DIFFERENTIAL NEUTRON EMISSION CROSS SECTIONS FROM
LEAD AND CARBON BOMBARDED WITH 14 MeV NEUTRONS
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Technische Universität Dresden, Sektion Physik,
Mommenstr. 13, Dresden, DDR-8027, GDR

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#### Abstract

Neutron emission cross sections measured with a time-of flight spectrometer which allows accurately to take angular distributions are presented. The date are compared with previous experimental results and with calculations basing on direct, pre-equilibrium and equilibrium emission models.


## 1. Introduction

Lead is used as neutron multiplier material in conceptual designs of fusion reactors $/ 1 /$. Therefore, the differential neutron emission cross sections at 14 MeV neutron incidence energy have to be determined with relatively high accuracy /2/. Direct and preequilibrium reaction components cause anisotropic, forward-peaked angular distributions, so that the emission spectra must be studied for a wide angular range, especially in their high-energy part. In earlier measurements, spectra were taken only at $90^{\circ}$ /3,4/. Later on, angular ranges from $25^{\circ}$ to $145^{\circ} / 5 /$ and from $40^{\circ}$ to $150^{\circ} / 6 /$, respectively, were covered. The low-energy part of the emission spectrum was angle-averaged measured by Vonach et al. /7/. Recently, Takahashi et al. /8/ determined spectra with a high-resolution spectrometer from $15^{\circ}$ to $154^{\circ}$.
At the TU Dresden, a time-of-flight (TOF) spectrometer was developed which allows by its arrangement and data acquisition procedure to take spectra from $15^{\circ}$ to $165^{\circ}$ with widely equal experimental conditions. The spectrometer is described in chapter 2. The obtained data and comparisions with those of previous works are given in chapter 3. A carbon sample was parallely with the lead sample used in the measurements to check spectrometer and data reduction. The obtained data from carbon are also given in chapter 3 .

## 2. Experiment

The geometrical arrangement is shown in Fig. 1. Ring geometry with flight path perpendicularly arranged to the deuteron beam direction, was chosen. The distance between tritium target and neutron detector was 4.9 m . Collimator channel, shadow bar, sample ring and neutron source diameter allowed to measure at scattering angles $15^{\circ} \leq \boldsymbol{n} \leq 165^{\circ}$.

The neutron generator operated in a pulsed regime with deuteron pulses of 2 ns f.w.h.m. and 5 MHz repetition rate /9/, produced
x-Zentralinstitut für Kernforschung, Rossendorf
with a mean deuteron beam of $30 \mu \mathrm{~A}$ a P i-T-target 2...5x $10^{9}$ neutrons/s. The source strength was determined by counting the $\alpha$-particles with a silicon surface-barrier detector at $\phi_{0}=166^{\circ}$ with respect to the deuteron beam direction. From $\mathrm{dN} \alpha\left(\phi_{0}\right) / \mathrm{d} \Omega$ the neutron production for all directions $\theta$ to the deuteron beam $d N_{n}(\theta) / d \Omega$ was determined calculating $f\left(\theta, \phi_{0}\right)=\frac{d N_{\alpha}}{d \Sigma}\left(\phi_{0}\right) / \frac{d N_{n}}{d \Sigma}(\theta)$ for the thick Ti-T-layers of the used targets and measuring the influence of tarcet tube, backing and cooling on the source neutron distribution with ${ }^{27} \mathrm{Al}(\mathrm{n}, \alpha)$-activation and recoil-proton counting (plastic scintillator, bias at 7 MeV ) for the full range of $\theta=0^{\circ} \ldots 180^{\circ}$. The $f\left(\theta, \phi_{0}\right)$ corrected for influences of the target construction were used to calculate for each sample position $f_{1}\left(M, \phi_{0}\right)=\frac{d x}{d}\left(\phi_{0}\right) / \frac{d M n}{d}(M)$ by averaging over all $\theta$ covered by the sample ring. The average neutron incidence energies $E_{0}(\{ )$ ) were analogously determined. The energy distributions of the neutrons were calculated as functions of $\theta$, and averaging the spectra of those $\theta$ covered by the given ring positions resulted in the incidence energy spectra for the $\boldsymbol{N}$, with their average $E_{0}(N) . E_{0}(N)$ and $f_{9}\left(N, \phi_{0}\right)$ are shown in Fig. 2. Their dependence on $g$ is very weak, since the flight path was arranged at $\theta=90^{\circ}$. Furthermore, both functions are symmetric to $\theta=90^{\circ}$, so that no asymmetries are induced in the neutron emission spectra.

The samples had natural isotopic compositions. The ring had inner diameters of 8.0 cm and outer diameters of 12.0 cm . Their thicknesses in flight-path direction were 1.0 cm for Pb and 1.5 cm for C (pressed powder of density $1.45 \mathrm{~g} / \mathrm{cm}^{3}$ ) respectively. A ring segment of 4.4 cm width was taken away at the deuteron-beam-tube position in measurements around $M=90^{\circ}$.

The block scheme of the spectrometer is shown in Fig. 3. The neutron TOF detector was a liquid scintillator NE 213 of 12.7 cm in diameter and 3.8 cm length coupled with a XP 2041 photomultiplier. Its anode signals were used for timing as well as for neutron-camma discrimination $/ 10 /$ and proton-recoil basing. The neutron detector efficiency $\varepsilon(E)$ was measured by TOF spectrometry of the neutrons emitted from a Cf-252 fission chamber $/ 11 /$, of the neutons scattered from H replacing the Pb sample in the spectrometer arrancement with a thin polyethylene rind (thickness 0.4 cm ) and of the 14 HeV neutrons of the generator removing the shadow bar in the spectrometer.
Besides this measurements, $\varepsilon(E)$ was calculated with the Monte Carlo code NEUCEF /12/. The results are shown in Fig. 4 together with the curve used for the data reduction.
'i'he neutron source strength monitored by the $\alpha$-particle counter was checked during foF measurements against the counts of two neutron monitors (a plastic scintillation detector with 7 MeV bias and a long counter).
A microcomputer controlled the rof runs. Sample shifting ( $M$ ) and changing were frec programmable.

Measurements of TOF spectra were carried out for $\boldsymbol{M}$ from $15^{\circ}$ to $165^{\circ}$ in steps of $15^{\circ}$. In one run, 5 or 6 of these $\boldsymbol{A}$ were chosen symmetrically to $\mathcal{M}=90^{\circ}$ and the run was so subdivided in shorttime data acquisition periods that the of could be successively covered more than 10 times. 'rhe spectra obtained in short-time measurements with and without sample were inspected using the number of events in a given part of the spectrum, the position of the 14 HeV neutron peak and the counts of the monitors and of

Fig. 1
Geometrical arrangement of the time-of-flight spectrometer. T, tritium target;
S, ring sample;
D, neutron detector.

Fig. 2
Average incidence neutron energy (upper part) and number of $\alpha$-particles/sr counted per neutron/sr (lower part) striking on the sample ring (dashed curves) and on the ring without a segment of 4.4 cm width (solid curves), respectively, as function of the scattering angle.

## Fig. 3

Block scheme of the spectrometer.
T, tritium target; $S$, sample;
D, neutron detector;
ZC, zero-crossing trigger;
CF, constant-fraction trigger;
$B_{n}$, proton-recoil-energy dis-
criminator; $n / \gamma$, neutron-
gamma discriminator;
CO, coincidence; 9, sample shifter; $太$, sample changer; TAC, time-to-amplitude converter; U/D-C, up-and-down counter; $A D C$, analog-to-digital converter; $C C$, controller of the CAMAC crate;
MPS, microcomputer.

a timer. The spectra were accumulated, if the inspected values were within given intervals. In this way, possible instabilities of the spectrometer or of the generator could be eliminated, and nearly equal experimental conditions, with the exception of the effect/background relation, were realized. Examples of TOF spectra are shown in Ref. 113/. The average width of the time channels was determined with 14 HeV source-reutron TOF peaks shifted by several delay lines in the Sl'Alit branch of the spectrometer. The differential linearity was measured vith the statistical events of a Po/Be neutron source.

In the data reduction at first the TOF spectra were corrected for dead time and differential nonlinearity of the spectrometer. Then the effect spectra $N(i)$ were calculated as differences of the spectra obtained with sample and the corresponding taken without sample and taking into account an additional background component determined in the channel refion between 14 HeV neutron peak and $\gamma$-peak position and assumed to be constant for all channels i. The N(i) were smoothed over about 10 channels with the exception of peak regions. The time scale $t$ was calculated with the average channel width $\Delta t$ beginning at the peak position of elastically scattered neutrons. The continuous parts of the time spectra $d N\left(t_{i}\right) / d t=N(i) / \Delta t$ were transtormed into energy spectra $\mathrm{dN}\left(\mathrm{E}_{\mathbf{i}}\right) / \mathrm{dE}$ resulting in laboratory system cross sections by:

$$
\sigma_{n m}\left(E_{1}, M\right)=\frac{d^{2} \sigma\left(E_{0} ; E_{, M}\right)}{d E \cdot d \Omega}=\frac{d N_{d t} \cdot \Delta \Omega_{s} \cdot L^{2} \cdot s^{2} \cdot f_{1}\left(\Omega_{1}, \phi_{0}\right) \cdot f_{2}\left(E_{1}, M\right) \cdot f_{3}\left(E_{1}, M\right)}{N_{c} \cdot Z_{H} \cdot F_{D} \cdot \varepsilon(E)} \text {, }
$$

with ${ }^{W} \alpha$ being $\alpha$-counts; $\Delta \Omega_{\alpha}$, solid angle of $\alpha$-counting; $f_{1}$, number oi $\propto$-particles/sr counted per neutron/sr striking on the sample; $s$, distance neutron source/sample; L, distance sample/neutron detector; l', neutron detector front-area; $\varepsilon$, neutron detector efficiencj; $Z_{N}$, number sample nuclei; $f_{2}$, correction of multiple scattering in the sample; $f_{3}$, correction of flux attenuation in the sample.
The ratio of single-scattered to multiple-scattered neutrons ( $f_{2}$ ) was calculated /14/ with the neutron transport code MORSE /15/ using ENDF/B-IV data $/ 16 /$. The factor $f^{-1}$ includes both flux attenuation of the incident neutrons up to the interaction and of the neutrons outgoing in direction of the TOF-detector. It was calculated by integration over the sample volume. The values of $f_{2} \cdot f_{3}$ were between 0.94 and 1.09 .
Transformation of the $\sigma_{n m}$ into center-of-mass system yielded
$\sigma_{\mathrm{mm}}^{\mathrm{mm}}$. The formulas used for the data reduction are described in fief. /17/.

