JAERI-M 9823

 $\frac{NEANDC(J) - 77/U}{INDC(JAP) - 64/L}$

EVALUATION OF RESONANCE PARAMETERS OF ²³³U, ²³⁵U, ²³⁸U, ²³⁹Pu, ²⁴⁰Pu, ²⁴¹Pu AND ²⁴²Pu

November 1981

Tsuneo NAKAGAWA, Yasuyuki KIKUCHI, Atsushi ZUKERAN,* Tadashi YOSHIDA,** Masayoshi KAWAI**and Akira ASAMI***

日本原子力研究所 Japan Atomic Energy Research Institute

この報告書は、日本原子力研究所がJAERI-Mレポートとして、不定期に刊行している 研究報告書です。入手、複製などのお問合わせは、日本原子力研究所技術情報部(茨城県 那珂郡東海村)あて、お申しこしください。

JAERI-M reports, issued irregularly, describe the results of research works carried out in JAERI. Inquiries about the availability of reports and their reproduction should be addressed to Division of Technical Information, Japan Atomic Energy Research Institute, Tokai-mura, Naka-gun, Ibaraki-ken, Japan. JAERI-M 9823

Evaluation of Resonance Parameters of 233_{U} , 235_{U} , 238_{U} , 239_{Pu} , 240_{Pu} , 241_{Pu} and 242_{Pu}

Tsuneo NAKAGAWA, Yasuyuki KIKUCHI, Atsushi ZUKERAN^{***} Tadashi YOSHIDA^{**}, Masayoshi KAWAI^{**} and Akira ASAMI^{***}

> Working Group on Heavy-Nuclide Nuclear Data Japanese Nuclear Data Committee Tokai Research Establishment, JAERI (Received November 9, 1981)

This report contains two papers entitled "Evaluation of Resonance Parameters of 233 U, 235 U, 239 Pu and 241 Pu" and "Evaluation of Resonance Parameters of 238 U, 240 Pu and 242 Pu", which were submitted to IAEA Consultants Meeting on Uranium and Plutonium Isotope Resonance Parameters held on the 28th Sept. - 2nd Oct., 1981 at Vienna as contributed papers. Summaries of the contributed papers will be quoted in the IAEA proceedings.

These two parts describe the evaluation of the resonance parameters of main fissile and fertile materials for JENDL-2, and discuss briefly the problems encountered in the evaluation. In part III of this report, the presently evaluated resonance parameters were tabulated.

Keywords : Evaluation, Resonance Parameters, JENDL-2, Uranium-233, Uranium-235, Uranium-238, Plutonium-239, Plutonium-240, Plutonium-241, Plutonium-242.

^{*} Energy Research Laboratory, Hitachi, Ltd.

^{**} Nippon Atomic Industry Group Co., Ltd.

^{***} National Laboratory for High Energy Physics

²³³U, ²³⁵U, ²³⁸U, ²³⁹Pu, ²⁴⁰Pu, ²⁴¹Pu, ²⁴²Puの共鳴パラメータの評価

日本原子力研究所東海研究所シグマ研究委員会重核評価ワーキンググループ 中川 庸雄・菊池 康之・瑞慶覧 篤*・吉田 正**

川合 将**義**•浅見 明^{***}

(1981年11月9日受理)

本報告書は2編の論文より成る。その各々の標題は「²³³U,²³⁵U,²³⁹Pu,²⁴¹Pu の共鳴 パラメータの評価」と「²³⁸U,²⁴⁰Pu,²⁴²Puの共鳴パラメータの評価」であり,1981年 9月28日~10月2日にウィーンで開催された「ウラン・フルトニウム同位体の共鳴パ ラメータに関するIAEAコンサルタント会議」に寄稿したものである。寄稿論文の要旨 はIAEA発行の報文集に掲載されるが、ここではその全体を発刊する。これら2編の論 文は、JENDL-2のために行なった主な核燃料および親物質核種の共鳴パラメータ の評価と、その際に指摘された諸問題を述べている。本報告書の第3部には、今回の評価 結果のパラメータが与えられている。

 [・] 株日立製作所 エネルギー研究所
 ・・ 株日本原子力事業・NAIG総合研究所

^{***} 高エネルギー物理学研究所

Contents

- Part I Evaluation of Resonance Parameters of 233 U, 235 U, 239 Pu and 241 Pu 1
 - 1. Introduction
 - 2. Evaluation Method
 - 3. Evaluation and Discussion
 - Concluding Remarks References

Part II Evaluation of Resonance Parameters of 238 U, 240 Pu and 242 Pu 17

- 1. Introduction
- 2. Evaluation of Resolved Resonance Parameters
- Concluding Remarks References

Part III Appendix: List of Resonance Parameters Adopted in JENDL-241

Part I

Evaluation of Resonance Parameters of 233 U, 235 U, 239 Pu and 241 Pu

Yasuyuki KIKUCHI[†] Akira ASAMI^{*} and

Tadashi YOSHIDA**

Japanese Nuclear Data Committee Tokai Research Establishment Japan Atomic Energy Research Institute

+ Japan Atomic Energy Research Institute

* National Laboratory for High Energy Physics

** Nippon Atomic Industry Group Co., Ltd.

Evaluation of Resonance Parameters of 233 U, 235 U, 239 Pu and 241 Pu

Yasuyuki KIKUCHI⁺, Akira ASAMI^{*} and Tadashi YOSHIDA^{**} Japanese Nuclear Data Committee, Japan Atomic Energy Research Institute

Abstract

The resonance parameters of ²³³U, ²³⁵U, ²³⁹Pu and ²⁴¹Pu were evaluated for Japanese Evaluated Nuclear Data Library Version 2 (JENDL-2). The evaluation was made by two steps. At first, the parameters were evaluated on the basis of the reported measured data with a suitable method which depends on the status of measured data. The most reliable parameter set could be found after some simple examinations for 233 U, 239 Pu and 241 Pu, since total number of measured parameter sets is limited for these nuclides. On the other hand, numerous measurements exist for 235 U, and the evaluation was made by taking a suitable average, considering the fission and capture areas. Secondly, the cross sections were calculated with the parameters thus obtained, and were compared with the measured cross sections. Then the parameters were so modified that the calculated cross sections well reproduced the measured data. After modifying the resonance parameters, the remaining discrepancies between the calculated and measured cross sections, which are mainly caused by the interference among levels and are inevitable with the single-level Breit-Wigner formula, were corrected by applying slight background cross sections. The resonance integrals calculated from the presently evaluated parameters agree well with the measured data.

** Nippon Atomic Industry Group Co., Ltd.

⁺ Japan Atomic Energy Research Institute

^{*} National Laboratory for High Energy Physics

1. Introduction

Evaluation of resonance parameters for main fissile and fertile materials has been made for several years by a working group of Japanese Nuclear Data Committee in order to provide the evaluataed resonance parameters to Japanese Evaluated Nuclear Data Library (JENDL). The evaluation of resonance parameters is a very complicated problem, and the working group recommended some existing evaluated data such as those of ENDF/B-IV for the first version of JENDL (JENDL-1)¹⁾ in 1975.

After that the evaluation was continued and finished in 1979, and the presently evaluated resonance parameters were adopted in the second version of JENDL (JENDL-2). The present paper describes the evaluation for the fissile materials, while the evaluation for the fertile materials is reported in another paper²⁾ presented in this meeting. The general evaluation method is described in Chapter 2. The detailed evaluation procedure is given in Chapter 3 for each nuclide. The presently evaluated resonance parameters are tabulated in Appendix.

2. Evaluation Method

Experimental data of resonance parameters were surveyed through CINDA³⁾ up to CINDA 78. The collected resonance parameters were stored in the resonance parameter storage system REPSTOR⁴⁾. In this system many types of resonance parameters including complicated forms such as $g\Gamma_n\Gamma_\gamma/\Gamma$ or $\sigma_0\Gamma$ can be stored and can be compared with one another in simple tabulation forms.

Experimental cross section data were also surveyed through CINDA. Most of numerical data were obtained from NEA Data Bank, and were stored in the neutron data storage and retrieval system NESTOR⁴⁾.

In evaluating nuclear cross sections, a common procedure is to plot at first all the experimental data as a function of neutron energy, and then deduce the most reasonable curve by carefully comparing the different sets of data and studying the accuracy and errors of the data. In the resonance region, however, this procedure is not always adequate, because a resonance shape usually depends on the resolution function of the spectrometer used for the measurement but this function is not well known in many cases. Furthermore, it is not practical to apply this procedure in the case where many resonances exist in a limited region.

-1-

In the present evaluation, therefore, two steps were taken. Firstly, the resonance parameters were evaluated on the basis of the reported measured parameters with a suitable method which depends on the status of measured data. As total number of measured parameter sets is limited for 233 U, 239 Pu and 241 Pu, the most reliable set could be found after some simple examinations for these nuclides. On the other hand, numerous measurements exist for 235 U, and the evaluation was made by taking a suitable average of the measured parameters.

Secondly, the cross sections were calculated with the parameters thus obtained, and were compared with the measured cross sections. Then the parameters were so modified that the calculated cross sections well reproduced the measured data. This process was made by using NDES⁵⁾ (Neutron Data Evaluation System) in which conversation with the computer is made from a terminal having a cathode ray tube. The calculated cross sections are displayed on the cathode ray tube with the experimental data, and the cross sections calculated with the modified parameters can be also displayed and compared. At present NDES has no function of automatic search for the resonance parameters, and the fitting procedure above mentioned was done by trial and error.

Even after modifying the resonance parameters, the calculated fission cross section failed to reproduce the measured data in limited energy ranges particularly in valleys between resonances. This is caused by the interference among resonances. The multi-level formula is essentially required for fissile nuclides. In the present work, however, the discrepancy was corrected by applying a positive or negative background cross section to the fission cross section. This work was made also by using NDES which has a function to record the X-Y coodinates of any point in the graph displayed on the cathode ray tube into computer memory by using a cross hair cursor.

The thermal cross sections below 1 eV cannot be well reproduced with the resonance parameters for the fissile nuclides because of the interference among levels. Hence the cross sections were given as point-wise data below 1 eV for these 4 nuclides.

- 2 -

3. Evaluation and Discussion

3.1 Uranium-233

This nuclide was not contained in JENDL-1. The resolved resonance region is defined between 1 and 100 eV. Details of the evaluation were described in Ref. (6).

A total of six parameter sets have so far been reported. After examing their experimental conditions and comparing the calculated areas and cross sections, it was concluded that the parameter set deduced by Nizamuddin and Blons⁷⁾ was the most reliable. Their parameters were deduced from both the high resolution measurements of fission cross section by Blons⁸⁾ and the transmission measurements by Kolar et al.⁹⁾ Nizamuddin and Blons gave the parameters for 169 levels, 33 of which are artificial levels added to partially compensate the interference effects among levels. In the energy range below 6 eV, where Nizamuddin and Blons did not give the parameters, the recommended data in BNL-325, 3rd edition¹⁰⁾ were adopted as the initial guess.

The cross sections were calculated from the parameters by assuming the effective scattering radius of 9.93 fm. The calculated total and fission cross sections agree well with the measured data within their scatters in most of energy ranges. It should be noted that the calculated capture cross section agreed well with the measured data by Weston et al.¹¹⁾, though the resonance parameters were deduced by Nizamuddin and Blons without considering the capture data. This suggests reliability of the parameters of Nizamuddin and Blons. In some energy ranges, however, agreement was not satisfactory between the calculated and measured cross sections. The resonance parameters were modified to improve the agreement in such energy ranges by using NDES⁵⁾.

After modifying the parameters, the remaining discrepancies between the calculated and measured fission cross sections were corrected by applying positive or negative background cross sections. Figure 1 shows the fission cross sections calculated with and without the background cross section as well as the measured data in the energy range between 13 and 16 eV. No background correction was applied to the capture and elastic scattering cross sections.

As shown in Table 1 the fission and capture resonance integrals calculated from the present parameters agree with the recommended values in BNL-325, 3rd edition¹⁰⁾ within the quoted errors. They also agree with those calculated from the ENDF/B-IV parameters.

- 3 -

3.2 Uranium-235

The parameters of ENDF/B-IV were recommended in JENDL-1. In JENDL-2, the presently evaluated parameters were applied in the energy region between 1 and 100 eV.

Tremendous number of measurements were made for the resonance parameters of ²³⁵U, since this nuclide is one of the most important nuclide in nuclear reactor development. In the present evaluation only the data reported in the last twenty years were collected and stored in REPSTOR.

The evaluation of the resonance parameters at the first step was made in the following way. Since $2g\Gamma_n$ values do not differ appreciably among those of different experiments, a simple average was taken over average was taken, where a weight of a half was given to those data which were obtained indirectly by analyzing the fission and total cross sections. The evaluation of $\Gamma_{\rm f}$ values seems to require a special care, as the reported values are considerably discrepant with one another. Hence the fission area $A_f = g\Gamma_n \Gamma_f / \Gamma$ was first calculated in this case. In the case where only $\Gamma_{\rm f}$ values were given, ${\rm A}_{\rm f}$ is calculated using the Γ_f and evaluated $g\Gamma_n$ and Γ_γ values. Discrepancy of A_f is usually less than that of $\Gamma_{\rm f}$. A resonance area is, as is well known, independent of the resolution of the spectrometer, and therefore is one of the most suitable quantities to be used in the resonance parameter evaluation. The value of fission width was calculated from the average of fission areas.

The fission, capture and total cross sections were calculated from these parameters thus obtained and were compared with the experimental data. As to the experimental data, we mainly relied on the data of Michaudon et al.¹²⁾, Cao et al.¹³⁾ and Blons et al.¹⁴⁾ for fission, those of de Saussure et al.¹⁵⁾ and Perez et al.¹⁶⁾ for capture and those of Garg et al.¹⁷⁾ and Michaudon et al.¹²⁾ for the total cross section. In the region where the difference is appreciable between the two, correction of the parameters was made for resonances responsible for this difference. If the magnitudes of the total and either of fission or capture areas were considered to deviate from the experimental values, the gr_n value was varied. If only the capture area was unsuitable, small corrections $\Delta\Gamma_{\gamma}$ and $\Delta\Gamma_{f}$ were obtained by

- 4 --

$$\Delta \Gamma_{\gamma} = \frac{\Delta A_{\gamma}}{A_{\gamma}} \frac{1 + r_{1}}{1 - r_{1} - 2r_{1}/r_{2}}, \qquad (1)$$
$$\Delta \Gamma_{f} = \Delta \Gamma_{\gamma}/r_{2},$$

where

$$r_1 = \frac{\Gamma_{\gamma}}{\Gamma_f}$$
, and $r_2 = \frac{1}{2}(r_1 - 1)$. (2)

If the fission cross section is to be varied, similar corrections are obtained by exchanging suffix γ and f. With these corrected parameters, the cross sections were calculated and compared again with the experimental values.

Figure 2 shows an example of the results thus obtained. All the experimental data of the capture and total cross sections available are shown, whereas only some typical data are shown for the fission cross sections. As is seen in the figure, there is a good agreement. In the calculation the Doppler broadening effect is included, which is essential to obtain good fit to the experimental data for most of the resonances in this nuclide. At some energies, particularly at the valleys of resonances, discrepancies still remain. The difference was corrected by the background cross sections. Table 2 compares the fission and capture resonance integrals with the recommended values in BNL-325, 3rd edition¹⁰⁾. The calculated integrals agree well with the recommended values.

3.3 Plutonium-239

In the compilation of JENDL-1, a set of resonance parameters evaluated by Ribon¹⁸⁾ was adopted, for it is a complete set of parameters which reproduces experimental data fairly well. This parameter set covers the energy range between 1 and 600 eV. Since then, no complete set of resonance parameters has been evaluated on the basis of new extensive cross section measurements.

For JENDL-2, Ribon's set was adopted again as the initial guess values. Modification of parameters was limited to several resonances, since his parameter set well reproduces the measured cross sections as a whole. Background cross sections were also added to improve agreement between the calculated and measured cross sections. We fitted the calculated data mainly to the fission cross section measured by Derrien et al.¹⁹ and the capture cross section by Gwin et al.^{20,21} by using NDES.

- 5 -

Figure 3 shows the fission cross section of JENDL-2 with those of JENDL-1 and ENDF/B-IV as well as the experimental data. The difference between JENDL-2 and JENDL-1 was mainly caused by the background cross section.

Table 3 compares the averaged values of the fission cross section and the capture to fission ratio (α -value) between the evaluated and the measured data. The fission cross section of JENDL-2 seems to be too small in the interval between 200 and 300 eV and too large between 300 and 400 eV. This is reflected on overestimate of the α -value between 200 and 300 eV. The present background correction was made by comparing the resonance cross sections without considering the average cross sections. This drawback on the average cross sections is left for future improvement. Table 2 also compares the fission and capture resonance integrals with those recommended in BNL-325, 3rd edition¹⁰. Satisfactory agreement is observed for both the integrals.

3.4 Plutonium-241

In JENDL-1, the resonance parameters recommended in BNL-325, 3rd edition¹⁰ were adopted²⁴⁾ in the energy range from 1 eV to 100 eV. These parameters were mainly taken from analyses by Blons et al.²⁵⁾ and by Kolar et al.²⁶⁾ These paremeters satisfactorily reproduce the total and fission cross sections but a little underestimate the capture cross section²⁴⁾.

In the evaluation of JENDL-2, the same parameters were adopted as the initial guess values, since no extensive measurements have so far been reported on the resonance parameters of 241 Pu after JENDL-1.

The cross sections were calculated by assuming the effective scattering radius of 10.0 fm. The resonance parameters were modified so that the calculated total, fission and capture cross sections might reproduce the measured data by Kolar and Carraro²⁷⁾, by Blons⁸⁾ and by Weston and $\text{Todd}^{28)}$, respectively. As the numerical data of Weston and Todd were not available at the time of the present evaluation, the fitting to the capture cross section was made to the resonances below 20 eV for which the peak values of Weston and Todd were read from graphs in Ref. (28).

The background cross sections were applied to both the fission and capture cross sections. The background fission cross section was determined by NDES so as to compensate the remaining discrepancies between the calculated and measured data due to the interference among levels.

- 6 -

As was pointed out previously, the present resonance parameters a little underestimate the capture cross section and the discrepancy was corrected by the smooth background cross section. Table 4 shows the average fission and capture cross sections calculated with and without the background cross sections as well as the average values of measured data. Figure 4 shows the calculated fission and capture cross sections with the measured data as an example.

Table 4 also compares the calculated resonance integrals with the measured data by Eiland et al.³¹⁾ The present parameters slightly overestimate the capture integral and underestimate the fission integral, but give better results than JENDL-1 and ENDF/B-IV. Further inprovement is required for the lowest few resonances taking account of the numerical cross section data of Weston and Todd.

4. Concluding Remarks

The resonance parameters were evaluated for ²³³U, ²³⁵U, ²³⁹Pu and ²⁴¹Pu, and were adopted in JENDL-2. In the present work, the resonance parameters were first evaluated on the basis of the measured parameter data, and then were adjusted by fitting the calculated cross sections to the measured ones. Hence the presently evaluated parameters can reproduce the measured total, fission and capture cross sections very well. The agreement was further improved by applying slight background corrections. Moreover the calculated resonance integrals agree well with the measured ones. Hence the data of JENDL-2 are expected to well predict the thermal reactor characteristics.

The authors wish to thank to members of Working Group on Heavy-Nuclide Nuclear Data of JNDC for their helpful discussion. They particularly acknowledge T. Nakagawa for his advice in using NDES and for his aid in treating the evaluated data files. One of the authors (A.A.) would like to express his sincere thanks to M. Sugimoto for his assistance in the evaluation.

-7-

References

- IGARASI, S., NAKAGAWA, T., KIKUCHI, Y., ASAMI, T. and NARITA, T.: "Japanese Evaluated Nuclear Data Library, Version-1 - JENDL-1 ---, JAERI-1261 (1979), NEANDC(J)-59/L, INDC(JAP)-45/L.
- 2) NAKAGAWA, T., ZUKERAN, A. and KAWAI, M.: "Evaluation of Resonance Parameters of ²³⁸U, ²⁴⁰Pu and ²⁴²Pu", Contributed paper to IAEA Consultants Meeting on Uranium and Plutonium Isotope Resonance Parameters, 28 Sept. - 2 Oct., 1981, Vienna.
- 3) IAEA: An Index to the Literature on Microscopic Neutron Data.
- NAKAGAWA, T.: Proc. 1978 Seminar on Nuclear Data, Dec. 20 21, 1978, Tokai, p.51, JAERI-M 8163 (1979) [in Japanese].
- 5) NAKAGAWA, T.: J. At. Energy Soc. Jpn., 22, 559 (1980) [in Japanese].
- 6) KIKUCHI, Y.: "Evaluation of Neutron Nuclear Data for ²³³U in Thermal and Resonance Regions", JAERI-M 9318 (1981), NEANDC(J)-69/U, INDC(JAP)-56/L.
- 7) NIZAMUDDIN, S. and BLONS, J.: Nucl. Sci. Eng., 54, 116 (1974).
- 8) BLONS, J.: Nucl. Sci. Eng., <u>51</u>, 130 (1973).
- 9) KOLAR, W., CARRARO, G., NASTRI, G.: "Nuclear Data for Reactors", Conf. Proc., Helsinki, 15 - 19 June 1970, Vol. 1, p. 387 (1970), IAEA.
- 10) MUGHABGAB, S. F. and GARBER, D. I.: "Neutron Cross Sections, Vol. 1, Resonance Parameters", BNL-325, 3rd Edition (1973).
- WESTON, L. W., GWIN, R., DE SAUSSURE, G., FULLWOOD, R. R. and HOCKENBURY, R. W.: Nucl. Sci. Eng., <u>34</u>, 1 (1968).
- 12) MICHAUDON, A., DERRIEN, H., RIBON, P. and SANCHE, M.: Nucl. Phys., 69, 545 (1965).
- 13) CAO, M. G., MIGNECO, E., THEOBALD, J. P., WARTENA, J. A. and WINTER, J.: J. Nucl. Energy, <u>22</u>, 211 (1968).
- BLONS, J., DERRIEN, H. and MICHAUDON, A.: "Neutron Cross Sections and Technology", Proc. Conf., Knoxville, Mar. 15 - 19, 1971, CONF-710301, p. 829 (1971).
- DE SAUSSURE, G., WESTON, L. W., GWIN, R., INGLE, R. W., TODD, J. H., HOCKENBURY,
 R. W., FULLWOOD, R. R. and LOTTIN, A.: "Nuclear Data for Reactors", Conf. Proc.
 Paris, 17 21 Oct. 1966, Vol. II, p. 233 (1967), IAEA.
- 16) PEREZ, R. B., DE SAUSSURE, G., SILVER, E. G., INGLE, R. W. and WEAVER, H.: Nucl. Sci. Eng., 52, 46 (1973).
- 17) GARG, J. B., HAVENS, W. W., Jr. and RAINWATER, J.: Taken from SCISRS Data (1964).
- 18) RIBON, P. and LE COQ, G.: "Evaluation des Données Neutroniques de ²³⁹Pu", CEA - N - 1484 (1971).
- 19) DERRIEN, H., BLONS, J. and MICHAUDON, A.: "Nuclear Data for Reactors", Conf. Proc., Helsinki, 15 - 19 June 1970, Vol. 1, p. 481 (1970), IAEA.
- 20) GWIN, R., WESTON, L. W., DE SAUSSURE, G., INGLE, R. W., TODD, J. H., GILLESPIE,
 F. E., HOCKENBURY, R. W. and BLOCK, R. C.: Nucl. Sci. Eng., <u>45</u>, 25 (1971).

- 8 -

- 21) GWIN, R., SILVER, E. G., INGLE, R. W. and WEAVER, H.: Nucl. Sci. Eng., <u>59</u>, 79 (1976).
- 22) WESTON, L. W. and TODD, J. H.: Private Communication to Chrien (1972). Data Taken from Table III of Ref. (20).
- 23) SOWERBY, M. G. and KONSHIN, V. A.: At. Energy Rev., 10, 453 (1972).
- 24) KIKUCHI, Y.: J. Nucl. Sci. Technol., <u>14</u>, 467 (1977).
- 25) BLONS, J., DERRIEN, H. and MICHAUDON, A,: "Neutron Cross Sections and Technology", Proc. Conf. Knoxville, Mar. 15 - 17, 1971, CONF-710301, p. 836 (1971).
- 26) KOLAR, W., THEOBALD, J. P. and WARTENA, J. A.: ibid., p. 823.
- 27) KOLAR. W. and CARRARO, G.: ibid., p. 707.
- 28) WESTON, L. W. and TODD, J. H.: Nucl. Sci. Eng., 65, 454 (1978).
- 29) MIGNECO, E., THEOBALD, J. P. and WARTENA, J. A.: "Nuclear Data for Reactors", Conf. Proc., Helsinki, 15 - 19 June 1970, Vol. 1, p. 437 (1970), IAEA.
- 30) JAMES, G. D.: ibid., Vol. 1, p. 267.
- 31) EILAND, H. M., ESCH, L. J., FEINER, F. and MEWHERTER, J. L.: Nucl. Sci. Eng., 44, 180 (1971).

				223
Table l	Resonance	Intgrals	of	² JJU.

			(barns)
	JENDL-2	ENDF/B-IV	BNL-325 ¹⁰⁾
fission	771	763	764 <u>+</u> 13
capture	138	135	140 <u>+</u> 6

			(barns)
	JENDL-2	ENDF/B-IV (JENDL-1)	BNL-325 ¹⁰⁾
fission	279	284	275 <u>+</u> 5
capture	146	139	144 <u>+</u> 6

							(barns)
	Energy (keV)	JENDL-2	JENDL-1	ENDF/B-IV	Gwin 76	21) Weston	72 ²²⁾
	0.05 ~ 0.1	60.17	60.30	56.94	56.90	5 58	.76
	0.1 ~ 0.2	18.67	18.42	18.38	17.96 <u>+</u> (0.04 18	.41
σ _f	0.2 ~ 0.3	17.21	17.49	17.64	17.90 <u>+</u> (0.05 17	.77
L	0.3 ~ 0.4	9.09	9.50	8.35	8.48 + (0.03 8	.43
	0.4 ~ 0.5	9.64	9.66	9.55	9.40 + 0	0.05 9	.47
	0.5 ~ 0.6	15.70	16.20	15.44	15.46 <u>+</u> ().09 15	.64
	Energy (keV)	JENDL-2	JENDL-1	ENDF/B-IV	Gwin 76 ²¹⁾	Sowerby 72 ²³⁾	Weston 72 ²²⁾
	0.05 ~ 0.1	0.62	0.61	0.64	0.63	-	0.64
	0.1 ~ 0.2	0.92	0.82	0.93	0.87 ± 0.015	0.845 <u>+</u> 0.077	0.87
α	0.2 ~ 0.3	0.98	0.89	0.99	0.94 + 0.010	0.912 + 0.094	0.92
	0.3 ~ 0.4	1,11	0.91	1.13	1.16 + 0.014	1.15 <u>+</u> 0.099	1.15
	0.4 ~ 0.5	0.51	0.40	0.46	0.44 + 0.013	0.483 + 0.058	0.42
	0.5 ~ 0.6	0.69	0.57	0.73	0.72 <u>+</u> 0.040	0.704 <u>+</u> 0.069	0.72
		JENDL-2	JENDL-1	ENDF/B-IV	BNL-325 ¹⁰⁾		
R.I.	fission	302	302	304	301 <u>+</u> 10		
	capture	195	193	194	200 <u>+</u> 20		

Table 3 Average cross sections and resonance integrals of 239 Pu.

Average cross sections and resonance integrals of 241 Pu. Table 4

Fission cross section

(barns) Calculated Experimental $^{\rm E}{}_{\rm max}$ E min Blons^{8)*} Migneco²⁹⁾ James³⁰⁾ Weston²⁸⁾ with B.C.S. wihout B.C.S. (ev) (eV) 10 20 149.1 147.2 145.9 146.8 ----151.7 20 30 83.9 86.3 81.5 82.9 74.9 86.2 30 40 49.1 50.1 46.6 46.5 45.0 49.3 40 50 40.6 41.5 38.9 36.5 41.0 43.7 50 60 16.7 17.3 15.9 16.8 20.3 17.5 60 70 56.7 59.1 56.5 53.8 59.0 58.7 70 80 22.6 21.6 24.8 28.9 28.7 25.7 80 90 68.9 68.3 65.6 68.6 64.5 73.7 90 100 25.4 25.4 24.9 27.7 31.3 27.2

(barns)

* Average value of the results with 11 and 50 m flight paths.

