, but with different initial conditions. So, for a given  $\ell$ -value, the  $b_{\ell m}^{r}$  coefficients may be considered as the elements of a matrix or as points on a (m,r) plane. It should be pointed out that to compute exactly the (m,r+1) coefficient, the (m+1,r) coefficient, among others, has to be known, as illustrated by the following diagram:



• As R becomes large when computing the elements of the matrices T and  $T^{-1}$  to high accuracy, the coefficients  $b_{\ell m}^r$  should be stored in most compact form in order to save memory-space.

All the above remarks apply also to the  $q_{m\ell}^r$  coefficients; one has only to permute indexes  $\ell$  and m.

## 3.1.2 Storage of the $b_{fm}^r$ coefficients.

To save memory-space we store only the non-vanishing  $b_{\ell m}^r$  coefficients in a one-dimension array either in central memory or on disk (in a sequential file), depending on the characteristics of the computer or on physical applications.

The non-vanishing coefficients are stored in the following order:

for a given l (l increasing), l = 0, 1, 2, ..., L,

- for a given r (r increasing), r = 0, 1, 2, ..., R,
- for a given m (m decreasing), m = 0, 1, 2, ..., M,

so the structure of the storage array is



Together with this structure of the array we have to define two additional quantities:

N( $\ell$ ) the number of non-zero  $b_{\ell m}^{r}$  matrix coefficients for a given  $\ell$ , n( $\ell$ ,r) the number of non-zero  $b_{\ell m}^{r}$  row coefficients for given  $\ell$  and r, so that, anywhere a  $b_{fm}^r$  coefficient has to be used in a routine, its location k in the array is obtained by the relation

$$k(\ell,m,r) = \sum_{i=0}^{\ell-1} N(i) + \sum_{j=0}^{r-1} n(\ell,j) + k_1 , \quad k_1 = (\ell+r-m)/2 + 1$$

where the first summation gives the total number of non-vanishing coefficients corresponding to all previous *l*-values, the second one the number of coefficients up to r-1 and the last term is the position of the considered coefficient in the row.

As a general property, the following relation holds

$$N(\mathcal{L}) = \sum_{r=0}^{R} n(\mathcal{L}, r)$$

n order to get the maximum size K to assign to the storage array we will now investigate in more detail the number of non-zero coefficients to be stored in both cases: with and without M limitation.

3.1.2.1 INDEXATION-SYSTEM.

3.1.2.1.1 Preliminary formulae.

In this section the  $b_{\ell_m}^r$  coefficients will be represented by points on a (m,r) plane and we will be interested in counting non-vanishing coefficients. As we will see below, these coefficients are contained within a combination of the two following types of triangles and their number is given by:



m m+1

1.





where IP stands for <u>integer</u> part. This function, which will appear frequently, is tabulated below,

Table: The function v(i) for i: 0 to 10.

i	0	1	2	3	4	5	6	7	8	9	10
v(i)	0	1	2	4	6	9	12	16	20	25	30

and satisfies the two following relations: v(i+1) + v(i) = (i+1)(i+2)/2 = u(i+1), v(i+1) - v(i) = IP(i) + 1.

3.1.2.2 NUMBER OF NON-VANISHING COEFFICIENTS WITHOUT M LIMITATION.

As mentioned in 3.1.2.2 we have to distinguish between the two cases: *1*-odd and *1*-even.

3.1.2.2.1 Non-vanishing coefficients for  $\ell$ -odd,  $\ell = 2\lambda + 1$ .



The non-vanishing coefficients are plotted in the following diagram

where the point A represents the initial condition (r = 0). Note that the coefficients whose representative points lie on the line  $r = -m+\ell$  are calculated by means of only the first part of the recurrence formula (involving the "m+1" term), whereas those lying on the line  $r = m-\ell$  are calculated by means of only the second part of the recurrence formula (involving the "m-1" term).

For a given odd  $\ell$ -value, the number of non-vanishing  $b_{\ell m}^r$  coefficients is deduced as follows:

#### for $\lambda + 1 < R$ :

The total number of elements we are looking for is contained in the quadrilateral AB'CC', i.e., the number of elements within the triangle ABC minus the number of elements within the triangle B'BC' (excluding the boarder B'C'), that is, using the first preliminary formula

$$N_{1}(\ell) = (R+1)(R+2)/2 - [R-(\lambda+1)][R-(\lambda+1)+1]/2$$
  
= [R(\ell+3) - (\ell^{2}-9)/4]/2 .

In this relation the index 1 means that  $\ell$  is odd.

The number of elements per row  $n_1(\ell,r)$  is constant and equal to  $n_1(\ell,r) = \lambda + 2 = (\ell+3)/2$ ;

for  $R \leq \lambda + 1$ :

 $I_1(\ell) = (R+1)(R+2)/2 ,$  $n_1(\ell,r) = r + 1 .$ 

The dependence of  $N_1(\mathcal{X})$  on  $\mathcal{X}$  and R is illustrated by the following **Table.** 

**Table:** Number of non-vanishing  $b_{\ell m}^{r}$  coefficients for  $\ell$ -odd and without M limitation.

R\l	1	3	5	7	9	11	13	15	17	19
1	З	3	3	3	3	3	3		3	3
2	5	6	6	6	6	6	6	6	6	6
5	11 i	15	18	20	21	21	21	21	21	21
10	21	30	38	45	51	56	60	63	65	66
20	41	60	78	95	111	126	140	153	165	176
50	101	150	198	245	291	336	380	423	465	506
100	201	300	398	495	591	686	780	873	965	1056
150	301	450	598	745	891	1036	1180	1323	1465	1606
200	401	600	798	995	1191	1386	1580	1773	1965	2156
500	1001	1500	1998	2495	2991	3486	3980	4473	4965	5456

3.1.2.2.2 Non-vanishing coefficients for  $\ell$ -even,  $\ell = 2\lambda$ .

The non-vanishing elements are plotted in the following diagram



where the point A represents the initial condition (r = 0). Note that the coefficients whose representative points lie on the line m = 0 are calculated by means of only the first part of the recurrence formula (involving the "m+1" term), wher-

eas those lying on the line  $r = m-\ell$  are calculated by means of only the second part of the recurrence formula (involving the "m-1" term).

For a given  $\ell$  (even), the number of non-vanishing coefficients is deduced as follows:

for 
$$\ell < R$$
:

The total number of elements we are looking for is contained in the quadrilateral ADBC, i.e., the number of elements within the triangle AB'C minus the number of elements within the triangle DB'B (excluding the boarder DB), that is, making use of both preliminary formulae

 $N_{2}(\ell) = (R+1)(R+2)/2 - v(R-\ell)$ .

In this relation the index 2 means that  $\ell$  is even.

The number of elements per row  $n_2(\ell,r)$  is given by:  $n_2(\ell,r) = r + 1 - IP[(r-\ell+1)/2]$ ;

for  $R \leq \ell$ :

 $N_2(\ell) = (R+1)(R+2)/2$  ,  $n_2(\ell,r) = r + 1$  .

The dependence of  $N_2(\ell)$  on  $\ell$  and R is illustrated by the following **Table** (where implicitly  $N_2(0) = 1$ ).

The large difference in the number of non-vanishing  $b_{\ell m}^{r}$  coefficients between  $\ell$ -odd and  $\ell$ -even exhibits once more the fact that  $T_{\ell m}(\gamma)$  are polynomials for  $\ell$ -odd and infinite series for  $\ell$ -even.

Knowing the number of coefficients for each *l*-value, let us now consider their total number.

3.1.2.2.3 Total number of coefficients.

The total number of non-vanishing coefficients up to a given L-value is given by

**Table:** Number of non-vanishing  $b_{\ell m}^r$  coefficients for  $\ell$ -even and without M limitation.

R\1	2	4	6	8	10	12	14	16	18	20
1	3	3	3	3	3	3	3	3	3	3
2	6	6	6	6	6	6	6	6	6	6
5	17	20	21	21	21	21	21	21	21	21
10	46	54	60	64	66	66	66	66	66	66
20	141	159	175	189	201	211	219	225	229	231
50	726	774	820	864	· 906	946	984	1020	1054	1086
100	2701	2799	2895	2989	3081	3171	3259	3345	3429	3511
150	5926	6074	6220	6364	6506	6646	6784	6920	7054	7186
200	10401	10599	10795	10989	11181	11371	11559	11745	11929	12111
500	63501	63999	64495	64989	65481	65971	66459	66945	67429	67911

$$K(L,R) = \sum_{\ell=1}^{L'} N_1(\ell) + \sum_{\ell=0}^{L''} N_2(\ell)$$

$$\ell = 1 \qquad \ell = 0$$

$$\Delta \ell = 2 \qquad \Delta \ell = 2$$

where L' (L") is the nearest lower odd (even) integer of L, and

$$\begin{array}{c} \overset{L'}{\Sigma} & N_{1}(\ell) = \frac{L'+1}{4} \left[ \frac{9}{4} + 3R + \frac{R}{2} (L'+1) - \frac{L'(L'+2)}{12} \right] \\ \Delta \ell = 2 \\ \\ \Delta \ell = 2 \\ \\ \overset{L''}{\Sigma} & N_{2}(\ell) = \frac{L''}{2} \left[ \frac{1}{2} (R+1)(R+2) - v(R) \right] + \frac{R+1}{8} L''(L''+2) - \frac{1}{24} L''(L''+1)(L''+2) + 1 \\ \Delta \ell = 2 \end{array}$$

The total number of coefficients is given for some L and R values in the following **Table**, which shows that this number may be very large.