For groups of monoenergetic, scattered neutrons well resolved in dN/dt, the peak areas $N_{Q}\left(\begin{array}{l}\text { ( }\end{array}\right)$ were determined which, replacing $d N / d E$ in eq. (1), yielded $d \boldsymbol{\sigma}\left(E_{0} ; Q, \mathcal{M}\right) / d \Omega=\sigma_{n n^{\prime}}(\boldsymbol{N})$. No mul-tiple-scattering correction was carried out for $\mathbb{N}_{Q}\left(\mathcal{O}_{\boldsymbol{\prime}}\right)$.

Fig. 4
Neutron detector efficiency measured with TOF spectrometry of 14 MeV source neutrons (口), of neutrons scattered from Hydrogen $(\Delta)$ and of Cf-252 fission neutrons (o) and calculated with Monte Carlo technique (-.-). The resulting solid courve was used for the data reduction.

Fig. 5
Angle-integrated emission cross sections of Pb obtained in the present work (o) and compared with experimental data of Hermsdorf et al. ( $0,16 /$ ), Vonach et al. $(+, / 7 /)$ and Takahashi et al. ( $\nabla, / 8 /$ ) and with the ENDF/B-IV evaluation (---).

Fig. 6
Measured neutron emission spectrum from Pb ( 0 , present data; $\nabla, / 8 /$ ) compared with a theoretical interpretation (—) as direct collective excitations, pre-equilibrium and equilibrium emission of primary neutrons (....) and secondary neutrons from ( $n, 2 n$ ).



The cross sections obtained for Pb are given in Table 1, for C in Table 2. The values $\Delta \sigma / \sigma$ in the tables include only the statistical uncertainties of $N(i)$ or ${ }^{N} Q$, respectively. Systematic uncertainties were estimated to $\Delta \Omega_{\alpha} / \Omega_{\alpha} \leqslant 1 \%$, $\Delta \mathrm{L} / \mathrm{L} \approx 0.4 \%, \Delta \mathrm{~s} \leqslant 0.5 \mathrm{~mm}, \quad \Delta \mathrm{f}_{1} / \mathrm{f}_{1} \approx 2 \alpha_{\%}, \Delta \Omega_{2}\left(\mathrm{f}_{2} \cdot \mathrm{f}_{3}\right) /$ $\left(\mathrm{I}_{2} \cdot \mathrm{f}_{3}\right) \leqslant 3 \%$ and $\Delta \mathrm{F}_{\mathrm{D}} / \mathrm{F}_{0} \approx 2 \%$. The N $\mathrm{N}_{\alpha}$ had statistical uncertainties which may be neglected but they contained background events which possibly contributed of the order of $1 \%$. Checks showed that the source-strencth monitoring had a total of uncertainties of $\approx 4 \%$. Calculations of $\varepsilon(E)$ with Monte Carlo methods can have uncertainties of $\approx 5 \% / 10 /$. Combining the calculation of $\mathcal{E}(E)$ with measured values, $\Delta \varepsilon / \mathcal{E}$ should be $\leqslant 5 \%$.
 Fb and $\leq \pm 5.0^{\circ}$ for $C$, respectively. the energy resolutions were $\Delta E / E=3 \%$ at $E=3 \mathrm{MeV}, 5 \%$ at 7 MeV and $7 \%$ at 14 MeV .

For comparisions of the data obtained for Pb with results of other experiments, with theoretical model predictions and with evaluated data, the angle-integrated emission spectrum was derivated,

$$
\begin{equation*}
\sigma_{n m}(E)=\frac{d \sigma\left(E_{0} ; E\right)}{d E}=\int_{4 \pi} d \Omega \cdot \frac{d^{2} \sigma\left(E_{0} E_{1} M\right)}{d E \cdot d \Omega} \tag{2}
\end{equation*}
$$

It is plotted in Fig. 5 together was the experimental data of Vonach et al. /7/, of Tahahashi et al. /8/ and those of a previous measurement at $T U / 6 /$. Taking into account statistical and systematic uncertainties of the data as given by the authors, the four measurements are consistent. Compared with the ENDF/B-IV evaluation the experimentally determined cross sections are obviously larger. Remarkable more neutrons as evaluated are observed in the energy range $1.5 \mathrm{MeV} \leq \mathrm{E} \leq 5 \mathrm{MeV}$. The deviation is up to $30 \%$ in the range $2=E=3.5 \mathrm{MeV}$.
In Fig. 6 the experimental data are theoretically interpreted as superposition of three components: direct excitations of vibrational modes calculated in DWBA approach /19/, pre-equilibrium and compound-nucleus neutron emission calculated with the Generalized Exciton Model code AMAPRE /20/ and secondarily emitted neutrons of ( $n, 2 n$ ) calculated with the statistical model code STAPRE /21/. The agreement of the calculated spectrum with the experimental is satisfactory in the low-enercy part. In the highenergy part the neutron emission is overestimated. The direct component with the averaged deformation parameters used would alone explain the neutron emission for $\mathrm{E}>8 \mathrm{MeV}$. But, reducing adequately the pre-equilibrium emission, discrepancies appear in the middle part of the spectrum where only the pre-equilibrium component is able sufficiently to describe the experimental data.

Angular distributions of neutrons emitted from Pb with $\mathrm{E}=3.5$, 5.5 and 7.5 MeV are presented in Fig. 7. The experimental data show with increasing $E$ a pronounced forward scattering. In the ENDF/B-IV evaluation these angular distributions are assumed to be isotropic. In the measurements of Kammerdiener /5/ and of


Fis. 7
Ancular distributions of neutron emitted from Pb with the energies E inserted. Experimental data (o, present wor:; $x, / 5 / ; \Delta, / 6 / ; \nabla, / 8 /$ ) are compared with the ENDF/B-IV evaluation (-) and with a calculation (-).
The pre-equilibrium and equilibrium component of primary neutron emission (....) is at $E=5.5 \mathrm{MeV}$ practically equal to the total emission (-).

Takahashi et al./8/ the increase of the incidence neutron energy $E_{0}$ by about 1.5 MeV going from backward to forward angles has the tendency to overestimate the forward-peaking. The theoretically obtained angular distributions describe the present experimental data at $E=5.5 \mathrm{MeV}$ satisfactory. At $E=3.5 \mathrm{MeV}$ they deviate for $\mathrm{M} \leqslant 30^{\circ}$ and at $E=7.5 \mathrm{MeV}$ the sum of the calculated direct collective excitations and of the pre-equilibrium emissions overestimates the neutron emission as discussed for the angle-integrated spectrum.

The data obtained for $C$ are compared in Fig. 8 with other experimental data and with the ENDF/B-V evaluation. Generally, they agree with the expected values so that this check of spectrometer and data reduction may be considered to be satisfying.



Fig. 8
Differential neutron scattering cross sections from Cor the levels inserted. The experimental data of the present work (o) are compared with those from other measurements ( $\Delta, / 8 / ; \square, / 22 / ; x, / 23 /$ ) and with the ENDF/B-V evaluation evaluation (---).

Table. 1.
Differential neutron emission cross sections
from Pb in the center-of-mass system (cm)