Capture cross section

E E E max	Calcu	lated	Experimental 28) (Weston and Todd)		
(eV)	(eV) (eV)	with B.C.S.	without B.C.S.	α	σ c
10	20	81.1	69.7	0.559	83.3 <u>+</u> 5.0
20	30	18.7	16.7	0.213	17.9 <u>+</u> 1.1
30	40	10.7	10.7	0,216	10.6 ± 0.6
40	50	7.38	4.49	0.184	7.47 <u>+</u> 0.44
50	60	3.01	1.35	0.198	3.31 <u>+</u> 0.20
60	70	14.2	7.49	0.279	15.8 <u>+</u> 0.9
70	80	15.2	15.2	0.572	12.9 ± 0.8
80	90	22.7	20.6	0.337	23.2 <u>+</u> 1.4
90	100	5.42	4.92	0.207	5.26 ± 0.32

* Deduced from α -values using the present evaluated fission cross section. Errors are quoted 6 % errors in $\alpha\text{-values.}$

Resonance	integral wi	th cut-off	energy of 3 e	V (barns)
Quantity	JENDL-2	JENDL-1	ENDF/B-IV	Eiland et al. $^{31)}$
fission	531	524	527	569 <u>+</u> 37
capture	172	138	115	162 <u>+</u> 8

-12-



Fig. 1 Fission cross sections of ²³³U in the energy range between 13 and 16 eV. The solid and dashdotted lines are calculated from the present resonance parameters with and without the background cross section, respectively. The dotted line represents the value of ENDF/B-IV.



Fig. 2 Total, fission and capture cross sections of 235 U in the energy range between 50 and 60 eV. Note that the capture cross section is multiplied by the square root of neutron energy ($\sigma_c \sqrt{E}$ in barn eV^{1 2} unit)



ິ

Fig. 3 Fission cross sections of ²³⁹Pu in the energy range between 60 and 70 eV. The solid line represents the value of JENDL-2, the dotted line JENDL-1 and the dot-dashed line ENDF/B-IV.



Fig. 4 Fission and capture cross sections of ²⁴¹Pu in the energy range between 40 and 50 eV. The thick solid and dotted lines are calculated from the present parameters with and without the background cross sections, respectively. The thin solid and dotted lines represent the values of JENDL-1 and ENDF/B-IV, respectively.

Part II

Evaluation of Resonance Parameters of 238 U, 240 Pu and 242 Pu

Tsuneo NAKAGAWA[†] Atsushi ZUKERAN^{*} and Masayoshi KAWAI^{**}

Japanese Nuclear Data Committee Tokai Research Establishment Japan Atomic Energy Research Institute

+ Japan Atomic Energy Research Institute

* Energy Research Laboratory, Hitachi, Ltd.

** Nippon Atomic Industry Group Co., Ltd.

Evaluation of Resonance Parameters of $^{238}\text{U}\text{,}~^{240}\text{Pu}$ and ^{242}Pu

T. Nakagawa⁺, A. Zukeran^{*} and M. Kawai^{**}

Japanese Nuclear Data Committee, Japan Atomic Energy Research Institute

Abstract

The evaluation of the resolved resonance parameters of 238 U, 240 Pu and 242 Pu was performed for the second version of Japanese Evaluated Nuclear Data Library JENDL-2. In this work, all the resonance parameters measured so far were compiled and examined. The evaluation was made by mainly using recent measurements for each isotope. The presently evaluated resonances are 183 s-wave and 265 p-wave resonances up to 4.73 keV for 238 U, 267 s-wave resonances up to 5.69 keV for 240 Pu and 95 s-wave resonances up to 1.89 keV for 242 Pu. For 238 U and 240 Pu, negative resonances were also recommended. The multi-level Breit-Wigner formula was applied, and the their resolved resonance regions were chosen to be from 10⁻⁵ eV to 4 keV for 238 U and 240 Pu and from 10⁻⁵ eV to 1.29 keV for 242 Pu. Furthermore, background cross sections were determined to correct the cross sections calculated from the evaluated resonance parameters.

⁺ Japan Atomic Energy Research Institute

^{*} Energy Research Laboratory, Hitachi, Ltd.

^{**} Nippon Atomic Industry Group Co., Ltd.

1. Introduction

The first version of Japanese Evaluated Nuclear Data Library JENDL-1¹⁾ was released in 1977. In JENDL-1, the resolved resonance parameters of 238 U and 240 Pu were mainly taken from ENDF/B-IV²⁾ because our own evaluation work had not been completed. The data of 242 Pu were not contained in JENDL-1.

New experimental data of resonance parameters for these three nuclides have been accumulated after the compilation of JENDL-1. For 238 U, low lying resonances were particularly investigated, because benchmark tests³⁾ for thermal reactors indicated that the underprediction of criticality was due to too large capture widths of the low lying resonances. Transmission measurements were carried out also at various laboratories in wide energy ranges. New measurements of the sub-threshold fission were also performed for 238 U, 240 Pu and 242 Pu. These new data are different from the evaluated parameters adopted in JENDL-1 more or less. This indicates the necessity for a new evaluation work of resolved resonance parameters for JENDL-2.

Our evaluation work of resolved resonance parameters was started around 1975. At first, measured resonance parameters were compiled by using the Resonance Parameter Storage and Retrieval System REPSTOR⁴⁾. Evaluation was performed on the basis of these compiled data. The present evaluation of resonance parameters was mainly based on the recent experiments. The evaluation and results are described in this paper. The results are tabulated in Appendix. The presently evaluated data were compiled in JENDL-2 with ENDF/B format⁵⁾.

2. Evaluation of Resolved Resonance Parameters

2.1 Uranium-238

At the time of the JENDL-1 compilation, the most reliable evaluated data were those by $McCrosson^{6)}$ for ENDF/B-IV who took account of data measured until about 1973. Many new experiments, however, have been made by various experiments since then.

In the present evaluation, the resolved resonance parameters measured until 1980^{7-44} were compiled by using REPSTOR. By comparing them with one another, it was found that there were discrepancies among resonance energies and parameters. The present evaluation was carried out as follows.

-19-

Resonance energy

Systematic discrepancies were found in resonance energies reported by various experimenters. These discrepancies can be interpreted in terms of systematic errors of flight-path length and initial time delay in time-of-flight spectrometers. Neutron energies are represented as follows by using flight-path length L(m), time of flight t(sec) and initial time delay t_0 (sec),

$$E(eV) = \left(\frac{72.2977 L}{t - t_0}\right)^2.$$
 (1)

A systematic error of E caused by errors of L and t_0 can be written as

$$\Delta E(eV) = \frac{2\Delta L}{L} E + \frac{2\Delta t_0}{72.2977 L} E^{3/2} .$$
 (2)

In the present evaluation, measured resonance energies were compared with those of Olsen et al. $^{39)}$ which were adopted as standards. An example of energy discrepancies between Rahn et al. $^{28)}$ and Olsen et al. is shown in Fig. 1 where these discrepancies were reproduced by Eq. (2) with the least squares method. The solid curves in Fig. 1 give the fitted one and one standard deviations. After correction of resonance energies in each measurement by using Eq. (2), the resonance energies were averaged over all the measurements in order to obtain an evaluated value. In the present work, resonance levels reported by neither Poortmans et al. $^{38)}$, Olsen et al. $^{36,39)}$ nor Nakajima⁴⁴⁾ were abandoned.

Finally we adopted 187 s-wave resonances including 4 negative ones and 265 p-wave resonances in the energy range from -113 eV to 4728.0 eV. The energy range where the cross sections are calculated from the resonance parameters was selected to be from 10^{-5} eV to 4 keV.

Neutron and capture widths

The neutron and capture widths were determined by taking account of resonance areas. In the case of 238 U, the resonance areas can be approximated as follows, because the sub-threshold fission widths are negligibly small.

(1) Thin sample transmission area

$$A_1 = 2\pi^2 \pi^2 g\Gamma_n .$$
 (3)

(2) Thick sample transmission area

$$A_2 = 2\pi \frac{1}{\lambda} \sqrt{g\Gamma_n(\Gamma_n + \Gamma_\gamma)} .$$
 (4)

-20-

(3) Thin sample capture area

$$A_{3} = 2\pi^{2} \lambda^{2} g \Gamma_{n} \Gamma_{\gamma} / (\Gamma_{n} + \Gamma_{\gamma}) .$$
⁽⁵⁾

(4) Thin sample scattering area

$$A_{4} = 2\pi^{2} \lambda^{2} g \Gamma_{n}^{2} / (\Gamma_{n} + \Gamma_{\gamma}) .$$
 (6)

For a certain resonance energy, these relations are essentially expressed as

$$a_1 = \Gamma_n, \qquad (3')$$

$$a_{2} = \sqrt{\Gamma_{n}(\Gamma_{n} + \Gamma_{\gamma})}, \qquad (4')$$

$$a_{3} = \Gamma_{n} \Gamma_{\gamma} / (\Gamma_{n} + \Gamma_{\gamma}), \qquad (5')$$

$$a_4 = \Gamma_n^2 / (\Gamma_n + \Gamma_\gamma).$$
(6')

In the present evaluation, the values of a_1 , a_2 , a_3 and a_4 were calculated from the reported values of Γ_n and Γ_γ for each measurement. The values of a_1 , a_2 , a_3 and a_4 are less discrepant than the values of Γ_n and Γ_γ among the different measurements. Then, averaged values of a_1 , a_2 , a_3 and a_4 were obtained, by giving especially high weights to new data measured after 1977. The best values of Γ_n and Γ_γ were so obtained as to minimize the following sum of squares of residuals.

$$I = w_{1}[\langle a_{1} \rangle - \Gamma_{n}]^{2} + w_{2}[\langle a_{2} \rangle - \sqrt{\Gamma_{n}(\Gamma_{n} + \Gamma_{\gamma})}]^{2} + w_{3}[\langle a_{3} \rangle - \frac{\Gamma_{n}^{\Gamma}\Gamma_{\gamma}}{\Gamma_{n} + \Gamma_{\gamma}}]^{2} + w_{4}[\langle a_{4} \rangle - \frac{\Gamma_{n}^{2}}{\Gamma_{n} + \Gamma_{\gamma}}]^{2}, \quad (7)$$

where w_1 , w_2 , w_3 and w_4 are weights for residuals, and $\langle a_1 \rangle$, $\langle a_2 \rangle$, $\langle a_3 \rangle$ and $\langle a_4 \rangle$ stand for averaged values of a_1 , a_2 , a_3 and a_4 , respectively. Figure 2 shows an example of the evaluation of Γ_n and Γ_γ of a resonance at 66.01 eV. Measured resonance parameters are shown in the figure together with errors, and four solid curves give the relations between Γ_n and Γ_γ corresponding to $\langle a_1 \rangle$, $\langle a_2 \rangle$, $\langle a_3 \rangle$ and $\langle a_4 \rangle$. In this example, the best values of Γ_n and Γ_γ were determined to be 24.9 and 22.9 meV, respectively. This method was applied to determine the neutron and capture widths of all the resonances where more than one experiments existed.

-21-

As the results of the present work, smaller capture widths were obtained for the low lying s-wave resonances on the basis of small values in recent measurements. An average capture width obtained from the present parameters is (23.6 ± 1.9) meV which agrees well with (23.5 ± 1.2) meV which is a weighted average of the reported values.

Sub-threshold fission width

The sub-threshold fission widths were determined from the fission resonance areas measured by Difilippo et al.⁴³⁾ Finally, a total of 28 s-wave resonances were given their sub-threshold fission widths.

Effective scattering radius and formula

Olsen et al.³⁹⁾ analyzed their transmission data with a shape analysis code by the multi-level Breit-Wigner formula in various energy intervals and obtained effective scattering radii for those intervals. We adopted the multi-level Breit-Wigner formula and the effective scattering radius of 9.48 fm obtained by averaging the values of Olsen et al. below 2.2 keV.

Correction of calculated cross sections

In order to take account of contributions from negative resonances, four s-wave resonances were added artificially. The first negative resonance was located at -41 eV and its neutron width was determined so as to reproduce at 0.0253 eV the capture cross section of (2.7 ± 0.02) barns, the elastic scattering cross section of (8.90 ± 0.16) barns and the total cross section of (11.60 ± 0.16) barns recommended in BNL-325 3rd edition⁴⁵⁾.

Contributions from the resonances lying outside of the presently considered resonance range (truncation effects) were taken into account by using the picket-fence model. The truncation effects were approximated by

$$\Delta \sigma_{\text{tot}} = \frac{4\pi}{k^2} S_0 \sqrt{E} \left[\frac{<\Gamma >}{4} - \frac{E^+ - E^- + D}{(E^+ - E^+ 0.5D)(E - E^- + 0.5D)} - \frac{1}{2} \ln \left(\frac{E - E^- + 0.582D}{E^+ - E^+ 0.582D} \right) kR \right],$$
(8)

$$\Delta \sigma_{cap} = \frac{\pi}{k^2} S_0 \sqrt{E} < \Gamma_{\gamma} > \frac{E^{-} - E^{-} + D}{(E^{+} - E + 0.5D)(E - E^{-} + 0.5D)}, \qquad (9)$$

$$\Delta \sigma_{\rm el} = \Delta \sigma_{\rm tot} - \Delta \sigma_{\rm cap} , \qquad (10)$$

-22-

where E^+ and E^- are the upper and lower limit energies, respectively, of the presently considered resonances. Equation (8) was derived by de Saussure et al.⁴⁶⁾ and Eq. (9) was obtained in this work with the same procedure. The following values were applied to calculate Eqs. (8), (9) and (10).

$$S_0 = 1.1 \times 10^{-4}$$
, $D = 23.92 \text{ eV}$,
 $E^+ = 4278.0 \text{ eV}$, $E^- = -113.0 \text{ eV}$,
 $R = 9.48 \text{ fm}$, $\langle \Gamma_{V} \rangle = 23.5 \text{ meV}$.

It was found out from a ploting of cumulative numbers of p-wave resonances that the number of p-wave resonances decreased above 1.5 keV. Taking account of contributions from the missed p-wave resonances, the capture cross section above 1.5 keV was corrected by adding small background cross section calculated by the following equation.

$$\Delta \sigma_{\rm cap} = 3.2 \times 10^{-3} \sqrt{E} - 4.8126 \frac{1}{\sqrt{E}} . \tag{11}$$

Figure 3 shows an example of the comparison of the calculated total cross section with measured one. The solid curve shows the present value and the dashed curve JENDL-1. Table 1 lists the thermal properties of the present results. The resonance integral of the capture cross section agrees with the recommended value within the quoted error. The thermal fission cross section also agrees with measured values of $(3 \pm 5) \times 10^{-6}$ barns by Silbert and Bergen²⁵⁾ and $(2.7 \pm 0.3) \times 10^{-6}$ barns by Slovacek et al.³⁷⁾

2.2 Plutonium-240

JENDL-1 adopted the resonance parameters of $ENDF/B-IV^{2}$ up to 3.91 keV, which used the multi-level Breit-Wigner formula in order to avoid the negative values of the elastic scattering cross section. The parameters were given for 201 s-wave resonances including a negative resonance at -4.099 eV, 20 of which were given the sub-threshold fission widths. The present evaluation of 240 Pu resonance parameters was made by using all the experimental data⁴⁷⁻⁶⁶) reported so far.

Resonance energy

The resonance energy of the lowest level was determined to be 1.056 eV on the basis of the measurement by Pattenden and Rainey⁵¹⁾. The other resonance energies above 20 eV were based on the transmission measurement by Kolar and Böckhoff⁵⁸⁾. A negative resonance at -4.099 eV was taken from ENDF/B-IV. Finally a total of 268 resonances from -4.099 eV to 5.692 keV were adopted, and the resolved resonance energy region was defined to be from 10^{-5} eV to 4 keV.

Neutron and capture widths

The resonance parameters of the first resonance at 1.056 eV were taken from the total cross section measurement made by Pattenden and Rainey, and those of the negative resonance from the ENDF/B-IV evaluation.

The neutron and capture widths of resonances from 20 eV to 500 eV were based on the experimental data by Hockenbury et al.⁶³⁾ which agree with those by Kolar and Böckhoff. For the resonances from 500 eV to 5.7 keV, the neutron widths obtained by Kolar and Böckhoff were adopted. For the resonances whose capture widths were not reported, the value of 29.5 meV was assumed by averaging the data of Hockenbury et al. This assumed value is higher than the average value of 23.2 meV obtained by Weigmann and Schmid⁵⁹⁾. Weigmann and Theobald⁶⁴⁾, however, reanalyzed the experimental data by Weigmann and Schmid, and obtained the higher average capture width of (32 ± 2) meV. The ENDF/B-IV evaluation also assumed the value of 29.5 meV.

Sub-threshold fission width

The sub-threshold fission widths were taken from the measured data by Auchampaugh and Weston⁶⁶⁾ in the energy range of 500 eV to 10 keV with the ORELA neutron facility. They obtained the sub-threshold fission widths for 82 resonances with the area and shape analyses by assuming the neutron widths deduced by Kolar and Böckhoff. Furthermore, Auchampaugh and Weston estimated the minimum fission width $\Gamma_{f,min}$ with the formula^{66,67)} by Gai et al. in terms of the penetrabilities through the inner and outer fission barriers,

-24-

$$\Gamma_{f,\min} = \frac{1}{2} \pi \left(\frac{\Gamma^{\dagger} \Gamma^{\dagger}}{D_{II}} \right) D_{I}, \qquad (12)$$

where $\Gamma^{\dagger} = \frac{P_A}{2\pi} D_{II}$, $\Gamma^{\dagger} = \frac{P_B}{2\pi} D_{II}$,

 P_{A}, P_{B} = penetrabilities for the inner and outer barriers, D₁,D₁₁ = average class-I and class-II level spacing.

Auchampaugh and Weston obtained the $\Gamma_{f,min}$ value of (0.22 ± 0.17) meV which was a little higher than 0.20 meV of the ENDF/B-IV value. These 82 sub-threshold fission widths and the minimum fission width of 0.22 meV were used in the present work.

Correction of calculated cross sections

The average capture cross section is compared in Table 2 with the measured data by Weston and Todd $^{68)}$. The differences between them were corrected by applying the background cross sections.

The multi-level Breit-Wigner formula was adopted together with the effective scattering radius of 9.184 fm which is the same as that of ENDF/B-IV. Figure 4 shows the fission cross sections calculated from the present and ENDF/B-IV parameters as well as experimental data. The capture and fission cross sections at 0.0253 eV and their resonance integrals are compared with the recommended values of BNL-325 3rd edition in Table 1. All the values are in agreement with the recommended ones in the quoted errors.

2.3 Plutonium-242

In the case of 242 Pu, resolved resonance parameters are given to only eleven levels up to 390 eV in $ENDF/B-IV^{2}$. They were evaluated on the basis of the data 69-74) measured until 1971. After the ENDF/B-IV evaluation, several new measurements were performed. Bergen and Fullwood⁽⁵⁾ measured the sub-threshold fission cross section by using nuclear explosion and obtained the fission widths of 23 resonances lying from 53.4 to 788.2 eV. Poortmans et al.⁷⁶⁾ determined Γ_{n} and Γ_{n} of 72 levels from 2.68 eV to 1286 eV on the basis of the scattering capture and transmission data measured with the CBNM linac. Harvey et al.⁷⁷⁾, Hockenbury et al.⁷⁸⁾ and Auchampaugh and Bowman⁷⁹⁾ obtained

 Γ_n values of resonances from 22.57 eV to 494.75 eV, from 205.0 eV to 382.4 eV and from 595.2 eV to 3836 eV, respectively, by using their transmission data. Auchampaugh and Bowman gave also the sub-threshold fission widths on the basis of another measurement⁸⁰⁾ of the sub-threshold fission cross section.

In the present evaluation, the measured data mentioned above were compiled together with old ones by using REPSTOR and examined, and a complete set of resolved resonance parameters was determined up to 1891 eV. The multi-level Breit-Wigner formula was applied.

Resonance energy

Resonance energies up to 1891 eV were taken from the recommended values of BNL-325 3rd edition⁴⁵, but the resolved resonance energy region was determined to be from 10^{-5} eV to 1290 eV because resonance parameters were not given between 1290 to 1700 eV.

Neutron and capture widths

The neutron and capture widths were determined by averaging the measured values. The obtained neutron widths are close to those of Poortmans et al.⁷⁶⁾ and Auchampaugh and Bowman⁷⁹⁾. For the resonances whose capture widths were not measured, the value of 24.2 meV was applied.

Sub-threshold fission width

The sub-threshold fission widths were deduced from the fission areas given by Bergen and Fullwood⁷⁵⁾ and by Auchampaugh and Bowman⁷⁹⁾. In order to give the sub-threshold fission widths to the resonances whose fission widths were not measured, an average was taken over the resonances locating outside an intermediate fission resonance near 750 eV. The average value of 0.116 meV was thus obtained in the energy range from 200 to 900 eV, and was applied in this energy region. For the other energy regions, $\Gamma_{\rm f} = 0.05$ meV was assumed, by taking account of the neutron energy dependence of the sub-threshold fission width near the intermediate fission resonance.

Correction of calculated cross sections

Using the resonance parameters thus obtained and the effective scattering radius of 9.6 fm recommended in BNL-325 3rd edition, the

-26-

cross sections were calculated. It was found that the thermal capture cross section agreed well with the experimental values $^{70,73,74,81,82)}$, and the thermal fission cross section fell below the experimental upper limit of 0.2 barns. The elastic scattering and total cross sections, however, were lower than recommended values of BNL-325 3rd edition. We corrected them by adding the background cross sections of 0.67 barns so as to reproduce the measured data of the elastic $^{83)}$ and total cross sections $^{73,74)}$.

Table 1 shows comparison of thermal cross sections and resonance integrals with values recommended in BNL-325 3rd edition. The present resonance integral for capture agrees well with the BNL-325 data and the measured data by Young et al.^{73,74)}, and the value for fission is slightly larger than the BNL-325 recommendation. Figure 5 displays the total cross section in the energy range of 1 eV to 100 eV. The present result shown with a thick solid line slightly underestimates the total cross section at off-resonance energies. The same problems are also found in the other evaluations. This disagreement may be diminished by the adjustment of the scattering radius. The evaluated fission cross sections are shown in Fig. 6 below 10 keV. There are very large discrepancies among the present results, ENDF/B-V⁸⁴⁾, KEDAK-3⁸⁵⁾ and ENDL-78⁸⁶⁾. Particularly the present fission cross section is higher than the others by an order of magnitude below 0.5 eV as seen in Fig. 6.

Average resonance parameters were obtained from the presently evaluated parameters below 500 eV which were regarded as s-wave resonances. They are $D_0 = 13.04$ eV, $S_0 = 0.85 \times 10^{-4}$ and $\overline{\Gamma}_{\chi} = 24.2$ meV.

3. Concluding Remarks

The evaluation of the resolved resonance parameters of ²³⁸U, ²⁴⁰Pu and ²⁴²Pu was performed for the second version of Japanese Evaluated Nuclear Data Library JENDL-2 by using all the experimental data reported so far. The evaluated parameters are listed in Appendix. The multilevel Breit-Wigner formula was adopted to avoid the negative values in the elastic scattering cross section.

The neutron and capture widths of 238 U were determined by applying the least squares method to resonance areas. The capture widths of the low lying resonances became smaller than those of ENDF/B-IV. The

-27-

evaluated fission widths were based on the measured fission areas. The resonance energies were determined by averaging the values of recent measurements after correction of their systematic errors. Finally 183 s-wave and 265 p-wave resonances were recommended up to 4.73 keV.

A total of 267 resonances up to 5.69 keV were recommended for 240 Pu. Their sub-threshold fission widths were obtained by taking account of the ORELA measurement by Auchampaugh and Weston. The resonance parameters of 242 Pu were determined for 95 resonances up to 1.89 keV. Their neutron and capture widths were obtained by averaging the measured values, and the sub-threshold fission widths were given to all the resonances on the basis of measured fission areas. All the resonances were assigned as s-wave resonances for 240 Pu and 242 Pu. This seems improbable taking account of the situation of 238 U. Probably some p-wave resonances were misassigned as s-wave ones and some p-wave resonances might be missing.

The energy region where the cross sections are calculated from the parameters were determined to be from 10^{-5} eV to 4 keV for 238 U and 240 Pu, and from 10^{-5} eV to 1.29 keV for 242 Pu. The background cross sections were also evaluated in order to reproduce well the measured cross sections. The thermal fission and capture cross sections and their resonance integrals agree with the recommended values in BNL-325 3rd edition.

The authors thank to the members of Working Group on Heavy-Nuclide Nuclear Data for their useful discussion during the present work.

References

- Igarasi, S., Nakagawa, T., Kikuchi, Y., Asami, T. and Narita, T.: "Japanese Evaluated Nuclear Data Library, Version-1, --JENDL-1--", JAERI 1261 (1979).
- 2) Compiled by Garber, D.: "ENDF/B Summary Documentation", ENDF-201 (1975).
- 3) Edited by Pearlstein, S.: "Seminar on ²³⁸U Resonance Capture", BNL-NCS-50451 (1975).
- Nakagawa, T.: "Computer Codes for Neutron Data Evaluation", JAERI-M 8163, 51 (1979) [in Japanese].
- 5) Garber, D., Dunford, C. and Pearlstein, S.: "Data Formats and Procedures for the Evaluated Nuclear Data File, ENDF", ENDF-102 (1975).
- 6) McCrosson, F. J.: "Evaluation of ²³⁸U cross sections for ENDF/B-IV", Seminar on ²³⁸U Resonance Capture, BNL-NCS-50451, p. 122 (1975).
- 7) Harvey, J. A., Hughes, D. J., Carter, R. S. and Pilcher, V. E.: Phys. Rev. <u>99</u>, 10 (1955).

- Lynn, J. E. and Pattenden, N. J.: "The Slow Neutron Cross Sections of the Uranium Isotopes", Proc. of the International Conference on the Peaceful Uses of Atomic Energy, Geneva (1955), vol. 4, 210.
- 9) Fluharty, R. G., Simpson, F. B. and Simpson, O. D.: Phys. Rev. 103, 1778 (1956).
- 10) Levin, J. S. and Hughes, D. J.: Phys. Rev. <u>101</u>, 1328 (1956).
- Bollinger, L. M., Cote, R. E., Dahlberg, D. A. and Thomas, G. E.: Phys. Rev. <u>105</u>, 661 (1957).
- 12) Radkevich, I. A., Vladimirsky, V. V. and Sokolovsky, V. V.: J. Nucl. Energy <u>5</u>, 107 (1957).
- Leonard, Jr. B. R. and Odegaaden, R. H.: "Sub-threshold Fission ²³⁶U, ²³⁸U, ²⁴⁰Pu, ²⁴¹Pu, ²³¹Pa", HW-67219 (1960).
- 14) Rosen, J. L., Desjardins, J. S., Rainwater, J. and Havens, Jr. W. W.: Phys. Rev. 118, 687 (1960).
- 15) Jackson, H. E. and Lynn, J. E.: Phys. Rev. <u>127</u>, 461 (1962).
- 16) Moxon, M. C. and Mycock, C. M.: Qouted from BNL 325 (2nd edition).
- 17) Firk, F. W. K., Lynn, J. E. and Moxon, M. C.: Nucl. Phys. <u>41</u>, 614 (1963).
- 18) Garg, J. B., Rainwater, J., Peterson, J. S. and Havens, Jr. W. W.: Phys. Rev. <u>134</u>, B985 (1964).
- 19) Asghar, M., Chaffey, C. M. and Moxon, M. C.: Nucl. Phys. <u>85</u>, 305 (1966).
- 20) Bollinger, L. M. and Thomas, G. E.: Phys. Rev. 171, 1293 (1968).
- 21) Glass, N. W., Schelberg, A. D., Tatro, L. D. and Warren, J. H.: "²³⁸U Neutron Capture Results from Bomb Source Neutrons", Proc. of the Second Conference on Neutron Cross Sections and Technology, Washington (1968), Vol. 1, 573.
- 22) Carraro, G. and Kolar, W.: "Neutron Widths of ²³⁸U from 60 eV to 5.7 keV", Proc. of the Conference on Nuclear Data for Reactors, Helsinki (1970), Vol. 1, 403.
- 23) Rohr, G., Weigmann, H. and Winter, J.: "Resonance Parameters from Neutron Radiative Capture in ²³⁸U", Proc. of the Conference on Nuclear Data for Reactors, Helsinki (1970), Vol. 1, 413.
- 24) Carraro, G. and Kolar, W.: "Total Neutron Cross Section Measurements of ²³⁸U", Proc. of the Third Conference on Neutron Cross Section and Technology, Knoxville (1971), Vol. 2, 701.
- 25) Silbert, M. G. and Bergen, D. W.: Phys. Rev. <u>C4</u>, 220 (1971).
- 26) Wasson, O. A., Chrien, R. E., Slaughter, G. G. and Harvey, J. A.: Phys. Rev. <u>C4</u>, 900 (1971).
- 27) Malecki, H., Pikel'ner, L. B., Salamatin, M. and Sharapov, F. I.: Atomnaya Energiya 32, 49 (1972).
- 28) Rahn, F., Camarda, H. S., Hacken, G., Hevens, Jr. W. W., Liou, H. I., Rainwater, J., Slagowitz, M. and Wynchank, S.: Phys. Rev. <u>C6</u>, 1854 (1972).
- 29) Block, R. C., Hockenbury, R. W., Slovacek, R. E., Bean, E. B. and Cramer, D. S.: Phys. Rev. Letters <u>31</u>, 247 (1973).