Table: Total number of non-vanishing coefficients without M limitation.

R\L	l	2	3	4	5	7	10	15	20
1	4	7	10	13	16	22	46	61	91
2	6	12	18	24	30	42	60	90	120
5	12	29	4.1	64	82	123	186	291	396
10	22	68	98	152	190	295	476	787	1116
20	42	183	243	402	480	750	1251	2100	3126
50	102	828	978	1752	1950	3015	5076	8145	12276
100	202	2903	3203	6002	6400	9790	16451	25220	37526
150	302	6228	6678	12752	13350	20315	34076	51045	75276
200	402	10803	11403	22002	22800	34590	57951	85620	125526
500	1002	64503	66003	130002	132000	198990	332451	476820	689526
1									

3.1.2.3 NUMBER OF NON-VANISHING COEFFICIENTS WITH M LIMITATION.

For physical applications we are only interested in the  $b_{\ell m}^{r}$  coefficients with limited m-range, m = 0, 1, 2, ..., M.

In all the relations given below the prime "'" means that the number of coefficients should be understood as being with M limitation and the index 1 (2) indicates that  $\ell$  is odd (even).

3.1.2.3.1 Non-vanishing coefficients for  $\ell$ -odd,  $\ell = 2\lambda + 1$ .

The number of non-vanishing coefficients for *4*-odd is given by the following relations:

 $R \leq \lambda + 1$ 

m < .	$\ell - R  N'_1(\ell)$	=	0
<i>l</i> −R ≤ m < .	$n_1^{\prime}(\ell)$	=	v(m- <i>ℓ</i> +R+1)
l ≤ m < .	(+R N'()	=	$(R+1)(R+2)/2 - v(\ell+R-m)$
<b>ℓ</b> +R ≤ m	N:( <i>1</i> )	=	$(R+1)(R+2)/2 = N_1(\ell)$ .

 $\lambda+1 < R \leq \ell$ 

$m < \lambda$	$N_1'(\mathcal{A}) = 0$
$\lambda \leq m < R$	$N_{1}(\mathcal{L}) = (m-\lambda+1)(m-\lambda+2)/2$
$R \leq m \leq \ell$	$N_{1}^{\prime}(\mathcal{X}) = (m-\lambda+1)(m-\lambda+2) - v(m-R+1)$
ℓ < m < ℓ+R	$N_1'(\ell) = (R+1)(R+2)/2 - (2R-\ell-1)(2R-\ell+1)/8 - v(\ell+R-m)$
<b>ℓ+</b> R ≤ m	$N_{1}(\ell) = (R+1)(R+2)/2 - (2R-\ell-1)(2R-\ell+1)/8 = N_{1}(\ell)$

1 < R	
$m < \lambda$	$N_{1}(\mathcal{L}) = 0$
$\lambda \leq m < \ell$	$N'_{1}(\ell) = (m-\lambda+1)(m-\lambda+2)/2$
$l \leq m \leq R-1$	$N'_{1}(\ell) = (\lambda+2)(\lambda+3)/2 + (\lambda+2)(m-\ell)$
R-1 < m < ℓ+R	$N_1(\ell) = (R+1)(R+2)/2 - (2R-\ell-1)(2R-\ell+1)/8 - v(\ell+R-R)$

$$\ell + R \le m$$
  $N'_1(\ell) = (R+1)(R+2)/2 - (2R-\ell-1)(2R-\ell+1)/8 = N_1(\ell)$ 

The dependence of  $N'_1(\ell)$  on  $\ell$  and R is illustrated by the following **Table** for M = 20.

**Table:** Number of non-vanishing  $b_{\ell m}^{r}$  coefficients for  $\ell$ -odd and with M limitation, M = 20.

	R\.	1	3	5	7	9	11	13	15	17	19
	1	3	3	3	3	3	3	3	3	3	3
	2	5	6	6	6	6	6	6	6	6	5
ļ	5	11	15	18	20	21	21	21	21	19	15
	10	21	30	38	45	51	55	56	54	49	41
	20	40	56	69	79	86	90	91	89	84	76
	50	41	57	70	80	87	91	92	90	85	77
	100	41	57	70	80	87	91	92	90	85	77
	150	41	57	70	80	87	91	92	90	85	77
	200	41	57	70	80	87	91	92	90	85	77
j	500	41	57	70	80	87	91	92	90	85	77

The number of coefficients per row is given by the following relations:

 $\boxed{r < \lambda + 1}$   $m < \ell - r \qquad n_{1}^{*}(\ell) = 0$   $\ell - r \le m < \ell + r \qquad n_{1}^{*}(\ell) = r + 1 - IP[(\ell + r - m + 1)/2]$   $\ell + r \le m \qquad n_{1}^{*}(\ell) = r + 1 = n_{1}(\ell, r) \qquad .$   $\boxed{\lambda + 1 \le r}$   $m < r - 1 \qquad n_{1}^{*}(\ell) = 0$   $r - 1 \le m < \ell + r \qquad n_{1}^{*}(\ell) = \lambda + 2 - IP[(\ell + r - m + 1)/2]$   $\ell + r \le m \qquad n_{1}^{*}(\ell) = \lambda + 2 = n_{1}(\ell, r) \qquad .$ 

3.1.2.3.2 Non-vanishing coefficients for  $\ell$ -even,  $\ell = 2\lambda$ .

The number of non-vanishing coefficients for *l*-even is given by the following relations:

R < 1

 $m < \ell - R \qquad N_{2}'(\ell) = 0$   $\ell - R \le m < \ell \qquad N_{2}'(\ell) = v(m - \ell + R + 1)$   $\ell \le m < \ell + R \qquad N_{2}'(\ell) = (R + 1)(R + 2)/2 - v(\ell + R - m)$   $\ell + R \le m \qquad N_{2}'(\ell) = (R + 1)(R + 2)/2 = N_{2}(\ell) \qquad .$   $\boxed{\ell \le R}$   $0 \le m < \ell \qquad N_{2}'(\ell) = v(m + R - \ell + 1) - v(R - \ell)$   $\ell \le m < \ell + R \qquad N_{2}'(\ell) = (R + 1)(R + 2)/2 - v(R - \ell) - v(\ell + R - m)$ 

$$\ell + R \le m$$
  $N'_{2}(\ell) = (R+1)(R+2)/2 - v(R-\ell) = N_{2}(\ell)$ 

The dependence of N'₂( $\ell$ ) on  $\ell$  and R is illustrated by the following **Table** for M = 20 (implicitly N'₂(0) = 1).

**Table:** Number of non-vanishing coefficients for  $\ell$ -even and with M limitation, M = 20.

	R\.	2	4	6	8	10	12	14	16	18	20
	1	3	3	3	3	3	3	3	3	3	2
	2	6	6	6	6	6	6	6	6	6	4
ļ	5	17	20	21	21	21	21	21	20	17	12
ļ	10	46	54	60	64	66	64	60	54	46	36
1	20	139	153	163	169	171	169	163	153	139	121
	50	454	468	478	484	486	484	478	468	454	436
	100	979	993	1003	1009	1011	1009	1003	993	979	961
ļ	150	1504	1518	1528	1534	1536	1534	1528	1518	1504	1486
	200	2029	2043	2053	2059	2061	2059	2053	2043	2029	2011
1	500	5179	5193	5203	5209	5211	5209	5203	5193	5179	5161

The numbers of coefficients per row is given by the following relations:

 $\frac{\mathbf{r} < \ell}{\mathbf{m}} = \mathbf{n}_{2}(\ell) = 0$   $\ell - \mathbf{r} \le \mathbf{m} \le \ell \qquad \mathbf{n}_{2}(\ell) = \mathrm{IP}[(\mathbf{m} - \ell + \mathbf{r} + 2)/2]$   $\ell < \mathbf{m} < \ell + \mathbf{r} \qquad \mathbf{n}_{2}(\ell) = \mathbf{r} + 1 - \mathrm{IP}[(\ell + \mathbf{r} - \mathbf{m} + 1)/2]$   $\ell + \mathbf{r} < \mathbf{m} \qquad \mathbf{n}_{2}(\ell) = \mathbf{r} + 1 = \mathbf{n}_{2}(\ell, \mathbf{r}) \qquad .$ 

 $\begin{array}{c} \underline{\ell \leq r} \\ m \leq \ell & n_2^*(\ell) = \mathrm{IP}[(m+r-\ell+2)/2] - \mathrm{IP}[(r-\ell+1)/2] \\ \ell < m < \ell + r & n_2^*(\ell) = r + 1 - \mathrm{IP}[(r-\ell+1)/2] - \mathrm{IP}[(\ell+r-m+1)/2] \\ \ell + r \leq m & n_2^*(\ell) = r + 1 - \mathrm{IP}[(r-\ell+1)/2] = n_2^*(\ell,r) & . \end{array}$ 

3.1.2.3.3 Total number of coefficients.

The total number of non-vanishing coefficients up to a given L-value is given by

$$K'(L,M,R) = \sum_{\ell=1}^{L'} N_1(\ell) + \sum_{\ell=0}^{L''} N_2(\ell)$$
  
$$\Delta \ell = 2 \qquad \Delta \ell = 2$$

where L' (L") is the nearest lower odd (even) integer of L.