$$
E_{0}=14.00 \mathrm{meV} \quad \boldsymbol{V}=15.0^{\circ}
$$

| $\begin{gathered} \mathrm{E}^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\begin{array}{r} \sigma_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{sr}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{array}$ | $\begin{gathered} \Delta \sigma_{6} \\ {[\%]} \end{gathered}$ | $\begin{gathered} \mathrm{E}^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\begin{gathered} \sigma_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{ar}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{gathered}$ | $\begin{gathered} \Delta 5 / \sigma \\ {[\%]} \end{gathered}$ | $\begin{gathered} \mathrm{E}^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\begin{array}{r} \boldsymbol{\sigma}_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{gr}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{array}$ | $\begin{gathered} \Delta \sigma / 6 \\ {[\%]} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2.99 | . 0771 | 27 | 4.78 | . 0215 |  | 8.92 | . 0147 |  |
| 3.02 | .0751 |  | 4.83 | . 0209 |  | 9.05 | .0155 |  |
| 3.04 | .0729 |  | 4.88 | . 0201 |  | 9.19 | . 0164 |  |
| 3.07 | . 0695 |  | 4.93 | .0195 |  | 9.33 | . 0181 |  |
| 3.09 | .0666 |  | 4.99 | . 0190 |  | 9.47 | . 0188 |  |
| 3.12 | .0638 |  | 5.04 | .0184 |  | 9.62 | . 0190 |  |
| 3.14 | .0621 |  | 5.10 | . 0179 |  | 9.77 | . 0198 |  |
| 3.17 | .0624 |  | 5.15 | . 0174 |  | 9.92 | . 0174 |  |
| 3.20 | . 0627 |  | 5.21 | . 0170 |  | 10.08 | . 0139 | 20 |
| 3.22 | .0631 |  | 5.26 | .0165 | 29 | 10.24 | . 0083 |  |
| 3.25 | . 0633 | 24 | 5.32 | . 0163 |  | 10.40 | . 0115 |  |
| 3.28 | . 0632 |  | 5.38 | . 0159 |  | 10.57 | . 0173 |  |
| 3.31 | .0634 |  | 5.44 | . 0155 |  | 10.74 | . 0172 |  |
| 3.34 | . 0632 |  | 5.50 | . 0153 |  | 10.92 | . 0223 |  |
| 3.36 | . 0632 |  | 5.56 | . 0146 |  | 11.10 | . 0286 |  |
| 3.39 | . 0631 |  | 5.63 | .0147 |  | 11.29 | . 0297 |  |
| 3.42 | . 0627 |  | 5.69 | . 0144 |  | 11.48 | . 0354 |  |
| 3.45 | . 0616 |  | 5.75 | . 0140 |  | 11.68 | . 0395 |  |
| 3.48 | . 0597 |  | 5.82 | . 0138 |  | 11.89 | . 0470 | 6 |
| 3.52 | . 0576 |  | 5.89 | . 0137 | 30 | 12.10 | . 0612 |  |
| 3.55 | . 0555 | 21 | 5.95 | . 0135 |  | 12.32 | .0928 |  |
| 3.58 3.61 | .0544 |  | 6.02 | -0132 |  | 12.54 | -1350 |  |
| 3.64 | . 0510 |  | 6.17 | . 0128 |  | 13.01 | . 3308 |  |
| 3.68 | . 0488 |  | 6.24 | . 0125 |  | 13.26 | . 6652 |  |
| 3.71 | . 0467 |  | 6.31 | .0122 |  | 13.51 | 1.4537 |  |
| 3.75 | . 0448 |  | 6.39 | . 0121 |  | 13.78 | 2.4018 |  |
| 3.78 | . 0431 |  | 6.47 | . 0120 |  | 14.05 | 2.5044 | 0 |
| 3.82 | . 0413 |  | 6.55 | .0119 |  | 14.32 | 2.4095 |  |
| 3.85 | . 0395 |  | 6.63 | . 0118 | 30 | 14.63 | 1.4469 |  |
| 3.89 | . 0378 | 24 | 6.71 | . 0118 |  | 14.94 | . 6669 |  |
| 3.92 | . 0364 |  | 6.79 | . 0117 |  | 15.25 | . 2918 |  |
| 3.96 | . 0352 |  | 6.88 | . 0118 |  | 15.58 | . 1845 |  |
| 4.00 | . 0340 |  | 6.97 | . 0118 |  | 15.88 | . 1143 |  |
| 4.04 | . 0331 |  | 7.06 | .0118 |  | 16.24 | . 0818 |  |
| 4.08 | . 0321 |  | 7.15 | . 0119 |  | 16.61 | . 0669 |  |
| 4.12 | . 0314 |  | 7.24 | . 0121 |  | 16.98 | . 0541 | 2 |
| 4.16 | . 0306 |  | 7.34 | . 0123 |  | 17.34 | . 0357 |  |
| 4.20 | . 0298 |  | 7.43 | . 0125 |  | 17.74 | .0194 |  |
| $4 \cdot 24$ | .0292 |  | 7.53 | .0128 | 24 |  |  |  |
| 4.28 | . 0285 | 22 | 7.63 | . 0124 |  |  |  |  |
| 4.32 | . 0278 |  | 7.74 | .0129 |  |  |  |  |
| 4.36 | . 0272 |  | 7.84 | . 0135 |  |  |  |  |
| 4.41 | . 0266 |  | 7.95 | . 0135 |  |  |  |  |
| 4.45 | .0261 |  | 8.06 | . 0138 |  |  |  |  |
| 4.50 | .0255 |  | 8.18 | . 0138 |  |  |  |  |
| 4.54 4.59 | . 0249 |  | 8.29 | . 0137 |  |  |  |  |
| 4.59 4.63 | .0243 |  | 8.41 | .0136 |  |  |  |  |
| 4.68 | .0229 |  | 8.53 8.66 | . 010135 | 22 |  |  |  |
| 4.73 | . 0221 | 26 | 8.79 | . 0140 | 22 |  |  |  |

$$
E_{0}=14.10 \mathrm{MeV} \quad \boldsymbol{J}=30.0^{\circ}
$$

| $\begin{gathered} \mathrm{E}^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\begin{array}{r} \boldsymbol{\sigma}_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{gr}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{array}$ | $\begin{gathered} \Delta 6 /{ }_{6} \\ {[\%]} \end{gathered}$ | $\begin{gathered} \mathbf{E}^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\begin{gathered} G_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{Br}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{gathered}$ | $\begin{gathered} \Delta \sigma / \sigma \\ {[\%]} \end{gathered}$ | $\begin{gathered} \mathrm{E}^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\left.\begin{array}{r} \boldsymbol{\sigma}_{n m}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{Br}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{array} \right\rvert\,$ | $\begin{gathered} \Delta \sigma / 6 \\ {[\%]} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2.99 | . 0662 | 12 | 4.57 | . 0176 |  | 7.90 | . 0083 |  |
| 3.02 | . 0651 |  | 4.62 | . 0170 |  | 8.01 | . 0084 |  |
| 3.04 | .0640 |  | 4.67 | .0164 | 13 | 8.11 | . 0082 |  |
| 3.06 | .0618 |  | 4.71 | . 0158 |  | 8.23 | . 0085 |  |
| 3.09 | . 0592 |  | 4.76 | . 0152 |  | 8.34 | . 0090 |  |
| 3.11 | . 0569 |  | 4.81 | . 0147 |  | 8.46 | . 0088 |  |
| 3.14 | . 0546 |  | 4.86 | . 0143 |  | 8.58 | . 0099 | 12 |
| 3.16 | . 0538 |  | 4.91 | . 0139 |  | 8.70 | . 0094 |  |
| 3.19 | . 0535 |  | 4.96 | .0135 |  | 8.82 | .0084 |  |
| 3.21 | . 0531 |  | 5.01 | . 0132 |  | 8.95 | .0081 |  |
| 3.24 | . 0527 | 10 | 5.07 | . 0128 |  | 9.08 | . 0065 |  |
| 3.27 | . 0520 |  | 5.12 | . 0125 |  | 9.22 | . 0082 |  |
| 3.30 | . 0512 |  | 5.17 | . 0122 | 15 | 9.35 | . 0091 |  |
| 3.32 | . 0504 |  | 5.23 | . 0119 | , | 9.49 | . 0106 |  |
| 3.35 3.38 | . 0496 |  | 5.28 | . 0116 |  | 9.64 | . 0104 | 10 |
| 3.38 3.41 | .0490 |  | 5.34 | . 0114 |  | 9.79 | . 0088 |  |
| 3.44 | . 0477 |  | 5.40 | . 0110 |  | 10.09 | . 0006 |  |
| 3.47 | . 0462 |  | 5.46 5.52 | . 0104 |  | 10.25 | . 0057 |  |
| 3.50 | . 0445 |  | 5.58 | . 0101 |  | 10.41 | . 0039 |  |
| 3.53 | . 0429 | 10 | 5.64 | . 0098 |  | 10.57 | . 0055 |  |
| 3.56 | . 0416 |  | 5.70 | . 0095 |  | 10.74 | . 0056 |  |
| 3.59 | . 0405 |  | 5.77 | . 0092 | 17 | 10.92 | . 0063 |  |
| 3.62 | . 0394 |  | 5.83 | . 0089 |  | 11.09 | . 0078 |  |
| 3.65 | . 0382 |  | 5.90 | . 0087 |  | 11.28 | . 0083 | 12 |
| 3.69 | . 0369 |  | 5.96 | . 0085 |  | 11.46 | .0083 |  |
| 3.72 | . 0356 |  | 6.03 | . 0033 |  | 11.66 | . 0064 |  |
| 3.75 | .0344 |  | 6.10 | . 0081 |  | 11.85 | . 0049 |  |
| 3.79 | . 0333 |  | 6.17 | . 0080 |  | 12.06 | . 0056 |  |
| 3.82 | . 0323 |  | 6.24 | . 0078 |  | 12.27 | . 0045 |  |
| 3.86 | . 0314 | 10 | 6.31 | . 0076 |  | 12.48 | . 0058 |  |
| 3.89 | . 0304 |  | 6.39 | . 0075 |  | 12.71 | . 0112 |  |
| 3.93 | . 0296 |  | 6.46 | . 0074 | 18 | 12.94 | . 0236 |  |
| 3.96 | . 0288 |  |  | . 0073 |  | 13.18 | . 0424 |  |
| 4.00 | . 0282 |  | 6.62 | . 0072 |  | 13.42 | . 0870 | 3 |
| 4.04 | . 0275 |  | 6.70 | . 0071 |  | 13.68 | . 1480 |  |
| 4.08 | . 0269 |  | 6.78 | . 0071 |  | 13.94 | . 2018 |  |
| $4 \cdot 11$ | . 0261 |  | 6.86 | . 0070 |  | 14.21 | . 2138 |  |
| 4.15 | . 0254 |  | 6.95 | . 0070 |  | 14.48 | . 1470 |  |
| 4.19 | . 0247 |  | 7.03 | . 0070 |  | 14.78 | -0848 |  |
| 4.23 | . 0239 | 11 | 7.12 | . 0070 |  | 15.09 | . 0398 |  |
| 4.27 | . 0230 |  | 7.21 | . 0071 |  | 15.40 | . 0209 |  |
| $4 \cdot 31$ | . 0221 |  | $7 \cdot 30$ | . 0071 | 16 | 15.73 | . 0119 |  |
| 4.36 4.40 | .0213 |  | 7.40 7.49 | . 00072 |  | 16.03 16.38 | .0081 | 10 |
| 4.44 | .0197 |  | 7.59 | . 0075 |  | 16.75 | . 0042 |  |
| 4.48 | . 0190 |  | 7.69 | . 0077 |  |  |  |  |
| 4.53 | . 0183 |  | 7.79 | . 0080 |  |  |  |  |