- 30) de Saussure, G., Silver, E. G., Perez, R. B., Ingle, R. and Weaver, H.: Nucl. Sci. Eng. <u>5</u>1, 385 (1973).
- 31) Ceulemans, H.: "Resonance Scattering Cross-Section of ²³⁸U below 220 eV", Proc. of the Specialist Meeting on Resonance Parameters of Fertile Nuclei and ²³⁹Pu, Saclay (1974), 145.
- 32) Corvi, F., Rohr, G. and Weigmann, H.: "p-wave Assignment of ²³⁸U Resonances", Proc. of a Conference on Nuclear Cross Sections and Technology, Washington (1975), Vol. 2, 732.
- 33) Wartena, J. A., Weigmann, H. and Migneco, E.: "On Sub-barrier Fission in ²³⁸U", Proc. of a Conference on Nuclear Cross Sections and Technology, Washington (1975), Vol. 2, 597.
- 34) Difilippo, F. C., Perez, R. B., de Saussure, G., Olsen, D. K. and Ingle, R. W.: Nucl. Sci. Eng. <u>63</u>, 153 (1977).
- 35) Liou, H. I. and Chrien, R. E.: Nucl. Sci. Eng. <u>62</u>, 463 (1977).
- 36) Olsen, D. K., de Saussure, G., Perez, R. B., Silver, E. G., Difilippo, F. C., Ingle, R. W. and Weaver, H.: Nucl. Sci. Eng. 62, 479 (1977).
- 37) Slovacek, R. E., Cramer, D. S., Bean, E. B., Valentine, J. R., Hockenbury, R. W. and Block, R. C.: Nucl. Sci. Eng. <u>62</u>, 455 (1977).
- 38) Poortmans, F., Cornelis, E., Mewissen, L., Rohr, G., Shelley, R., van der Veen, T., Vanpraet, G. and Weigmann, H.: "Cross Sections and Neutron Resonance Parameters for ²³⁸U below 4 keV", Proc. of the International Conference on the Interactions of Neutrons with Nculei, Lowell (1976), 1264.
- 39) Olsen, D. K., de Saussure, G., Perez, R. B., Difilippo, F. C., Ingle, R. W. and Weaver, H.: Nucl. Sci. Eng. 69, 202 (1979).
- 40) Stavealoz, P., Poortmans, F., Mewissen, L. and Cornelis, E.: Nucl. Sci. Eng. <u>66</u>, 349 (1978).
- 41) Block, R. C., Harris, D. R., Kim, S. H. and Kobayashi, K.: "²³⁸U Resonance Self-Indication Capture Measurements and Analysis", EPRI NP-996 (1979).
- 42) Haste, T. J. and Moxon, M. C.: "Resonance Parameters of ²³⁸U below a Neutron Energy of 520 eV", Proc. of an International Conference on Neutron Physics and Nuclear Data, Harwell (1978), 337.
- 43) Difilippo, F. C., Perez, R. B., de Saussure, G., Olsen, D. K. and Ingle, R. W.: Phys. Rev. <u>C21</u>, 1400 (1980).
- 44) Nakajima, Y.: Ann. Nucl. Energy 7, 25 (1980).
- 45) Mughabghab, S. F. and Garber, D. I.: "Neutron Cross Sections Vol. 1, Resonance Parameters", BNL-325, 3rd Edition Vol. 1 (1973).
- 46) de Saussure, G., Olsen, D. K. and Perez, R. B.: Nucl. Sci. Eng. <u>61</u>, 496 (1976).
- 47) Estwood, T. A., Baerg, A. P., Bigham, C. B., Brown, F., Cabell, M. J., Grummitt, W. E., Roy, J. C., Roy, L. P. and Schuman, R. P.: "Radiochemical Methods Applied to the Determination of Cross Sections of Reactor Interest", Proc. of the Second United Nations International Conference on the Peaceful Uses of Atomic Energy, Geneva (1958), Vol. 16, 54.

- 48) Fields, P. R., Ryle, G. L., Inghram, M. G., Diamond, H., Studier, M. H. and Manning, W. H.: Nucl. Sci. Eng. <u>1</u>, 62 (1956).
- 49) Roose, H., Cooper, W. A. and Tattersall, R. B.: "The Use of the Pile Oscillator in Thermal Reactor Problems", Proc. of the Second United Nations International Conference on the Peaceful Uses of Atomic Energy, Geneva (1958), Vol. 16, 34.
- 50) Halperin, J. H., Oliver, J. O. and Pamerance, H. S.: J. Inorg. Nucl. Chem. <u>9</u>, 1 (1959).
- 51) Pattenden, N. J. and Rainey, V. S.: J. Nucl. Energy <u>11</u>, 14 (1959).
- 52) Block, R. C., Slaughter, G. G., Pattenden, N. J. and Harvey, J. A.: "The ORNL Fast-Chopper Time-of-Flight Neutron Spectrometer", Proc. of IAEA Symposium on Pile Neutron Research, Vienna (1960), 535.
- 53) Block, R. C., Slaughter, G. G. and Harvey, J. A.: Nucl. Sci. Eng. 8, 112 (1960).
- 54) Cabell, M. J. and Wilkins, M.: J. Inorg, Nucl. Chem. 28, 2467 (1966).
- 55) Lounsbury, M., Durham, R. W. and Hanna, G. C.: "Measurements of Alpha and Fission Cross Section Ratios for U-233, U-235 and Pu-239 at thermal Energies", Proc. of the Conference on Nuclear Data for Reactors, Helsinki (1970), Vol. 1, 287.
- 56) Ramakrishina, D. V. S. and Navalkar, M. P.: "Determination of Resonance Parameters of Pu-240 using a Crystal Spectrometer", Proc. of the Conference on Nuclear Data for Reactors, Helsinki (1970),
- 57) Asghar, M., Moxon, M. C. and Pattenden, N. J.: "Neutron Resonance Parameters of ²⁴⁰Pu", Proc. of Conference on Nuclear Data for Reactors, Paris (1966), Vol. 2, 145.
- 58) Kolar, W. and Böckhoff, K. H.: J. Nucl. Energy 22, 299 (1968).
- 59) Weigmann, H. and Schmid, H.: J. Nucl. Energy 22, 317 (1968).
- 60) Migneco, E. and Theobald, J. P.: "Resonance Grouping Structure in Neutron Induced Sub-threshold Fission of Pu-240", Proc. of the Second Conference on Neutron Cross Sections and Technology, Washington (1968), Vol. 1, 527.
- 61) Cao, M. G., Migneco, E., Theobald, J. P. and Wartena, J. A.: "Scattering Cross Section of Pu-240", Proc. of the Second Conference on Neutron Cross Sections and Technology, Washington (1968), Vol. 1, 513.
- 62) Asghar, M., Moxon, M. C. and Pattenden, N. J.: "Neutron Capture Measurements in the Resonance Parameters of Pu-240", EANDC(UK) 103AL (1968).
- 63) Hockenbury, R. W., Moyer, W. R. and Block, R. C.: Nucl. Sci. Eng. <u>49</u>, 153 (1972).
- 64) Weigmann, H. and Theobald, J. P.: J. Nucl. Energy 26, 643 (1972).
- 65) Moxon, M. C.: private communication to Weigmann, H. and Theobald, J. P., see Ref. 64.
- 66) Auchampaugh, G. F. and Weston, L. W.: Phys. Rev. <u>C12</u>, 1850 (1975).
- 67) Lynn, J. E.: "Structure in Sub-threshold Fission Modes", AERE-R 5891 (1968).
- 68) Weston, L. W. and Todd, J. H.: Nucl. Sci. Eng. <u>63</u>, 143 (1977).
- 69) Egelstaff, P. A., Gayther, D. B. and Nicholson, K. P.: J. Nucl. Energy <u>6</u>, 303 (1958).

- 70) Coté, R. E., Bollinger, L. M., Barnes, R. F. and Diamond, H.: Phys. Rev. <u>114</u>, 505 (1959).
- 71) Pattenden, N. J.: "Slow Neutron Transmission Measurements on Pu-242", Proc. of the International Conference on the study of Nuclear Structure with Neutrons, Antwerp (1965), 93.
- 72) Auchampaugh, G. F., Bowman, C. D., Coops, M. S. and Fultz, S. C.: Phys. Rev. <u>146</u>, 840 (1966).
- 73) Young, T. E. and Reeder, S. D.: Nucl. Sci. Eng. <u>40</u>, 389 (1970).
- 74) Young, T. E., Simpson, F. B. and Tate, R. E.: Nucl. Sci. Eng. <u>43</u>, 341 (1971).
- 75) Bergen, D. W. and Fullwood, R. R.: Nucl. Phys. <u>A163</u>, 577 (1971).
- 76) Poortmans, F., Rohr, G., Theobald, J. P., Weigmann, H. and Vanpraet, G. J.: Nucl. Phys. <u>A207</u>, 342 (1973).
- 77) Harvey, J. A., Hill, N. W., Benjamin, R. W., Ahlfeld, C. E., Simpson, F. B., Simpson, O. D. and Miller, H. G.: "Neutron Total Cross Section of ²⁴⁸Cm and ²⁴²Pu from 0.5 to 5000 eV", ORNL-4844, 90 (1973).
- 78) Hockenbury, R. W., Sanislo, A. J. and Kaushal, N. N.: "KeV Capture Cross Section of ²⁴²Pu", Proc. of Fourth International Conference on Nuclear Cross Sections and Technology, Washington (1975), 584.
- 79) Auchampaugh, G. F. and Bawman, C. D.: Phys. Rev. <u>C7</u>, 2085 (1973).
- 80) Auchampaugh, G. F., Farrell, J. A. and Bergen, D. W.: Nucl. Phys. <u>A171</u>, 31 (1971).
- 81) Durham, R. W. and Molson, F.: Can. J. Phys. <u>48</u>, 716 (1970).
- 82) Butler, J. P., Lousbury, M. and Merritt, J. S.: Can. J. Phys. <u>35</u>, 147 (1957).
- 83) Lander, G. H. and Mueller, M. H.: Acta Crystallographica <u>B27</u>, 2284 (1971).
- 84) Mann, F. M. and Schenter, R. E.: "HEDL Evaluation of Actinide Cross Sections for ENDF/B-V", HEDL-TME 77-54 (1977).
- 85) Goel, B.: Contribution to the NEANDC Specialist Meeting on Nuclear Data of Higher Plutonium and Americium Isotopes for Reactor Applications, BNL (1978).
- 86) Howerton, R. J. and MacGregor, M. H.: "The LLL Evaluated Nuclear Data Library (ENDL) Descriptions of Individual Evaluations for Z = 0 - 98", UCRL-50400, Vol. 15, Part D (1978).

Isotope	Quantity	BNL-325 (3rd)	JENDL-2
	бсар	2.70 <u>+</u> 0.02	2.699
238 ₁₁	σ _f		3.86×10^{-6}
C	I	275 <u>+</u> 5	279
	ľ		2.05
	o cap	289.5 <u>+</u> 1.4	288.5
240 _{Pu}	σ _f	0.030 <u>+</u> 0.045	0.0676
	I,	8013 <u>+</u> 960	8454
	If		10.1
·····	σ cap	18.5 <u>+</u> 0.4	18.43
242 _{Pu}	σ _f	<0.2	0.013
± G	I	1130 <u>+</u> 60	1117
	If	5	6.3

					*
T a ble	1	Comparison	of	thermal	properties

* All the values are given in barns.

E (keV)	experiment ⁶⁸⁾ (E)	calculated (C)	E-C	adopted ^{**} background
0.1 - 0.3	8.71 + 0.61	7.15	1,56)
0.3 - 0.4	10,27 <u>+</u> 0,72	8,00	2,27	} 1.92
0.4 - 0.5	6.60 <u>+</u> 0.46	6.24	0.36)
0.5 - 0,6	7.14 <u>+</u> 0.50	6.34	0.80	0.80
0.6 - 0.7	5.09 <u>+</u> 0.36	3,85	1.24	J
0.7 - 0.8	2.63 ± 0.18	1,71	0.92	
0.8 - 0.9	6.63 <u>+</u> 0.46	3,73	2.92	1.60
0.9 - 1.0	5.53 <u>+</u> 0.39	4.55	0.98	}
1.0 - 1.5	3.50 <u>+</u> 0.25	2.44	1.06	\mathbf{i}
1.5 - 2.0	3.03 <u>+</u> 0.21	2.01	1.02	∫ ^{1.04}
2.0 - 3.0	2,42 <u>+</u> 0,17	1.43	0.99	0.99
3.0 - 4.0	1,89 <u>+</u> 0,13	0.798	1.092	1,092

Table 2 Background values for the ²⁴⁰ pu capture cross section*

* All the values are given in barns.

** Average values of (E-C) were adopted as background cross
sections.



Fig. 1 Resonance energy discrepancies in ²³⁸U between the measurements by Rahn et al. and by Olsen et al. Solid curves show the fitted values with the least squares method and its one standard deviations.



Fig. 2 Typical example of relations between neutron and capture widths of 238 U resonance at 66.01 eV. Four curves a_1 , a_2 , a_3 and a_4 represent the relations by Eqs. (3'), (4'), (5') and (6'), respectively, corresponding to the average values obtained from the reported resonance parameters.



-36 -

Fig. 3 Total cross sections of 238 U in the energy range from 50 eV to 100 eV.



Fig. 4 Fission cross sections of 240 Pu up to 100 eV.



-38-

Fig. 5 Total cross sections of 242 Pu in the energy range from 1 to 100 eV.



Fig. 6 Average fission cross sections of ²⁴²Pu in the energy range from 0.01 eV to 10 keV.

Part III

Appendix

List of Resonance Parameters Adopted in JENDL-2

U-2	233
-----	-----

ENERGY (EV)	L	J	TOTAL WIDTH (MEV)	NEUTRON WIDTH	CAMMA WIDTH (MEV)	FISSION WIDTH	REFERENCE
-2.81	0	2.5	754.5	4.5	30.0	720.0	JENDL-2
0.17	D	2.5	100.0	0.0002	40.0	50.0	JENCL - 2
1.45	0	2.5	530-11	0.11	30.0	500.0	JENCL 2
2.17	0	2.5	250-334	0.03	50.0	210.0	JENUL 2
2.29	0	2.5	123.03	0.17	50.0	50.0	IENOL 2
3.49	õ	2.5	500.07	0.07	45.C	455.0	JENCL 2
3.62	С	2.5	185.1	0.1	50.C	135.0	JENDL - 2
4.76	C	2.5	900 - 31	0.31	45. C	855.0	JENDU-2
5.89	0	2.5	320.133	C - 1 3282	39.0	281.0	JENOL-2
6.27	U 0	2.5	530.062	0.21264	39.0	499.0	JENUL-2
6.82	0	2.5	138.796	0.79645	19+C	401.0 99.0	I JENOL - 2
7.5	õ	2.5	200.028	0.028	39.0	161.0	JENDL-2
8.0	D	2.5	2039.08	0.08	39.0	2000.0	JENDL-2
8.64	0	2.5	339.05	0.05	39.0	300.0	JENDL-2
9.26	0	2.5	298.12	0.12	39.0	259.0	JENOL - 2
9-71	C O	2.5	500.05	0.06	39.0	461.0	JENDL-2
10.39	c c	2.5	1000.01	8.676-3	27.0	258.0	JENUL-2 JEND -2
11.3:	č	2.5	439.2	0.2	39.0	400.0	JEND 2
11.89	Ĉ	2.5	2000.5	0.5	39.0	1961.0	JEND, -2
12.79	С	2.5	310.446	1.4457	55.0	254.0	JEND2
13.45	0	2.5	144.056	5.619-2	39.0	105.0	LJEND2
13.73	0	2.5	255.309	0,30863	39.0	216.0	JEND2
10-33	U	2.5	122.404	0.40445	2070 39 h	92-0 216 0	JENUL 7 JENDI - 2
15.82	C C	2.5	200.02	0.02	39.0	161.0	JENDLEZ
16-2	õ	2.5	425.896	C-89638	39.0	387.0	JENDL 2
16.56	Ō	2.5	219.706	0 70587	39.0	180.0	JENOL-2
17.97	0	2.5	208:32	C.32005	39.0	169.0	JEND 2
18-28	0	2.5	379.015	0.015	39.0	340.0	JEND_ 2
18.48	U	2.5	135.158	0.15834	39.0	96.0	JEND: -2
19.63	0	2.5	2500.39	0.39487	39.0	294.0	JENUL-2 JEND -2
20.59	õ	2.5	364.773	0.77279	39.0	325.0	JEND2
21.58	0	2.5	2000.59	J.58669	39.0	1961.0	JENDL-2
2:.86	0	2.5	255.062	1-3621	29.0	215.0	JENDL-2
22.34	U	2.5	415.332	1-111/ D 55449	48.0	364.0	JENDL-2
23.75	U C	2.5	453.554	1.554:9	39.0	414 0	IEND 2
24.3	õ	2.5	1000.52	0.51997	39.0	961.0	JENDL - 2
25.25	0	2.5	274.74	0.73993	39.0	235.0	JENOL - 2
25.78	0	2.5	660.522	0.52169	39 - C	621.0	JENDL - 2
26.25	0	2.5	495.239	0.23872	39.0	456.0	JENOL - 2
26.62	U	2.5	260-358	0.35778	39.0	221.0	JENUL-2 JEND 0
20.30	0	2.5	900.508	0.5083	39.0	861.0	JEND -7
25.07	õ	2.5	168.028	2.754-2	39.0	129.0	JENDL-2
28.28	0	2.5	230.233	0.23343	39.0	19:.0	JENDL-2
29.04	С	2.5	541.764	1.7641	39.0	201-0	JENDL - 2
29.58	U	2.5	112-138	0.13826	39.0	73.0	JENDL - 2
30.33	0	2.5	261.627	0.62701	37.0	224 0	I JENDL-2
31.33	Ō	2.5	325 298	0.29827	39.0	286.0	JENDL-2
31.69	С	2.5	600.465	0.45464	39.0	561.0	JENOL-2
32.01	0	2.5	217.951	0.95107	39.0	17 8. 0	JENOL-2
33.14	0	2.5	740.719	C.71939	39.0	701.0	JENDL-2
33.95	U	2.5	1301+/9	1./05	39.0	1261.0	
35.25	n n	2.5	395.238	0.2383	39.0	356.0	JEND2
35.75	ō	2.5	900.683	0.68306	39.0	861.0	JENDL-2
36.53	0	2.5	197.798	0.79785	39.0	150.0	JENDL-2
37.2	0	2.5	420.094	9.359-2	39.0	381-0	JENOL-2
34.40	U	2.5	343-647 686.704	0,050/9	39.0	356-U 647 0	JENUL-2 JEND: -2
39,83	U N	2.5	445.266	0.794	39.0 79.0	0≁/-U 406.0	JENUL - 2 JENDI - 2
40.41	0	2.5	901.062	1.0616	39.0	861.0	JENOL-2
41.03	0	2.5	175.34	0.34	39.0	136.C	JENOL - 2
41.79	0	2,5	392.035	3.534-2	39.0	353.0	JENOL - 2
42.09	0	2.5	592-137	0.13727	39.0	553.0	JENDL-2
43.5	U N	2.5	209.77	0.4	20.0	321.0	JENUL-2 IEND: - 2
44.52	õ	2.5	519.3	0.3	19.0	500.0	JENOL -2
45.25	0	2.5	138.025	0.025	39.0	99.0	JENDL-2
45.45	D	2.5	150.025	0.025	39.0	111.0	JENDL-2
46.1	0	2.5	192-39	0.39	39.0	153.0	JENOL-2
47.22	U N	2.5	243.00 507.88	0.00	0. PE	200-0 468-0	JENUL-2
48.68	Ċ	2.5	172.6	1.6	40.0	131.0	JENOL - 2
49.1	ō	2.5	516.5	0.5	39.0	477.0	JENOL -2
50.4	0	2.5	1100-84	0.84	39.0	1061-0	JENOL - 2
51.0	D	2.5	500.114	0.114	39.0	461.0	JENOL-2
52.1	U N	2.5	150+021 280+055	0+021 0-055	39.0 39.0	241.0	IJENUL-Z
53.03	D	2.5	240.47	0.47	39.0	201.0	JENDL - 2
53.32	0	2.5	360.44	0.44	39.0	321.0	, JENOL - 2
. <u> </u>							_ +