This total number of coefficients is given for some L and R values in the following Table for the case M = 20.

<b>Table:</b> Total number of non-vanishing $b_{\ell m}^{r}$ coefficients with M limitation, M = 20	).
-----------------------------------------------------------------------------------------------------	----

R/L	1	2	3	4	5	7	10	15	20
1	4	7	10	13	16	22	31	46	60
2	6	12	18	24	30	42	60	90	117
5	12	29	44	64	82	123	186	291	374
10	22	68	98	152	190	295	476	765	991
20	41	180	236	389	458	700	1126	1728	2301
50	42	496	553	1021	1091	1649	2706	3941	5461
100	42	1021	1078	2071	2141	3224	5331	7616	10711
150	42	1546	1603	3121	3191	4799	7956	11291	15961
200	42	2071	2128	4171	4241	6374	10581	14966	21211
500	42	5221	5278	10471	10541	15824	26331	37016	52711

In **conclusion**, we can say that the counting of the non-vanishing  $b_{\mathcal{M}}^{r}$  coefficients, with and without M limitation, was not a useless exercice as it results in considerable saving of memory-space. For example, in the case  $\ell = 20$ , R = 500, there could be 135561 vanishing and non-vanishing  $b_{\mathcal{M}}^{r}$  coefficients, whereas there are 67911 non-vanishing coefficients without M limitation. With M limitation (M = 20) this number is even reduced to the value 5161.

# 3.1.3 Storage of the $q_m^r$ , coefficients.

Quite analogously to the  $b_{\ell m}^{r}$  coefficients we have chosen to store only the non-vanishing  $b_{\ell m}^{r}$  coefficients in a one-dimension array.

The non-vanishing coefficients are stored in the following order:

- for a given m (m increasing), m = 0, 1, 2, ..., M,
- for a given r (r increasing), r = 0, 1, 2, ..., R,
- for a given l (l decreasing), l = 0, 1, 2, ..., L,

so the structure of the storage array is



Together with this structure of the array we have to define two additional quantities:

N(m) the number of non-zero  $q_{m,\ell}^r$  matrix coefficients for a given m, n(m,r) the number of non-zero  $q_{m,\ell}^r$  row coefficients for given m and r,

so that, anywhere a  $q_{m,\ell}^r$  coefficient has to be used in a routine, its location k in the array is obtained by the relation

$$k(m,\ell,r) = \sum_{i=0}^{m-1} N(i) + \sum_{j=0}^{r-1} n(m,j) + k_{1} , k_{1} = (m+r-\ell)/2 + 1$$

where the first summation gives the total number of non-vanishing coefficients corresponding to all previous m-values, the second one the number of coefficients up to r-1 and the last term is the position of the considered coefficient in the row. In order to get the maximum size K to assign to the storage array we will now investigate in more detail the number of non-zero coefficients to be stored in both cases: with and without L limitation.

3.1.3.1 NUMBER OF NON-VANISHING COEFFICIENTS WITHOUT L LIMITATION.

As mentioned in 3.1.2.2 we have to distinguish between the two cases: m-odd and m-even.

3.1.3.1.1 Non-vanishing coefficients for m-odd.

 $N_1(m) = (R+1)(R+2)/2 - v(R-m+1)$ .

In this relation the index 1 means that m is odd.

The number of elements per row  $n_1(m,r)$  is given by  $n_1(m,r) = r + 1 - IP[(r-m+2)/2]$ ;

 $N_{1}(m) = (R+1)(R+2)/2 ,$  $n_{1}(m,r) = r + 1 .$ 

R ≤ m-1

The dependence of  $N_1(m)$  on m and R is illustrated by the following **Table.** 

3.1.3.1.2 Non-vanishing coefficients for m-even.

### m/2 < R

 $N_2(m) = (R+1)(R+2)/2 - (2R-m)(2R-m+2)/8$ .

In this relation the index 2 means that m is even.

Table:	Number	of	non-vanishing	ar m.	coefficients	for	m-odd	anđ	without	L	limita-
tion.											

2												
	R/m	1	3	5	7	9	11	13	15	17	19	
	1	2	3	3	3	3	3	3	3	3	3	
	2	4	6	6	6	6	6	6	6	6	6	
	5	12	17	20	21	21	21	21	21	21	21	
Į	10	36	46	54	60	64	66	66	66	66	<del>6</del> 6	
l	20	121	141	159	175	189	201	211	219	225	229	
	50	676	726	774	820	864	906	946	984	1020	1054	
	100	2601	2701	2799	2895	2989	3081	3171	3259	3345	3429	
	150	5776	5926	6074	6220	6364	6506	6646	6784	6920	7054	
	200	10201	10401	10599	10795	10989	11181	11371	11559	11745	11929	
	500	63001	63501	63999	64495	64989	65481	65971	66459	66945	67429	
I												

The number of elements per row  $n_2(m,r)$  is given by:

 $n_2(m,r) = m/2 + 1$ ;

 $R \le m/2$ 

 $N_2(m) = (R+1)(R+2)/2$  ,  $n_2(m,r) = r + 1$  .

The dependence of  $N_2(m)$  on m and R is illustrated by the following **Table** (where implicitly  $N_2(0) = 1$ ).

Table: Number of non-vanishing  $q_{m\ell}^r$  coefficients for m-even and without L limitation.

R\m	2	4	6	8	10	12	14	16	18	20
1	3	3	3	3	3	3	3	3	3	3
2	5	6	6	6	6	6	6	6	6	6
5	11	15	18	20	21	21	21	21	21	21
10	21	30	38	45	51	56	60	63	65	66
20	41	60	78	95	111	126	140	153	165	176
50	101	150	198	245	291	336	380	423	465	506
100	201	300	398	495	591	686	780	873	965	1056
150	301	450	598	745	891	1036	1180	1323	1465	1606
200	401	600	798	995	1191	1386	1580	1773	1965	2156
500	1001	1500	1998	2495	2991	3486	3980	4473	4965	5456

Knowing the number of coefficients for each m-value, let us now consider their total number.

3.1.3.1.3 Total number of coefficients.

The total number of non-vanishing coefficients up to a given M-value given by

 $K(\mathbf{M},\mathbf{R}) = \begin{array}{c} \mathbf{M}' & \mathbf{M}'' \\ \mathbf{\Sigma} & \mathbf{N}_{1}(\mathbf{m}) + \mathbf{\Sigma} & \mathbf{N}_{2}(\mathbf{m}) \\ \mathbf{m} = 1 & \mathbf{m} = 0 \\ \Delta \mathbf{m} = 2 & \Delta \mathbf{m} = 2 \end{array}$ 

where M' (M") is the nearest lower odd (even) integer of M, and

 $\sum_{\substack{m=1\\m=1\\m=2}}^{M'} N_1(m) = \frac{M'-1}{2} \left[ \frac{1}{2} (R+1) (R+2) - v(R) \right] + \frac{R+1}{8} (M'-1) (M''+1) - \frac{1}{24} M'(M'-1) (M''+1)$  $\Delta m=2$   $\sum_{\substack{m=0\\m=0}}^{M''} N_2(m) = \frac{M''}{4} \left[ \frac{9}{4} + 3R + \frac{RM''}{2} - \frac{(M''-1)(M''+1)}{12} \right] .$ 

The total number of coefficients is given for some M and R values in the following **Table**, which shows that this number may be very large.