| $\mathrm{E}_{\mathrm{o}}=14.12$ |  |  |  | $\boldsymbol{V}=45.0^{\circ}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \mathrm{E}^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ |  | $\Delta \sigma / 6$ $[\%]$ | $\begin{gathered} \mathrm{E}^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\left.\begin{array}{r} \boldsymbol{\sigma}_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{Br}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{array} \right\rvert\,$ | $\Delta \sigma / \sigma$ [\%] | $\begin{gathered} \mathrm{E}^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\left.\begin{array}{c} \mathcal{G}_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{Br}^{-1}\right.} \\ \cdot \mathrm{MeV}^{-1} \end{array}\right]$ | $\begin{gathered} \Delta / / \sigma \\ {[\%]} \end{gathered}$ |
| 3.00 | .0597 | 9 | 4.58 | . 0148 |  | 7.96 | . 0065 |  |
| 3.02 | . 0586 |  | 4.58 4.63 | .0143 | 11 | 8.07 | . 0065 |  |
| 3.05 | . 0573 |  | 4.67 | . 0139 |  | 8.18 | . 0067 | 11 |
| 3.07 | . 0548 |  | 4.72 | . 0135 |  | 8.29 | . 0071 |  |
| 3.10 | . 0519 |  | 4.76 | . 0131 |  | 8.40 | . 0073 |  |
| 3.12 | . 0492 |  | 4.81 | . 0127 |  | 8.52 | . 0073 |  |
| 3.15 | . 0465 |  | 4.86 | . 0123 |  | 8.64 | . 0067 |  |
| 3.17 | .0449 |  | 4.91 | . 0120 |  | 8.76 | . 0075 |  |
| 3.20 | . 0439 |  | 4.96 | . 0116 |  | 8.89 | .0062 |  |
| 3.22 | . 0433 |  | 5.01 | .0113 |  | 9.02 | . 0069 |  |
| 3.25 | . 0420 | 10 | 5.06 | . 0110 |  | 9.15 | . 0088 |  |
| 3.30 | . 0397 |  | 5.11 | .0107 | 12 | 9.28 | .0080 |  |
| 3.33 | . 0388 |  | 5.17 5.22 | . 0101 |  | 9.56 | .0086 | 9 |
| 3.35 | . 0379 |  | 5.27 | . 0099 |  | 9.71 | . 0078 |  |
| 3.38 | . 0374 |  | 5.33 | .0096 |  | 9.85 | . 0073 |  |
| 3.41 | . 0370 |  | 5.39 | .0093 |  | 10.01 | . 0068 |  |
| 3.44 3.47 | .0367 |  | 5.44 | -0090 |  | 10.16 10.32 | . 0060 |  |
| 3.50 | . 0352 |  | 5.50 | .0085 |  | 10.48 | . 0059 |  |
| 3.53 | . 0344 | 9 | 5.62 | .0083 |  | 10.65 | . 0052 |  |
| 3.56 | . 0336 |  | 5.68 | . 0080 | 13 | 10.82 | . 0056 |  |
| 3.59 | . 0332 |  | 5.74 | . 0078 | 13 | 11.00 | . 0065 | 10 |
| 3.62 | . 0328 |  | 5.81 | . 0077 |  | 11.18 | . 0060 |  |
| 3.65 | .0323 |  | 5.87 | . 0076 |  | 11.37 | . 0068 |  |
| 3.68 3.71 | .0307 |  | 5.94 | . 0074 |  | 11.56 11.75 | .0055 |  |
| 3.74 | .0299 |  | 6.07 | . 0074 |  | 11.95 | .0036 |  |
| 3.77 | . 0290 |  | 6.14 | . 0072 |  | 12.16 | . 0038 |  |
| 3.81 | . 0281 |  | 6.21 | .0071 |  | 12.37 | . 0030 |  |
| 3.84 | . 0271 |  | 6.29 | . 0070 |  | 12.59 | . 0086 |  |
| 3.88 | -0262 | 9 | 6.36 | .0069 |  | 12.81 | . 0200 |  |
| 3.91 | . 0252 |  | 6.44 | . 0068 | 14 | 13.84 | . 0383 | 3 |
| 3.94 3.98 | . 0224 |  | 6.51 | . 0066 |  | 13.28 | -0872 |  |
| 4.02 | .0226 |  | 6.59 6.67 | . 0065 |  | 13.52 13.77 | . 1509 |  |
| 4.05 | . 0219 |  | 6.75 | .0063 |  | 14.02 | . 2378 : |  |
| 4.09 | . 0212 |  | 6.83 | . 0062 |  | 14.30 | . 2479 | 0 |
| 4.13 | . 0205 |  | 6.92 | .0061 |  | 14.57 | . 1900 |  |
| 4.17 | . 0199 | 10 | 7.00 | . 0060 |  | 14.83 | . 0976 |  |
| 4.20 | .0192 |  | 7.09 | . 0060 |  | 15.12 | . 0483 |  |
| $4 \cdot 24$ | -0186 |  | 7.18 | . 0060 | 14 | 15.43 | . 0260 |  |
| 4.28 | . 0180 |  | 7.27 | . 0060 |  | 15.75 | . 0186 | 3 |
| 4.32 4.36 | .0174 |  | 7.36 7.46 | . 0066 |  | 16.05 16.38 | .0135 |  |
| 4.41 | . 0165 |  | 7.45 | .0062 |  | 16.72 | .0041 |  |
| 4.45 | . 0160 |  | 7.65 | . 0063 |  | 17.07 | . 0015 |  |
| 4.49 | . 0156 |  | 7.75 | . 0064 |  | 17.41 | . 0007 |  |
| 4.54 | .0152 |  | 7.85 | . 0065 |  |  |  |  |


| $\mathrm{E}_{\mathrm{o}}=14.14 \mathrm{Me} \mathrm{V}$ |  |  |  | $\boldsymbol{V}=60.0^{\circ}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \mathrm{E}^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\left.\begin{gathered} \boldsymbol{\sigma}_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{Br}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{gathered} \right\rvert\,$ | 滑/6 | $\begin{gathered} \mathrm{E}^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\left.\begin{gathered} \boldsymbol{G}_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{sr}^{-1}\right.} \\ \cdot \mathrm{MeV}^{-1} \end{gathered} \right\rvert\,$ | $\begin{gathered} 45 / 6 \\ {[\%]} \end{gathered}$ | $\begin{gathered} \text { E }^{\text {cm }} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\begin{gathered} \boldsymbol{\sigma}_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{Br}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{gathered}$ | $\begin{gathered} \Delta \sigma / 6 \\ {[\%]} \end{gathered}$ |
| 2.99 | . 0574 | 8 | 4.68 | . 0134 |  | 8.49 | . 0063 |  |
| 3.01 | . 0562 |  | 4.72 | . 0130 |  | 8.61 | . 0064 |  |
| 3.04 | .0549 |  | 4.77 | . 0126 |  | 8.73 | . 0063 |  |
| 3.06 | . 0535 |  | 4.82 | . 0122 |  | 8.85 | . 0063 |  |
| 3.08 | . 0511 |  | 4.86 | . 0119 |  | 8.98 | . 0070 |  |
| 3.11 | . 0483 |  | 4.91 | . 0115 |  | 9.11 | . 0072 |  |
| 3.13 | . 0456 |  | 4.96 | .0112 |  | 9.24 | .0073 | 7 |
| 3.16 | . 0432 |  | 5.01 | . 0109 |  | 9.38 | .0071 | 7 |
| 3.18 3.21 | . 0418 |  | 5.06 | . 0106 | 9 | 9.52 | . 0056 |  |
| 3.21 | . 04404 | 7 | 5.12 | . 0103 |  | 9.66 | . 0057 |  |
| 3.26 | . 0398 |  | 5.17 5.22 | . 0100 |  | 9.81 | . 0061 |  |
| 3.28 | . 0391 |  | 5.28 | .0095 |  | 9.96 | -0058 |  |
| 3.31 | . 0383 |  | 5.33 | .0092 |  | 10.27 | . 0051 |  |
| 3.34 | . 0376 |  | 5.39 | . 0089 |  | 10.43 | . 0046 |  |
| 3.37 | .0370 |  | 5.44 | .0087 |  | 10.59 | . 0052 |  |
| 3.39 | . 0366 |  | 5.50 | . 0084 |  | 10.76 | . 0050 | 10 |
| 3.42 | . 0362 |  | 5.56 | . 0081 |  | 10.93 | . 0059 |  |
| 3.45 | . 0359 |  | 5.62 | . 0078 |  | 11.11 | . 0064 |  |
| 3.48 | . 0352 |  | 5.68 | . 0076 | 10 | 11.30 | . 0060 |  |
| 3.51 | . 0341 | 7 | $5 \cdot 74$ | .0073 |  | 11.48 | . 0060 |  |
| 3.54 | .0330 |  | 5.80 | . 0071 |  | 11.68 | . 0047 |  |
| 3.57 | . 0320 |  | 5.87 | .0069 |  | 11.87 | . 0040 |  |
| 3.60 | . 0312 |  | 5.93 | .0067 |  | 12.07 | . 0028 | 19 |
| 3.63 | . 0305 |  | 6.00 | . 0065 |  | 12.28 | . 0013 |  |
| 3.66 | . 0298 |  | 6.07 | . 0064 |  | 12.72 | . 0021 |  |
| 3.69 | . 0290 |  | 6.14 | .0063 |  | 12.94 | . 0059 |  |
| 3.72 | . 0281 |  | 6.21 | . 0061 |  | 13.18 | . 0152 |  |
| 3.75 | . 0272 |  | 6.28 | . 0060 | 12 | 13.41 | . 0298 |  |
| 3.78 | . 0265 |  | 6.35 | .0059 |  | 13.66 | . 0432 |  |
| 3.82 | . 0257 | 7 | 6.43 | .0058 |  | 13.91 | . 0477 |  |
| 3.85 | . 0250 |  | 6.50 | . 0058 |  | 14.18 | . 0534 | 1 |
| 3.88 | . 02243 |  | 6.58 | . 0057 |  | 14.44 | . 0472 |  |
| 3.92 3.95 | . 0236 |  | 6.66 | . 0057 |  | 14.70 | . 0297 |  |
| 3.95 3.99 | .0229 |  | 6.74 6.82 | . 00056 |  | 14.99 | . 0142 |  |
| 4.02 | . 0219 |  | 6.90 | .0056 |  | 15.29 | . 00631 |  |
| 4.06 | . 0213 |  | 6.99 | . 0057 |  | 15.89 | . 0026 |  |
| 4.10 | . 0207 |  | 7.08 | . 0057 | 11 | 16.22 | . 0018 | 11 |
| $4 \cdot 14$ | . 0202 |  | 7.16 | . 0058 |  | 16.55 | .0015 |  |
| 4.17 | . 0196 | 8 | 7.25 | . 0058 |  | 16.89 | .0009 |  |
| 4.21 4.25 | . 0190 |  | 7.35 | . 0058 |  | 17.23 | . 0004 |  |
| 4.25 4.29 | .0184 |  | 7.44 | . 0058 |  |  |  |  |
| 4.33 | .0172 |  | 7.53 | . 00059 |  |  |  |  |
| $4 \cdot 37$ | .0166 |  | 7.73 | . 0062 |  |  |  |  |
| 4.41 | . 0161 |  | 7.83 | .0062 |  |  |  |  |
| 4.46 | . 0155 |  | 7.93 | . 0058 |  |  |  |  |
| $4 \cdot 50$ | . 0151 |  | 8.04 | . 0059 | 9 |  |  |  |
| 4.54 | . 0147 |  | 8.15 | . 0061 |  |  |  |  |
| 4.59 4.63 | .0143 | 8 | 8.26 8.37 | .0062 |  |  |  |  |