U	2	3	3
 _	_	_	

n	
Ζ.	
-	

53-64 0 2.5 220.198 0.19788 19.0 461.0 J.KNL-2 54-05 0 2.5 50.3 1.1 13.0 256.0 J.KNL-2 54-16 0 2.5 285.05 39.0 256.0 J.KNL-2 55.2 0 2.5 480.178 0.179.3 39.0 461.0 J.KNL-2 55.4 2.5 574.04 2.107.3 39.0 461.0 J.KNL-2 55.46 2.5 574.04 2.107.3 39.0 461.0 J.KNL-2 55.48 2.2.5 1501.25 1.245.4 39.0 461.0 J.KNL-2 56.49 2.2.5 1201.55 1.5 52.2 1.607.5 39.2 180.0 J.KNL-2 56.49 2.2.5 121.55 1.5 52.2 100.0 J.KNL-2 J.KNL-2 56.49 2.2.5 230.783.0 0.15277 39.0 99.0 J.KNL-2 J.KNL-2 56.49 2.2.5 230.783.0 </th <th>ENERGY (EV)</th> <th>2</th> <th>J</th> <th>TOTAL WIDTH</th> <th>NEUTRON WIDTH</th> <th>GAMMA WIDTH (MEV I</th> <th>FISSION WIDTH</th> <th>REFERENCE</th> <th></th>	ENERGY (EV)	2	J	TOTAL WIDTH	NEUTRON WIDTH	GAMMA WIDTH (MEV I	FISSION WIDTH	REFERENCE	
54.05 0 2.5 501.3 1.3 39.0 461.0 JEND2 54.78 0 2.5 225.0 95.657-2 39.0 224.0 JEND2 55.2 0 2.5 267.0 1.0 JEND2 JEND2 55.45 0 2.5 37.0 1.0 JEND2 JEND2 55.48 2 2.5 170.125 1.2454 39.0 1.0 JEND2 57.48 2 2.5 170.151 1.5075 39.0 1.011.0 JEND2 38.58 0 2.5 213.55 1.56 39.0 1.061.0 JEND2 61.38 0 2.5 213.5 1.55 39.0 1.061.0 JEND2 62.49 2 2.5 100.0 1.22 39.0 39.0 31.0 JEND2 64.401 2 2.5 200.468 1.469.0 39.0 31.0 JEND2 64.401 2 2.5 200.477 39.0 31.0 JEND2 64.401 2 2.5	53.94	0	2.5	230.198	0.19788	39.0	191.0	JENOL-2	
64.41 0 2.5 285.05 9.550-2 39.0 256.0 JEMO2 55.22 0 2.5 284.1 1.1 13703 39.0 451.0 JEMO2 55.26 0 2.5 89.0 2.13703 39.0 451.0 JEMO2 55.86 2 2.5 1501.25 1.245.4 49.0 1461.0 JEMO2 55.86 2 5.6 3.05 49.0 1461.0 JEMO2 58.16 2 2.5 1301.5 1.55 39.2 160.0 JEMO2 56.38 0 2.5 490.87 1.5 32.2 100.0 JEMO2 66.43 0 2.5 1.5 1.5 32.2 100.0 JEMO2 65.49 2 2.5 1.65.29 0.56217 39.0 199.0 JEMO2 65.49 2 2.5 240.4652 39.2 200.0 JEMO2 65.49 2 2.5 240.4652 39.2 39.0 JEMO2 65.49 2 2.5 <td>54.05</td> <td>0</td> <td>2.5</td> <td>501.3</td> <td>1.3</td> <td>39.0</td> <td>461.D</td> <td>JENDL-2</td> <td></td>	54.05	0	2.5	501.3	1.3	39.0	461.D	JENDL-2	
64.78 C 2.5 264.1 1.1 39.0 224.0 JeR02 55.52 D 2.5 490.137 C.1373 39.0 61.0 JeR02 55.54 D 2.5 65.75 1.25	54.41	С	2.5	295.095	9.550-2	39.0	256.0	JENDL - 2	
55:2 C 2.5 490.137 0.13703 39.0 451.0 L#002 55:94 2 2.5 852.678 1.0572 49.0 39.10 L#002 55:48 2 2.5 852.678 1.0572 49.0 39.10 L#002 56:18 2 2.5 1301.51 1.5075 39.0 1261.0 L#002 56:35 3 2.5 940.67 0.87 39.0 901.0 L#002 60:35 3 2.5 940.67 0.87 39.0 91.0 L#002 61:49 2 2.5 101.45 1.45 39.0 93.0 181.0 L#002 64:403 2 2.5 1000.7 1.72 19.0 1160.0 L#002 65:49 2 2.5 1000.7 1.72 19.0 131.0 L#002 64:43 2 2.5 210.468 0.47853 39.0 131.0 L#002 65:49 2 2.5 1002.3 2.3044 39.0 100.0 L#002	54.78	G	2.5	264-1	1.1	39.0	224.0	JENDL-2	
55-96 2 2.5 B62,678 2,6782 39.0 B71.0 LFM02 57.46 2 2.5 374.02 1.04 39.0 131.0 LFM02 57.46 2.5 127.5 127.5 39.0 1261.0 LFM02 58.18 2 2.5 225.5 0.56 39.0 1261.0 LFM02 58.18 2 2.5 401.45 1.45 39.0 361.0 LFM02 51.88 0 2.5 401.47 1.57 39.0 361.0 LFM02 52.43 0 2.5 401.47 0.57 39.0 361.0 LFM02 54.43 0 2.5 401.46 1.455 39.0 200.0 LFM02 55.49 2 2.5 240.466 1.4562 39.0 200.0 LFM02 56.49 2 2.5 530.496 0.5972 39.0 39.0 139.0 LFM02 57.33 0 2.5 540.4991 0.46914 39.0 290.40 LFM02	55.2	С	2.5	490.137	0.13703	39. 0	451.0	JENOL-2	
56.44 2 2.5 334.04 1.04 42.0 331.0 4.80.2 57.48 2.5 150.125 1.244.4 30.0 1141.0 4.80.2 57.48 2.5 253.54 49.0 776.0 4.80.2 58.52 2.5 255.55 5.56 39.0 90.0 90.0 4.80.2 60.95 0 2.5 900.67 0.27 39.0 90.0 4.80.2 61.38 0 2.5 213.5 1.5 52.2 160.0 4.80.2 64.44 2 2.5 239.6 0.480.2 39.0 991.0 4.80.2 64.69 2 2.5 239.469 0.47653 39.0 731.0 4.80.2 65.66 2 2.5 730.763 0.47653 39.0 731.0 4.80.2 65.49 2 2.5 533.469 0.47651 39.0 731.0 4.80.2 65.30 2.5 331.69 0.46114 39.0 94.0 4.80.2 70.13 2 2.5 534.496	55.95	3	2.5	862.678	2.6782	39.0	821.0	JENDL - 2	
56.88 1 2.5. 1501.75 1.2464 39.0 161.0 LF0.12 35.84 2 2.5. 762.95 1.255 39.0 731.0 LF0.0 LF0.12 35.84 2 2.5. 762.95 1.255 39.0 731.0 LF0.0 LF0.0 35.84 2 2.5. 940.47 0.87 39.0 361.0 LF0.0	56.44	2	2.5	374.04	1.04	42.0	331.0	JENOL-2	
5:4:48 2:5:5 130:55 2:5:5 49:0 75:0 AM0:2 56:182 2:5:5 130:55 1:55	56.88	2	2.5	1501.25	1.2454	39.0	1461.0	JENOL-2	
Basility C C D Lobits Lobits <thlobits< th=""> Lobits Lobits</thlobits<>	57.48	5	2.5	/82 36	2.36	49.0	731.0	JENUL-2	
38-32 J 4.13 4.23 4.23 4.24 4.24 61 38 0 2.5 91.14 4.5 59.2 31.0 4.40 2.40 62 39 0 2.5 100.2 0.72 39.0 391.0 4.4002 64.43 2 2.5 100.12 0.76317 39.0 391.0 4.4002 65.49 2 2.5 230.466 1.4652 39.2 290.0 4.4002 65.49 2 2.5 230.478 0.47853 39.0 991.0 4.4002 65.49 2 2.5 31.463 0.469144 39.0 291.0 4.4002 67.33 2 2.5 340.246 0.24608 39.0 291.0 4.4002 71.75 2 2.5 340.246 0.24608 39.0 291.0 4.4002 73.43 2 2.5 12.5 14.702 39.0 461.0 4.4002	58.18	2	2-5	1301-51	1.5075	39.0	1261.0	JENUL-2	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	50.52	5	2.5	225.56	J.56	39.0	186.0	JENUL-2	
b. 30 c. 40 c. 145 39.0 181.0 480.0 b. 400 c. 25 100.0 1.2 39.0 381.0 480.0 b. 440.0 c. 25 200.0 250.0 39.0 381.0 480.0 b. 64.44 c. 25.5 220.466 1.4662 39.0 39.0 39.0 $480.0.2$ b. 65.49 c. 2.5 230.478 0.47853 39.0 591.0 $460.0.2$ b. 65.69 c. 2.5 230.478 0.47853 39.0 39.0 39.0 $480.0.2$ b. 67.33 c. 2.5 331.469 0.46773 39.0 39.0 49.0 $480.0.2$ 75.73 c. 2.5 331.469 0.46914 39.0 491.0 $480.0.2$ 72.22 c. 2.5 331.469 0.5204 39.0 491.0 $480.0.2$ 72.403 c. 2.5 534.926 0.5204 39.0 $480.0.2$ $480.0.2$	60.95	J	2.5	940.87	0.87	39.0	901-0	JENUL-2	
b 3 a 3 c 2 c 3 c 1 2 s 3 c 0 b 1 0 c 1 4 0 0 64 (03) c 2 (5) 240 (466) 1 (462) 39.0 39.0 199.0 (460, 2) 64 (44) c 2 (5) 240 (466) 1 (462) 39.0 199.0 (460, 2) 65 (49) c 2 (5) 630 (478) 0 (47853) 39.0 291.0 (470, -2) 65 (39) c 2 (5) 700.641 0 (47853) 39.0 291.0 (470, -2) 67 (38) c 2 (5) 940 (386) 0 (38572) 39.0 291.0 (470, -2) 67 (38) c 2 (5) 1002 (3) c (3044) 39.0 2961.0 (470, -2) 71 (19) c 2 (5) 1002 (3) c (3042) 39.0 761.0 (470, -2) 72 (3) c 2 (5) 11 (462) 39.0 761.0 (470, -2) 73 (40) c 2 (5) 591.052 39.0 251.0 (470, -2) 74 (40) c 2 (5) 591.053 39.0 251.0 (470, -2) </td <td>01+30 co co</td> <td>5</td> <td>2.3</td> <td>4U1-43 212 E</td> <td>1.40</td> <td>39.0</td> <td></td> <td>JENUL-2</td> <td></td>	01+30 co co	5	2.3	4U1-43 212 E	1.40	39.0		JENUL-2	
b 4 c3 c 4 c 3 1 20 c 65 1 40 c 65 1 46 c 7 1 45 c 7	63.40	2	2.0	1000.2	1.3	32.0	100-0	JENUL-2	
b c	64 03	2	2.3	220 262	0.36313	39.0	901-0	JENUL*2	
65.69 2 2.6 63.69 36.0 69.0 14.60.5 65.49 2 2.5 53.478 0.47863 39.0 591.0 14.60.5 65.66 2 2.5 533.469 0.447853 39.0 501.0 14.60.5 67.3 2 2.5 333.469 0.46914 39.0 291.0 14.60.5 67.38 2 2.5 534.989 1.9892 46.0 467.0 34.002 70.19 2 2.5 534.989 1.9892 46.0 467.0 34.002 72.42 2 2.5 125.070 1.707 39.0 461.0 34.02 73.43 2 2.5 514.752 4.752 39.0 21.0 34.02 73.43 2 2.5 51.0 1.707 39.0 851.0 34.02 73.43 2 2.5 51.0 33.0.0 851.0 34.02 75.60 2.5 51.755	64.44	-	2.3	240.466	1 4662	39.0	300 0	JENDL-2	
65.49 2 2 5 60.776 39.0 60.73 10.70.641 0.64077 39.0 37.0 12.802 67.38 2 2.5 940.386 0.39572 39.0 901.0 18.002 67.38 2 2.5 1002.3 2.3044 39.0 991.0 18.002 70.19 2 2.5 1002.3 2.3044 39.0 991.0 18.002 71.75 2 2.5 1000.52 0.520.4 39.0 461.0 18.002 72.22 2 2.5 126.707 1.707 39.0 461.0 18.002 73.43 2 2.5 126.707 1.707 39.0 461.0 18.002 75.49 2 2.5 23.255 39.0 251.0 18.002 75.49 2 2.5 23.255 39.0 251.0 18.002 76.77 C 2.5 250.0506 39.0 216.10.0 18.002	65 09	ň	2.5	238 503	1.4002	30 0	100.0	JENUL-2	
66 5 7 2 7 9 7 9 7 12 2 14 10 14 10 14 10 10 14 10 10 14 10	65 49	ň	2.5	2 JO - J JJ 6 J O - 4 7 B	0.03203	30.0	591.0	JEND - 2	
bb 1 C 1 + 0 C + 00 C + 00 <thc +="" 00<="" th=""> <thc +="" 00<="" th=""> C +</thc></thc>	66 56	2	2.5	770 641	0.64033	30.0	33.•0 19:0	JEND 2	
B7:3B C 2.5 333.463 C 46914 39.0 244.0 250.0 70.19 C 2.5 1007.3 2.3044 39.0 961.0 350.0 250.0 71.75 C 2.5 534.989 1.9992 46.0 497.0 350.0 350.0 250.0 250.2 39.0 761.0 350.0 250.0 250.2 255.2 255.2 255.2 350.0 250.0 250.0 250.0 250.0 250.0 39.0 251.0 350.0 370	67.3	2	2.5	940 396	0.39572	30.0	901 0	IENDL - 2	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	67.98	5	2.5	333.469	G.46914	39.0	294.0	JEND: -2	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	69.23	5	2.5	1002.3	2.3044	39.0	961.0	IEND: -2	
1.12 2 2.14 2	70.19	Š	2.5	534.989	1.9892	46.0	487.0	IEND: -2	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	71.75	-	2.5	349.246	0.24608	39.0	310.0	IEND -2	
13 12 12 12 12 12 12 12 12 112 110 1200 14 133 12 25 514 762 39 0 411.0 1200 75 0 225 232.55 32.55 39.0 219.0 1200 1200 75 0 225 232.55 32.55 39.0 251.0 1200 76 12 25 571.981 1.9914 39.0 531.0 1200 1200 79.6 2.55 571.981 1.9914 39.0 557.0 1200 1200 12000 12000 12000 12000 12000 120000 1200000 12000000 $12000000000000000000000000000000000000$	72.22	~	2.5	800.52	0.5204	39.0	761.0	LIEND: -2	
24.03 C 2.5 514.762 47.62 99.0 471.0 $JEN02$ 75.49 C 2.5 299.673 0.57293 99.0 219.0 $JEN02$ 75.49 C 2.5 293.255 3.255 99.0 251.0 $JEN02$ 76.77 C 2.5 $972.551.0$ 0.55066 39.0 833.0 $JEN02$ 79.6 C 2.5 903.375 0.37478 39.0 861.0 $JEN02$ 79.6 C 2.5 596.536 2.53556 39.0 157.0 $JEN02$ 81.47 C 2.5 596.536 2.5356 39.0 1261.0 $JEN02$ 82.76 C 2.5 741.721 1.7214 39.0 76.0 $JEN02$ 82.76 C 2.5 590.349 0.47454 39.0 76.0 $JEN02$ 84.75 Z 2.5 590.349 0.34957 39.0 361.0 $JEN02$ 85.73 <t< td=""><td>73.43</td><td>ĩ</td><td>2.5</td><td>126.707</td><td>1.707</td><td>39.0</td><td>86.0</td><td>IEND -2</td><td></td></t<>	73.43	ĩ	2.5	126.707	1.707	39.0	86.0	IEND -2	
75.0 2 25 26 225 3255 39.0 225.0 320.0 $320.$	74.03	-	2.5	514.762	4.762	39.0	471.0	IEND2	
75.49 2 2.5 233 3.255 33.0 251.0 LEND2 75.77 C 2.5 231.0 L55066 33.0 LEND2 78.16 C 2.5 571.981 1.9814 39.0 631.0 LEND2 79.46 C 2.5 900.375 0.37478 39.0 957.0 LEND2 79.70 C 2.5 596.536 2.5355 39.0 S57.0 JEND2 81.47 C 2.5 596.536 2.5355 39.0 S57.0 JEND2 82.78 C 2.5 741.721 1.7214 39.0 701.0 JEND2 84.75 C 2.5 741.721 1.7214 39.0 701.0 JEND2 84.75 C 2.5 400.791 0.79108 39.0 361.0 JEND2 85.73 C 2.5 500.349 0.34957 39.0 256.0 JEND2 86.76 C 2.5 540.590 0.3697 39.0 301.0 JEND2 87.7<	75.0	ĥ	2.5	258.673	0.57293	39.0	219.0	JENDL-2	
75, 77 C 2.5 $872, 551$ 0.55086 39.0 833.0 14802 $78, 166$ C 2.5 900.375 0.37478 39.0 531.0 $4EN02$ $79, 6$ C 2.5 900.375 0.37478 39.0 161.0 $4EN02$ $79, 78$ C 2.5 1200.66 0.66400 39.0 155.0 $dEN02$ 81.47 C 2.5 1301.6 1.5992 39.0 255.0 $dEN02$ 82.35 C 2.5 131.6 1.5992 39.0 95.7 $dEN02$ 82.35 C 2.5 131.22 2.1276 39.0 96.0 $dEN02$ 82.78 C 2.5 137.128 2.1276 39.0 775.0 $dEN02$ 84.75 C 2.5 305.7 0.34957 39.0 251.0 $dEN02$ 85.73 C 2.5 280.75 $7.615.2$ 39.0 211.0 $dEN02$ 87.73	75.49		2.5	293.255	3.255	39.0	251.0	JEND: -2	
78:18 C 2.5 571.981 1.9814 39.0 531.0 16002 $78:46$ C 2.5 900.375 0.37478 39.0 861.0 16002 79.0 C 2.5 590.375 0.37478 39.0 1161.0 16002 79.78 C 2.5 590.536 2.5556 39.0 1561.0 16002 81.477 C 2.5 741.721 1.7214 39.0 760.0 46002 82.79 C 2.5 815.475 0.47454 39.0 361.0 46002 85.73 C 2.5 590.349 0.34957 39.0 251.0 4602 87.73 C 2.5 590.349 0.34957 39.0 251.0 4602 87.73 C 2.5 590.359 0.3597 39.0 33.0 4802 87.7 O 2.5 $680.393.0$	76.77	č	2.5	872,551	0.55086	39.0	833.0	JENDL-2	
78.46C2.5900.3750.3747839.0861.0 4602 79.6 C2.51200.680.6840839.01161.0JEND2 79.78 C2.5598.5362.535639.0557.0JEND2 81.47 C2.51301.61.599239.01261.0JEND2 82.78 C2.5137.1282.127839.0701.0JEND2 82.78 C2.5137.1282.127839.096.0JEND2 84.75 C2.5815.4750.4745439.0776.0LEND2 85.22 C2.5900.7910.7910839.0361.0JEND2 85.73 C2.5590.3490.3495739.0256.0JEND2 86.78 C2.5295.0757.616-239.0256.0JEND2 87.7 02.560.121.99-239.0111.0JEND2 89.76 02.5546.5890.586939.051.9.0JEND2 91.72 02.5250.2567.256439.051.9.0JEND2 91.72 02.5510.561.589339.065.0JEND2 91.72 02.5510.561.599339.065.0JEND2 91.72 02.5510.561.599339.065.0JEND2 91.72 02.5510.561.599339.065.0	78.18	ċ	2.5	571.981	1.9814	39.0	531.0	JENOL-2	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	78.46	С	2.5	900.375	0.37478	39.0	861.0	JENOL-2	
79.78 C 2.5 598.536 2.5356 39.0 557.0 JEND2 81.47 C 2.5 1301.6 1.5992 39.0 1261.0 JEND2 82.35 C 2.5 741.721 1.7214 39.0 701.0 JEND2 82.78 C 2.5 137.128 2.1278 39.0 761.0 JEND2 84.75 C 2.5 90.1475 0.74108 39.0 761.0 JEND2 85.73 C 2.5 590.349 0.34957 39.0 561.0 JEND2 86.78 C 2.5 295.076 7.616-2 39.0 256.0 JEND2 87.7 O 2.5 80.012 1.199-2 39.0 49.0 JEND2 87.6 O 2.5 580.580 0.5807 39.0 303.0 JEND2 87.7 O 2.5 580.5808 0.5809 39.0 701.0 JEND2 90.55 D 2.5 580.5809 0.38024 39.0 701.0 JEND2 <td>79.0</td> <td>C</td> <td>2.5</td> <td>1200.68</td> <td>0.68408</td> <td>39.0</td> <td>1161-D</td> <td>JENDL-2</td> <td></td>	79.0	C	2.5	1200.68	0.68408	39.0	1161-D	JENDL-2	
B: .47 C 2.5 1301.6 1.5992 39.0 1261.0 JEND2 B2.35 C 2.5 741.721 1.7214 39.0 701.0 JEND2 B2.78 C 2.5 137.128 2.1278 39.0 96.0 96.0 JEND2 B4.75 C 2.5 805.475 0.47454 39.0 361.0 JEND2 B5.73 C 2.5 590.349 0.34957 39.0 251.0 JEND2 B6.78 C 2.5 150.359 0.3567 39.0 111.0 JEND2 B6.79 0 2.5 160.359 0.3567 39.0 131.0 JEND2 B7.7 0 2.5 68.09 0.556 7.256 39.0 49.0 JEND2 93.75 0 2.5 580.588 0.588 39.0 519.0 JEND2 93.77 0 2.5 740.59 0.5893 39.0 62.0 JEND2 93.77 0 2.5 102.654 1.5597 39.0 65.0 <td>79.78</td> <td>С</td> <td>2.5</td> <td>598-536</td> <td>2.5356</td> <td>39.0</td> <td>557.0</td> <td>JENDL-2</td> <td></td>	79.78	С	2.5	598-536	2.5356	39.0	557.0	JENDL-2	
B2:35 C 2:5 741.721 1.7214 39.C 701.0 JENDL-2 B2:76 C 2:5 137.128 2.1276 39.C 96.0 JENDL-2 B4:75 C 2:5 815.475 0.47454 39.C 776.0 JENDL-2 B5:73 C 2:5 500.349 0.34957 39.C 551.0 JENDL-2 B6:78 C 2:5 150.359 0.3567 39.C 11.0 JENDL-2 B7.7 O 2:5 88.012 1.199-2 39.C 49.0 JENDL-2 B3.76 O 2:5 580.359 0.3567 39.C 49.0 JENDL-2 B3.76 O 2:5 580.580 0.5809 39.C 701.0 JENDL-2 91.72 O 2:5 740.59 0.58093 39.C 701.0 JENDL-2 93.75 O 2:5 590.38 0.38024 39.C 551.0 JENDL-2 93.77	8: 47	С	2.5	1301.6	1.5992	39.0	1261.0	JENDL -2	
B2.78 C 2.5 137.128 2.1278 39.C 96.0 $deN01-2$ B4.75 C 2.5 815.475 0.47454 39.C 776.0 $deN01-2$ B5.22 C 2.5 400.791 0.79108 39.C 361.0 $deN01-2$ B5.73 C 2.5 590.349 0.34957 39.C 256.0 $deN01-2$ B6.78 C 2.5 295.075 7.616-2 39.C 256.0 $deN0-2$ B7.7 O 2.5 80.12 $1.199-2$ 39.C 49.0 $deN0-2$ B7.7 O 2.5 586.588 0.588 303.0 $deN0-2$ B9.76 O 2.5 586.588 0.588 39.C 201.0 $deN0-2$ 91.72 O 2.5 740.59 0.58993 39.C 701.0 $deN0-2$ 93.77 O 2.5 102.664 1.6593 39.C 551.0 $deN0-2$ 93.77 O 2.5 102.664 1.6539 39.C 100.0 $deN0-2$	82.35	С	2.5	741.721	1.7214	3 9. C	701.0	JENDL-2	
84.75 2 2.5 815.475 0.47454 39.C 776.0 JENDU-2 85.73 2 2.5 400.791 0.79108 39.C 361.0 JENDU-2 85.73 2 2.5 590.349 0.34957 39.C 551.0 JENDU-2 86.78 2 2.5 150.359 0.3567 39.C 111.0 JENDU-2 87.7 0 2.5 80.012 1.199-2 39.C 49.0 JENDU-2 83.76 0 2.5 586.588 0.5868 39.C 303.0 JENDU-2 90.55 0 2.5 740.59 0.58993 39.C 701.0 JENDU-2 91.72 0 2.5 590.38 0.38024 39.C 701.0 JENDU-2 93.75 0 2.5 105.6 1.5639 39.C 551.0 JENDU-2 93.77 0 2.5 102.654 1.6539 39.C 65.0 JENDU-2 93.77 0 2.5 102.654 1.6539 39.C 100.0 JENDU-2	82.78	С	2.5	137.128	2.1278	39.C	96.0	JÉNDL-2	
85.22 2 2.5 400.791 0.79108 39.0 361.0 JEND2 85.73 2 2.5 590.349 0.34957 39.0 551.0 JEND2 86.78 2 2.5 590.75 7.616-2 39.0 256.0 JEND2 87.7 0 2.5 150.359 0.3587 39.0 303.0 JEND2 88.89 0 2.5 344.139 2.1396 39.0 303.0 JEND2 93.75 0 2.5 558.588 0.586 39.0 303.0 JEND2 93.75 0 2.5 740.59 0.5893 39.0 701.0 JEND2 93.77 0 2.5 590.38 0.38024 39.0 478.0 JEND2 93.77 0 2.5 105.6 1.5937 39.0 470.0 JEND2 93.77 0 2.5 105.6 1.5939 39.0 62.0 JEND2 93.77 0 2.5 105.6 1.5939 39.0 62.0 JEND2	84.75	5	2.5	815.475	0.47454	39.C	776.0	JENOL-2	
85.73 C 2.5 590.349 0.34957 39.0 551.0 JEND2 86.78 C 2.5 295.076 7.616-2 39.0 256.0 JEND2 87.13 C 2.5 150.359 0.3667 39.0 111.0 JEND2 87.7 O 2.5 86.012 1.199-2 39.0 30.0 JEND2 89.76 O 2.5 558.580 0.580 39.0 30.0 JEND2 90.55 D 2.5 540.590 0.58993 39.0 701.0 JEND2 91.72 D 2.5 70.59 0.38024 39.0 551.0 JEND2 92.67 O 2.5 50.38 0.38024 39.0 65.0 JEND2 93.77 D 2.5 105.6 1.5977 39.0 65.0 JEND2 95.22 O 2.5 105.6 1.6539 39.0 150.0 JEND2 96.42 <td< td=""><td>85.22</td><td>2</td><td>2.5</td><td>400-791</td><td>0.79108</td><td>39.0</td><td>361.0</td><td>JENOL -2</td><td></td></td<>	85.22	2	2.5	400-791	0.79108	39.0	361.0	JENOL -2	
66.76 C 2.5 295.076 7.616-2 39.0 256.0 JENOL-2 87.13 C 2.5 150.359 0.3567 39.0 111.0 JENOL-2 87.7 O 2.5 68.012 1.199-2 39.0 303.0 JENOL-2 88.76 O 2.5 558.588 0.589 39.0 214.0 JENOL-2 91.72 O 2.5 560.256 7.2564 39.0 214.0 JENOL-2 91.72 O 2.5 740.59 0.58993 39.0 701.0 JENOL-2 92.67 O 2.5 580.38 0.38024 39.0 551.0 JENOL-2 93.25 O 2.5 102.654 1.6539 39.0 65.0 JENOL-2 93.77 O 2.5 102.654 1.6539 39.0 1561.0 JENOL-2 96.42 O 2.5 102.654 1.6539 39.0 1561.0 JENOL-2 97.81 C 2.5 102.654 1.6539 39.0 1501.0 JENOL-2 <td>85.73</td> <td>2</td> <td>2.5</td> <td>590.349</td> <td>0.34957</td> <td>39.0</td> <td>551.0</td> <td>JENDL-2</td> <td></td>	85.73	2	2.5	590.349	0.34957	39.0	551.0	JENDL-2	
67:3C2.5150.3590.356739.C11.1.0JENOL 2 87.7 02.588.012 $1.199-2$ 39.C49.0JENOL -2 86.89 02.5344.1392.139639.C303.0JENOL -2 89.76 02.5558.5880.58839.C214.0JENOL -2 91.72 02.5740.590.5899339.C701.0JENOL -2 91.72 02.5518.2981.297739.C551.0JENOL -2 93.25 02.5590.380.3802439.C551.0JENOL -2 93.77 02.5105.61.599739.C551.0JENOL -2 95.22 02.5102.6541.653939.C1561.0JENOL -2 95.42 02.5102.6541.653939.C1561.0JENOL -2 97.81 C2.5102.6541.653939.C190.0JENOL -2 99.3 02.5542.6262.625639.C190.0JENOL -2 99.3 02.5542.6262.625639.C190.0JENOL -2 99.45 02.5542.6262.625639.C501.0JENOL -2 102.99 02.5100.240.2408239.C501.0JENOL -2 102.99 02.5100.240.2408239.C501.0JENOL -2 102.99 02.5100.240.2408239.C	86.78	2	2.5	295.075	7.616-2	39.0	256.0	JENOL - 2	
87.702.5 60.012 $1.199-2$ 39.0 49.0 $JENOL-2$ 80.89 02.5 344.139 2.1396 39.0 303.0 $JENOL-2$ 90.76 02.5 556.586 0.568 39.0 519.0 $JENOL-2$ 91.72 02.5 740.59 0.58993 39.0 214.0 $JENOL-2$ 92.67 02.5 740.59 0.58993 39.0 701.0 $JENOL-2$ 93.25 02.5 510.299 1.2977 39.0 478.0 $JENOL-2$ 93.77 02.5 105.6 1.5997 39.0 65.0 $JENOL-2$ 95.22 02.5 100.654 1.6539 39.0 65.0 $JENOL-2$ 95.642 02.5 1603.31 3.3119 39.0 1561.0 $JENOL-2$ 97.61 C2.5 233.759 4.7586 39.0 200.0 $JENOL-2$ 99.3 0 2.5 541.366 1.3858 39.0 501.0 $JENOL-2$ 99.3 0 2.5 542.626 2.6256 39.0 501.0 $JENOL-2$ 101.29 0 2.5 100.24 0.24082 39.0 501.0 $JENOL-2$ 102.80 0 2.5 246.517 1.5167 39.0 501.0 $JENOL-2$ 102.80 0 2.5 $401.40.6$ 1.5581 39.0 361.0 $JENOL-2$ 102.80 0 2.5 273.034	87.13	C	2.5	150.359	0.3587	39.0	1:1.0	JENOL 2	
88.89 0 2.5 344.139 2.1396 39.0 303.0 JKNU-2 89.76 0 2.5 558.588 0.596 39.0 519.0 JKNU-2 90.55 0 2.5 260.256 7.2564 39.0 2:4.0 JKNU-2 91.72 0 2.5 740.59 0.58993 39.0 478.0 JENU-2 93.75 0 2.5 580.38 0.38024 39.0 65.0 JENU-2 93.77 0 2.5 105.6 1.5997 39.0 65.0 JENU-2 95.22 0 2.5 105.64 1.6539 39.0 62.0 JENU-2 95.42 0 2.5 163.31 3.3119 39.0 1561.0 JENU-2 97.61 C 2.5 316.971 1.9708 39.0 276.0 JENU-2 99.55 0 2.5 541.386 1.3858 39.0 501.0 JENU-2 101.29 0 2.5 542.626 2.6256 39.0 501.0 JENU-2 <	87.7	0	2.5	88.012	:.199-2	39 · C	49.0	JENOL-2	
88.76 0 2.5 558.588 0.588 39.0 519.0 JEND2 90.55 0 2.5 260.256 7.2564 39.0 214.0 JEND2 91.72 0 2.5 518.298 1.2977 39.0 478.0 JEND2 92.67 0 2.5 518.298 1.2977 39.0 455.0 JEND2 93.77 0 2.5 590.38 0.38024 39.0 65.0 JEND2 95.22 0 2.5 105.6 1.5997 39.0 65.0 JEND2 95.42 0 2.5 102.654 1.6539 39.0 1561.0 JEND2 96.42 0 2.5 316.971 1.9708 39.0 1561.0 JEND2 97.81 C 2.5 541.366 1.3658 39.0 501.0 JEND2 99.3 0 2.5 542.626 2.6256 39.0 501.0 JEND2 101.29 0 2.5 543.368 39.0 361.0 JEND2 101.2	88.89	0	2.5	344.139	2.1396	39-C	303.0	JENOL-2	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	89.76	0	2.5	558.588	0.588	39.0	519.0	JENDL-2	
91.72 0 2.5 740.59 0.56993 39.C 701.0 JEND2 92.67 0 2.5 518.298 1.2977 39.0 478.0 JEND2 93.25 0 2.5 590.38 0.38024 39.0 65.0 JEND2 93.77 0 2.5 105.6 1.5997 39.0 62.0 JEND2 95.42 0 2.5 102.654 1.6539 39.0 62.0 JEND2 97.81 C 2.5 163.31 3.3119 39.0 1561.0 JEND2 99.85 0 2.5 542.626 2.6256 39.0 501.0 JEND2 99.3 0 2.5 542.626 2.6256 39.0 501.0 JEND2 99.95 0 2.5 542.626 2.6256 39.0 501.0 JEND2 102.89 0 2.5 100.24 0.24082 39.0 961.0 JEND2 102.99 0 2.5 102.6517 1.5167 39.0 185.0 JEND2	90.55	D	2.5	260.256	7.2564	39.C	2:4.0	JENOL-2	
92.67 0 2.5 518.298 1.297 39.0 478.0 JEND2 93.25 0 2.5 590.38 0.38024 39.C 551.0 JEND2 93.77 0 2.5 105.6 1.5997 39.0 65.0 JEND2 95.22 0 2.5 102.654 1.6539 39.0 62.0 JEND2 96.42 0 2.5 1603.31 3.3119 39.0 1561.0 JEND2 97.81 C 2.5 316.971 1.9708 39.0 501.0 JEND2 99.58 0 2.5 541.366 1.3658 39.0 501.0 JEND2 99.3 0 2.5 541.366 1.3658 39.0 501.0 JEND2 101.29 0 2.5 542.626 2.6256 39.0 501.0 JEND2 102.289 0 2.5 46140.6 1.5581 39.0 46100.0 JEND2 102.290 0 2.5 46140.6 1.5581 39.0 391.0 JEND2 <td>91.72</td> <td>D</td> <td>2.5</td> <td>740.59</td> <td>0.58993</td> <td>39.C</td> <td>701.0</td> <td>JENDL-2</td> <td></td>	91.72	D	2.5	740.59	0.58993	39.C	701.0	JENDL-2	
33.25 0 2.5 540.36 0.38024 49.C 551.0 JEND2 93.77 0 2.5 105.6 1.5997 39.0 65.0 JEND2 95.22 0 2.5 102.654 1.6539 39.0 62.0 JEND2 96.42 0 2.5 1603.31 3.3119 39.0 1561.0 JEND2 97.81 C 2.5 233.759 4.7586 39.0 276.0 JEND2 98.56 0 2.5 541.366 1.9708 39.0 501.0 JEND2 99.3 0 2.5 541.366 1.9858 39.0 501.0 JEND2 99.3 0 2.5 542.626 2.6256 39.0 501.0 JEND2 101.29 0 2.5 1000.24 0.24082 39.0 961.0 JEND2 102.89 0 2.5 265.517 1.5167 39.0 391.0 JEND2 105.23 0 2.5 430.086 6.813-2 39.0 391.0 JEND2	92.67	0	2.5	518-298	1.29/7	39-0	478.0	JENUL-2	
95.77 0 2.5 105.6 1.5997 39.0 65.0 J.ML-2 95.22 0 2.5 102.654 1.6539 39.0 62.0 JEND-2 96.42 0 2.5 102.654 1.6539 39.0 62.0 JEND-2 97.81 C 2.5 233.759 4.7586 39.0 276.0 JEND-2 99.3 0 2.5 541.366 1.3858 39.0 501.0 JEND-2 99.95 0 2.5 542.626 2.6256 39.0 501.0 JEND-2 101.29 0 2.5 542.626 2.6256 39.0 501.0 JEND-2 102.69 0 2.5 246.77 1.5167 39.0 186.0 JEND-2 104.79 0 2.5 46140.6 1.5581 39.0 391.0 JEND-2 105.23 0 2.5 192.437 2.4368 39.0 151.0 JEND-2 105.51 0 2.5 327.869 2.46694 39.0 281.0 JEND-2	93.25	U	2.5	590.38	U-38U24	J. 60	551.U	JENUL-2	
95.22 0 2.5 102.054 1.0539 39.0 1561.0 JENU2 96.42 0 2.5 1603.31 3.3119 39.0 1561.0 JENU2 97.81 C 2.5 316.971 1.9708 39.0 1561.0 JENU2 99.3 0 2.5 316.971 1.9708 39.0 501.0 JENU2 99.3 0 2.5 541.386 1.3858 39.0 501.0 JENU2 99.3 0 2.5 542.626 2.6256 39.0 501.0 JENU2 101.29 0 2.5 100.24 0.24082 39.0 166.0 JENU2 102.89 0 2.5 46140.6 1.5581 39.0 166.0 JENU2 104.79 0 2.5 46140.6 1.5581 39.0 391.0 JENU2 105.23 0 2.5 430.086 6.613-2 39.0 391.0 JENU2 105.95 </td <td>93.77</td> <td>U</td> <td>2.5</td> <td>103.654</td> <td>1.233/</td> <td>0.05</td> <td>62.0</td> <td>JENUL-2</td> <td></td>	93.77	U	2.5	103.654	1.233/	0.05	62.0	JENUL-2	
Bit C <thc< th=""> C <thc< th=""> <thc< th=""></thc<></thc<></thc<>	93.22	U	2.5	102.004	1.0277	0.0C	52-U	JENUL-Z	
9*.61 C 2.5 233.759 4.7586 39.C 193.0 D.U2 98.58 0 2.5 316.971 1.9708 39.C 276.0 JENU2 99.3 0 2.5 541.386 1.3858 39.C 501.0 JENU2 99.3 0 2.5 542.626 2.6256 39.0 501.0 JENU2 101.29 0 2.5 542.626 2.6256 39.0 961.0 JENU2 102.89 0 2.5 100.024 0.24082 39.0 186.0 JENU2 104.79 0 2.5 46140.6 1.5581 39.0 186.0 JENU2 105.73 0 2.5 430.088 8.813-2 39.0 391.0 JENU2 105.95 0 2.5 132.4368 39.0 151.0 JENU2 106.51 0 2.5 327.3669 2.6694 39.0 286.0 JENU2 106.55 0 <td>90.42</td> <td>U</td> <td>2.5</td> <td>1003-31</td> <td>3.3119</td> <td>30.0</td> <td>1001-0</td> <td>JENUL-Z</td> <td></td>	90.42	U	2.5	1003-31	3.3119	30.0	1001-0	JENUL-Z	
30.30 0 2.5 310.31 1.300 39.3 24.5 246.0 JENU-2 99.35 0 2.5 541.366 1.3958 39.0 501.0 JENU-2 99.95 0 2.5 542.626 2.6256 39.0 501.0 JENU-2 101.29 0 2.5 1000.24 0.24082 39.0 961.0 JENU-2 102.89 0 2.5 265.517 1.5167 39.0 186.0 JENU-2 104.79 0 2.5 46140.6 1.5581 39.0 46100.0 JENU-2 105.73 0 2.5 430.088 8.813-2 39.0 391.0 JENU-2 105.73 0 2.5 192.437 2.4368 39.0 151.0 JENU-2 106.51 0 2.5 327.369 2.46694 39.0 286.0 JENU-2 106.55 0 2.5 327.869 2.6694 39.0 311.0 JENU-2	00 C0 34+01	L C	2.5	233-739	4,/300	30 C	190-0	JENUL-Z	
39.3 0 2.5 54.300 1.300 39.4 301.0 U	30.30	U C	2.5	JID-9/1	1.9/00	30.0	2/0.0	JENUL-2	
53-53 0 2-5 3-2-020 2-0250 39-0 301-0 JUL-2 101-29 0 2-5 1000-24 0-24082 39-0 961-0 JEND2 102-89 0 2-5 1000-24 0-24082 39-0 186-0 JEND2 104-79 0 2-5 46140-6 1-5581 39-0 391-0 JEND2 105-23 0 2-5 46140-6 1-5581 39-0 391-0 JEND2 105-95 0 2-5 430-088 8-813-2 39-0 391-0 JEND2 105-95 0 2-5 132-437 2-4368 39-0 151-3 JEND2 106-51 0 2-5 273-034 3-0341 39-0 286-0 JEND-2 106-55 0 2-5 327-869 2-8694 39-0 286-0 JEND-2 107-83 0 2-5 400-822 0-82178 39-0 361-0 JEND-2 108-6	00 05 9313	U	2.5	J41-J00 542 626	1.3030	30.0	501.0	JENUL-Z	
101.25 0 2.5 100.24 0.2002 39.0 301.0 10.00.22 102.89 0 2.5 226.517 1.5167 39.0 186.0 j.END2 104.79 0 2.5 46140.6 1.5581 39.0 186.0 j.END2 105.73 0 2.5 430.088 6.813-2 39.0 391.0 j.END2 105.95 0 2.5 192.437 2.4368 39.0 151.0 j.END2 106.51 0 2.5 327.3669 2.6694 39.0 281.0 j.END2 106.55 0 2.5 351.479 1.4788 39.0 311.0 j.END2 107.83 0 2.5 400.822 0.82178 39.0 361.0 j.END2 108.64 0 2.5 400.822 0.40228 39.0 181.0 j.END2 109.96 0 2.5 400.422 0.40228 39.0 181.0 j.END2	33.33	U	2.5	J#2.020	2.0230	30.0	061.0		
104.79 0 2.5 46140.6 1.5581 39.0 46100.0 JENU-2 105.23 0 2.5 46140.6 1.5581 39.0 46100.0 JENU-2 105.23 0 2.5 430.088 8.813-2 39.0 391.0 JENU-2 105.55 0 2.5 132.437 2.4368 39.0 231.0 JENU-2 106.51 0 2.5 327.869 2.8694 39.0 286.0 JENU-2 106.95 0 2.5 327.869 2.8694 39.0 311.0 JENU-2 107.83 0 2.5 351.479 1.4788 39.0 311.0 JENU-2 108.2 0 2.5 400.822 0.62178 39.0 361.0 JENU-2 108.4 0 2.5 20.402 0.40228 39.0 181.0 JENU-2 108.64 0 2.5 520.815 0.81499 39.0 461.0 JENU-2 109.98 </td <td>101.29</td> <td>U</td> <td>2.5</td> <td>226 517</td> <td>1 5167</td> <td>30.0</td> <td>196 0</td> <td>I JENUE-Z</td> <td></td>	101.29	U	2.5	226 517	1 5167	30.0	196 0	I JENUE-Z	
105.23 2 5 101.00 1.050 39.0 391.0 JEN02 105.23 2 2.5 430.086 8.613-2 39.0 391.0 JEN02 105.95 2 2.5 192.437 2.4368 39.0 151.3 JEN02 106.51 2 2.5 273.034 3.0341 39.0 286.0 JEN02 106.95 0 2.5 327.869 2.8694 39.0 286.0 JEN02 107.83 0 2.5 351.479 1.4788 39.0 361.0 JEN02 108.64 0 2.5 220.402 0.40228 39.0 361.0 JEN02 108.64 0 2.5 220.402 0.40228 39.0 361.0 JEN02 109.96 0 2.5 520.815 0.81499 39.0 361.0 JEN02 109.98 0 2.5 520.815 0.81499 39.0 461.0 JEN02 11	104 79	J 0	2.3	220+31/ 46140 F	1.510/	0.0E	46100 0	JENDL-2	
105.95 0 2.5 132.4368 39.0 151.0 JENDL-2 106.51 0 2.5 273.034 3.0341 39.0 151.0 JENDL-2 106.51 0 2.5 327.869 2.8694 39.0 231.0 JENDL-2 107.83 0 2.5 351.479 1.4788 39.0 311.0 JENDL-2 108.2 0 2.5 351.479 1.4788 39.0 361.0 JENDL-2 108.4 0 2.5 220.402 0.40228 39.0 361.0 JENDL-2 108.64 0 2.5 220.402 0.40228 39.0 361.0 JENDL-2 109.96 0 2.5 520.815 0.81499 39.0 361.0 JENDL-2 109.98 0 2.5 520.815 0.81499 39.0 365.0 JENDL-2 110.88 0 2.5 409.234 5.2344 39.0 365.0 JENDL-2	105.23	2	2.5	430.088	8.813-2	19-0 19-0	391.0	IEN01 -2	
106.51 0 2.5 273.034 3.0341 39.0 231.0 LENDL-2 106.51 0 2.5 327.669 2.6694 39.0 286.0 JENDL-2 106.52 0 2.5 327.669 2.6694 39.0 311.0 JENDL-2 107.83 0 2.5 351.479 1.4768 39.0 311.0 JENDL-2 108.2 0 2.5 400.822 0.82178 39.0 361.0 JENDL-2 108.64 0 2.5 220.402 0.40228 39.0 181.0 JENDL-2 109.96 0 2.5 520.815 0.81499 39.0 461.0 JENDL-2 109.98 0 2.5 520.815 0.81499 39.0 461.0 JENDL-2 110.68 0 2.5 409.234 5.2344 39.0 365.0 JENDL-2	105.95	ĩ	2.5	192.437	2.4368	39.0	151.0	JENDL-2	
106.85 0 2.5 327.869 2.8694 39.0 286.0 JENU-2 107.83 0 2.5 351.479 1.4788 39.0 311.0 JENU-2 108.82 0 2.5 361.479 1.4788 39.0 361.0 JENU-2 108.2 0 2.5 400.822 0.82178 39.0 361.0 JENU-2 108.4 0 2.5 220.402 0.40228 39.0 181.0 JENU-2 109.36 0 2.5 419.045 4.0449 39.0 376.0 JENU-2 109.98 0 2.5 520.815 0.81499 39.0 481.0 JENU-2 109.98 0 2.5 409.234 5.2344 39.0 365.0 JENU-2	106.51	2	2.5	273.034	3.0341	39.0	231.0	JENOL-2	
107.83 0 2.5 351.479 1.4788 39.0 311.0 JENDL-2 108.2 0 2.5 400.822 0.82178 39.0 361.0 JENDL-2 108.4 0 2.5 220.402 0.40228 39.0 161.0 JENDL-2 109.64 0 2.5 419.045 4.0449 39.0 376.0 JENDL-2 109.98 0 2.5 520.815 0.81499 39.0 461.0 JENDL-2 110.88 0 2.5 409.234 5.2344 39.0 365.0 JENDL-2	106.95	ő	2.5	327.869	2.8694	39.0	286.0	JENDL-2	
108.2 0 2.5 400.822 0.82178 39.0 361.0 JENDL-2 108.64 0 2.5 220.402 0.40228 39.0 181.0 JENDL-2 109.64 0 2.5 220.402 0.40228 39.0 181.0 JENDL-2 109.98 0 2.5 520.815 0.81499 39.0 461.0 JENDL-2 110.88 0 2.5 520.815 0.81499 39.0 365.0 JENDL-2	107.83	ő	2.5	351.479	1.4788	39.0	311.0	JENOL-2	
108.64 0 2.5 220.402 0.40228 39.0 181.0 JEN0L-2 109.36 0 2.5 419.045 4.0449 39.0 376.D JEN0L-2 109.98 0 2.5 520.815 0.81499 39.0 481.0 JEN0L-2 110.88 0 2.5 409.234 5.2344 39.0 365.0 JEN0L-2	108.2	ñ	2.5	400.822	0.82178	39.0	361.0	JENDL-2	
109.36 0 2.5 419.045 4.0449 39.0 376.0 JENOL-2 109.96 0 2.5 520.815 0.81499 39.0 481.0 JENOL-2 110.88 0 2.5 409.234 5.2344 39.0 365.0 JENOL-2	108.64	ñ	2.5	220.402	0.40228	39.0	181.0	JENOL -2	
109.98 0 2.5 520.815 0.81499 39.0 481.0 JENDL-2 110.88 0 2.5 409.234 5.2344 39.0 365.0 JENDL-2	109.36	ñ	2.5	419.045	4.0449	39.0	376.0	JENOL-2	
10.88 0 2.5 409.234 5.2344 39.0 365.0 JEND-2	:09.98	õ	2.5	520.815	0.81499	39.0	481.0	JENOL-2	
	110.88	õ	2.5	409.234	5.2344	39.0	365.0	JENOL - 2	
112.53 0 2.5 1203.37 3.3662 39.0 1161.0 JENDL-2	112.53	ō	2.5	1203.37	3.3662	39.0	1161.0	JENDL-2	
113-55 0 2-5 1003-78 3-7796 39-0 961-0 JENGL-2	113.55	0	2.5	1003.78	3.7796	39.0	961.0	JENOL-2	