										_
r/m	1	2	3	4	5	7	10	15	20	
1	4	7	10	13	16	22	46	61	91	
2	7	12	18	24	30	42	60	90	120	
5	18	29	46	61	81	120	182	287	392	
10	47	68	114	144	198	296	456	770	1096	
20	142	183	324	384	543	796	1191	2088	3036	
50	727	828	1554	1704	2478	3496	4896	8448	11916	
100	2702	2903	5604	5904	8703	11996	16071	27048	36716	
150	5927	6228	12154	12604	18678	25496	33496	55648	74016	
200	10402	10803	21204	21804	32403	43996	57171	94248	123816	
500	63502	64503	128004	129504	193503	259996	330471	5358 <b>4</b> 8	685116	

**Table:** Total number of non-vanishing  $q_{m\ell}^r$  coefficients without L limitation.

3.1.3.2 NUMBER OF NON-VANISHING COEFFICIENTS WITH L LIMITATION.

For physical applications we are only interested in the  $q_{m\ell}^r$  coefficients with limited  $\ell$ -range,  $\ell = 0, 1, 2, ..., L$ .

In all the relations given below the prime "'" means that the number of coefficients should be understood as being with L limitation and the index 1 (2) indicates that m is odd (even).

3.1.3.2.1 Non-vanishing coefficients for m-odd.

The number of non-vanishing coefficients for m-odd is given by the following relations:

#### R < m

		2 <	m-R	№'(m) 1	#	0		
m-R	≤	1 <	m	N;(m)	=	v( <b>/-</b> m+R+1)		
m	≤	1 <	: m+R	N'(m) 1	=	(R+1)(R+2)/2	-	v(m+R-ℓ)
m+R	≤	1		N'(m)	=	(R+1)(R+2)/2	=	N ₁ (m) .

m≤R

1 ≤ <b>ℓ</b> < m	$N_{1}(m) = v(\ell + R - m + 1) - v(R - m + 1)$
m ≤ ℓ < m+R	$N_1'(m) = (R+1)(R+2)/2 - v(R-m+1) - v(m+R-\ell)$
m+R ≤ ℓ	$N_1(m) = (R+1)(R+2)/2 - v(R-m+1) = N_1(m)$

The dependence of N'₁(m) on m and R is illustrated by the following **Table** for L = 20.

The number of coefficients per row is given by the following relations:

 $\frac{\mathbf{r} < \mathbf{m}}{\ell} < \mathbf{m} - \mathbf{r} \qquad \mathbf{n}_{1}'(\mathbf{m}) = 0$  $\mathbf{m} - \mathbf{r} \le \ell \le \mathbf{m} \qquad \mathbf{n}_{1}'(\mathbf{m}) = \mathbf{IP}[(\ell - \mathbf{m} + \mathbf{r} + 2)/2]$  **Table:** Number of non-vanishing  $q_{m\ell}^r$  coefficients for m-odd and with L limitation, L = 20.

R/m	1	3	5	7	9	11	13	15	17	19
1	2	3	3	3	3	3	3	З	3	3
2	4	6	6	6	6	6	6	6	6	5
5	12	17	20	21	21	21	21	21	19	15
10	36	46	54	60	64	65	62	57	50	41
20	120	137	150	159	164	165	162	155	144	129
50	420	437	450	459	464	465	462	455	444	429
100	920	937	950	959	964	965	962	955	944	929
150	1420	1437	1450	1459	1464	1465	1462	1455	1444	1429
200	1920	1937	1950	1959	1964	1965	1962	1955	1944	1929
500	4920	4937	<b>49</b> 50	4959	4964	4965	4962	4955	4944	4929

m < l < m+r  $n_1'(m) = r + 1 - IP[(m+r-l+1)/2]$ 

 $m+r \leq \ell$   $n_1(m) = r + 1 = n_1(m,r)$ .

m≤r	
$\ell \leq m$	$n_1(m) = IP[(\ell+r-m+2)/2] - IP[(r-m+2)/2]$
m < l < m+r	$n_1(m) = r + 1 - IP[(r-m+1)/2] - IP[(m+r-\ell+1)/2]$
m+r ≤ ℓ	$n_1(m) = r + 1 - IP[(r-m+1)/2] = n_1(m,r)$ .

3.1.3.2.2 Non-vanishing coefficients for m-even.

The number of non-vanishing coefficients for m-even is given by the following relations:

 $R \leq m/2$  $\ell < m-R$ .  $N_2'(m) = 0$  $m-R \leq \ell < m$   $N_2^{\prime}(m) = v(\ell-m+R+1)$  $m \leq \ell < m+R$   $N_{2}^{\prime}(m) = (R+1)(R+2)/2 - v(m+R-\ell)$  $m+R \leq \ell$   $N_{2}(m) = (R+1)(R+2)/2 = N_{2}(m)$ •

$$\boxed{m/2 < R \le m}$$

$$\ell < m/2 \qquad N'_{2}(m) = 0$$

$$m/2 \le \ell < R \qquad N_2^{\dagger}(m) = (\ell - m/2 + 1)(\ell - m/2 + 2)/2$$

$$R \le \ell \le m \qquad N_2^{\dagger}(m) = (\ell - m/2 + 1)(\ell - m/2 + 2) - v(\ell - R + 1)$$

$$m < \ell < m + R \qquad N_2^{\dagger}(m) = (R + 1)(R + 2)/2 - (2R - m)(2R - m + 2)/8 - v(m + R - \ell)$$

$$m + R \le \ell \qquad N_2^{\dagger}(m) = (R + 1)(R + 2)/2 - (2R - m)(2R - m + 2)/8 = N_2(m) \qquad .$$

The dependence of  $N'_2(m)$  on m and R is illustrated by the following **Table** for L = 20 (implicitly  $N'_2(0) = 1$ ).

**Table:** Number of non-vanishing  $q_{m,\ell}^r$  coefficients for m-even and with L limitation, L = 20.

R\m	2	4	6	8	10	12	14	16	18	20
1	3	3	3	3	3	3	3	3	З	2
2	5	6	6	6	6	6	6	6	6	4
5	11	15	18	20	21	21	21	20	17	12
10	21	30	38	45	51	54	54	51	45	36
20	39	54	66	75	81	84	84	81	75	66
50	39	54	66	75	81	84	84	81	75	66
100	39	54	66	75	81	84	84	81	75	66
150	39	54	66	75	81	84	84	81	75	66
200	39	54	66	75	81	84	84	81	75	66
500	39	54	66	75	81	84	84	81	75	<del>6</del> 6

The numbers of coefficients per row is given by the following relations:

 $\frac{\mathbf{r} < \mathbf{m}/2}{\ell < \mathbf{m} - \mathbf{r}} \quad n_2^{i}(\mathbf{m}) = 0$ m-r  $\leq \ell < \mathbf{m} + \mathbf{r}$   $n_2^{i}(\mathbf{m}) = \mathbf{r} + 1 - IP[(\mathbf{m} + \mathbf{r} - \ell + 1)/2]$ m+r  $\leq \ell$   $n_2^{i}(\mathbf{m}) = \mathbf{r} + 1 = n_2(\mathbf{m}, \mathbf{r})$ .
$\frac{m/2 \le r}{\ell < r}$   $\ell < r \qquad n_2'(m) = 0$   $r \le \ell < m+r \qquad n_2'(m) = m/2 + 1 - IP[(m+r-\ell+1)/2]$   $m+r \le \ell \qquad n_2'(m) = m/2 + 1 = n_2(m,r) \qquad .$ 

3.1.3.2.3 Total number of coefficients.

The total number of non-vanishing coefficients up to a given M-value is given by

 $K'(M,L,R) = \sum_{\substack{m=1\\M=2}}^{M'} N_1(m) + \sum_{\substack{m=0\\M=2}}^{M''} N_2(m) ,$ 

where M' (M") is the nearest lower odd (even) integer of M.

This total number of coefficients is given for some M and R values in the following **Table** for the case L = 20.

**Table:** Total number of non-vanishing  $q_{m\ell}^r$  coefficients with L limitation, L = 20.

R\M	1	2	3	4	5	7	10	15	20
1	3	6	9	12	15	21	30	45	59
2	5	10	13	22	28	40	58	88	115
5	13	24	41	56	76	115	177	282	365
10	37	58	104	134	188	286	446	738	961
20	121	160	297	351	501	726	1046	1696	2191
50	421	460	897	951	1401	1926	2546	4096	5191
100	921	960	1897	1951	2901	3926	5046	8096	10191
150	1421	1460	2897	2951	4401	5926	7546	12096	15191
200	1921	1960	3897	3951	5901	7926	10046	16096	20191
500	4921	4960	9897	9951	14901	19926	25046	401.96	50191

#### 3.1.4 Conclusion.

The present indexation-system appears to be cumbersome. However, it has the following merits:

- it is appropriate for the problem studied,
- it avoids the use of heavy systems for file manipulation (e.g., ISAM and VSAM),
- it is machine and system independent,
- it can be implemented on small computers.