| $\begin{gathered} \mathrm{E}^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\left.\begin{array}{r} \boldsymbol{\sigma}_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{gr}^{-1}\right.} \\ \cdot \mathrm{Mle}^{-1} \end{array}\right]$ | $\Delta 5 / 6$ <br> [\%] | $\begin{gathered} \mathrm{E}^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\begin{array}{r} \left\|\begin{array}{r} \mathcal{G}_{n m}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{ar}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{array}\right\| \end{array}$ | $\begin{gathered} \Delta \sigma / \sigma \\ {[\%]} \end{gathered}$ | $\begin{aligned} & \mathrm{E} \mathrm{~cm} \\ & {[\mathrm{MeV}]} \end{aligned}$ | $\begin{gathered} \sigma_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{gr}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{gathered}$ | $\Delta \sigma / \sigma$ <br> [\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3.01 | .0583 | 11 | 4.61 | . 0143 |  | 7.93 | . 0049 |  |
| 3.03 | . 0573 |  | 4.65 | . 0139 |  | 8.03 | . 0049 |  |
| 3.06 | . 0561 |  | 4.70 | . 0135 |  | 8.13 | . 0050 |  |
| 3.08 | . 0548 |  | 4.74 | . 0131 |  | 8.24 | . 0052 |  |
| 3.11 | . 0521 |  | 4.79 | . 0127 |  | 8.34 | . 0052 |  |
| 3.13 | . 0493 |  | 4.83 | . 0123 |  | 8.45 | . 0053 |  |
| 3.15 | . 0466 |  | 4.88 | . 01118 |  | 8.55 | . 0054 |  |
| 3.18 | . 0441 |  | 4.93 | . 0114 |  | 8.67 | . 0055 |  |
| 3.20 | . 0430 |  | 4.98 | . 0109 |  | B. 79 | . 0055 |  |
| 3.23 | . 0423 | 9 | 5.02 | . 0104 | 13 | 8.91 | . 0055 | 13 |
| 3.25 | . 0416 |  | 5.08 | . 0100 |  | 9.03 | . 0055 |  |
| 3.28 | . 0410 |  | 5.13 | . 0096 |  | 9.15 | . 0061 |  |
| 3.31 | . 0403 |  | 5.18 | . 0092 |  | 9.27 | . 0056 |  |
| 3.33 | . 0395 |  | 5.23 | . 0088 |  | 9.40 | . 0052 |  |
| 3.36 | . 0389 |  | 5.29 | . 0084 |  | 9.53 | . 0056 |  |
| 3.39 | . 0383 |  | 5.34 | . 0081 |  | 9.67 | . 0057 |  |
| 3.41 | .0380 |  | 5.40 | . 0078 |  | 9.80 | . 0050 |  |
| 3.44 | . 0377 |  | 5.46 | -0075 |  | 9.94 | . 0057 |  |
| 3.47 | .0373 |  | 5.51 | . 0073 |  | 10.09 | . 0049 |  |
| 3.50 | . 0365 | 9 | 5.57 | . 0071 | 16 | 10.23 | . 0056 | 13 |
| 3.53 3.56 | . 0354 |  | 5.63 5.69 | . 00069 |  | 10.38 | . 0054 |  |
| 3.56 | . 0343 |  | 5.69 5.76 | . 00067 |  | 10.53 | . 0033 |  |
| 3.59 3.62 | .0331 |  | 5.76 5.82 | . 0066 |  | 10.68 | . 0038 |  |
| 3.65 | .0314 |  | 5.88 | .0063 |  | 11.00 | . 0051 |  |
| 3.68 | . 0304 |  | 5.95 | . 0062 |  | 11.17 | . 0039 |  |
| 3.71 | . 0293 |  | 6.01 | .0061 |  | 11.33 | . 0038 |  |
| 3.75 | . 02832 |  | 6.08 | . 0060 |  | 11.51 | . 0037 |  |
| 3.78 | . 0270 |  | 6.15 | .0059 |  | 11.68 | . 0048 |  |
| 3.81 | . 0260 | 9 | 6.22 | .0058 | 17 | 11.86 | . 0030 | 23 |
| 3.85 | . 0250 |  | 6.29 | .0056 |  | 12.04 | . 0024 |  |
| 3.88 | . 0240 |  | 6.36 | . 0055 |  | 12.23 | . 0018 |  |
| 3.91 | .0231 |  | 6.43 | . 0054 |  | 12.42 | . 0000 |  |
| 3.95 | . 0222 |  | 6.50 | .0053 |  | 12.62 | . 0000 |  |
| 3.98 | . 0213 |  | 6.57 | .0051 |  | 12.82 | . 0019 |  |
| 4.02 | . 0206 |  | 6.65 | . 0050 |  | 13.03 | . 0060 |  |
| 4.06 | . 0200 |  | 6.73 | . 0049 |  | 13.24 | . 0170 |  |
| 4.09 | . 0194 |  | 6.80 | . 0048 |  | 13.46 | . 0296 |  |
| $4 \cdot 13$ | . 0189 |  | 6.88 | . 0047 |  | 13.68 | . 0390 |  |
| 4.17 | .0183 | 11 | 6.96 | . 0047 | 18 | 13.92 | . 0417 |  |
| 4.21 | . 0178 |  | 7.04 | . 0046 |  | 14.15 | . 0465 | 2 |
| 4.24 | . 0174 |  | 7.12 | . 0046 |  | 14.40 | . 0463 |  |
| 4.28 4.32 | . 0169 |  | 7.20 7.29 | . 00046 |  | 14.65 | . 0365 |  |
| 4.36 | .0161 |  | 7.38 | . 0046 |  | 14.90 15.18 | . 0070 |  |
| 4.40 | . 0157 |  | 7.46 | . 0046 |  | 15.46 | . 0028 |  |
| 4.44 | . 0154 |  | 7.55 | . 0046 |  | 15.74 | . 0016 |  |
| 4.48 4.52 | . 0151 |  | 7.64 7.74 | . 00047 |  | 16.02 | .0012 |  |
| 4.57 | . 0146 | 11 | 7.83 | . 0048 | 15 |  |  |  |