ENERGY (EV)	Ĺ	J	TOTAL WIDTH (MEV)	NEUTRON WIDTH	Crima W107H (Mey)	FISSION WIDTH (MEV)	REFERENCE
-1.49	0	3.5	245-881	3,68	35.2015	207.0	JENDL-2
0.273	0	3.5	135.003	0.0032	36.0	99.0	JENOL-2
1.14	0	3.5	162.015	0.0154	41.0	121.0	JENOL-2
2.035	0	3.5	48.0081	0.0081	37.0	11.0	JENDL-2
2.84	C	3.5	191.005	0.0048	40.0	151.0	JENDL -2
3.14	C	3.5	131-021	0.021	36.0	95.0	JENUL-2
3.01	U C	3.5	30.462	0.047	30.0	34.0	
4.03	C C	3.5	90.0029	0.002	50.0	30.0	JENDL-2
5.6	C C	3.5	620.033	0.033	20.0	600.0	JENDL -2
6.21	č	3.5	269.056	0.056	42.0	227.0	JENDL-2
6 - 39	С	3.5	49.27	0.27	38.0	11.J	JENDL-2
7.08	С	3.5	51.125	0.125	35.0	26.0	JENDL-2
8.79	С	3.5	131.15	1.15	33.0	97.0	JENOL-2
9.29	C	3.5	137-182	0.182	42.0	95.0	JENOL-2
9.73	L O	3.5	245.045	0.063	45.0	200.0	JENUL-2
10.8	с с	3.5	927.093	0.093	41.0 67.0	860.0	IENDL-2
11.65	ŏ	3.5	48.103	0,603	42.0	5.5	JENDL-2
12.4	0	3.5	69.28	1.28	43.0	25.0	JENDL-2
12.86	0	3.5	79.0448	0.0448	31.0	48.0	JENDL-2
13.28	Ű	3.5	98.047	0.047	36.0	62.0	JENDL-2
13.69	0	3.5	115.046	0.046	34.0	81.0	JENDL-2
14-0	5	1.5	459-48	0.48	36-U	433-0	JENUL-2
14.01	5	3.5 7 E	03+130 85.245	0.135	9J-U 43 C	23.U 42 D	
16-CB	J J	3.5 3.5	51.36	0.36	-5.0	16.0	UENDL-2
15.69	Š	3.5	124.283	0.283	34.C	90.0	JENDL -2
19.07	ō	3.5	169.37	0.37	40.C	129.0	JENOL-2
18.96	2	3.5	91.095	0.095	48.0	43.0	JENOL-2
19.31	С	3.5	104.14	3.14	42.0	59.0	JENOL - 2
20.13	D	3.5	260.12	0.12	31.C	229.0	JENOL-2
20.00	J	3.5	92.2	0.2	44.0	48.0	JENUL-2
21.00	-	3.5	0/-49 84 47	0.47	42.0	24.0	JENUL-2
23.42	ă	3.5	37.66	0.66	30.0	7.0	JENOL -2
23.63	ō	3.5	185.77	0.77	45.C	140.0	JENDL-2
24.25	0	3.5	70.322	0.322	37.0	33.0	JENOL-2
24.37	Э	3.5	88 - 1 399	0.14	35.0	53.0	JENOL-2
25.2	2	3.5	770.5	0.5	40.0	730.0	JENOL -2
25.59	5	3.5	414,66	0.66	24.0	390.0	JENOL-2
20.40	ž	3.5	192.48	0.12	32.0	160.0	JENUL-Z
27.82	õ	3.5	129.68	0.68	44.0	A5.0	JENOL-2
28.38	c	3.5	146.17	0.17	35.0	111.0	JENOL-2
28.71	Ĉ	3.5	202.055	0.055	50.0	152.0	JENOL-2
29.64	C	3.5	68.18	0.18	40.C	28.0	JENOL-2
30.59	C	3.5	149.21	0.21	50.0	99.0	JENOL - 2
30.86	5	3.5	60.5	0.5	39.C	21.0	JENOL-2
32.07	5	3.5	50.02	2.04	46.U 26.C	55.U	JENUL-2
34.39	ž	3.5	83.2199	2.22	30.C	37.0	JENUL-2
34.83	ā	3.5	118.95	0.95	40.0	78.0	JENOL -2
35.2	2	3.5	134.6	3.6	43.0	88.D	JENOL - 2
35.3	Э	3.5	691.57	1.57	40.0	650.0	JENOL-2
36.4	5	3.5	1540.12	0.12	40.0	1500.0	JENOL-2
37.5	5	3.5	1540-17	0.17	40.0	1500.0	JENOL-2
38.3	2	1.5	308.34	0.34	42.0	266.0	JENOL~2
39.9	ň	3.5	34.4333	2.5 0.29	30.U 28.0	54.U 84.0	JENUL-2
40.54	č	3.5	222.43	0.43	36.0	186.0	JENOL -2
4:.35	ŝ	3.5	347.38	0.38	37.0	310.0	JENOL-2
41.59	2	3.5	165.224	0.224	31.0	134.0	JENOL-2
41.88	С	3.5	72.4	1.4	47.0	24.0	JENDL-2
42.23	S	3.5	139-3	0.3	53.0	86.0	JENOL-2
42.1	2	3.5	62.1 68.7	0.3	47.0	15.0	JENOL-2
43.99	2	3.5	103.17	U./ D.17	44.U 29.0	2¶.U 75.0	UENOL-2
43.97	ň	3.5	250.34	0.34	20.J 20.D	230.0	IENDI -2
44.6	ŏ	3.5	186.93	0.93	40.0	145.0	JENOL-2
45.0	0	3.5	535.76	0.76	31.0	504.0	JENOL-2
45.79	Э	3.5	105.188	0.188	26 . D	79.0	JENOL-2
46.79	5	3.5	152.65	0.65	34.0	118.0	JENOL - 2
47.01	3	3.5	140.96	0.96	39.0	101.0	JENOL-2
4/.95	3	3.5	165 771	0.88	41.0	37.0	JENOL-2
48.8	2	כ.נ קוב	79.87	0.77	23.U 29.D	50.0	JENUL-2
49.0	5	1.5	240.177	0.177	20.0	220.0	JENDL-2
49.43	õ	3.5	60-82	0.82	40.0	20.0	JENDL-2
50.14	Э	3.5	53.27	0.27	32.0	21.0	JENDL-2
50.49	Э	3.5	96.09	1.09	43.0	52.0	JENDL~2
51.27	0	3.5	190.67	3.67	51.0	136.0	JENDL-2
51.72	õ	3.5	62.29	0.29	36.0	26.0	JENOL-2
53 46	U n	1.5 7 E	353-25 100-61	2.20	20.U 22.0	323-0	JENUL-2
54.13	0	3.5	142.23	0.23	36.0	106.0	JENUL - 2
55.08	õ	3.5	107-16	3.16	48.0	56.0	JENOL-2
L							

ENERGY (EV)	L	J	TOTAL HIDTH (MEV.)	NEUTRON WIDTH (MEV I	GAMMA WIDTH (MEV)	FISSION WIDTH (MEV)	REFERENCE
55.84	0	3.5	335.5	2.5	45.0	288.0	JENOL-2
56.5	0	3.5	125.92	4.92	43.0	78.0	JENOL-2
57.8	0	3.5	221.13	1.13	35.0	185.0	JENOL-2
58.06	0	3.5	69.36	1.36	32.0	36.0	JENDL-2
58.7	0	3.5	127.25	1.25	30.0	96.0	JENDL-2
59.76	0	3.5	267.245	D.245	41-0	226.0	JENDL-2
60.19	0	3.5	129.9	0.9	18-0	111.0	JENOL-2
60.85	0	3.5	148-51	0.51	25.0	123.0	JENDL-2
61.18	0	3.5	100.35	0,35	30.0	70.0	JENDL-2
61.57	<u>o</u>	3.5	540.23	0.23	40.0	500.0	JENDL-2
61.9	0	3.5	540-17	0.17	40.0	500.0	JENUL-2
62.4	0	3.5	460.26	0.26	60.0	400.0	JENDL-2
63.02	0	3.5	240.091	0.091	40.0	200.0	JENOL-2
63.32	0	3.5	250-102	0.102	50.0	200.0	JENOL-2
63.69	0	3.5	592-8	0.8	16.0	576.0	JENUL-2
64.31	D	3.5	54.25	1.25	45.0	8.0	JENUL-2
65.82	U	3.5	83+42	0.42	40-0	4J.U	JENUL-2
65.38	0	3.5	01.4699	0.47	19-U	42.0	
67.25	U	3.5	A1.080A	0.10	40.U	49.0	
68.53	U	3.5	150-12	0.72	60.0	90.0	
69.29	U	3.5	200+72	0+72	4U.U 50.0	130.0	
/0.4	U	3.5	182.8	2.8	50.0	130.0	JENUL-2
/0./5	U	3.5	229.3	2.3	35-0	191-0	JENUL-2
71.61	U	3.5	110.25	0.25	15.0	95.0	JENUL-2
12.4	U	3.5	141.7	2.7	31.0	108.0	JENUL-2
72.91	U	3.5	5/1.33	0.33	40.0	531-0	JENUL-2
74.57	U	3.5	103.9	2.9	40.0	33.0	
75.17	U	3.5	258.9	1.27	45.0	213.0	JENUL-2
73.54	0	3.5	237-27	1.27	20.0	200.0	
77 53	0	3.5	147.01	1 01	30.0	107.0	JENDL-2
77.33	0	3.5	147-01	1.01	45 0	107.0	
70.11	0	3.5	96 13	0.13	48.0	39.0	
76 69	0	3.5	137 79	0.15	46.0	91.0	IENDI - 2
90.37	0	3.5	203 8	0.70	35.0	169.0	JENDL -2
81.46	0	3.5	128 93	0.0	36.0	00.0 02.0	
92.06	0	3.5	64 05	0.05	40.0	24.0	IENDL-2
82.76	0	3.5	82.9	1.9	56-0	25.0	IENOL -2
83.59	n	9.5	111.17	1.17	55.0	55.0	FNDL-2
84.05	C	3.5	285.65	1.65	36.0	248.0	FNDI -2
84.37	ñ	3.5	234.1	2.1	29.0	203.0	JENDL -2
85.04	n	9.5	403.66	1.66	35.0	367.0	JENDI -2
85.57	ñ	3.5	390.6	0.6	40.0	350.0	JENDL-2
86.14	ñ	3.5	118.05	0.05	40.0	78.0	JENDL-2
86.88	õ	3.5	127.58	0.58	41.0	86.0	JENOL-2
87.54	ō	3.5	208.47	0.47	43.0	165.0	JENDL-2
88.75	õ	3.5	340.28	2.28	18.0	320.0	JENOL-2
89.11	Ō	3.5	135.18	0.18	50.0	85.0	JENOL-2
89.85	õ	3.5	134.79	0.79	45.0	89.0	JENDL-2
90.44	Ō	3.5	60.23	4.83	46.0	9.4	JENUL-2
91.28	õ	3.5	286.96	2.96	33.0	251.0	JENDL-2
92.06	ō	3.5	119.72	0.72	44.0	75.0	JENDL-2
92.6	ċ	3.5	94.53	2.53	48.0	44.0	JENDL-2
93.23	Ō	3.5	83.33	0.33	26.0	57.0	JENDL-2
94.12	ō	3.5	75.4999	4.0	62.0	9.5	JENDL-2
94.76	õ	3.5	107.5	0.5	41.0	66.0	JENDL-2
95.58	0	3.5	481.96	0.96	34.0	447.0	JENDL-2
96.5	0	3.5	255.59	0.59	18.0	237.0	JENDL-2
98.13	0	3.5	219-5	2.5	34.0	183-0	JENDL-2
99.6	0	3.5	145-53	0.53	35.0	110.0	JENDL-2
100.4	0	3.5	1 33.6 6	0.66	60.0	73.0	JENDL-2
							1