## 3.2 CALCULATION OF THE COEFFICIENTS b

We have given in **Taole 3.1** the matrices  $b_{Am}^r$  whose elements are represented as fractions in their lower terms. The calculation of these elements has been carried out by means of the program **MICOF** which uses, in order to avoid round-off errors, integer arithmetic to compute recurrently the numerator and the denominator of the fractions. More precisely, putting

$$b_{\ell m}^{r} = a_{\ell m}^{r} / \beta_{\ell m}^{r}$$
, where  $a_{\ell m}^{r}$  and  $\beta_{\ell m}^{r}$  are integers,

the recurrence formula (3.10) becomes

$$\frac{a_{\ell m}^{r+1}}{\beta_{\ell m}^{r+1}} = \frac{(m+1)(2m-1)(m+2-r) a_{\ell,m+1}^{r} \beta_{\ell,m-1}^{r} - m(2m+3)(m+r-1) a_{\ell,m-1}^{r} \beta_{\ell,m+1}^{r}}{(2m-1)(2m+3)(r+1) \beta_{\ell,m-1}^{r} \beta_{\ell,m+1}^{r}}$$

with the initial conditions

$$a_{\ell m}^0 = \delta_{\ell m}$$
 and  $\beta_{\ell m}^0 = 1$ .

This recurrence relation is equivalent to the two following coupled ones

$$a_{\ell m}^{r+1} = (m+1)(2m-1)(m+2-r) a_{\ell,m+1}^{r} \beta_{\ell,m-1}^{r} - m(2m+3)(m+r-1) a_{\ell,m-1}^{r} \beta_{\ell,m+1}^{r},$$
  
$$\beta_{\ell m}^{r+1} = (2m-1)(2m+3)(r+1) \beta_{\ell,m-1}^{r} \beta_{\ell,m+1}^{r},$$

where the last one has to be considered only if the numerator is non-vanishing (otherwise the denominator is equal to 1). At each step the fraction  $a/\beta$  is reduced by calculating the greatest common divisor of a and  $\beta$ .

Two particular cases have to be considered when m reaches the extreme values 0 and  $\ell$ +r:

m = 0

$$a_{\ell 0}^{r+1} = (r-2) a_{\ell 1}^{r}$$
  

$$\beta_{\ell 0}^{r+1} = -3(r+1) \beta_{\ell 1}^{r} ;$$
  

$$\boxed{m = \ell + r}$$
  

$$a_{\ell,\ell+r}^{r+1} = -(\ell + r)(2\ell + 2r + 3)(\ell + 2r - 1) a_{\ell,\ell+r-1}^{r}$$
  

$$\beta_{\ell,\ell+r}^{r+1} = (2\ell + 2r - 1)(2\ell + 2r + 3)(r+1) \beta_{\ell,\ell+r-1}^{r} .$$

But this type of integer calculations is rapidly limited by the maximum value of an integer variable on a CDC-7600 (2⁴⁰ in practice). So this program was only used to clearly show how the  $b_{\ell m}^r$  coefficients look for the first few values of the indexes (as given in **Table 3.1**). To go further into the calculation of the coefficients we had to use real arithmetic, making directly use of (3.10), especially to create a file of the  $b_{\ell m}^r$  coefficients.

As we have seen in Subsection 3.3.1 the calculation of the matrix elements  $T_{\ell m}(\gamma)$  could be splitted into two parts:

- the calculation of the coefficients b^r_{fm}, and
- the summation of the power series (3.9).

In order to avoid wasteful computation, we have created a sequential binary file by means of the program **MIFILE** making use of the indexation system previously described. The structure of this file is defined in Subsection 1.1.2 of this annex. To cover most of physical applications we have chosen the following limit values: L = M = 30, R = 500 with M limitation, so that the file contains 116516 non-vanishing  $b_{AIR}^{r}$  coefficients. As this file is a binary one it is computer dependent. To have the possibility to export the file we have transformed it into a formated one under the FORTRAN format E20.13 (14 significant figures). This relatively large number of significant figures was dictated by the simple following calculation. Starting from the internal binary set of  $b_{AIR}^{r}$  coefficients we have performed the calculation of the  $T_{AIR}(\gamma)$  with three different representations of the  $b_{AIR}^{r}$  coefficients:

 the binary file (which gives the maximum accuracy available) used as a standard,

- 14 significant figures (FORTRAN format E20.13),
- 10 significant figures (FORTRAN format E19.9).

The details of the calculations are given in the following **Table** where we present the partial sums of the series (3.9) for the matrix element  $T_{1,1,1}$ , ( $\gamma$ =0.9) (which is in fact a polynomial).

**Table:** Partials sums up to r of (3.9) using three different representations of the coefficients  $b_{,m}^{r}$  for the matrix element  $T_{1,1,1}(\gamma=0.9)$ .

r	internal	formated E20.13	formated E16.9
0	1.00000 00000E+00	1.00000 00000E+00	1.00000 00000E+00
2	-7.60007 25115E+01	-7.60007 25115E+01	-7.60007 2511 <u>6</u> E+01
4	1.39848 08941E+03	1.39848 08941E+03	1.39848 08938E+01
6	-1.08183 61150E+04	-1.08183 61150E+04	-1.08183 61150E+04
8	4.33346 83667E+04	4.33346 83667E+04	4.33346 83684E+04
10	-9.88802 95690E+04	-9.88802 95690E+04	-9.88802 95684E+04
12	1.33265 02262E+05	1.33265 02262E+05	1.33265 02263E+05
14	-1.04822 30428E+05	-1.04822 30428E+05	-1.04822 304 <u>37</u> E+05
16	4.44378 66155E+04	4.44378 66155E+04	4.44378 66076E+04
18	-7.83918 82422E+03	-7.83918 82422E+03	-7.83918 8 <u>3163</u> E+03
20	-4.24514 03075E-02	-4.24514 0 <u>7673</u> E-02	-4.2 <u>5254</u> 84692E-02

It appears from this **Table** that, even with 14 significant figures, the round-off errors are sensitive, but remain below the generally adopted relative error,  $\epsilon_{me} = 10^{-4}$ . On the other hand, the use of only 10 significant figures is not sufficient to ensure this relative accuracy.

3.3 CALCULATION OF THE FUNCTIONS  $T_{m}(\gamma)$  AND  $T_{m\ell}^{-1}(\gamma)$ .

Having now at our disposal a file of the coefficients  $b_{\ell m}^{\Gamma}$ , the computation of the functions  $T_{\ell m}(\gamma)$  is reduced to the summation of the power series (3.9) and the error check (3.41). The program **MlEPS** computes, for a given  $\gamma$ -value and relative error  $\epsilon_{me}$ , the matrices T,  $T^{-1}$  and the products  $T \cdot T^{-1}$ . This program is actually designed for calculations up to  $L = M \approx 20$ , R = 140 without M limitation or R = 400 with M limitation.

#### ANNEX 4. REPERTORY OF SOME USEFUL FORMULAE.

The following compilation of formulae is intended to help the reader of this report. They are either frequently used in it or are key-relations of this work.

This annex is subdivided into four parts, the first of which concerns key-relations of physical quantities, the second is devoted to Legendre polynomials, the third deals with Gegenbauer polynomials and the fourth is related to Gamma-functions.

#### 4.1 FORMULAE CONCERNING PHYSICAL QUANTITIES.

### **4.1.1** Relations of $\mu(\gamma)$ , $\tilde{\mu}(\gamma)$ .

$$\begin{aligned} \frac{1-\bar{\mu}^2}{1-\mu^2} &= \frac{(\gamma+\bar{\mu})^2}{\mu^2} , \\ \mu &= \cos(\theta), \ \gamma \text{ is defined in (2.5).} \\ \mu &= (\gamma+\bar{\mu})(1+2\gamma\bar{\mu}+\gamma^2)^{-1/2} , \quad \bar{\mu} &= \gamma(\mu^2-1) + \mu[\gamma^2(\mu^2-1)+1]^{1/2} , \\ \frac{\partial\mu}{\partial\bar{\mu}} &= (1+\gamma\bar{\mu})(1+2\gamma\bar{\mu}+\gamma^2)^{-3/2} , \quad \frac{\partial\bar{\mu}}{\partial\mu} &= 2\gamma\mu + \frac{1+2\gamma^2\mu^2-\gamma^2}{[1+\gamma^2(\mu^2-1)]^{1/2}} \\ &= \frac{\{\gamma\mu + [1+\gamma^2(\mu^2-1)]^{1/2}\}^2}{[1+\gamma^2(\mu^2-1)]^{1/2}} \\ &= \gamma[2\mu + (\mu^2+a^2)^{1/2} + \mu^2(\mu^2+a^2)^{-1/2}] \\ &a^2 &= \frac{1-\gamma^2}{\gamma^2} , \end{aligned}$$

 $\frac{\partial \mu}{\partial \bar{\mu}} = \sum_{n=0}^{\infty} (-\gamma)^n (n+1) P_n(\bar{\mu}) ,$ 

$$\frac{\partial \mu}{\partial \gamma} = (1 - \bar{\mu})^2 (1 + 2\gamma \bar{\mu} + \gamma^2)^{-3/2} , \quad \frac{\partial \bar{\mu}}{\partial \gamma} = (\mu^2 - 1)(1 + \frac{\gamma \mu}{[1 + \gamma^2(\mu^2 - 1)]^{1/2}}) .$$

#### 4.1.2 Relations concerning the scattering angular distribution.

We present in this subsection some basic kinematic definitions and transformation formulae concerning the scattering reactions within a non-relativistic description.