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| $\begin{gathered} E^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\begin{gathered} \boldsymbol{\sigma}_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{gr}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{gathered}$ | $\begin{gathered} \Delta \sigma 6 \\ {[\%]} \end{gathered}$ | $\begin{gathered} E^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\begin{array}{r} \boldsymbol{\sigma}_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\begin{array}{r} \mathrm{b} \mathrm{gr}^{-1} \\ \cdot \mathrm{MeV}^{-1} \end{array}\right]} \end{array}$ | $\begin{gathered} \Delta \sigma / \sigma \\ {[\%]} \end{gathered}$ | $\begin{gathered} \mathrm{E}^{\mathrm{cm}} \\ {[\mathrm{MeV}]} \end{gathered}$ | $\left[\begin{array}{r} \sigma_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\begin{array}{ll} \mathrm{br} \\ \cdot \mathrm{MeV}^{-1} \end{array}\right]} \end{array}\right.$ | $\Delta \sigma / \sigma$ $[\%]$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3.00 | . 0557 | 11 | 4.65 | . 0130 | 11 | 8.15 | . 0041 |  |
| 3.03 | . 0555 |  | 4.69 | . 0126 |  | 8.26 | . 0041 |  |
| 3.05 | . 0551 |  | 4.74 | . 0121 |  | 8.36 | . 0041 |  |
| 3.07 | . 0545 |  | 4.78 | . 0117 |  | 8.47 | . 0040 |  |
| 3.10 | . 0536 |  | 4.82 | .0113 |  | 8.58 | . 0039 |  |
| 3.12 | .0522 |  | 4.87 | . 0110 |  | 8.69 | . 0046 |  |
| 3.14 | . 0495 |  | 4.92 | . 0106 |  | 8.80 | . 0038 | 19 |
| $3 \cdot 17$ | . 0470 |  | 4.97 | . 0103 |  | 8.92 | . 0031 |  |
| 3.19 | .0444 |  | 5.01 | . 0099 | 15 | 9.04 | . 0018 |  |
| 3.22 3.24 | . 04420 | 10 | 5.00 5.11 | .0096 |  | 9.16 | . 0038 |  |
| 3.27 | . 0401 | 10 | 5.16 | .0089 |  | 9.28 9.41 | . .0037 |  |
| 3.29 | . 0392 |  | 5.22 | -0086 |  | 9.54 | . 0026 |  |
| $3 \cdot 32$ | . 0383 |  | 5.27 | . 0083 |  | 9.67 | . 0031 |  |
| $3 \cdot 35$ | .0373 |  | 5.32 | -0080 |  | 9.81 | . 0032 |  |
| $3 \cdot 37$ | . 0364 |  | 5.38 | . 0077 |  | 9.95 | . 0025 |  |
| 3.40 | .0355 |  | 5.43 | .0074 |  | 10.09 | . 0025 | 28 |
| 3.43 3.45 | .0347 |  | 5.49 | .0071 | 17 | 10.23 | . 0028 |  |
| 3.48 | . 0336 |  | 5.61 | . 0065 |  | 10.38 10.53 | . 00023 |  |
| 3.51 | . 03330 | 11 | 5.67 | -0063 |  | 10.68 | . 0015 |  |
| 3.54 | . 0320 |  | 5.73 | -0060 |  | 10.84 | . 0010 |  |
| 3.57 | . 0309 |  | 5.79 | . 0057 |  | 10.99 | . 0017 |  |
| 3.60 | . 0299 |  | 5.85 | . 0055 |  | 11.16 | . 0029 |  |
| 3.63 | . 0289 |  | 5.92 | . 0053 |  | 11.32 | . 0023 |  |
| 3.66 | . 0282 |  | 5.98 | .0051 |  | 11.49 | . 0024 |  |
| 3.69 | . 0275 |  | 6.05 | .0050 |  | 11.66 | . 0016 | 40 |
| 3.72 3.75 | . 02625 |  | 6.11 6.18 | . 00048 |  | 11.84 | . 0025 |  |
| 3.75 3.78 | .0259 |  | 6.18 6.25 | .0046 | 21 | 12.02 | . 0019 |  |
| 3.82 | . 0242 | 11 | 6.32 | . 0043 |  | 12.210 | .0010 |  |
| 3.85 | . 0235 |  | 6.39 | . 0042 |  | 12.59 | .0006 |  |
| 3.88 | . 0228 |  | 6.46 | . 0040 |  | 12.79 | . 0000 |  |
| 3.92 | . 0221 |  | 6.53 | .0039 |  | 12.99 | . 0037 |  |
| 3.95 | . 0215 |  | 6.61 | . 0039 |  | 13.20 | . 0054 | 20 |
| 3.99 4.02 | . 02209 |  | 6.68 6.76 | .0038 |  | 13.42 | . 0107 |  |
| 4.06 | . 0198 |  | 6.83 | -0038 |  | 13.64 13.86 | . 0127 |  |
| 4.10 | . 0194 |  | 6.91 | . 0038 | 23 | 14.10 | .0155 |  |
| 4.13 | .0190 |  | 6.99 | . 0038 |  | 14.34 | .0148 |  |
| $4 \cdot 17$ | . 0186 | 11 | 7.07 | . 0038 |  | 14.58 | .0129 |  |
| $4 \cdot 21$ | .0181 |  | 7.15 | . 00338 |  | 14.84 | .0109 |  |
| $4 \cdot 24$ | . 0177 |  | 7.23 7.32 | . 00339 |  | 15.10 | . 0045 | 14 |
| 4.28 4.32 | .0172 |  | 7.32 7.40 | .0039 |  | 15.37 | .0013 |  |
| $4 \cdot 36$ | .0168 |  | 7.49 | . 0040 |  | 15.65 | . 0006 |  |
| 4.40 | .0157 |  | 7.58 | . 0041 |  | 15.94 | .0005 |  |
| 4.44 | . 0152 |  | 7.67 | . 0041 |  |  |  |  |
| 4.48 | .0147 |  | 7.76 | . 0041 | 19 |  |  |  |
| $4 \cdot 52$ | . 0143 |  | 7.86 | . 0042 |  |  |  |  |
| 4.56 | . 0138 |  | 7.95 | . 0043 |  |  |  |  |
| 4.61 | . 0134 |  | 8.05 | . 0042 |  |  |  |  |

$E_{0}=14.12 \mathrm{MeV} \quad \boldsymbol{F}=120.0^{\circ}$

| $\mathrm{E}^{\mathrm{cm}}$ <br> [MeV] | $\sigma \mathrm{cm}$ $[\mathrm{mm}$ $[\mathrm{sr}$ $\cdot \mathrm{MeV}$ | $\begin{gathered} \Delta \% / \sigma \\ {[\%]} \end{gathered}$ | [MeV] | $\begin{array}{r} \sigma_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{Er}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{array}$ | $\Delta \sigma / \sigma$ <br> [\%] | $\begin{aligned} & \mathrm{E}^{\mathrm{cm}} \\ & {[\mathrm{MeV}]} \end{aligned}$ | $\begin{aligned} & \sigma_{\mathrm{nm}}^{\mathrm{cm}} \\ & {\left[\mathrm{~b} \cdot \mathrm{Br}^{-1}\right.} \\ & \left.\cdot \mathrm{MeV}^{-1}\right] \end{aligned}$ | $4 \sigma / 6$ <br> [\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2.98 | . 0564 | 8 | 4.62 | . 0117 | 10 | 8.17 | . 0028 |  |
| 3.01 | . 0552 |  | 4.66 | . 0114 |  | 8.28 | -0029 |  |
| 3.03 | . 0540 |  | 4.71 | . 0110 |  | 8.39 | . 0029 |  |
| 3.05 | . 0533 |  | 4.75 | . 0106 |  | 8.50 | .0029 |  |
| 3.08 | . 0522 |  | 4.80 | . 0102 |  | 8.61 | . 0030 |  |
| 3.10 | . 0512 |  | 4.84 | .0098 |  | 8.73 | .0030 |  |
| 3.12 | . 0500 |  | 4.89 | . 0094 |  | 8.85 | . 0032 | 14 |
| 3.15 | .0481 |  | 4.94 | . 0090 |  | 8.97 | . 0034 |  |
| 3.17 | . 0457 |  | 4.99 | . 0086 | 11 | 9.90 | .0031 |  |
| 3.19 | .0433 |  | 5.04 | . 0082 |  | 9.23 | . 0028 |  |
| 3.22 | . 0410 | 7 | 5.09 | . 0079 |  | 9.26 | . 0028 |  |
| 3.24 | . 0395 |  | 5.14 | . 0075 |  | 9.49 | . 0024 |  |
| 3.27 | . 0386 |  | 5.19 | . 0072 |  | 9.63 | .0022 |  |
| 3.29 | -0377 |  | 5.24 | . 0069 |  | 9.77 | -0021 |  |
| 3.32 | -0367 |  | 5.30 | . 0067 |  | 9.92 | . 0020 |  |
| 3.35 | . 0357 |  | 5.35 | . 0064 |  | 10.06 | . 0021 |  |
| 3.37 | . 0346 |  | 5.41 | . 0062 |  | 10.21 | . 0010 | 25 |
| 3.40 | . 0335 |  | 5.47 | . 0060 |  | 10.37 | . 0014 | 25 |
| 3.43 | . 0325 |  | 5.52 | . 0058 | 13 | 10.52 | . 0009 |  |
| 3.46 | . 0316 |  | 5.58 | . 0056 |  | 10.69 | .0014 |  |
| 3.48 | . 0309 | 8 | 5.64 | . 0054 |  | 10.85 | .0012 |  |
| 3.51 | . 0303 |  | 5.70 | . 0053 |  | 11.02 | .0012 |  |
| 3.54 | . 0295 |  | 5.76 | . 0051 |  | 11.19 | . 0010 |  |
| 3.57 3.60 | .0285 |  | 5.82 | . 0049 |  | 11.37 | . 0019 |  |
| 3.60 | . 0276 |  | 5.89 | . 0048 |  | 11.55 | . 0016 |  |
| 3.63 3.66 | . 0267 |  | 5.95 | . 0046 |  | 11.74 | . 0012 | 35 |
| 3.66 3.69 | .0261 |  | 6.01 6.08 | . 0044 |  | 11.93 | . 0004 |  |
| 3.69 3.72 | . 02527 |  | 6.08 | . 0043 |  | 12.12 | . 0007 |  |
| 3.75 | .0247 |  | 6.15 6.21 | .0047 | 17 | $12 \cdot 32$ | . 0010 |  |
| 3.79 | . 0241 | 8 | 6.28 | . 0039 |  | 12.53 | . 00 |  |
| 3.82 | . 0235 |  | 6.35 | . 0038 |  | 12.97 | . 0017 |  |
| 3.85 | . 0229 |  | 6.42 | . 0036 |  | 13.19 | . 0037 |  |
| 3.89 | . 0223 |  | 6.50 | . 0036 |  | 13.42 | . 0055 |  |
| 3.92 | . 0216 |  | 6.57 | . 0035 |  | 13.66 | . 0068 |  |
| 3.95 | . 0208 |  | 6.65 | . 0034 |  | 13.92 | . 0066 |  |
| 3.99 | . 0201 |  | 6.72 | .0034 |  | 14.17 | . 0065 | 11 |
| 4.02 | . 0193 |  | 6.80 | . 0034 |  | 14.44 | . 0045 |  |
| 4.06 | .0186 |  | 6.88 | . 0034 | 17 | 14.71 | . 0037 |  |
| $4 \cdot 10$ | . 0179 |  | 6.96 | . 0034 |  | 15.00 | . 0030 |  |
| 4.13 4.17 | .0173 | 8 | 7.04 | . 0034 |  | 15.27 | . 0029 |  |
| $4 \cdot 17$ 4.21 | . 0166 |  | 7.13 | . 0034 |  | 15.59 | . 0014 |  |
| 4.21 4.25 | . 016154 |  | 7.21 7.30 | . 0034 |  | 15.91 | . 0010 | 33 |
| $4 \cdot 29$ | .0149 |  | 7.39 | .0033 |  | 16.24 16.58. | . 00005 |  |
| 4.33 | . 0144 |  | 7.48 | .0033 |  | 16.89 | . 0006 |  |
| $4 \cdot 37$ | . 0139 |  | 7.57 | . 0032 |  |  |  |  |
| 4.41 | . 0134 |  | 7.67 | .0030 |  |  |  |  |
| $4 \cdot 45$ | . 0130 |  | 7.76 | . 0029 | 17 |  |  |  |
| 4.49 | . 0127 |  | 7.86 | .0031 |  |  |  |  |
| $4 \cdot 53$ | .0124 |  | 7.96 | .0032 |  |  |  |  |
| $4 \cdot 57$ | .0120 |  | 8.07 | . 0031 |  |  |  |  |