U-238

ENERGY (EV)	Ĺ	J	TOTAL WIDTH	NEUTRON WIDTH	CAMMA WIDTH CMEV D	FISSION WIDTH IMEV 1	REFERENCE
-113.0	0	0.5	51.5	28.0	23.5		JENDL-2
-89.0	0	0.5	48.5	25.0	23.5		JENOL-2
-65-0	0	0.5	44.5	21.0	23.5		JENOL-2
-41.0	0	0.5	35-35	11.85	23.5		JENDL-2
4.404	1	0.5	25.2	1.5	23.7	5.2 F	JENDL-2
0.235	1	0.5	23.6016	0.00159	23.6	J.C 2	JENDL -2
1.307		0.5	23.6004	3.69 -4	23.6		JENOL-2
:5.28	1	0.5	23.6001	5.04 -5	23.6		JENOL - 2
:9.524	1	0.5	23.80:4	0.00136	23.8		JENOL-2
20.864	0	0.5	33-1	10.1	23.0	4.8 5	JENOL-2
35-671	0	U.5	56-8	2010	22.5	1.2 =	JENUL-Z
40.170	1	0.5	24.9009	9.22 -4	2740		JENO 2
53.504	1	0.5	23,9098	0.00978	23.9		JENO: -2
56.015	ċ	0.5	47.8001	24.9	22.9	5.1 -5	JEND2
80.729	С	0.5	26-2701	1.87	24.4	6 6 E	JENDL+2
83.56	1	0.5	24.4:04	0.0104	24.4		JENDL-2
89.219	1	2.5	24.0851	8,509-2	24.2		JENDL-2
93-109	1	5.5	24.4054	0.00535	24.4		JENUL-2 (ENO -2
111.25		0.5	23.1084	0.00842	23.1		JEND -2
116.97	ċ	0.5	48.7	25.6	23.1		JENDL-2
124.89	:	0.5	24.0206	0.0206	24.0		UENDL-2
133-29	:	0.5	23,4083	0.00835	23.4		JENDL-2
145-63	0	0.5	23,909	0.909 0.0150	23.C		JENGL-2
152.41	•	0.5	24.0400	ט-ט4סט גביה ה	24.5		ENDL /
160.8	:	0.5	23,605	2,035	23.6		LENCL 2
165.26	ò	0.5	27.2:	3.31	23.9		LENCL - 2
173.18	:	0.5	23.846:	0.0461	23.8		JENDL - 2
189.54	0	0.5	199.1	175.0	23.:	4.8 5	JENCL - Z
194.73	:	0.5	24.7455	0.0455	24.7		JENOL-2
203.68	:	0.5	24-155/	0.0344	24 23.6		JENJU Z
203.03	'n	0.5	71.8001	49.5	22.3	8.8 -5	JENGL 7
214.86	ĩ	0.5	24.3595	0.0595	24.3		JENDU-2
218.37	1	0.5	23.5302	0.0302	23.5		JENCL-2
224.57	1	0.5	23.62	0.02	23.6		JENDL - 2
237.34	0	0.5	50+7001	20.5	24.2	0.00006	UENCLI-2
242-71	1	1.5	23.507	0.105	23.3		JENGLI 2
257.19	i	3.5	24.0175	0.0176	24.0		JENCL -2
263.94	1	0.5	23.868	0.268	23.6		JENCL - 2
273.62	0	2.5	48.4	25.3	23.1		JENOL - 7
275.2	1	0.5	23,792	0-192	23.6		UENDU-2
202-44	1	0.5	23.700	5.5	23.0		JENDL-2 JENDL-2
311.28	a	0.5	24,35	1.05	23.3		JENDI -2
322.85	1	0.5	22.0417	0.C417	22.0		JENDL 2
332.02	1	0.5	23.1518	0.0518	23.1		JENDL-2
337.27	1	0.5	23.708	0.108	23.6	0.60	JENDL-2
347.75	U	0.5	102.1	/9.2	22.9	2.68 - 4	JENUL-2
372.91	ţ.	0.5	23,033	0.04	24.3		IFNO -2
376.89	ò	0.5	25.8502	1.25	24.6	2.05 -4	JEND: -2
395.33	1	0.5	21.4709	0.0709	21.4		JENOL-2
397.58	0	0.5	30.52	6.12	24.4		JENDL-2
408.15	1	0.5	23.8807	9.0807	23.8		JENDL-2
410.21	2	0.5	42.3	:9 -8	22.5		JENDL-2
439.75	ر ۱	0.5 0.5	23.888	3 - 70 0 - 288	24-1 23.6		ENDL-2
448.5	1	3.5	23.9462	0.0462	23.9		JENDL 2
454.06	i	0.5	24.022	0.422	23.6		JENOL-2
463.14	С	0.5	28.6415	5.54	23.1	0.00147	JENCL-2
467.21	1	0.5	24-4613	0.0613	24.4	5 1 1	JENCL-7 }
4/0.4	ن ۱	0.5 n c	21.04U2 23.742	4.[4 0.142	23.7	∠.44	JENUL-2
488.87	1	2.5	24.614	C.B14	23.8		JENCL-2
498-96	1	2.5	23.207	0.107	23.1		JENCL-2
518-33	С	с. <u>5</u>	73-0003	48.9	24.:	2.93 -4	JENCL-2
523-35	1	0.5	23.686	0.286	23.4		JENCL - 2
535 20	:	0.5	23.1687	0.0687	23.		I JENUL - 2 JENUL - 2
333-28 542.41	U 1	0.5	0/+/UU4 25.452	43+0 0.152	24	3-04	JENULIZ IENDI - 2
550.71	:	0.5	23.5855	8.549-2	23.5		JENDL -2
556.25	ī	0.5	24.398	0.898	23.5		JENCL-2
580.08	0	0.5	61.6	36.5	25.1		JENDL-2
584.47	:	0.5	23.911	0.1:1	23.8		JENDL-2
595.01	0	0.5	108.901	85-8	23.1	2.DC11	JENDL 2 JENDL 2
615.78	1	0.5	23.304	0.204	23.3		IFND: -2
619.95	0	0.5	53.5002	30.2	23.3	2.15 -4	JENOL -2
624.23	ĩ	0.5	24.303	0.803	23.5		JENDL-2
628.53	0	0.5	30.2	6.3	23.9		JENDL-2
633.34	1	0.5	23.52	U.12	23.4		JENDL-2
001-14	U	0.5	120.8	120-0	24.3		JENUL 12

U-2	3	З
-----	---	---

ENERGY LEV I	L	J	TOTAL WIDTH EMEV 3	NEUTRON WIDTH (MEV.)	GAMMA WIDTH (MEV)	FISSION WIDTH	REFERENCE
668.5S	1	0.5	23.706	0.206	23.5		JENOL - 2
677.75	1	D.5	24.3	0.7	23.6		JENDL-2
681.67	1	0.5	22.6525	0.0525	22.6		JENOL-2
593.05	C	D.5	63.3	40.4	22.9		JENDL-2
208.27	-	D.5	46.626	21.1	24.1	0.026	JENUL-2
710.52	1	0.5	25.85	1.05	24.8	0.020	JENOL-2
713.54	1	0.5	23.917	D.217	23.7		JENDL-2
721.58	Э	0.5	26.49	1.76	23.7	1.03	JENOL-2
730.12	0	0.5	24.884	1.0	23.8	0.084	JENOL-2
734.9		0.5	20.30	1-78 0-163	24.0		I JENUL - 2 IENDI - 2
743.14	÷	0.5	23.759	0.359	23.4		JENDL-2
756.2	:	0.5	24.129	0.529	23.6		JENOL - 2
765.05	2	0.5	31 0773	7.57	23.5	C.0073	JENOL -2
. 770.89	i T	0.5	23.72	0.12	23.6		JENOL-2
779.3:	I	0.5	25.64	2.14	23.5		JENDL-2
785.9	I	0.5	26.35	0.15	26.2		JENDL-2
-787.3	1	0.5	24.473	0.473	24.0		JENDL - 2
790.82	2	0.5	30.24	6.84	23.4		JENDL-2
808.2		J.5 0.5	23-903	0.403	23.5		JENUL - 2 JENUL - 2
828.46	1	0.5	24.486	0.186	24.3		JENOL-2
833.86	ī	0.5	25.2947	0.0947	25.2		JENDL-2
846.68	I	0.5	24.269	0.869	23.4		JENDL-2
950.99	Ĉ,	0.5	86.9011	62.9	24.0	0.0011	JENDL-2
000-00 859,44	ĩ	0.5 1.5	24.1'4	00.0	23.7	0.001	JENUL-2 JEND: - 2
866.42	ċ	0.5	28.9.	5.41	23.5		JENDL 2
891.23	ī	0.5	24.197	0.697	23.5		JENDL - 2
905.03	0	0.5	77.9	54.2	23.7		JENDL-2
910-01	1	0.5 DE	24.85	1 35	23.5		JENUL-2 JENDL-2
	1	0.5	23.029	0.229	20.0 22.8		JENUL-2 IENDi-2
937.02	ż	0.5	173.7	150.0	23.7		JENDL -2
940.94	1	0.5	24.557	0.657	23.9		JENDL-2
958.52	2	0.5	227-B	205.0	22.8		JENDL-2
904+08	1	0.5	24.404	0.304	24.1		JENUL-2
982.32	1	0.5	23.69	0.09	23.6		JENDL-2
985 . : 7	1	0.5	24.969	J.169	24.5		JENDL-2
991.63	С	Э.5	407.2	378.0	29.2		JENDL-2
1003-67		0.5	28.107	0.107	28.0		JENOL-2
1011.44	O	0.5	25.40	1.86	23.6 22.8		JENUL-2 JENO: -2
1029.12	:	C.5	25.81	2.31	23.5		JENDL-2
:033.38	:	2.5	23.833	0.733	23.1		JENDL-2
1047.27	:	C.5	23-897	0.397	23.5		JENDL-2
1054.45	0	0.5	117.8	94.6	23.2		JENDL-2
1067.68	÷	0.5	25.02	1.12	23.0		JENUL-2
1074.07	÷	0.5	24.323	0.923	23.4		JENDL-2
1081.7	1	3.5	25.25	1.55	23.7		JENDL~2
1095.18	1	0.5	25.88	2.28	23.6		JENOL-2
1098-62	U ,	2.5	45.2	21.4	23.8		JENUL-2
1109-08	ò	0.5	58.0	34.6	23.4		JENOL-2
11:8.97		0.5	23.221	0.521	22.7		JENOL-2
1131.37	1	0.5	27.61	3.71	23.9	0.0515	JENOL - 2
1140+35	- 1	U.5 n =	258-701	235.0	23.7 23.6	0.0015	I JENDL - 2
1147.97	1	0.5	23.7	0.3	23.4		JENGL-2
1152.57	i	0.5	25.176	0.476	24.7		JENOL-2
1155-07	!	0.5	23.925	0.825	23.1		JENDL - 2
1159.38	1	0.5	23.44	0.74	22.7	0.011	JENOL-2
110/-03	U O	0.5	01'0 103*311	80.8 69.2	23.1	0.011	JENUL = 2 JENUL = 2
1194.8:	Ő	C.5	115.7	94.6	21.1		JENOL-2
1201.57		0.5	23.724	0.524	23.2		JENCL-2
1211.11	0	0.5	33.495	9.64	23.6	0.255	JENDL-2
1219-51		0.5	24.881	0.581	24.3		JENOL-2
1233.17	;	0.5	23.099	0.399	23.5		JENUL-2
1238.36	i	0.5	23.166	0.465	22.7		JENOL -2
1245.06	0	0.5	276.8	254.0	22.8		JENOL-2
1249.85	1	0.5	23.9	0.3	23.6		JENOL-2
1251.42	1	U-5 0-5	24.000	0.208	24.U 23.5		JENUL-2 JEND: -2
1267.04	ċ	0.5	54.3041	29.6	24,7	0.0041	JENOL-2
1272.97	С	0.5	52.0	28.3	23.7		JENOL -2
1276.53	1	0.5	24.142	0.542	23.6		JENDL-2
12/8.04	!	0.5	24.3	U.7	23.6		JENOL-2
1285.4		0.5	22.91	D.41	22.5		JENUL-2
1289.04	1	0.5	24.45	0.25	24.2		JENDL-2
1296-14	1	0.5	23.7	0.1	23.6		JENDL-2
L							1

U-2	238
-----	-----

ENERGY LEV 1	L	J	TOTAL HIOTH (MEV.)	NEUTRON WEDTH	CAMMA WIDTH	FISSION WIDTH	REFERENCE
1298,69	0	0.5	27.09	3.49	23.6		JENOL - 2
1310.99	1	0.5	23.125	0.225	22.9		JENOL-2
1317.01	1	0.5	28.29	4.99	23.3		JENOL-2
1324.85	1	0.5	22.915	0.315	22.6		JENOL - 2
1331-48		0.5	25.05		23.7		JENUL-2
1385.15	;	0.5	27.329	0.329	23.2		JENOL-2
1387.22	1	0.5	23.68	0.08	23.6		JENDL-2
1393.81	0	0.5	235.2	211.0	24.2		JENDL-2
1405.43	0	0.5	98.2	72.0	25.4		JENDL-2
1416.92	1	0.5	27.47	3.47	24.0		JENDL-2
1419.76	U	0.5	32.66	.9.15	23-5		JENDL-2
1420-01		0.5	23.9	20.3	23.4		JENDL-2
1444.05	'n	0.5	37.7	15.0	22.7		JENDL-2
1447.65	1	0.5	24.95	1.15	23.8		JENDL-2
1455.1	1	0.5	26.504	0.204	26.3		JENDL-2
1456.7	1	0.5	23.84	0.24	23.6		JENOL-2
1473.82	0	2.5	144.9	121.0	23.9		JENCL - 2
1487-04	1	0.5	27.025	J+225 0.23	20.0		JENUL-2 JENUL 2
1504.5	1	5.5	27.03	0.23	23.5		ENDL-2
1510.53	i	3.5	25.044	0.844	24.2		JENDL-2
1522.7	0	2.5	268.8	245.0	23.8		JENDL-2
1527.86	l	2.5	24.394	0.794	23.6		: JENOL-2
1534.79	1	2.5	24.086	0.786	23.3		JENDL-2
1547-18	1	2.5	27.81	3-81	24.0		UENUL 2
1000-0	1	J.5 n 5	20.10	3-10 0.34	20.0		IENDL-2
1565.45	ć	0.5	28.97	5.67	23.3		JENDL-2
1568.23	Ĩ	õ.5	24.87	1.27	23.6		JENOL-2
1591-52	1	0.5	24.77	1.17	23.6		JENOL-2
1597.89	2	0.5	400 . :	378.0	22.1		JENDL-2
1622.67	ž	0.5	123.3	101-0 50 B	22.3		JENUL-2
1646.69	ĩ	0.5	22.775	0.475	22.3		JENDL-2
1662.45	ċ	0.5	248.1	224.0	24.1		JENOL-2
.672.74	1	0.5	24.6952	9-519-2	24.6		JENDL-2
1688 - 78	2	0.5	1 30 - 5	107.0	23.5		JENDL-2
1695.99	1	0.5	22.985	U-386	22.6		JENUL-2
1719.85	à	0.5	24.9	89.5	23.5		IENDL-2
1722-89	0	0.5	40-1	17.4	22.7		JENOL -2
1745.65	ī	0.5	24.69	1.69	23.0		JENOL-2
1755.89	0	0.5	165.0	139.0	25.0		JENOL - 2
1776.4		0.5	24.185	C.685	23.5		JENOL-2
1782.69	1	0.5	24.7	1.2 662.0	23.5		JENUL-2
1797.35		0.5	27.12	2.92	24.2		JENDL-2
1808.4	O	0.5	38.1	19.0	.9.1		JENOL - 2
1823.59	:	0.5	24.188	0.788	23.4		JENDL-2
1834-22	:	0.5	25.01	C.41	24.6		JENDL-2
1845-1	U ,	U-5 n s	30.4	11.1	19.3		JENUL-Z
1869.64	÷	0.5	26.42	2.52	23.9		JENDI -2
1881.09	2	0.5	24.97	1.47	23.5		JENDL-2
1893.88	:	0.5	25.05	1.55	23.5		JENDL-2
1902-83	0	0.5	68.3	44.2	24.1		JENOL-2
1913-28	:	0.5	35.66	3.56	32.1		JENUL-2
1917-10		0.5	24.55	0.951	22		JENCL-2
1942.7	÷	0.5	24.077	0.677	23.4		JENOL-2
1953.79	С	0.5	27.95	4.25	23.7		JENDL-2
1968.98	0	0.5	850.8	822.0	28.8		JENDL-2
1974-91	C	0.5	461.4	4 38 .0	23.4		JENUL-2
2001.15	1	2.5	22.758	0.568	23.7		FNOL-2
2023.68	ċ	0.5	250.4	227.0	23.4		JENOL-2
2030.49	2	2.5	69.9	46.9	23.0		JENOL-2
2049-02	1	2.5	25.48	2.18	23.3		JENDL-2
2052.8	1	2.5	24.56	0.86	23.7		JENDL-2
2063-38	÷	0.5	23.85	2.11	23.0		IENDL-2
2080.7	i	0.5	25.22	1.62	23.6		JENDL-2
2086.04	i	0.5	27.99	4.39	23.6		JENOL - 2
2088.62	С	0.5	48.4	25.6	22.8		JENDL-2
2096-29	÷.	0.5	50.6	26.3	24.3		JENDL - 2
2104.07	1	J.5 n ⊑	25.14	L 44 D 5	23.6		JENUL-2 IENDL-2
2114.05	i	0.5	27.745	0.845	26.9		JENDL -2
2121.27	1	0.5	23.85	0.25	23.6		JENDL - 2
2124-18	:	0.5	28.0	3.7	24.3		JENDL-2
2140.67	1	0.5	24.6	1.0	23.6		JENOL-2
2152.76	U N	0.5 0.5	30.4	300.0	23.1		JENOL-2
2:73.12	1	0.5	25.89	2.19	23.7		JENOL - 2
2:78.96	1	0.5	24.4	0.8	23.6		JENOL→2

U-	2	38

ENERGY (EV)	L	J	TOTAL WIDTH (MEV)	NEUTRON WIDTH (MEV)	GAMMA WIDTH FISSION WIDTH LMEV I LMEV I	REFERENCE
2:86.58	0	0.5	615.2	591-0	24.2	JENOL - 2
2201.26	ō	0.5	130.2	105-0	25.2	JENOL-2
2215.44	1	0.5	27.02	3.42	23.6	JENOL-2
2241.41	1	0.5	20.32	1.02	25.3	JENUL-2
2266.54	Ö	0.5	256.0	234.0	22.0	JENOL-2
2270.15	1	0.5	27.58	3.88	23.7	JENOL - 2
2281.92	0	0.5	209.0	168.0	21.0	JENOL-2
2293.95	1	0.5	24.0	5.61	23.5	JENUL-2
2315.93	ċ	0.5	43.1	19.1	24.0	JENDL-2
2327.28	1	0.5	30.24	1-14	29.1	JENDL-2
2334.83	1	0.5	26.86	1.65	25.2	JENUL-2
2352.75	, D	0.5	83-4	55.2	28.2	JENOL-2
2355.73	Ō	0.5	102.0	77.9	24.1	JENDL-2
2368.75	1	0.5	30.38	5.78	24.6	JENOL-2
2384.94	1	0.5	24.0	2.0	23.5	JENOL-2
2391-98	O	0.5	54.1	30.1	24.0	JENOL-2
2397.8	1	0.5	29.9	5.2	24.7	JENDL-2
2401-82	1	0.5	28.22	4.42	23.8	JENUL-2 JENUL-2
2418.17	1	0.5	26.169	0.969	25.2	JENOL - 2
2426 89	0	0.5	180.7	157.0	23.7	JENOL-2
2446.7	o	0.5	246.6	223.0	23.6	JENOL-2
2447.31	1 0	0.5	24.U 41.3	17.3	23·6 24-D	IFN0L-2
2489-18	õ	0.5	129.4	105.0	24.4	JENOL-2
2502.22	1	0.5	27.45	3.85	23.6	JENDL-2
2521.49	D	0.5	43.3	19.0	24.3	JENUL-2
2548.19	ò	0.5	761.5	738.0	23.5	JENOL - 2
2559.59	ō	0.5	3D1 .7	278.0	23.7	JENOL - 2
2581.15	D	0.5	470.6	447.0	23.6	JENOL-2
2597.61	1	0.5	/83.7	761.0	22.7	JENUL-2 JENUL-2
2612.02	1	0.5	28.53	4.93	23.6	JENDL - 2
2620.05	0	0.5	71.9	48.1	23.8	JENOL-2
2632.73	1	0.5	28.64	4.44	24.2	JENOL-2
2654.08	ł	0.5	24.6	1.0	23.6	JENOL-2
2658.73	i	0.5	27.97	4.17	23.8	JENDL-2
2672-22	0	0.5	312.0	288-0	24.0	JENOL - 2
2682-61	1	0.5	26.22	2.32	23.9	JENUL-2 IENUL-2
2701.95	1	0.5	25.93	1.93	24.0	JENDL-2
2717.33	Ō	D.5	200.6	177.0	23-6	JENDL-2
2750.74	0	0.5	65.6	41.7	23.9	JENOL-2
2766.69	1	0.5	42.7	3.23	23.9	JENOL-2
2774.55	i	0.5	25.14	1.54	23.6	JENOL - 2
2778.46	1	0.5	24.9	1.3	23.6	JENOL-2
2/8/-43	1	0.5	39.6 29.43	15.0	24.b 24.3	JENUL-2
2806.38	Ď	0.5	34.8	10.2	24.6	JENOL - 2
2811.62	1	0.5	29.05	5.05	24.0	JENOL-2
2815.93	1	0.5	25.05	1.35	23.7	JENOL-2
2829.32	0	0.5	44.4	20.8	23.6	JENOL-2
2845.95	Ī	0.5	24.2	0.6	23.6	JENDL-2
2865.39	0	0.5	240.2	218.0	22.2	JENOL-2
2882.78	ò	0.5	632.4	608.0	24.4	JENOL-2
2897 23	Ō	0.5	41.7	17.8	23.9	JENDL-2
2918.38	1	0.5	30.86	6-86	24.0	JENOL-2
2922-92	1	0.5	29-97	5-07	24.9 24.6	JENUL-2
2933.65	ò	0.5	62.4	38.3	24.1	JENOL -2
2945.37	1	0.5	25.98	2.08	23.9	JENOL -2
2956.93	D ,	0.5	46.3	21.8	24.5	JENOL-2
2988.56	1	0.5	30,39	6.59	23.8	JENOL - 2
3003-62	Ď	0.5	146.7	122.0	24.7	JENUL-2
3014.99	1	0.5	24.88	1.18	23.7	JENOL-2
3024+7	ı n	0.5	27.9	4.4	23.5 23.7	JENUL-2
3043.72	1	0.5	27.69	3.49	24.2	JENOL -2
3059-64	0	0.5	57.2	32.9	24.3	JENOL - 2
3072+14	ļ	0.5	25.18	1.08	24.1	JENOL-2
3088.71	1	0.5	27.21	3.51	23.7	JENOL-2
3103.55	1	0.5	26.37	2.07	24.3	JENOL-2
3109.91	0 ,	0.5	253.6	230.0	23.6	JENOL-2
3133.86	1	0.5	20.72	3.12 8.91	23.0 24.2	JENOL-2
3149.03	ċ	0.5	136-6	113.0	23.6	JENOL -2
						L

U	-2	3	8

ENERGY LEV 1	 L	J	TOTAL WIDTH (MEV.)	NEUTRON WIDTH	GAMMA WIDTH	FIS510N HIOTH (MEV)	REFERENCE
3169.8	0	0.5	34.5	10.9	23.6		JENOL-2
3178.63	0	0.5	117-3	93.5	23.8		JENOL-2
3188.91	U N	0.5	133-1	96.2	22.1		JENUL-2 JENUL-2
3219.67	õ	0.5	34.32	9.52	24.8		JENOL-2
3226 . 34	0	0.5	49.3	24.9	24.4		JENOL -2
3240.23	1	0.5	26.45	1.45	25.0		JENUL-2
3263.89	1	0.5	27.31	1.71	25.6		JENOL-2
3267.53	1	0.5	33.8	9.5	24.3		JENOL-2
3273.29	0	0.5	43.0	13.6	29-4		JENOL-2
32 /9 -51	0	0.5	35.6	10.1	25.5		JENOL - 2
3307 BI	ĩ	0.5	28.5	5.0	23.5		JENOL-2
3312.18	0	0.5	189.6	166.0	23-6		JENOL - 2
3333.66	0	0.5	130.1	106.0	24.1		JENOL-2
3341.25	1	0.5	27.75	4.15	23.6		JENOL-2
3346.82	1	0.5	25.0	1.5	23.5		JENOL-2
3355.81	1	0.5	24.5	0.9	23.6		JENOL-2 JENOL-2
3378.3	i	0.5	31.35	7.75	23.6		JENOL-2
3383.59	1	0.5	27.95	3.35	24.6		JENOL-2
3399.28	1	0.5	50-9 31-43	20.0	24.9		JENUL-2
3408.77	Ó	0.5	266.7	243.0	23.7		JENOL -2
3417.93	1	0.5	28.22	3.92	24.3		JENOL-2
3436-49	0	0.5	448.9 755.7	425.0 731.0	23.9		JENUL-2 JENOL-2
3485.8	ō	0.5	122.6	98.8	23.8		JENOL-2
3495.64	0	0.5	35.7	10.7	25.0		JENDL-2
3513.02	1	0.5	25.52	1.92	23.6		JENUL~2 JENDL~2
3522.39	1	0.5	26.08	2.18	23.9		JENOL-2
3528.51	1	0.5	30.04	6.34	23.7		JENOL-2
3561.59	0	0.5	293.6	270.0	23.6		JENUL-2 JENUL-2
3595.02	0	0.5	61.4	57.6	23.8		JENDL-2
3623.24	0	0.5	52.3	24.3	28.0		JENOL-2
3629-8	0	0.5	558.6	535.0	23.6		IENOL-2
3653.99	1	0.5	26.63	2.63	24.0		JENOL - 2
3662.39	1	0.5	26.83	2.53	24.3		JENOL-2
3673.35	1	0.5	28.74	5-14	23.6		JENDL-2 JENDL-2
3693.19	Ů	0.5	442.6	419.0	23.6		JENDL-2
3716-8	0	0.5	137.9	114-0	23.9		JENDL-2
3724.77	1	0.5	32.11	6-81 219 0	25.3		JENOL-2
3741.55	I	0.5	25.5	2.0	23.5		JENDL-2
3742.53	L	0.5	24.4	0.8	23.6		JENDL-2
3745.43	I I	0.5	24.4	0.8	23.6		JENDL-2
3765.11	ů.	0.5	127.9	104.0	23.9		JENDL-2
3781.96	0	0.5	504-0	480.0	24.0		JENDL-2
3791.13	1	0.5	26-5 24-25	2.9	23.6		JENUL-2 JENOL-2
3825.68	1	D.5	28.17	4.57	23.6		JENDL-2
3831-6	0	0.5	38.0	13.8	24.2		JENDL-2
3857-79	0	0.5	623-6 203-9	600+0 180+0	23.6		UENUL-2
3880.06	1	D.5	26.68	2.98	23.7		JENDL-2
3894 .84	1	0.5	32.49	8.49	24.0		JENDL -2
3902-22	0	0.5	324.3	300.0 107.0	24-3 23.1		JENUL-2 JENOL-2
3927.9	1	0.5	36.4	12.0	24.4		JENOL-2
3930.21	1	0.5	37.6	14.0	23.6		JENOL-2
3933,38	1	U-5 N.5	36-2 204.1	12+7	23.5		JENUL-2 JENOL-2
3948-81	1	0.5	27.6	4.0	23.6		JENDL-2
3954.94	D	0.5	151.9	128.0	23.9		JENDL-2
3992.71	1	0.5	26.6	3.U 4.0	23.6		JENUL-2
4014-11	1	0.5	26.2	2.6	23.6		JENDL-2
4024.9	1	0.5	25.0	1.4	23.6		JENDL-2
4040.62	U n	U-5 0.5	88-9 45-3	ы4-ы 20₊2	24-3		JENUL-2 JENDL-2
4080.4	ĭ	0.5	27.4	3.8	23.6		JENDL-2
4083.6	1	0.5	27.6	4.0	23-6		JENDL-2
4090-29	U 1	U-5 D-5	117-6 25-3	93.4 1.7	24.2		JENUL-2 JENDL-2
4103.8	i	0.5	25.6	2.D	23.6		JENDL-2
4125-12	0	0.5	65.3	41.4	23-9		JENOL-2
4132-19	1	0.5 0.5	40.6 27.9	4.3	23.6		JENUL-2
4167.95	o	0.5	229.3	205.0	24.3		JENOL - 2
4179-31	0	0.5	55.4	31.5	23.9		JENOL-2

ENERGY (EV)	L	J	TOTAL WIDTH	NEUTRON WIDTH	GAMMA WIDTH (MEV)	FISSION WIDTH (MEV.)	REFERENCE
4201.99	1	0.5	27.6	4.D	23.6		JENDL~2
4210.72	0	0.5	62.9	38.4	24.5		JENDL-2
4225.52	1	0.5	33.6	10.0	23.6		JENDL-2
4258.76	0	0.5	55.8	31.2	24.6		JENDL-2
4299.54	D	0.5	162.0	138.0	24.0		JENDL-2
4307.04	٥	0.5	134.3	110.0	24.3		JENDL-2
4325.15	0	0.5	106.0	81.3	24.7		JENDL-2
4371.D	0	0.5	176.1	152.0	24.1		JENDL-2
4435.55	0	0.5	124.5	100.0	24.5		JENDL-2
4511.74	0	0.5	607.4	583.0	24.4		JENOL-2
4543.45	0	0.5	117.8	93.1	24.7		JENDL-2
4567.76	0	0.5	68-1	43.6	24.5		JENDL-2
4594.67	Ó	0.5	48.3	22.8	25.5		JENDL-2
4632.17	Ō	D.5	52.1	27.6	24.5		JENOL-2
4662.9	Ō	0.5	170.2	146.0	24.2		JENDL-2
4705.73	0	0.5	356.1	332.0	24.1		JENDL-2
4727.89	Ď	0.5	43.8	19.4	24.4		JENOL-2