4.1.2.1 Definitions.

The physical process under study is schematized in the following diagram in both systems of reference:

- the laboratory system, defined as the reference system where the target particle is at rest, and
- the center-of-mass system, defined as the reference system where the sum of the momenta is zero.



The definitions of most of the physical quantities involved in a scattering process are given in the following **Table**.

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- the four particles move in a same plane, and
- the process is symmetric with respect to the z axis ( $\phi$  angle).

Table: Definitions of physical quantities involved in a scattering process.

Quantity System	Laboratory	Center-of-mass
Before scattering		
Total mass	$M = m_1 + m_2$	$M = m_1 + m_2$
Energy		^m 2 _
Total kinetic	$E = E_1 + E_2$	$\mathbf{E} = \mathbf{E}_1 + \mathbf{E}_2 = \mathbf{\overline{M}} \mathbf{E}_1$
Incident particle	E1	$\bar{E}_{1} = \frac{m_{2}}{M} \bar{E} = (\frac{m_{2}}{M})^{2} E_{1}$
Target particle	E ₂ (=0)	$\overline{E}_2 = \frac{m_1}{M} E = \frac{m_1 m_2}{M^2} E_1$
Center-of-mass motion	m	
VCM	$\frac{m_1}{M}$ v ₁	
E _{CM}	^m 1 E ₁	
After scattering		
Total mass	$M = m_3 + m_4 = m_1 + m_2$	$M = m_3 + m_4 = m_1 + m_2$
Energy Total kinetic	E ₃ +E ₄ = E ≺ Q	$\bar{E}_3 + \bar{E}_4 = \bar{E} + Q$
Outgoing particle	$E_3(\theta_3)$	$\bar{E}_3 = \frac{m_4}{M} (\bar{E}+Q) = \frac{m_2m_4}{M^2} (E_1 + \frac{M}{m_2}Q)$
Residual particle	$E_4(\theta_4)$	$\bar{E}_4 = \frac{m_3}{M} (\bar{E}+Q) = \frac{m_2m_3}{M^2} (E_1 + \frac{M}{m_2}Q)$
Constants of motion		
Q	$Q = E_3 + E_4 - E$	$Q = \tilde{E}_3 + \tilde{E}_4 - \tilde{E}$
$\gamma = \frac{v_{\rm CM}}{\bar{v}_3}$	$\gamma^{2} = \frac{m_{1}m_{3}}{m_{2}m_{4}} \frac{1}{1 + \frac{M}{m_{2}}} \frac{Q}{E}$	$\gamma^{2} = \frac{m_{1}m_{3}}{m_{2}m_{4}} \frac{1}{1 + \frac{Q}{E}}$
Solid angle	sinθ dθ dφ	sin <del>0</del> d <del>0</del> d <del>0</del>
Differential cross section	₫ơ/đω	รสิต/สมี

The kinematic parameter  $\gamma$  is defined as the ratio of the velocity of the center-of-mass measured in the laboratory system and the velocity of the outgoing particle in the center-of-mass system. The six quantities characterizing a scattering process:  $m_1$ ,  $m_2$ ,  $m_3$ ,  $m_4$ ,  $E_1$  and Q are thus combined into a single parameter. This parameter, which is a constant of motion, is also a characteristic quantity of angular distributions just as the coefficients a or  $\bar{a}$  and gives a measure of the distorsion of angular distributions when transforming them from one reference system to the other.

From these definitions it appears, in particular, that the kinetic energy of the outgoing particle is, for a given incident particle energy, constant in the center-of-mass system, whereas this energy is angle dependent in the laboratory system. This dependence may be written

 $x = \pm (1 - \gamma^2 \sin \theta)^{1/2} + \gamma \cos \theta$ , where  $x = v_3 / \bar{v}_3 = (E_3 / \bar{E}_3)^{1/2}$ 

This relation shows that:

- If  $\gamma < 1$ , the outgoing particle kinetic energy is a single valued function of the scattering angle,
- if  $\gamma \ge 1$ , this energy is a **double valued** function of the laboratory scattering angle. Moreover, there is a limit angle  $\theta_{\max}$  beyond which no particle can be scattered. This angle is defined by

$$\theta_{\max} = \operatorname{Arc} \sin(1/\gamma)$$

In other words, there are, in the case  $\gamma \ge 1$ , two different center-of-mass scattering angles leading to the same laboratory angle at which the outgoing particle can have two different energies.

4.1.2.2 Transformation of physical quantities for  $\gamma < 1$ .

The main kinematic formulae, used in the transformation of physical quantities from one system of reference to the other, are, for the case  $\gamma < 1$ , given in the subsequent **Table**.

Transformation Quantity	Center-of-mass to laboratory	Laboratory to center-of-mass
Angle	$tg\theta = \frac{\sin\bar{\theta}}{\gamma + \cos\bar{\theta}}$	$\overline{\theta} = \theta + \operatorname{Arc} \sin(\gamma \sin \theta)$
	$\mu = \frac{\gamma + \bar{\mu}}{(1+2\gamma\bar{\mu}+\gamma^2)^{1/2}}$	$\bar{\mu} = \gamma(\mu^2 - 1) + \mu [\gamma^2(\mu^2 - 1) + 1]^{1/2}$
Solid angle	$d\omega = \frac{1 + \gamma \bar{\mu}}{(1 + 2\gamma \bar{\mu} + \gamma^2)^{3/2}} d\bar{\omega}$	$d\tilde{\omega} = \frac{\{\gamma \mu + [\gamma^2(\mu^2 - 1) + 1]^{1/2}\}^2}{[\gamma^2(\mu^2 - 1) + 1]^{1/2}} d\omega$
Energy	$E = \vec{E} (1+2\gamma \vec{\mu} + \gamma^2)$	$\bar{E} = E / \{\gamma \mu + [\gamma^2 (\mu^2 - 1) + 1]^{1/2}\}^2$
Integrated cross section	$\sigma = \overline{\sigma}$	$\overline{\sigma} = \sigma$
Differential cross section	$\frac{d\sigma}{d\omega} = \frac{1+2\gamma\bar{\mu}+\gamma^2}{1+\gamma\bar{\mu}} \frac{d\bar{\sigma}}{d\omega}$	$\frac{d\bar{\sigma}}{d\bar{\omega}} = \frac{\{\gamma\mu + [\gamma^2(\mu^2 - 1) + 1]^{1/2}\}^2}{[\gamma^2(\mu^2 - 1) + 1]^{1/2}} \frac{d\sigma}{d\omega}$

**Table:** Transformation formulae of physical quantities for  $\gamma < 1$ .

# 4.2 FORMULAE CONCERNING LEGENDRE POLYNOMIALS P.

There exist excellent books treating these very important polynomials. We only mention here some classical works [HE78], [RO57], [HO55] and the well known general mathematical formulae compilations [AB64], [GR65].

#### 4.2.1 Definition and representation.

$$P_{n}(\mu) = \frac{1}{2^{n} n!} \frac{d^{n}}{d\mu^{n}} (\mu^{2} - 1)^{n}$$

Legendre polynomials written in expanded form:

.

$$\begin{split} P_{n}(\mu) &= \frac{1}{2^{n}} \sum_{k=0}^{\left[n/2\right]} \frac{(-1)^{k} (2n-2k)!}{k! (n-k)! (n-2k)!} \mu^{n-2k} = \sum_{k=\text{mod}(n,2)}^{n} a_{nk} \mu^{k} \\ &= \frac{(2n)!}{2n (n!)^{2}} (\mu^{n} - \frac{n(n-1)}{2(2n-1)} \mu^{n-2} + \frac{n(n-1)(n-2)(n-3)}{2.4(2n-1)(2n-3)} \mu^{n-4} - \dots) \\ &= \frac{(2n-1)!!}{n!} \mu^{n} F(-\frac{n}{2}, \frac{1-n}{2}; \frac{1}{2} - n; \mu^{-2}) , \\ P_{2n}(\mu) &= (-1)^{n} \frac{(2n-1)!!}{2^{n} n!} (1 - \frac{2n(2n+1)}{2!} \mu^{2} + \frac{2n(2n-2)(2n+1)(2n+3)}{4!} \mu^{4} - \dots) \\ &= (-1)^{n} \frac{(2n-1)!!}{2^{n} n!} F(-n, n+\frac{1}{2}; \frac{1}{2}; \mu^{2}) , \\ P_{2n+1}(\mu) &= (-1)^{n} \frac{(2n+1)!!}{2^{n} n!} (\mu - \frac{2n(2n+3)}{3!} \mu^{3} + \frac{2n(2n-2)(2n+3)(2n+5)}{5!} \mu^{5} - \\ &= (-1)^{n} \frac{(2n+1)!!}{2^{n} n!} \mu F(-n, n+\frac{3}{2}; \frac{3}{2}; \mu^{2}) . \end{split}$$