| [me V] | $\begin{gathered} \boldsymbol{\sigma}_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{gr}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{gathered}$ | $\begin{gathered} \Delta \sigma / \sigma \\ {[\%]} \end{gathered}$ | [ MeV] | $\left.\begin{array}{c} \sigma_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{sr}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{array}\right]$ | $\begin{gathered} \Delta \sigma / \sigma \\ {[\%]} \end{gathered}$ | [MeV] | $\begin{gathered} \sigma_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{sr}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{gathered}$ | $\begin{gathered} \Delta \sigma / \sigma \\ {[\%]} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3.00 | . 0550 | 10 | $4 \cdot 55$ | . 0121 |  | 7.86 | . 0032 |  |
| 3.02 | . 0536 |  | 4.59 | . 0117 |  | 7.96 | . 0032 |  |
| 3.04 | . 0521 |  | 4.63 | -0112 |  | 8.06 | . 0032 |  |
| 3.06 | . 0510 |  | $4 \cdot 68$ | . 0108 |  | 8.17 | . 0033 |  |
| 3.09 | . 0498 |  | $4 \cdot 72$ | . 0104 |  | 8.27 | . 0033 |  |
| 3.11 | . 0487 |  | $4 \cdot 77$ | . 0100 |  | 8.38 | . 0033 |  |
| 3.13 | . 0474 |  | 4.87 | . 0096 |  | 8.50 | .0033 |  |
| 3.16 | . 0457 |  | $4 \cdot 86$ | . 0093 |  | 8.61 | . 0033 |  |
| 3.18 | . 0435 |  | $4 \cdot 91$ | . 0089 |  | 8.73 | . 0032 | 19 |
| 3.20 | . 0414 |  | $4 \cdot 95$ | -0086 | 15 | 8.85 | . 0031 |  |
| 3.23 | . 0395 | 10 | 5.00 | . 0083 |  | 8.97 | . 0031 |  |
| 3.25 | . 0381 |  | 5.05 | . 0081 |  | 9.99 | . 0030 |  |
| 3.28 | . 0377 |  | $5 \cdot 10$ | . 0078 |  | 9.22 | . 0029 |  |
| $3 \cdot 30$ | . 0373 |  | $5 \cdot 15$ | . 0076 |  | 9.35 | . 0028 |  |
| 3.33 | . 0369 |  | $5 \cdot 20$ | -0074 |  | 9.48 | . 0026 |  |
| 3.35 | . 0364 |  | 5.25 | -0072 |  | 9.62 | .0025 |  |
| $3 \cdot 38$ | . 0357 |  | $5 \cdot 31$ | . 0069 |  | 9.76 | . 0023 |  |
| 3.41 | . 0350 |  | $5 \cdot 36$ | -0067 |  | 9.91 | . 0022 |  |
| 3.43 | . 0342 |  | $5 \cdot 42$ | . 0065 |  | 10.05 | . 0020 | 29 |
| 3.46 | . 0336 |  | $5 \cdot 47$ | -0062 | 18 | 10.20 | . 0019 |  |
| 3.49 | . 0330 | 9 | 5.53 | . 0060 |  | 10.36 | . 0018 |  |
| 3.52 | . 0323 |  | 5.58 | -0057 |  | 10.52 | . 0016 |  |
| 3.55 | .0317 |  | 5.64 | . 0055 |  | 10.68 | . 0013 |  |
| 3.57 | . 0305 |  | $5 \cdot 70$ | . 0053 |  | 10.84 | . 0012 |  |
| 3.50 | . 0293 |  | $5 \cdot 76$ | . 0050 |  | 11.01 | . 0012 |  |
| 3.63 | .0281 |  | 5.82 | -0048 |  | 11.19 | . 0012 |  |
| 3.66 | . 0271 |  | 5.88 | . 0045 |  | 11.37 | . 0012 |  |
| 3.69 | . 0263 |  | 5.94 | . 0043 |  | 11.55 | .0012 |  |
| 3.72 | . 0255 |  | 6.01 | -0041 |  | 11.74 | .0010 | 52 |
| 3.75 | -0248 |  | 6.07 | . 0039 | 24 | 11.93 | . 0008 |  |
| 3.78 | . 0239 | 10 | 6.14 | . 0037 |  | 12.13 | . 0007 |  |
| 3.82 | . 0231 |  | 6.21 | . 0035 |  | 12.33 | . 0007 |  |
| 3.85 | . 0222 |  | 6.28 | .0034 |  | 12.54 | . 0009 |  |
| 3.88 | . 0215 |  | $6 \cdot 35$ | . 0032 |  | 12.75 | .0014 |  |
| 3.91 | . 0208 |  | 6.42 | . 0030 |  | 12.97 | . 0024 |  |
| 3.95 | . 0202 |  | 6.49 | . 0029 |  | 13.20 | .0036 | 22 |
| 3.98 | . 0195 |  | 6.57 | . 0028 |  | 13.43 | . 0049 | 22 |
| 4.02 | . 0189 |  | 6.64 | . 0027 |  | 13.68 | . 0065 |  |
| 4.05 | . 0183 |  | 6.72 | . 0026 |  | 13.91 | . 0071 |  |
| 4.08 | . 0179 |  | 6.80 | . 0025 | 31 | 14.16 | .0073 | 13 |
| 4.12 4.16 | . 0174 | 11 | 6.88 6.96 | . 0025 |  | 14.42 | -0065 | 13 |
| 4.16 4.19 | .0169 |  | 6.96 7.04 | . 0025 |  | 14.70 14.97 | . 0059 |  |
| 4.23 | . 0160 |  | $7 \cdot 12$ | . 0026 |  | 15.23 | . 0028 | 33 |
| 4.27 | . 0156 |  | $7 \cdot 21$ | . 0026 |  | 15.53 | . 0014 | 33 |
| $4 \cdot 31$ | . 0151 |  | 7.30 | -0027 |  | 15.84 | . 0004 |  |
| $4 \cdot 34$ | . 0146 |  | $7 \cdot 39$ | -0028 |  |  |  |  |
| $4 \cdot 38$ | . 0141 |  | 7-48 | . 0029 |  |  |  |  |
| $4 \cdot 42$ | . 0136 |  | $7 \cdot 57$ | . 0029 |  |  |  |  |
| 4.46 | . 0130 |  | 7.67 | . 0030 | 22 |  |  |  |
| 4.51 | . 0126 | 12 | 7.76 | . 0031 |  |  |  |  |