Pu-	23	19
-----	----	----

ENERGY (EV)	L	J	TOTAL WIOTH (MEV)	NEUTRON WIDTH	(Hev)	FISSION WIDTH	REFERENCE
-0.22	0	0	504.644	0.0437	46.6	458.0	JENOL-2
0.297	0	0	98-84	0.24	38.2	60.4	JENDL-2
7.82	0	1.0	88.3997	0.7997	40.0	47.6	JENOL-2
10.93	U	1.0	199.8//	1.8/69	55.0	143.0	JENOL-2
14.31	0	1.0	101.601	0.6015	42-0 34-0	24.U 67.0	JENUL-2 JENUL-2
14.68	õ	1.0	69.8903	1.8903	38.0	30.0	JENGL-2
15.46	Ō	0	994.4	2.4	42.0	950 0	JENOL-2
17.66	0	1.0	74.8109	1.8109	39.0	34.0	JENOL-2
22.29	0	1.0	108.644	2.6437	44.0	62.0	JENDL-2
23.94	U O	1.0	/U+1288 93 454	0.1288	32.0	38.0	JENUL-2
27.24	ŏ	0.5	42,2082	0,2082	37.0	5.0	JENDL-2
32.31	ō	Ō	151.833	0.8328	41.0	110.0	JENOL-2
34.6	0	0.5	91.5198	0.0198	41.5	50.0	JENOL-2
35.5	0	1.0	47.2841	0.2841	43.0	4.0	JENOL-2
41-42	U	1.0	52.0977	4.0977	44.0	4.0	JENDL-2
44.48	0	1.0	58.5895	6.5895	47.0	46.0	JENUL-2
47.6	õ	0	311.671	5.6708	58.0	248.0	JENOL-2
49.71	0	Ð	800 - 362	4.352	50.0	746.0	JENDL-2
50.08	0	1.0	57.0072	3.0072	41-0	13.0	JENDL-2
52.6	0	1.0	68.3765	10.3765	49.0	9.0	JENOL-2
55.03	0	1.0	38.434 400 898	12 899	36.0	21.0	JENUL-2
58.64	ő	ŏ	1099.91	10.9052	42.0	1047.0	IFNOL-2
59.22	ō	1.0	180.42	5.4196	52.0	123.0	JENDL-2
60.94	0	0	6797-83	19.828	42.0	6736.0	JENOL-2
63.08	0	0.5	155.19	1-1896	43.0	111.0	JENOL-2
65.36	0	0.5	92.0354	0-5354	41.5	50.0	JENOL -2
74.05	0	1.0	13/+U42 71.1393	12-0421	0. PC	71.0	IENOL 2
74.95	ő	1.0	146.943	21.9427	41.0	84.0	JENDL-2
78.95	0	0.5	91.66	0.16	41.5	50.0	JENDL-2
81.76	0	0	2047.91	9.914	42.0	1996-0	JENOL-2
82.68	0	0.5	70.7436	0.7436	40.0	30.0	JENOL-2
85.32	0	0	2096 0	2-3/92	42.0	1/06.0	JENOL-2
85.48	Ö	1.0	74,7989	7.7989	51.0	16-0	IENOL-2
90.75	Ō	1.0	59.7941	12-1941	39.0	8.6	JENOL-2
92.97	0	0.5	57.041	1-041	47.0	9.0	JENOL - 2
95.36	0	1.0	98-0819	2.0819	66.0	30.0	JENDL-2
96.491	U	0	1700-24	13.2448	42.0	1645.0	JENOL-2
102.99	n	1.0	47.5993	1.5993	42+U 0. AF	10 0	JENUL-2
105.3	õ	1.0	48.0	4.6	38.0	5.4	JENOL-2
106.67	0	1.0	75.6265	9.2265	40.0	26.4	JENOL-2
110.38	D	0.5	43.6542	0.6542	30.0	13.0	JENDL-2
114.44	0	0	1499.39	1.388	42.0	1456.0	JENOL-2
115-1	0	0.5	203.317	U-J1/2	40.0	165-0	JENDL-2
118.83	0	i.0	102.831	17.8307	43.0	42.0	JENUL-2
120.99	0	0	78.336	7.336	32.0	39.0	JENDL-2
123.44	0	0.5	63-694	0.694	24.0	39.0	JENDL-2
126.22	0	0	95.8688	5.8688	70.0	20.0	JÉNOL-2
131.75	0	0.5 N	3799.69	U-/634 35.6904	40.0	24.0	JENOL-2
133.78	õ	1.0	55.5385	5.5385	44.0	6.0	JENUL-2
136.75	Ō	0	70.1516	10.1516	32.0	28.0	JENOL-2
139.28	0	0.5	321-678	0.1784	41.5	280-0	JENOL-2
142.92	0	1.0	137-212	3.2121	52.0	82-0	JENOL-2
146.25	U N	1.0	03+U440 69-9927	4 +U440 6 -9927	40.U 50 5	J1-U 12 5	JENUL-2
147.44	ŏ	0	1000.38	2.3792	42.0	956.0	JENUL-2
148-21	0	0.5	149.694	0.694	47.0	102.0	JENOL-2
149.42	0	0.5	119.597	2.5974	67.0	50.0	JENOL-2
157.08	0	0	621.6	33.6	48.0	540.0	JENOL-2
161.06	U	0.5	141-208	0.2081	41.0	100-0	JÉNOL-2
164.54	ñ	1.0	78.7587	27.7587	40.0	110.0	JENUL-2
167.1	ŏ	1.0	111.783	5.7831	37.0	69.0	JENOL-2
170.49	0	0.5	158.853	0.8526	38.0	120.0	JENOL-2
171.08	0	0	999.765	1.7648	42.0	956-0	JENDL-2
175 08	0	0.5	241-559	0.0594	41.5	200-0	JENOL-2
177.22	0 N	1.0	/3+1120 51.5425	3.5425	39.U 41.S	31.0	JENOL-Z
178.9	ŏ	1.0	58-2095	1.2095	43.0	14.0	JENUL-2
183.64	0	0.5	72.2702	2.2702	42.0	28.0	JENOL-2
184.87	0	0	2098-64	18.638	42-0	2038.0	JENOL-2
188-27	0	0.5	52.912	0.912	43.0	9.0	JÉNOL-2
190+04	U n	U 0	00-9/00	4.9/68	49.0	13.0	JENOL-2
196.69	n	1.0	111.653	4.6529	52.0 53.0	335-U 54 0	JENUL-2
199.39	õ	1.0	132.577	9.5768	43.0	80.0	JENOL-2
203.46	Ō	0.5	72.4484	5-9484	41.5	25.0	JENDL-2
203.93	0	0	440.6	53.6	42.0	345.0	JENOL-2
20/13/	U	1-0	56 9397	6.9397	44.0	6.0	JENOL-2

Pu-2	239
------	-----

	ENERGY LEV 1	L	J	total wioth (MeV)	NEUTRON HIDTH (MEV)	Camma Hidth (mev)	FISSION WIDTH (MEV)	REFERENCE
	211.09	0	0	789.776	2.776	42.0	745.0	JENDL-2
	212.02	0	0	1500.38	2.3792	42.0	1456.0	JENDL-2
	213.20	0	0.5	199.694	0.694	42.0	157.0	JENOL-2
	216.35	0	1.0	5/-212/ 70 5425	5+212/ 3 5425	50.0	11.0	JENUL~2
	220.22	0	1.0	52.3627	7.3627	41.0 34.0	11.0	JENOL-2
	223.16	õ	1.0	59,3839	3.3839	47.0	9.0	JENOL-2
	224.89	0	0.5	85.5378	2.5378	58.0	25.0	JENOL-2
	227.77	0	0	8096.03	30.5348	41.5	8024.0	JENOL-2
	227.89	0	1.0	66.6787	1.6787	33.0	32.0	JENOL-2
	232.63	0	0.5	120.654	0.6544	40.0	5.U 80.0	IENDL-2
	234.32	õ	1.0	74.1452	10-1452	49.0	15.0	JENDL-2
	239.04	D	1.0	72.3865	5.3865	51.0	16.0	JENOL-2
1	240.6	0	0.5	241.55	0.0496	41.5	200.0	JENOL-2
	242,00	0	1.0	96,5564 280 348	b-5564 1 3482	34.U AS 0	56-U 234 0	JENUL-2 IENOL-2
	248.86	5 0	1.0	61.6253	14.6253	42.0	5.0	JENOL-2
Í	251.23	0	1.0	82.2293	27.2293	43.0	12.0	JENOL-2
	254.5	0	1.0	54.7759	2.7759	27.0	25.0	JENDL-2
l	256.11	0	1.0	91.2788	6,2788	53.0	32.0	JENUL-2
	262.73	0	0.5	6299.14	99.14	42.0	6158.0	JENDU-2
	262.74	Ō	0.5	59.6086	3.6086	46 · D	10.0	JENOL-2
	264.23	0	D.5	341.748	0.2478	41.5	300.0	JENOL-2
	269-11	0	0.5	130.082	2.0818	42.0	86.0	JENOL-2
	272.62	0	1.0	/1-8333	3.8333	40.0	28.0	JENUL-2
-	274.8	ŏ	0.5	791.88	13,8796	42.0	736.0	JENOL-2
İ	275.57	0	1.0	149.199	23.1987	54.0	72.0	JENOL-2
1	277.23	2	0	5299.85	17.8452	42.0	5240.0	JENOL - 2
ł	2/9-59	0	1 0	111.097 BA 083	21.0968	34.0	56.0	I JENUL - 2
	285.73	Ğ	0.5	341.599	9.919-2	41.5	300.0	JENOL-2
i	288.0	Ō	0	6498-55	28.552	42.0	6428-0	JENOL-2
ĺ	200.3	0	0.5	341.579	7.939-2	41.5	300.0	JENOL-2
	292.33	U	1 0	1 4.54	11.5396	31.0	72.0	JENUL-2
	298.59	õ	1.0	73.4427	10.4427	43.0	20.0	JENOL-2
	301.81	0	1.0	108.043	18-043	42-0	48.0	JENOL-2
	308.2	3	0.5	150.362	4.362	48-0	98.0	JENOL -2
	309.01	0	1-0	84-945 82-2238	13.945	4/.0	24.0	JENUL-2 IENOL-2
Ì	3:3.62	Ö	1.0	61.483	13.483	38.0	10.0	JENOL-2
i	316.6	0	1.0	73.1221	5.1221	43.0	25.0	JENOL - 2
	320.0	0	0.5	5061.5	20.0	41.5	5000.0	JENOL-2
1	321 - 75	0	0.5	341+090 159.88	U-1982 59-88	41+5 53.0	47.0	JENUL-2
	325.3	õ	1.0	104.46	8.4599	50.0	46.0	JENDL - 2
;	329.65	0	0	1999.71	10.7068	42-0	1947.0	JENOL-2
	333-91	0	1.0	67.446	5-446	52.0	10.0	JENUL-2
	337.95	0	1.0	73.991	7,991	55.0	11.0	JENOL-2
	339-24	Ô	0	80.7552	9.7552	37.0	34.0	JENOL - 2
1	343-18	0	1.0	74.657	15-657	41.0	18.0	JENOL-2
	340,30 350,3	0	U 1.0	1200-31 97,315	21.315	4∠-U 41.0	1140.0 35.0	JENUL-Z JENUL-2
	352.82	ö	1.0	68.8597	3.8597	48.0	17.0	JENOL-2
	354.89	0	0.5	79.0948	0.5948	41.5	37.0	JENDL-2
	357.87	0	0	5999.92	8.9224	42.0	5949.0	JENDL-2
	361.28	0	0.5	341.827	1,0400	52.0 41.5	300.0	JENOL-2
}	364.0	õ	0.5	3051.5	10.0	41.5	3000.0	JENOL-2
	366.0	0	0	4999.71	10.7068	42.0	4947.0	JENOL - 2
	368.33	0	0.5	162.095	0.5948	41.5	120.0	JENOL-2
	371.72	0 0	0.3	3399.8	22,802	42.0	3335.0	JENOL-2
	375.02	ō	ō	42.9312	7.9312	29.0	6.0	JENOL - 2
	377.1	0	0.5	99.9542	2.9542	58.0	39.0	JENOL - 2
	378-04	0	0.5	224+364	1.8638	41-5	181.0	JENUL-2
	384.26	0	1.0	129-625	5.6509	43-0 28-0	75.0	JENOL -2
	385.9	Ō	o -	999.776	2.776	42.0	955.0	JENOL -2
	389.51	0	0.5	74.072	2.072	51.0	21.0	JENOL-2
	391-52 304 43	0	0.5	124.874	1.8738	55.0	58.0 52.0	JENUL-2
	396.91	0	0.5	108.143	3.1426	44.0	61.0	JENOL -2
	401-56	ō	1.0	219.232	19.232	46.0	154.0	JENOL -2
	404.24	0	1.0	155.0	23.0	56-0	76.0	JENDL-2
	406-95	0	0.5	321-206 331-447	∠•/U64 1.4474	41-5	277.0	JENUL-2
	408-71	õ	0.5	114.924	1.9238	55.0	58.0	JENOL -2
	412.31	0	1.0	144.863	8.8631	66.0	70.0	JENDL-2
	415.66	0	0.5	61-8478	4.8478	50.0	7.0	JENOL-2
	419.85	0	1.0	230,399	6.0211	50.0 59.0	74.0	JENOL-2
	425.67	õ	0.5	341.897	0.3966	41.5	300.0	JENDL-2
1								1

Pu-2.

ENERGY LEV I	£	J	TOTAL WIDTH (MEV)	NEUTRON WIDTH (MEV)	GANNA MIDTH (MEV)	FISSION WIDTH (MEV.)	REFERENCE
426.37	n	0	6996 35	29.3452	42.0	6075 0	IENOL 2
429.64	ů Ú	0.5	779.411	5.4112	42.0	732 0	JENOL-2
431-29	ō	0.5	3491.44	6,9398	41.5	3443.0	JENDL-2
432.73	Ð	0.5	341.027	1,5268	41.5	298.0	JENOL-2
437.76	0	1.0	61.6701	2.6701	49.0	10.0	JENOL-2
438.72	0	1.0	60.0835	2.8835	55.0	3.0	JENOL-2
440.07	0	0.5	341.916	0.4154	41.5	300.0	JENOL-2
442.41	0	0	411.819	20.819	44.0	347.0	JENOL - 2
449.75	0	0.5	133.483	1.9828	41.5	90.0	JENDL-2
451.35	0	1.0	59.145	13.945	41.5	3.7	JENOL - 2
454.45	0	0.5	402.194	0.694	41.5	360.0	JENOL - 2
455.73	0	0	615-216	78.716	41.5	495.0	JENOL - 2
457.33	U	0.5	1/0.504	11-0044	41.5	118.0	JENUL-2
451.25	0	1.0	/9.0004	4.0004	41.5	33.U 53.4	JENUL-2
462.64	0	0.5	128 203	0 7932	41.5	96.0	JENUL-2
468.2	ñ	0.5	2092.94	6.444	41.5	2045 0	JENOL - 2
470.0	õ	0.5	5086.37	14.871	41.5	5030 0	
473.1	ō	1.0	55.5977	4.0977	41.5	10.0	IENOL -2
475.31	0	0.5	582.052	5.5518	41.5	535.0	JENOL - 2
476.9	0	0.5	1994.18	2.6766	41.5	1950.0	JENOL-2
479.24	0	0.5	201.698	0.1982	41.5	160.0	JENOL-2
484.15	0	0.5	59.8654	3.8664	41.5	14.5	JENOL-2
487-29	0	0.5	224.772	3.2716	41.5	180.0	JENDL-2
487-81	0	0.5	226.655	5.1552	41.5	180.0	JENDL-2
490.65	0	0.5	2281.33	19.828	41.5	2220.0	JENDL-2
494.1	0	1.0	116.06	4.5604	41.5	70.0	JENOL-2
432.03	U	0.5	202,69	1.1899	41.5	160.0	JENOL-2
502.86	0	1.0	10.0/U/ 85.2545	3-3/0/	41.5	J2.U	JENUL-2
505.78	n	1-0	442,392	11 + /040 0.8022	41.5	32.U 400 0	I JENUL-2
508.22	n n	0.5	692.194	0.694	41.5	400.0 650 n	JENUL-2 JENDI-2
509.74	ũ	1.0	260.184	51.684	41.5	167.0	JENOL-2
511.52	õ	0.5	3354.29	12.789	41.5	3300.0	IENDI -2
515.16	õ	0.5	482.491	0.9914	41.5	440.0	JENDL-2
516.57	0	0.5	321.797	0.2974	41.5	280.0	JENOL-2
517.98	0	0.5	362.194	0.694	41.5	320.0	JENOL - 2
520.22	0	1.0	99.304	14.804	41.5	43.0	JENDL-2
524.21	0	1.0	91.836	30.336	41.5	20.0	JENOL-2
525.4	0	0.5	10661-4	119.898	41.5	10500.0	JENOL-2
526.0	0	0.5	92.987	1.487	41.5	50.0	JENOL-2
527.38	U	0.5	58.98/	1.487	41.5	16.0	JENDL-2
530.52	0	10	243.0	126.5	41.5	/5.0	JENUL-2
540.71	0	0.5	85 4656	3 9556	41.5	40.0	
541.65	0	0.5	89.431	7.93	41.5	40.0	JENOL-2
543.08	Ō	1.0	58,1324	11.6324	41.5	5.0	JENDL - 2
545.85	Ō	0.5	1178.85	17.3494	41.5	1120.0	JENDL-2
547.14	0	0.5	843-285	1.7846	41.5	800.0	JENOL-2
549.67	Ð	1.0	60.1984	11-6984	41.5	7.0	JENDL-2
550.5	0	0.5	61.3538	16.8538	41.5	3.0	JENOL-2
554.13	0	0.5	1233.25	51.75	41.5	1140.0	JENOL-2
555.72	C	0.5	446.358	4.8578	41.5	400.0	JENOL-2
559.10	U	1.0	03.4003	26.9653	41.5	21.0	JENOL-2
564 03	U	0.5	2/4.030	53-138	41.5	180.0	JENUL-2
565.81	0	0.5	60.5778	3./100 14 0778	41.5	2.0	
571.11	ñ	1.0	83.026	8.526	41.5	33.0	IENOL-2
574.0	õ	a	419.132	157.632	41.5	220.0	LIENOL-2
575.77	ō	1.0	66.957	39.457	41.5	8.0	JENDL-2
578.0	0	0.5	79.9784	2.4784	41.5	36.0	JENOL-2
579.04	0	1.0	55.3076	6.8076	41.5	7.0	JENOL-2
584.81	0	0.5	322.194	0.694	41.5	280.0	JENOL-2
588.09	٥	1.0	62 6697	11.1697	41.5	10.0	JENOL - 2
589.94	0	0.5	441.996	0.4956	41.5	4D0.D	JENOL - 2
593.52	U	0.5	48.6724	3.1724	41.5	4.0	JENOL -2
597.35	U	1.0	55.026	0.526	41.5	5.0	JENOL-2
590.04 604.01	U a	0.5	59//.32	20.010	41.5	2912.0	
607.64	0	1.0	03.00UD	2 9 +03UD 9 6496	41.5	ט.ט ר ר	JENUL-2
609.29	n n	1.0	63.6973	15.5973	41.5	5.5	IENDI - 2
612.8	õ	0.5	64.2242	8.7242	41.5	14.0	JENOL -2
620.48	õ	1.0	58.6645	11.7645	41.5	5.4	JENOL -2
622.59	õ	1.0	61.0156	9.7156	41.5	9.5	JENOL -2
625.17	0	1.0	56 . 7989	7.7989	41.5	7.5	JENDL-2
628.21	0	0.5	52.681	2.181	41.5	9.0	JENOL-2
632.97	0	0.5	3875.21	33.706	41.5	3800.0	JENOL-2
636.47	0	0.5	65.431	7.931	41.5	16.0	JENOL - 2
639.28	0	1.0	56.6869	9.1869	41.5	6.0	JENOL-2
641.42	0	0.5	522.194	0.694	41.5	480.0	JENOL-2
D44.94	U	1.0	50.3161	5.0161	41.5	3.0	JENUL-2
658 20	U C	1.5	242-98/	1.40/	41.5	200.0	JENUL-2
000.25	U	1.0	141.133	60.00	=1.5	13.0	JENUL-2

Pu-	2	4	0
-----	---	---	---

.

ENERGY (EV)	L	L	TOTAL WIDTH (MEV.)	NEUTRON HIDTH	Gamma Width (mev)	FISSION WIDTH (MEV)	REFERENCE
-4.099	0	0.5	34.0582	4.0492	30.0	0.009	JENDI -2
1.056	õ	0.5	32.0457	2.44	29.6	0,0057	JENDL-2
20.46	ō	0.5	32.42	2.2	30.0	0.22	JENOL - 2
38.34	Ō	0.5	47.22	17.0	30.0	0.22	JENOL -2
41.64	0	0.5	48.72	15.5	33.0	0.22	JENOL-2
66.66	0	0.5	81-22	50.0	31.0	0.22	JENDL - 2
72.83	0	0.5	53.22	21.0	32.0	0.22	JENUL-2
90.78	0	0.5	42.52	3.2	29.5	0.22	JENUL-2
105.05	0	0.5	78.72	43.0	35.5	0.22	JENOL-2
121.67	ō	0.5	44.22	14.5	29.5	0.22	JENOL-2
130.9	0	0.5	30.41	0.19	30.0	0.22	JENDL-2
135.3	0	0.5	47.72	18.0	29.5	0.22	JENOL-2
151.9	0	0.5	44.12	14.4	29.5	0.22	JENDL-2
162.7	0	0.5	38.72	9.0	29.5	0.22	JENUL-2
185.8	0	0.5	44.02	16.2	29.5	0.22	JENOL-2
192.2	õ	0.5	30.52	0.3	30.0	0.22	JENDL -2
199.6	0	0.5	30.72	1.0	29.5	0.22	JENOL-2
239.3	0	0.5	42.82	13.1	29.5	0.22	JENOL-2
260.5	0	0.5	55-42	23.2	32.0	0.22	JENOL-2
287.1	0	0.5	155.22	125.0	30.0	0.22	JENOL-2
318.5	U	0.5	3/-12 35 92	6.2	29.3	0.22	JERUL-2
320.9	n	0.5	49.42	19.7	29.5	0.22	JENOL-2
338.4	õ	0.5	37.12	7.4	29.5	0.22	JENOL-2
346-0	0	0.5	47.42	17.7	29.5	0.22	JENOL-2
363.7	0	0.5	67.72	32.5	35.0	0.22	JENOL-2
372.0	0	0.5	44.42	14.7	29.5	0.22	JENOL-2
405-0	U	0.5	137+72	108-0	29.5	0.22	JENUL-2
446.2	n	0.5	32.42	2.2	30.0	0.22	JENOL -2
449.8	õ	0.5	49.42	19.7	29.5	0.22	JENOL-2
466.4	σ	0.5	33-12	3.4	29.5	0.22	JENOL-2
473.2	0	0.5	34.52	4.8	29.5	0.22	JENOL - 2
493.9	0	0.5	30.32	8.6	29.5	0.22	JENOL-2
499.3	0	0.5	44.5/	19.3	25.05	0.22	JENUL-2
526.1	ő	0.5	33.76	4.04	29.5	0.22	JENDI-2
530.8	ō	0.5	30.42	0.7	29.5	0.22	JENOL-2
546-4	0	0.5	60.72	31.0	29.5	0.22	JENOL-2
553.2	0	0.5	49.92	20.2	29.5	0.22	JENOL-2
566.3	0	0.5	61.22	31.5	29.5	0.22	JENOL-2
596.8	0	0.5	3U.00	57 5	29.5	0.22	JENUL-2
608.0	ő	0.5	45.945	22,685	23.2	0.06	JENOL -2
632.0	Ō	0.5	36.964	13.324	23.2	0.44	JENOL-2
637.0	0	0.5	34.98	11.61	23.2	0.17	JENOL-2
665.0	0	0.5	220.697	197.017	23.2	0.48	JENOL-2
712 1	0	0.5	50.018	26-038	23.2	0./8	JENOL-2
743.0	a	0.5	27.209	1.009	23.2	3.0	JENOL-2
750.0	ō	0.5	104.091	68.191	23.2	12.7	JENOL - 2
759.0	Э	Ũ.5	30.681	6.061	23.2	1.42	JENDL-2
778.3	0	0.5	124.4	1.2	23.2	100.0	JENDL-2
791 0	Ű	0.5	14/6-0	2-8	23.2	12 5	JENUL-2
810.5	n n	0.5	248.955	214.155	23.2	12.5	JENUL-2
819.9	õ	0.5	35.2901	10.9981	23.2	1.1	JENDL-2
845.6	Ō	0.5	34.31	10.18	23.2	0.93	JENOL-2
054.9	Ō	0.5	71.454	47.954	23.2	0.3	JENOL - 2
8/6-5	0	0.5	38.071	13.911	23.2	U-96	JENOL-2
904-0	U N	0.5	45,819	94+323 21.949	23.2	0.67	JENUL-2
909.0	0	0.5	102.252	78.992	23.2	0.06	JENDL-2
915.3	Ō	0.5	59.756	35 996	23.2	0.56	JENOL-2
943-5	0	0.5	146.353	122.833	23.2	0.32	JENOL-2
958-4	0	0.5	94.008	71.498	23.2	0.19	JENOL-2
979.2	U	0.5	104-005	80 - 395 7 104	23.2	U-4]	JENUL-2
1001.8	n	0.5	122.449	98.129	23.2	1.12	JENOL-2
1024.1	ō	0.5	34.72	5.0	29.5	0.22	JENDL-2
1041.6	0	0.5	36-919	12.589	23.2	1.13	JENDL-2
1045.7	0 Q	0.5	33.72	4.0	29.5	0.22	JENDL-2
10/2.6	U	0.5	132.917	109+407	23.2	0.31	JENOL-2
1115.7	Ő	0.5	32.32	2.6	29.5	0.23	JENOL -2
1129.0	õ	0.5	73.295	49.395	23.2	D.7	JENOL-2
1134-0	0	0.5	30.535	6.735	23.2	0.6	JENDL-2
1143.0	0	0.5	63.89	40.57	23.2	0.12	JENDL-2
1159-0	U	0.5	45-609	22.129	23.2	0.20	JENUL-2
1191.0	0	0.5	138.461	114.921	23.2	0.34	JENOL-2
1208.9	õ	0.5	86.239	62.909	23.2	0.13	JENDL -2
1228.0	0	0.5	39.72	10.0	29.5	0.22	JENDL-2
1236-5	0	0.5	35.04	11.25	23.2	0.59	JENDL-2
		0.5	101+004	/0.0/4	23-2	1.79	JENUL-2