**Table:** Leading terms of Legendre polynomials  $P_n(\mu)$  (d is common denominator).

_	đ	μ ⁰	μ ¹	μ ²	μ ³	μ ⁴	μ ⁵	μ ⁶
Po	1	1						
P1	1		1					
P ₂	2	-1		З				
P ₃	2		-3		5			
P.	8	3		-30		35		
Ps	8		15		-70		63	
P.	16	-5		105		-315		231

$$P_{n}(1-2\mu^{2}) = \sum_{j=0}^{n} b_{nj} \mu^{2j}$$

**Table:** Leading terms of Legendre polynomials  $P_n(1-2\mu^2)$ .

•

	μ ⁰	μ ²	μ ⁴	μ ⁶	μ ⁸	µ ¹⁰	µ ¹²
P.	1						
P ₁	1	-2					
$P_2$	1	-6	6				
P3	1	-12	30	-20			
P4	1	-20	90	-140	70		
P _s	1	-30	210	-560	630	-252	
P.	1	-42	420	-1680	3150	-2772	924

## 4.2.2 The generating function.

$$(1 - 2\gamma\mu + \gamma^{2})^{-1/2} = \sum_{k=0}^{\infty} \gamma^{k} P_{k}(\mu) , \quad |\gamma| < \min |\mu \pm (\mu^{2} - 1)^{1/2}|$$
$$= \sum_{k=0}^{\infty} \frac{1}{\gamma^{k+1}} P_{k}(\mu) , \quad |\gamma| > \max |\mu \pm (\mu^{2} - 1)^{1/2}|$$

•

$$\frac{1-\gamma^2}{(1-2\gamma\mu+\mu^2)^{3/2}} = \sum_{n=0}^{\infty} (2n+1) \gamma^n P_n(\mu)$$

# 4.2.3 The zeros of $P_n(\mu)$ .

The zeros of  $P_n(\mu) = 0$  are all real, distinct and lie in the interval: [-1,1].

## 4.2.4 Recurrence formulae.

$$P_{n+1}(\mu) = \frac{1}{n+1} [(2n+1) \mu P_n(\mu) - n P_{n-1}(\mu)] ,$$
  

$$\mu P_n(\mu) = \frac{1}{2n+1} [(n+1) P_{n+1}(\mu) + n P_{n-1}(\mu)] ,$$
  

$$\mu^2 P_n(\mu) = \frac{1}{2n+1} [\frac{(n+1)(n+2)}{2n+3} P_{n+2}(\mu) + \frac{(2n+1)(2n^2+2n-1)}{(2n-1)(2n+3)} P_n(\mu) + \frac{n(n-1)}{2n-1} P_{n-2}(\mu)] ,$$
  

$$(1 - \mu^2) \frac{dP_n}{d\mu} = n [\mu P_n(\mu) - P_{n-1}(\mu)] = \frac{1}{2n+1} [P_{n+1}(\mu) - P_{n-1}(\mu)] .$$

## 4.2.5 Inequalities.

.

,

$$\begin{split} \left[ P_{n}(\cos\theta) \right]^{2} &> \frac{\sin(2n+1)\theta}{(2n+1)\sin\theta} \qquad (0 < \theta < \pi) \\ \sqrt{n \sin\theta} \left| P_{n}(\cos\theta) \right| \leq 1 \quad , \\ \left| P_{n}(\cos\theta) \right| \leq 1 \quad , \\ \left| P_{n}(\cos\theta) \right| \leq 2 \left( n \pi \sin\theta \right)^{-1/2} \quad . \end{split}$$

#### 4.2.6 Products.

$$P_{n}(\mu) P_{m}(\mu) = \sum_{k=0}^{m} \frac{a_{m-k} a_{k} a_{n-k}}{a_{n+m-k}} \frac{(2n+2m-4k+1)}{(2n+2m-2k+1)} P_{n+m-2k}(\mu)$$

$$a_{k} = \frac{(2k-1)!!}{k!} , \quad a_{0} = 1 ,$$

$$P_{n}(\mu) P_{m}(\mu) = \sum_{\substack{k=|m-n|\\\Delta k=2}}^{m+n} < n \circ m \circ |k \circ|^{2} P_{k}(\mu) .$$

where  $\langle n 0 m 0 | k \rangle$  denotes CLEBSCH-GORDON coefficients.

### 4.2.6.1 CLEBSCH-GORDON COEFFICIENTS.

The particular CLEBSCH-GORDON coefficients  $C(n,m,k) = \langle n \ 0 \ m \ 0 \ k \ 0 \rangle$  are equal to zero if n+m+k is odd. If n, m, k satisfy the triangular inequalities and n+m+k = 2p is even, they are calculated by means of the relation [ED60]  $c^{2}(n,m,k) = \frac{1}{(2p+1)(2k+1)} \frac{r(p-n) \ r(p-m) \ r(p-k)}{r(p)}$ , where  $r(p) = \frac{(2p)!}{(p!)^{2}}$ .

We give in the following Table some explicit values of these coefficients.

Note that the CLEBSCH-GORDON coefficients are related to the 3-j symbols by  $(n \ 0 \ m \ 0 \ k \ 0)^2 = \frac{2k+1}{2} \begin{pmatrix} n \ m \ k \\ 0 \ 0 \ 0 \end{pmatrix}^2$ . **Table:** Explicit values of some CLEBSCH-GORDON coefficients  $C^{2}(n,m,k)$ , n = 0, 1, 2, 3, 4.

n		$c^2(n,m,k)$	]
L			
0	k = m	1	
1	k = m+1 k = m-1	$\frac{m+1}{2m+1}$	
		2m+1	
2	k = m+2	$\frac{3}{2} \frac{(m+1)(m+2)}{(2m+1)(2m+3)}$	
	k = m	$\frac{m(m+1)}{(2m-1)(2m+3)}$	
	k = m−2	$\frac{3}{2} \frac{(m-1)m}{(2m-1)(2m+1)}$	
3	k = m+3	$\frac{5}{2} \frac{(m+1)(m+2)(m+3)}{(2m+1)(2m+3)(2m+5)}$	$\begin{vmatrix} n+m \\ \Sigma \\ j= n-m  \end{vmatrix} c^2(n,m,j) = 1.$
	k = m+1	$\frac{3}{2} \frac{m(m+1)(m+2)}{(2m+1)(2m+5)}$	
	k = m-1	$\frac{3}{2} \frac{(m-1)m(m+1)}{(2m-3)(2m+1)(2m+3)}$	
	k = m−3	$\frac{5}{2} \frac{(m-2)(m-1)m}{(2m-3)(2m-1)(2m+1)}$	
4	k = m+4	35 (m+1)(m+2)(m+3)(m+4) 8 (2m+1)(2n+3)(2m+5)(2m+7)	
	k = m+2	$\frac{5}{2} \frac{m(m+1)(m+2)(m+3)}{(2m-1)(2m+1)(2m+3)(2m+7)}$	
	k = m	$\frac{9}{4} \frac{(m-1)m(m+1)(m+2)}{(2m-3)(2m-1)(2m+3)(2m+5)}$	
	k = m−2	$\frac{5}{2} \frac{(m-2)(m-1)m(m+1)}{(2m-5)(2m-1)(2m+1)(2m+3)}$	
	k = m-4	$\frac{35}{8} \frac{(m-3)(m-2)(m-1)m}{(2m-5)(2m-3)(2m-1)(2m+1)}$	

4.2.7 Integrals.

$$\int_{-1}^{1} P_{n}^{m}(\mu) P_{k}^{m}(\mu) d\mu = 0 \qquad n \neq k$$
$$= \frac{2}{2n+1} \frac{(n+m)!}{(n-m)!} \qquad n = k \quad .$$

------

•

$$I_{k\ell}^{0} = \int_{0}^{1} \mu^{k} P_{\ell}(\mu) d\mu = \frac{\sqrt{\pi} \Gamma(k+1)}{2^{k+1} \Gamma(1 + \frac{k-\ell}{2}) \Gamma(\frac{3}{2} + \frac{k+\ell}{2})} \qquad k > -1$$