| [ HeV ] | $\begin{gathered} \sigma_{\mathrm{nm}}^{\mathrm{nm}} \\ {\left[\mathrm{~b} \cdot \mathrm{gr}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{gathered}$ | $\begin{gathered} \Delta \sigma / \sigma \\ {[\%]} \end{gathered}$ | $\mathrm{E}^{\mathrm{cm}}$ $[\mathrm{MeV}]$ | $\begin{gathered} \sigma_{\mathrm{nm}}^{\mathrm{cm}} \\ {\left[\mathrm{~b} \cdot \mathrm{Br}^{-1}\right.} \\ \left.\cdot \mathrm{MeV}^{-1}\right] \end{gathered}$ | $\begin{gathered} \Delta \sigma / 6 \\ {[\%]} \end{gathered}$ | $\mathrm{E}^{\mathrm{cm}}$ $[\mathrm{HeV}]$ | $\left\|\begin{array}{r} 6_{\mathrm{nm}}^{\mathrm{cm}} \\ \mathrm{nb} \cdot \mathrm{sr} \\ \cdot \mathrm{MeV} \\ -1 \end{array}\right\|$ | $\Delta \sigma / \sigma$ <br> [\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3.01 | . 0662 | 13 | 4.62 | . 0125 |  | 8.08 | . 00 |  |
| 3.03 | . 0642 |  | 4.66 | . 0121 |  | 8.19 | . 0024 |  |
| 3.05 | . 0621 |  | 4.71 | . 0117 |  | 8.29 | . 0024 |  |
| 3.08 | . 0603 |  | 4.75 | . 0112 |  | 8.40 | . 0023 |  |
| 3.10 | . 0584 |  | 4.80 | . 0107 |  | 8.51 | . 0023 |  |
| 3.12 | . 0565 |  | 4.84 | . 0102 |  | 8.63 | . 0023 | 46 |
| 3.15 | . 0546 |  | 4.89 | -0097 |  | 8.74 | .0022 |  |
| 3.17 | . 0519 |  | $4 \cdot 94$ | . 0092 | 24 | 8.86 | . 0022 |  |
| 3.19 | . 0487 |  | $4 \cdot 98$ | -0087 |  | 8.98 | . 0021 |  |
| 3.22 | . 0458 | 14 | 5.03 | . 0082 |  | 9.10 | . 0020 |  |
| 3.24 | . 0431 |  | 5.08 | -0078 |  | 9.23 | . 0019 |  |
| 3.27 | . 0412 |  | 5.13 | . 0074 |  | 9.36 | .0017 |  |
| 3.29 | . 0401 |  | $5 \cdot 18$ | . 0.070 |  | 9.49 | .0015 |  |
| $3 \cdot 32$ | . 1391 |  | 5.24 | . 0066 |  | 9.62 | .0016 |  |
| 3.34 | .0382 |  | 5.29 | . 0063 |  | 9.76 | .0013 |  |
| 3.37 3.39 | . 0372 |  | 5.34 | . 0061 |  | 9.90 | .0011 |  |
| 3.39 3.42 | .0363 |  | $5 \cdot 40$ | .0058 |  | 10.05 | . 0010 | 90 |
| 3.42 3.45 | .0354 |  | $5 \cdot 45$ | . 0056 | 33 | 10.20 | . 0009 |  |
| 3.45 3.48 | .0346 |  | 5.51 5.57 | . 0053 |  | 10.35 | . 0007 |  |
| 3.48 | .0341 | 15 | $5 \cdot 57$ | . 0051 |  | 10.50 | . 0006 |  |
| 3.50 | . 0337 |  | 5.62 | . 0049 |  | 10.66 | . 0006 |  |
| 3.53 | . 0333 |  | 5.68 | . 0047 |  | 10.82 | . 00008 |  |
| 3.56 | .0329 |  | $5 \cdot 74$ | . 0045 |  | 10.99 | . 0014 |  |
| 3.59 | . 0319 |  | 5.80 | . 0043 |  | 11.16 | . 0016 |  |
| 3.62 | .0309 |  | 5.86 | . 0044 |  | 11.33 | . 0018 |  |
| 3.65 | . 0299 |  | 5.93 | . 0040 |  | 11.51 | . 0013 | 55 |
| 3.68 | -0290 |  | 5.99 | . 0038 |  | 11.69 | . 0009 |  |
| 3.71 | .0283 |  | 6.05 | . 0036 | 42 | 11.87 | . 0004 |  |
| 3.74 | . 0275 |  | 6.12 | . 0035 |  | 12.07 | . 0002 |  |
| 3.77 | . 0266 | 15 | 6.19 | . 0033 |  | 12.26 | . 0008 |  |
| 3.80 | . 0255 |  | 6.25 | .0032 |  | 12.46 | . 0012 | 100 |
| 3.83 | . 0244 |  | $6 \cdot 32$ | . 0031 |  | 12.67 | . 0013 |  |
| 3.87 | . 0234 |  | 6.39 | . 0029 |  | 12.89 | . 0025 |  |
| 3.90 | . 0224 |  | 6.46 | . 0029 |  | 13.11 | . 0050 |  |
| 3.93 | . 0214 |  | 6.53 | . 0028 |  | 13.33 | . 0062 |  |
| 3.97 | . 0205 |  | 6.61 | . 0028 |  | 13.57 | . 0073 |  |
| 4.00 | . 0196 |  | 6.68 | . 0027 |  | 13.81 | . 0079 | 20 |
| 4.04 | . 0188 |  | 6.76 | . 0027 | 49 | 14.06 | . 0064 |  |
| 4.07 | . 0180 |  | 6.83 | . 0027 |  | 14.31 | . 0040 |  |
| 4.11 | . 0174 | 18 | 6.91 | . 0027 |  | 14.58 | . 0019 |  |
| $4 \cdot 14$ | . 0169 |  | 6.99 | . 0027 |  | 14.85 | . 0017 |  |
| 4.18 4.22 | .0164 .0160 |  | 7.07 | . 0027 |  | 15.14 | . 0027 |  |
| $4 \cdot 22$ $4 \cdot 26$ | . .0156 |  | 7.16 7.24 | . 0027 |  | 15.42 | . 0029 | 42 |
| 4.29 | . 0152 |  | 7.33 | . 0027 |  | 16.05 | . 0020 |  |
| $4 \cdot 33$ | . 0149 |  | 7. 42 | . 0026 |  | 16.38 | . 0010 |  |
| $4 \cdot 37$ | . 0145 |  | $7 \cdot 51$ | . 0026 |  | 16.72 | . 0006 |  |
| $4 \cdot 41$ | . 0142 |  | $7 \cdot 60$ | . 0026 | 45 |  |  |  |
| $4 \cdot 45$ | . 0138 |  | 7.69 | . 0025 |  |  |  |  |
| 4.49 | . 0135 | 19 | 7.79 | . 0025 |  |  |  |  |
| $4 \cdot 54$ | .0132 |  | 7.88 | . 0025 |  |  |  |  |
| $4 \cdot 58$ | . 0128 |  | $7 \cdot 98$ | . 0024 |  |  |  |  |

Tab. 2. Angular distributions of neutronselestically and inelastically scattered from $C$ in the center-of-mass system (cm).

| $\stackrel{\mathrm{E}_{\mathrm{O}}}{\mathrm{MeV}]}$ | $\left[{ }^{\circ}\right.$ | $\begin{gathered} \boldsymbol{s}^{\mathrm{cm}} \\ {[\mathrm{o}]} \end{gathered}$ | $\begin{gathered} \sigma_{\mathrm{nn}}^{\mathrm{cm}} \pm \boldsymbol{\sigma} \\ {\left[{\mathrm{mb} \cdot \mathrm{sr}^{-1}}^{ \pm}\right]} \end{gathered}$ | $\left[\begin{array}{c} p^{\mathrm{cm}} \\ 0 \end{array}\right]$ | $\left[\begin{array}{l} \sigma_{\mathrm{nn}}^{\mathrm{cm}} \pm \boxed{ \pm} \\ {\mathrm{mb} \cdot \mathrm{gr}^{-1}}{ }^{-1} \end{array}\right.$ | $\left[\begin{array}{l} j^{\mathrm{j} m} \\ 0 \end{array}\right]$ | $\begin{aligned} & \sigma_{\mathrm{nn}^{\prime}}^{\mathrm{cm}} \Delta \sigma^{ \pm} \\ & {\left[\mathrm{mb}_{\mathrm{sr}}{ }^{-1}\right]} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{Q}=0$ |  | $\mathrm{Q}=-4.439 \mathrm{MeV}$ |  | $Q=-7,653 \mathrm{MeV}$ |  |
| 14.08 | 15.0 | 16.2 | $430.6 \pm 1.2$ | 16.5 | $37.3 \pm 0.5$ | 16.9 | $4.6 \pm 0.3$ |
| 14.10 | 30.0 | 32.4 | $224.5 \pm 0.8$ | 32.9 | $30.0 \pm 0.2$ | 33.7 | $1.9 \pm 0.1$ |
| 14.11 | 40.3 | 43.4 | $118.1 \pm 0.6$ | 44.1 | $27.3 \pm 0.3$ | 45.1 | $1.0 \pm 0.3$ |
| 14.11 | 45.0 | 48.4 | $74.8 \pm 0.3$ | 49.2 | $22.4 \pm 0.2$ | 50.3 | $1.0 \pm 0.2$ |
| 14.12 | 55.6 | 59.5 | $33.7 \pm 0.4$ | 60.4 | $19.5 \pm 0.3$ | 61.7 | $1.1 \pm 0.1$ |
| 14.12 | 60.0 | 64.1 | $22.6 \pm 0.2$ | 65.1 | $15.7 \pm 0.2$ | 66.4 | $0.97 \pm 0.1$ |
| 14.24 | 75.0 | 79.6 | $20.1 \pm 0.2$ | 80.7 | $10.3 \pm 0.1$ | 82.2 | $0.85 \pm 0.1$ |
| 14.25 | 90.6 | 95.4 | $29.3 \pm 0.2$ | 96.5 | $7.5 \pm 0.1$ | 98.0 | $0.69 \pm 0.1$ |
| 14.24 | 104.5 | 109.1 | $30.4 \pm 0.3$ | 110.2 | $8.9 \pm 0.1$ | 111.7 | $0.75 \pm 0.1$ |
| 14.12 | 120.0 | 124.1 | $22.2 \pm 0.3$ | 125.1 | $11.3 \pm 0.1$ | 126.4 | $0.84 \pm 0.2$ |
| 14.11 | 135.0 | 138.4 | $15.7 \pm 0.2$ | 139.2 | $14.2 \pm 0.2$ | 140.3 | $0.46 \pm 0.1$ |
| 14.10 | 150.0 | 152.4 | $17.9 \pm 0.5$ | 152.9 | $19.9 \pm 0.3$ | 153.7 | $0.94 \pm 0.2$ |
| 14.08 | 165.0 | 166.2 | $27.1 \pm 1.3$ | 166.5 | $28.5 \pm 0.7$ | 166.9 | $1.8 \pm 0.6$ |

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