**Table:** Values of the integral  $I_{k,\ell}^0$ .

k (	0	1	2	3	4	5
0	1	1/2	0	<u>-1</u> 8	0	$\frac{1}{16}$
1	$\frac{1}{2}$	1	18	0	$\frac{-1}{48}$	0
2	13	$\frac{1}{4}$	$\frac{2}{15}$	$\frac{1}{24}$	0	$\frac{-1}{192}$
з	$\frac{1}{4}$	15	1 8	$\frac{2}{35}$	$\frac{1}{64}$	0
4	$\frac{1}{5}$	16	4 35	$\frac{1}{16}$	<u>8</u> 315	$\frac{1}{160}$
5	$\frac{1}{6}$	$\frac{1}{7}$	$\frac{1}{48}$	$\frac{4}{63}$	$\frac{1}{32}$	<u>4</u> 693

**Table:** Values of the integral  $I_{k\ell}^1$ .

				-		
<u>k</u> 1	0	1	2	3	4	5
0	2					
1	٥	2 3				
2	$\frac{2}{3}$	0	$\frac{4}{15}$			
3	o	2 5	0	$\frac{4}{35}$		
4	2 5	0	<u>8</u> 35	0	$\frac{16}{315}$	
5	0	$\frac{2}{7}$	0	<u>8</u> 63	0	<u>8</u> 693

$$\int_{-1}^{1} \frac{\mu^{2k-1}}{(1-2\mu^2)} P_n(1-2\mu^2) d\mu = \frac{(-1)^n [\Gamma(k)]^2}{2 \Gamma(k+n+1) \Gamma(k-n)} \qquad \text{Re}(k) > 0 \qquad .$$

$$\int_{-1}^{1} \frac{P_n(\mu) d\mu}{(1-2\gamma\mu+\gamma^2)^{1/2}} = \frac{2\gamma^n}{2n+1} \qquad .$$

$$\int_{-1}^{1} P_{k}(\mu) P_{p}(\mu) P_{n}(\mu) d\mu = \frac{2}{2s+1} \frac{A_{s-k} A_{s-p} A_{s-n}}{A_{s}} , A_{s} = \frac{(2s-1)!!}{s!}$$
$$= \frac{2}{2k+1} ^{2}$$
$$= (\frac{p \ n \ k}{0 \ 0 \ 0})^{2} .$$

### 4.2.8 Particular values.

$$P_{n}(1) = 1 , P_{n}(-1) = (-1)^{n} ,$$

$$P_{n}(0) = 0 \qquad n - odd,$$

$$= (-1)^{n/2} \frac{1 \cdot 3 \cdot 5 \cdot . \cdot (n - 1)}{2 \cdot 4 \cdot . \cdot n} \qquad n - even.$$

## 4.2.9 Particular relations.

$$\frac{dP_{n}(\mu)}{d\mu} = \sum_{p=0}^{\left[\frac{n-1}{2}\right]} (2n-4p-1) P_{n-1-2p}(\mu) ,$$

$$\frac{d^{m}P_{n}(\mu)}{d\mu^{m}} = \frac{1}{(m-1)!} \sum_{\substack{p=0 \\ p=0}}^{m-m} (2n-2m-4p+1)(p+1)(p+2) \dots (2n-2p-3) \dots$$

$$P_{n}\left[\frac{\mu + N}{(N + 2\mu N + 1)^{1/2}}\right] = \left[\frac{N + P(\mu)}{(N^{2} + 2\mu N + 1)^{1/2}}\right]^{n}$$

(from [R057, Vol.3, p.27]) where the successive powers of  $P(\mu)$  are to be replaced by Legendre polynomials of the same order.

#### 4.3 FORMULAE CONCERNING GEGENBAUER POLYNOMIALS.

#### 4.3.1 Definition.

The polynomials  $C_n^{\lambda}(\mu)$  of degree n are the coefficients of  $\gamma^n$  in the power-series expansion of the function

$$(1-2\gamma\mu+\gamma^2)^{-\lambda} \approx \sum_{n=0}^{\infty} C_n^{\lambda}(\mu) \gamma^n \quad , \quad |\gamma| < |\mu-(\mu^2-1)^{1/2}| \quad .$$

Thus, the polynomials  $C_n^{\lambda}(\mu)$  are a generalization of the Legendre polynomials.

#### 4.3.2 Recurrence relation.

$$(2\lambda+n) \ c_n^{\lambda}(\mu) = 2\lambda \ [c_n^{\lambda+1}(\mu) - \mu \ c_{n-1}^{\lambda+1}(\mu)]$$

## 4.3.3 Connection with Legendre polynomials.

$$C_{n-m}^{m+1/2}(\mu) = \frac{1}{(2m-1)!!} \frac{d^{m}P_{n}(\mu)}{d\mu^{m}} = (-1)^{m} \frac{(1-\mu^{2})^{-m/2} m! 2^{m}}{(2m)!} P_{n}^{m}(\mu) ,$$

$$C_{n}^{1/2}(\mu) = P_{n}(\mu) .$$

## 4.3.4 Integral.

$$\int_{-1}^{+1} (1-x)^{a} (1+x)^{\nu-1/2} C_{m}^{\mu}(x) C_{\ell}^{\nu}(x) dx =$$

$$= \frac{2^{a+\nu+1/2} \Gamma(a+1) \Gamma(\nu+1/2) \Gamma(\nu-a+\ell-1/2) \Gamma(2\mu+m) \Gamma(2\nu+\ell)}{m! \ell! \Gamma(\nu-a-1/2) \Gamma(\nu-a+\ell+3/2) \Gamma(2\mu) \Gamma(2\nu)} \cdot$$

$$\cdot \frac{4^{F_{3}}(-m,m+2\mu,a+1,a-\nu+3/2;\mu+1/2,a+\nu+\ell+3/2,a-\nu-\ell+3/2;1)}{R\epsilon a > -1, R\epsilon \nu > -1/2,$$

where  ${}_4F_3$  is a hypergeometric series and  $\Gamma$  denotes the Gamma-function.

### 4.4 FORMULAE CONCERNING GAMMA-FUNCTION.

#### 4.4.1 Definitions.

$$\Gamma(n+1) = n \Gamma(n) , \qquad \Gamma(n+1) = n! ,$$

$$\Gamma(1/2+n) = \frac{\sqrt{\pi}}{2^{n}} (2n-1)!! , \qquad \Gamma(1/2-n) = \frac{(-2)^{n}}{(2n-1)!!} \sqrt{\pi}$$

$$\Gamma(1/2+n) \Gamma(1/2-n) = (-1)^{n} \pi .$$

,

$$(2n-1)!! = 1.3.5. \dots (2n-1) = \frac{(2n)!}{2^{n} n!}$$

$$(2n+1)!! = \frac{(2n+1)!}{2^{n} n!},$$

$$(-1)!! = 1 .$$

Throughout this report we have also used the notation

.

$$[-(2n+1)]!! = \frac{(-1)^n}{(2n-1)!!}$$

,

## 4.4.2 Special values.

We give in the following **Table** some special values of the Gamma-function for half integer values of the argument.

Table: Some special values of the Gamma-function.

n	0	1	2	3	4	5
$\frac{1}{\sqrt{\pi}} \Gamma(\frac{1}{2} + n)$	1	$\frac{1}{2}$	<u>3</u> 4	<u>15</u> 8	<u>105</u> 16	<u>945</u> 32
$\frac{1}{\sqrt{\pi}} \Gamma(\frac{1}{2} - n)$	1	-2	<u>4</u> 3	<u>-8</u> 15	<u>16</u> 105	<u>-32</u> 945

Symbols preceded by the bold point "•" denote physical quantities which exist in both reference systems: laboratory and center-of-mass. In the latter case they are marked with a bar, for example,  $\bar{\mu}$ .

A	Accuracy matrix (4.4), (4.8)
• a _l (E)	Coefficients of the Legendre polynomials series (2.7)
ar <i>t</i> m	Polynomials coefficients (3.60)
br em	Taylor series coefficients (3.9)
$c_n^{\lambda}(\mu)$	Gegenbauer polynomials
C(n,m,k)	Clebsch-Gordon coefficients (4.1) <n 0="" m=""  k=""></n>
• E	Incident particle energy
e	Relative error
γ	Physical quantity (2.5)
Г	Gamma function
Log	Natural logarithm
• μ	$\cos \theta$
( <mark>n</mark> )	Binomial coefficients (3.29)
Pn	Legendre polynomials
ar m.ℓ	Taylor series coefficients (3.48)
R	Precision matrix (3.41)
S	Precision matrix (3.80)
• σ	Integrated cross-section
• $\frac{\mathrm{d}\sigma(\mu, \mathrm{E})}{\mathrm{d}\mu}$	Angular distribution cross section (2.7), (2.8)
T, T ⁻¹	Transformation matrices (2.13), (2.15)
Ŧ	Computing time (seconds)

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