P	u-	2	4	0

ENERGY (EV)	L	J	total Width (NeV)	NEUTRON WIDTH (HEV)	Gahna W1Dth (MeV)	FISSION HIDTH (MEV)	REFERENCE
1281.4	0	0.5	34.02	4.3	29.5	D.22	JENDL-2
1300.3	۵	0.5	269-581	244.911	23-2	1-47	JENDL-2
1328.1	D	0.5	393 . 336	369 296	23.2	0.64	JENOL-2
1345.D	0	0.5	49-709	26-039	23-2	0.47	JENOL-2
1350.9	0	0.5	38-02	U.J 7 304	29-5	0.22	JENUL-2
1303.0	0	0.5	31+204 88-868	64.568	23.2	1.1	JENDL-2
1389.0	õ	0.5	42.362	14.162	23.2	5.0	JENDL-2
1402.2	Ō	0.5	2028.44	5.24	23.2	2000.0	JENOL-2
1408.5	0	0.5	1524.29	1.09	23.2	1500.0	JENOL-2
1426.0	0	0.5	65.13	36.63	23.2	5.3	JENOL-2
1429.0	0	0.5	39.926	15.126	23.2	1.6	JENOL-2
1450.0	U	0.5	90-212	03.592	23.2	3.42	JENUL-2
1481.2	0	0.5	34.145	9.245	23.2	1.7	JENDL-2
1540.7	õ	0.5	130.72	101.0	29.5	0.22	JENOL-2
1549.5	Ō	0.5	186-42	156.7	29.5	0.22	JENOL-2
1563.7	9	0.5	144.42	114.7	29.5	0-22	JENOL-2
1575.3	0	0.5	149-952	126.242	23.2	0.51	JENOL-2
1609-6	0	0.5	59.229	34,909	23.2	1.12	JENOL-2
1621.4	U	0.5	580+32	28.6	29.5	0.22	JENUL-2
1662.6	0	0.5	93.62	63.9	29.5	0.22	JENOL-2
1688.0	ō	0.5	57.138	32.868	23.2	1.07	JENOL-2
1724-0	Ō	0.5	108.817	83.457	23-2	2.16	JENOL-2
1741-6	0	0.5	49.072	25.042	23.2	0.83	JENOL-2
1764.0	0	0.5	75.51	51.66	23.2	0.65	JENOL-2
1771.4	0	0.5	39.52	9.8	29.5	0.22	JENUL-2
1841.0	0	0.5	159.617	125.717	23.2	10.7	JENOL-2
1853.0	õ	0.5	61.787	34.437	23.2	4.15	JENDL-2
1873.0	0	0.5	105-578	77.468	23.2	4.91	JENDL-2
1901-0	0	0.5	235-482	209.282	23.2	3-0	JENOL-2
1916.6	0	0.5	129-103	35,903	23.2	70.0	JENOL-2
1936-0	U	0.5	2225.10	1+90	23.2	2200.0	JENUL-2
1944.0	0	0.5	32.936	7,936	23.2	1.8	JENOL-2
1949-1	ŏ	0.5	112.077	82.577	23.2	6.3	JENOL-2
1956-2	0	0.5	309-204	261.004	23.2	25.0	JENOL-2
1973.0	0	0.5	92 - 96	67.96	23.2	1.8	JENDL-2
1991.5	0	0.5	144.22	114.5	29.5	0.22	JENOL-2
2016 7	U	0.5	30+32 78,363	5.0	29.5	2.64	JENUL-2
2022.9	ő	0.5	85.22	55.5	29.5	0.22	JENDL-2
2033.4	ō	0.5	134.465	101.475	23.2	9.79	JENOL - 2
2056-0	0	0.5	97.398	68 - 468	23.2	5.73	JENOL-2
2082.8	0	0.5	128.52	98-8	29.5	0.22	JENDL-2
2110.7	0	0.5	43,42	13.7	29.5	0.22	JENUL-2
2134.0	0	0.5	115.32	14-307	23.2	0.22	JENDI-2
2198-2	ŏ	0.5	159.72	130.0	29.5	0.22	JENOL-2
2240.6	0	0.5	63.82	34.1	29.5	0.22	JENOL-2
2256.6	0	0.5	164-22	134.5	29.5	0.22	JENDL-2
2277.9	0	0.5	456.72	427.0	29.5	0.22	JENDL-2
2290.7	0	0.5	230+22 45 92	208-5	29.5	0.22	JENUL-2
2334.4	õ	0.5	66.32	36.6	29.5	0.22	JENOL-2
2350.9	Ď	0.5	61.32	31.6	29.5	0.22	JENDL-2
2365-8	0	0.5	270.72	241.0	29.5	6.22	JENOL-2
2373.4	0	0.5	39.44	9.74	29.5	0.2	JENOL-2
2305-1	U n	0.5	40.42	10./	29.5	0.22	JENUL-2
2416.0	0	0.5	94.62	64.9	29.5	0.22	JENOL-2
2434.3	ō	0.5	234.72	205.0	29.5	0.22	JENOL-2
2459.4	0	0.5	55.32	25.6	29.5	0.22	JENDL-2
2470.8	0	0.5	75.22	45.5	29.5	0.22	JENOL-2
2485.3	0	0.5	50.92	21.2	29.5	0.22	JENUL-2
2521.0	ů n	0.5	317.22	297 5	29.5	0.22	JENDL-2
2549.2	ŏ	0.5	109.42	79.7	29.5	0.22	JENOL-2
2575.3	0	0.5	71.398	47.718	23.2	0.48	JENDL-2
2639.5	0	0.5	460-587	425.867	29.5	5.22	JENDL-2
2652.0	0	0.5	74.223	36.563	23.2	14.46	JENDL-2
2092.8	0	0.5	531-905	344 - /05	23.2	104.0	JENDL-2
2739.2	0	0.5	208.24	177.0	29.5	1.74	JENDL-2
2748.4	ō	0.5	136-629	102.259	23.2	11.17	JENDL-2
2817.6	0	D.5	66-594	41-414	23.2	1.98	JENOL-2
2843.5	0	0.5	160 705	156.015	23.2	0.69	JENDL-2
2000.0	U n	U-5	53.284	27.274	23.2	2.01	JENOL-2
2895.6	n	0.5	89.72	60.0	29.5	0.22	JENOL -2
2905.0	ŏ	0.5	144.72	115.0	29.5	0.22	JENOL - 2
2938.0	0	0.5	161.72	132.0	29.5	0.22	JENDL-2
2968.6	0	0.5	114.72	85.0	29.5	0.22	JENDL-2
2980.5	0	0.5	137.72	108.0	29.5	0.22	JENUL-2
2300.2	U	0.5	42-22	12.0	23.0	0-22	

Pu-240

ENERGY (EV	L	L	TOTAL HIDTH (Hev)	NEUTRON WIDTH (MEV)	GANNA WIOTH (NEV)	FISSION WIDTH	REFERENCE
2994.7	0	0.5	85.72	56.0	29.5	0.22	JENOL-2
3004.0	Ō	0.5	106.22	76.5	29.5	0.22	JENOL-2
3018.0	D	0.5	146.72	117.0	29.5	0.22	JENDL-2
3029.0	0	0.5	50.72	21.0	29.5	0.22	JENDL-2
3054.7	D	0.5	76.72	47.0	29.5	0.22	JENDL-2
3077.4	0	0.5	157.72	128.0	29.5	0.22	JENUL-2
3088.0	0	0.5	64 • /2 69 00	33.0	29.5	0.22	JENUL-2
3172.5	n n	0.5	254.72	225.0	29.5	0.22	JENOL-2
3192.5	Ö	0.5	378.72	349.0	29.5	0.22	JENOL-2
3237.5	0	0.5	101.72	72.0	29.5	0.22	JENDL-2
3268 .5	0	0.5	163.72	134.0	29.5	0.22	JENDL-2
3332.0	0	0.5	44.22	14.5	29.5	0.22	JENDL-2
3423.0	0	0.5	64.22	34.5	29.5	0.22	JENUL-2
3455 5	0	0.5	9/./2	344 0	29.5	0.22	JENDL-2
3493.5	ő	0.5	94.72	65.0	29.5	0.22	JENOL-2
3555.0	ő	0.5	120.72	91.0	29.5	0.22	JENOL-2
3567.5	0	0.5	191.72	162.0	29.5	0.22	JENOL-2
3595.0	0	0.5	58.22	28.5	29.5	0.22	JENOL-2
3657.0	0	0.5	322.72	293.0	29.5	0.22	JENDL-2
3000.0	U	0.5	84.22	54.5	29.5	0.22	JENUL-2
3723.0	n n	0.5	89.72	60.0	29.5	0.22	JENOL-2
3800.0	õ	0.5	130.72	101.0	29.5	0.22	JENOL-2
3844.0	ō	0.5	105.72	76.0	29.5	0.22	JENDL-2
3852.0	0	0.5	127.72	98.0	29.5	0.22	JENDL-2
3872.0	0	0.5	75.72	46.0	29.5	0.22	JENOL-2
3900-0	0	0.5	236.72	209.0	29.5	0.22	JENUL-2
3954.0	n	0.5	192 . 72	92.0	29.5	0.22	JENDL-2
3975.0	õ	0.5	131.72	102.0	29.5	0.22	JENDL-2
3990.0	0	0.5	58.72	29.0	29.5	0-22	JENDL-2
4031.0	0	0.5	138-72	109.0	29.5	0.22	JENDL-2
4084-0	0	0.5	149.72	120.0	29.5	0.22	JENOL-2
4100.0	U	0.5	286 - 72	257.0	29.5	0.22	JENUL-2
4134.0	ŭ	0.5	96.72	67.0	29.5	0.22	JENOL-2
4149.0	õ	0.5	294.72	265.0	29.5	0.22	JENOL-2
4161.0	0	0.5	118.72	89.0	29.5	0.22	JENDL-2
4203.0	0	0.5	467 - 72	438-0	29.5	0.22	JENOL-2
4221.0	0	0.5	97.72	68.C	29.5	0.22	JENOL-2
4270.0	Ŭ	0.5	100 - 72	316.0	29.5	0.22	JENUL-2 IFNOL-2
4329.0	ŏ	0.5	331.72	302.0	29.5	0.22	JENDL-2
4376-0	Ō	0.5	111.72	82.C	29.5	0.22	JENDL-2
4386.0	0	0.5	61.72	32.0	29.5	0.22	JENOL-2
4398.0	0	0.5	107.72	78.0	29.5	0.22	JENDL-2
4422.0	U	0.5	90.72	61.0	29.5	0.22	JENUL-2
4458.0	0	0.5	131.72	102.0	29.5	0.22	JENDL-2
4570.0	ō	0.5	249.72	220.0	29.5	0.22	JENDL-2
4588.0	0	0.5	555.72	526.0	29.5	0.22	JENDL-2
4599.0	0	0.5	104.72	75.0	29.5	0.22	JENDL-2
4615-0	U	0.5	291.72	262-0	29.5	0.22	JENUL-2
4721.0	n	0.5	539.72	510.0	29.5	0.22	JENDL-2
4745.0	ŏ	0.5	274.72	245.0	29.5	0.22	JENOL-2
4755.0	0	0.5	85.72	56.0	29.5	0.22	JENDL-2
4766.0	0	0.5	-44.72	15.0	29.5	0.22	JENDL-2
4771.0	0	0.5	51.72	22.0	29.5	0.22	JENUL-2
4792.0	n	0.5	162.72	133.0	29.5	0.22	JENDL-2
4812.0	õ	0.5	201.72	172.0	29.5	0.22	JENOL-2
4823.0	0	0.5	92.72	63.0	29.5	0.22	JENDL-2
4894.0	0	0.5	88.72	59.0	29.5	0.22	JENOL-2
4958-0	0	0.5	320.72	291.0	29.5	0.22	JENDL-2
4903.0	U n	0.5	10/+/2	92.0	29.5	0.22	JERUL-2
5072.0	ŏ	0.5	538.72	509.0	29.5	0.22	JENOL-2
5113.0	0	0.5	122.72	93.0	29.5	0.22	JENOL-2
5134.0	D	0.5	71.72	42.0	29.5	0.22	JENOL-2
5148-0	0	0.5	79.72	50.0	29.5	0.22	JENDL-2
5194.0	0	0.5	342.72	40.0 313.0	29.5	0.22	JENOL-2
5215.0	ŏ	0.5	192.72	163.0	29.5	0.22	JENOL -2
5249.0	Ō	0.5	553.72	524.0	29.5	0.22	JENDL-2
5279.0	0	0.5	169.72	140.0	29.5	0.22	JENDL-2
5299-0	0	0.5	299.72	270-0	29.5	0.22	JENDL-2
5350.0	U N	0.5	232+72	203-0	23.5 29.5	0.22	JERUL-2
5367.0	ŏ	0.5	99.72	70.0	29.5	0.22	JENOL-2
5393.0	0	0.5	113.72	84-0	29.5	0.22	JENDL-2
5417.0	0	0.5	284.72	255.0	29.5	0.22	JENOL-2
5409-0	U N	0.5	79.72	50-0 87-0	29.5	0.22	JENUL-2 JENUL-2
5510.0	0	0.5	384.72	355.0	29.5	0.22	JENOL-2
L							1

Pu-2	240
------	-----

ENERGY (EV)	L	Ļ	TOTAL HEDTH	NEUTRON WIDTH	Ganna Width (MeV)	FISSION WIDTH (MEV)	REFERENCE
5522.0	0	0.5	201.72	172-0	29.5	0.22	JENOL-2
5544.0	0	0.5	611.72	582.0	29.5	0.22	JENDL-2
5574.0	0	0.5	787.72	758.0	29.5	0.22	JENOL-2
5592.0	D	0.5	236.72	207.0	29.5	0.22	JENOL-2
5615.0	0	0.5	91.72	62.0	29.5	0.22	JENDL-2
5681.0	0	0.5	135.72	106.0	29.5	0.22	JENOL-2
5692.0	0	0.5	120.72	91-0	29.5	0.22	JENOL-2

Pu-	2	4	1
-----	---	---	---

ENERGY (EV)	L	j	TOTAL WIDTH (MEV.)	NEUTRON WIDTH (MEV)	CANNA HIDTH	FISSION WIDTH (MEV)	REFERENCE
-0.209	D	3.0	132+063	0.063	35.0	97.0	JENDL-2
0.257	D	3.0	132.051	0.05143	35.0	97.0	JENDL-2
4.28	0	3.0	95.69	0.69	50.0	45.0	JENOL-2
4.58	U	2.0	1339 24	0.42	49.0	135.0	JENUL-2
6.93	0	3.0	155.72	0.72	35.0	120.0	IENOL-2
8.62	D D	3.0	141.94	0.94	41.0	100.0	JENOL-2
9.57	D	2.0	385.528	0.528	35.0	350.0	JENOL-2
10.06	0	2.0	63 6 .32	1.32	35.0	600-0	JENOL-2
12.79	0	3.0	280.677	0.67714	50.0	230.0	JENOL-2
13.42	U	2.0	123.55	3.55	60.0	50-0 130 0	JENOL-2
15.97	0	3.0	556 42	1 42	40.U 35.0	520.0	IENDI -2
16.67	D	2.0	227.28	1.28	42.0	184.0	JENOL-2
17.85	Ō	2.0	64.98	2.9B	39.0	23.0	JENOL-2
18.22	0	2.5	75.15	0.15	35.0	40.0	JENOL-2
20.69	0	3.0	105.309	0.30857	43.0	62.0	JENOL-2
21.05	0	2.5	335.01	0.01	35.0	300.0	JENOL-2
21.91	0	2.5	10.17	0.09571	50.0	20.0	JENUL-2
23.7	n	2.5	380.39	0.30377	55.0	325.0	IENOL-2
24.04	ō	3.0	127.183	1.18286	46.0	80.0	JENOL-2
24.61	0	2.5	549.15	0.15	40.0	509.0	JENOL-2
26.39	ō	3.0	313.857	3.85714	45.0	265.0	JENOL-2
28.89	0	2.0	700.76	5.76	40.0	655.0	JENOL-2
29.42	U	1.U 1.U	123.4/1	0.4/143	4U+U 56 0	241 0	JENUL-2
32.5	n	2.5	2541.0	1.0	40.0	2500.0	JENDL-2
33.3	õ	2.5	160.17	0.17	40.0	120.0	JENOL-2
33.77	0	2.5	140.3	0.3	40.0	100-0	JENOL - 2
34.9	D	2.5	1142-07	2.07	40.0	1100.0	JENOL-2
34.98	D	2.5	55.41	0.41	40.0	15.0	JENOL-2
37.5	U	2.5	240 5	0.15	40.0	500.0	JENUL-2
39.35	0	2.5	201.49	1.49	40.0	160.0	JENOL - 2
39.89	D	2.5	154.59	1.59	53.0	100.0	JENOL - 2
40.87	D	2.5	1042.12	2.12	40.0	1000-0	JENOL-2
42.77	D	2.5	240.28	0.28	40.0	200.0	JENOL - 2
43.45	0	2.5	70,25	0-25	40.0	30.0	JENOL-2
48.11	0	2.5	626.2	6.2	40.0	580.0	IENOL-2
50.35	ō	2.5	540.69	0.69	40.0	500.0	JENDL - 2
52.07	0	2.5	140-04	0.04	40.0	100.0	JENOL-2
58.37	0	2.5	621.75	1.75	40.0	580.0	JENOL-2
59.28	0	2.5	582-2	2.2	40.0	540-0	JENOL - 2
62.25	0	2.5	644.62	4.62	40.0	600.0	I JENDL-2
63.C	ŏ	2.5	1242.0	2.0	40.0	1200.0	JENOL-2
64.52	0	2.5	316.25	0.25	40.0	276.0	JENOL-2
65.68	0	2.5	344.26	5.26	39.0	300.0	JENOL-2
50.55	U	2.5	243.04	3.04	40.0	200.0	JENUL-2
69.18	0	2.5	160.7	0.7	40.0	120.0	JENOL-2
71.77	ō	2.5	100.07	0.07	53.0	47.0	JENOL -2
72.17	0	2.5	411.53	1.53	40.0	370.0	JENOL-2
73.8	0	2.5	53.5	0.5	40.0	13.0	JENOL-2
75.94	U	2.5	159.75	4./6	52.0	103-0	JENUL-2
77.73	n	2.5	1698.7	1.7	50.0	1637.0	JENOL-2
80.14	õ	2.5	124.87	4.87	40.0	80.0	JENOL-2
B1.36	C	2.5	261.9	6.9	40.0	215.0	JENOL-2
81.98	0	2.5	1017.9	2.9	40.0	975.0	JENDL-2
85.25	0	2.5	118.02	5.02	40.0	73-0	JENUL-2
85.67	n	2.5	272.8	2.8	40.0	230.0	JENOL-2
86.0	õ	2.5	350.72	0.72	40.0	310.0	JENOL -2
86.93	0	2.5	130.4	7.4	43.0	80.0	JENOL-2
87.8	0	2.5	322.35	2.35	40.0	280.0	JENOL-2
89,12	0	2.5	792.23	2.23	40.0	750.0	JENOL-2
91.4	0	2.5	60.1	1.7	40-0	21.0	JENUL-2
91.68	õ	2.5	60.12	0.12	35.0	25.0	JENOL - 2
93.77	D	2.5	296.4	0.4	46-0	250.0	JENOL-2
95.24	0	2.5	683.6	0.6	40-0	643.D	JENOL - 2
96.18	0	2.5	1041.5	1.5	40.0	1000.0	JENOL-Z
98.28	n	2.5	+33-00 193.28	7.28	40.0	459.0 146.0	JENUL-2
99.74	ŏ	2.5	350.16	2.16	18.0	330.0	JENOL-2
100.5	0	2.5	55.6	1.3	40.0	14.3	JENOL - 2
101.42	0	2.5	147.61	1.61	72.0	74.0	JENOL - 2
102.33	0	2.5	58.7	1.4	40.0	17.3	JENOL - 2
107.54	n	2.5	41.2	0.5	40.0	0.7	JENDL-2
107.85	ō	2.5	92.2	1.2	40.0	51.0	JENOL-2
109.05	0	2.5	491.92	1.92	40.0	450.0	JENOL - 2
110-2	Û	2.5	791-45 96 75	0.45	40.0	751.0	JENOL-2
112.12	U	2.3	60.10	0.75	₩ U-U	4D.U	

Pu-	2	4	1	
			_	

ENERGY (EV)	L	J	TOTAL WIDTH	NEUTRON WIDTH (MEV)	Gamma W10th (Mev I	FISSION WIDTH (MEV)	REFERENCE
115.4	0	2.5	1581.7	1.7	40.0	1540.0	JENOL-2
117.23	0	2.5	357.48	3.48	40.0	314.0	JENOL-2
120.33	0	2.5	545.8	0.8	40.0	505+0	JENOL-2
122.11	0	2.5	465.95	6.95	40.0	419.0	JENOL-2
123.24	0	2.5	101.35	2.35	40.0	59.0	JENOL - 2

Pu-2	4	2
------	---	---

ENERGY (EV)	L	J	TOTAL HIDTH (MEV.)	NEUTRON WIDTH	ORNHA WIDTH	FISSION WIDTH (MEV.)	REFERENCE
2.67	0	0.5	27.387	1.97	25.4	0.017	JENDL-2
14-6	Ō	0.5	24.311	0.061	24.2	0.05	JENDL-2
22.57	0	0.5	2D-336	0.286	20.0	0.05	JENDL-2
40.95	0	0.5	29.501	0.451	29.0	0.05	JENDL-2
53.46	0	0.5	75.0949	51.95	23.9	0.045	JENDL-2
67.6	0	0.5	27.1225	4.578	22.5	0.0445	JENDL-2
88.45	0	0.5	24.8782	D-64	24.2	0.0382	JENDL-2
107.32	U	0.5	38,5394	16.99	21.5	0.0494	JENDL-2
131.4	0	0.5	37.0335	0.110	30.0	0.0635	JENUL-2
141.43	0	0.5	24.309	14 24	24.2	0.05	JENUL-2
163.5	ñ	0.5	24.787	0.537	24.2	0.05	JENDI -2
204.8	õ	0.5	73.5847	52.73	20.8	0.0548	JENDL-2
210.0	ō	0.5	24.74	0.424	24.2	0.116	JENOL-2
215.3	0	0.5	41,384	5.2	36.0	0.184	JENDL-2
219.3	0	0.5	24,606	0.29	24.2	0.116	JENDL-2
232.7	0	0.5	33.071	4.94	28.0	0.131	JENDL-2
264.5	0	0.5	24.697	0.381	24.2	0.116	JENDL-2
271.95	0	0.5	24.481	0.165	24.2	0.116	JENDL-2
273.8	0	0.5	39.332	15.43	23.8	0.102	JENDL-2
274.75	0	0.5	24.486	0.17	24.2	0.116	JENDL-2
201.05	U	0.5	24.445	U.[]	24.2	0.116	JENUL-2
230+/	U	0.5	39.920	0.31	20.0	0.110	JENUL-2
319.9	U n	0.3	256.478	232.9	22.5	0.007	FNDL-2
327.6	U N	0.5	230.470	2J2.5 0.5	23.3	0.116	JENDL-2
332.4	n	D.5	107.822	77.21	30.5	0.112	JENDL-2
374.3	õ	0.5	30.696	6.38	24.2	0.116	JENOL-2
379.63	õ	0.5	24.586	0.27	24.2	0.116	JENDL-2
382.2	Ď	0.5	68.0247	44.68	23.26	0.0847	JENDL-2
396 . 1	D	0.5	26.816	2.5	24.2	0.116	JENOL-2
399.9	0	0.5	25-936	1.62	24.2	0.116	JENDL-2
410.6	0	0.5	31-646	7.33	24.2	0.116	JENDL-2
424.1	0	0.5	28-546	4.23	24.2	0.116	JENOL-2
425.15	0	0.5	24.596	0.28	24.2	0.116	JENDL-2
473.7	0	0.5	25.106	0.79	24.2	0.116	JENDL-2
482.5	0	0.5	44-502	20-27	23.5	0.732	JENDL-2
494.75	0	0.5	24.586	0.27	24.2	0.116	JENDL-2
503.9	U	0.5	1/4.305	150.0	24.2	0.186	JENUL-2
530.0	0	0.5	121-1//	74.0	21.0	0.104	JENUL-2
576 1	0	0.5	54 316	30.0	23.0	0.115	JENOL-2
595.0	0	0.5	53.0611	32.04	24.2	0.0211	JENOL-2
599.8	ñ	0.5	33.412	9.11	24.2	0.102	JENDI -2
610.8	õ	0.5	36.214	11.95	24.2	6.399-2	JENGL-2
638-5	õ	0.5	28.65	4.41	24.2	0.04	JENDL-2
665.0	D	0.5	26-966	2.7	24.2	0.066	JENDL-2
669.3	0	0.5	37.432	13.14	24.2	9.199-2	JENDL-2
693.2	0	0.5	61.052	38.65	22.0	0.402	JENDL-2
711.6	0	0.5	141-233	121.57	19.5	0.163	JENDL-2
727.6	0	0.5	27.42	3.17	24.2	0.05	JENOL-2
736.7	0	0.5	126.566	101.59	24.2	0.776	JENDL-2
755.1	D	0.5	159.623	135.4	21.5	2.723	JENOL-2
761-2	U	0.5	208-24	4.14	24.2	1/9.9	JENUL-2
704.0	U	0.5	0/ .2/4	205 5	24.2	1.0/4	JENUL-2
824.5	0	0.5	230.057	4 65	24.2	0.043	JENDL-2
837.7	n	0.5	57.491	37.45	20.0	0.041	IFNDL-2
856.6	ň	0.5	57.441	35.9	22.0	0,141	JENDL-2
865.6	õ	0.5	34.553	10.31	24.2	0.043	JENDL-2
878.1	Ō	0.5	83.0469	58.82	24.2	0.027	JENDL-2
886.5	0	0.5	51.7555	22.74	29.0	0.0155	JENDL-2
923.2	0	0.5	77.4789	59.45	18.0	0.029	JENDL-2
935.4	0	0.5	35.25	11.0	24.2	0.05	JENDL-2
939.6	O	0.5	34.25	10.0	24.2	0.05	JENDL-2
949 - 1	0	0.5	40.05	14.0	26.0	0.05	JENDL-2
977.9	0	0.5	38.75	14.5	24.2	0.05	JENDL-2
1004-0	0	0.5	67.2499	43.0	24.2	0.05	JENDL*2
1030-0	U	0.5	/0+2499	40-U	24.2	0.05	JENUL-2
1043.0	0	0.5	192.20	33 0	24.2	0.05	JENDL-2
1087.5	0	0.5	224.25	200 0	24.2	0.05	FN0L-2
1117.0	0	0.5	29.25	5.0	24.2	0.05	JENDL-2
1129.5	ň	0.5	34.25	10.0	24.2	0.05	JENDL-2
1148.0	ñ	0.5	324.25	300.0	24.2	0.05	JENDL-2
1182.5	õ	0.5	37.25	13.0	24.2	0.05	JENDL-2
1197.0	Ō	0.5	119.25	95.0	24.2	0.05	JENDL-2
1207.0	0	0.5	64.2499	40-0	24.2	0.05	JENDL-2
1248.0	U		22.05	9.0	24.2	0.05	JENOL-2
	0	0.5	33.25	-		a ar	
1267.0	0	0.5 0.5	51.25 51.25	27.0	24.2	0.05	JENDL-2
1267.0 1286.0	0 0 0	0.5 0.5 0.5	51.25 51.25 83.2499	27.0 59.0	24.2 24.2	0.05	JENDL-2 JENOL-2
1267.0 1286.0 1696.0	0 0 0 0	0.5 0.5 0.5 0.5	33-25 51-25 83-2499 63-3609	27.0 59.0 39.1	24.2 24.2 24.2	0.05 0.05 0.061	JENDL-2 JENOL-2 JENOL-2
1267.0 1286.0 1696.0 1708.0	0 0 0 0 0	0.5 0.5 0.5 0.5	51-25 51-25 83-2499 63-3609 117-401	27.0 59.0 39.1 93.2	24.2 24.2 24.2 24.2	0.05 0.05 0.061 0.001	JENDL-2 JENOL-2 JENOL-2 JENOL-2 JENOL-2
1267.0 1286.0 1696.0 1708.0 1708.0		0.5 0.5 0.5 0.5 0.5	53.25 51.25 83.2499 63.3609 117.401 33.385	27.0 59.0 39.1 93.2 9.1	24.2 24.2 24.2 24.2 24.2 24.2 24.2	0.05 0.05 0.061 0.001 0.005	JE NOL - 2 JE NOL - 2 JE NOL - 2 JE NOL - 2 JE NOL - 2
1267-0 1286-0 1696-0 1708-0 1737-0 1739-0		0.5 0.5 0.5 0.5 0.5 0.5	33.25 51.25 83.2499 63.3609 117.401 33.385 45.789	27.0 59.0 39.1 93.2 9.1 21.5	24.2 24.2 24.2 24.2 24.2 24.2 24.2	0.05 0.05 0.061 0.001 0.085 0.089	JENOL - 2 JENOL - 2 JENOL - 2 JENOL - 2 JENOL - 2 JENOL - 2
1267.0 1286.0 1696.0 1708.0 1737.0 1739.0 1751.0		0.5 0.5 0.5 0.5 0.5 0.5	33.25 51.25 83.2499 53.3609 117.401 33.385 45.789 33.685	27.0 59.0 39.1 93.2 9.1 21.5 9.4	24.2 24.2 24.2 24.2 24.2 24.2 24.2 24.2	0.05 0.05 0.061 0.001 0.085 0.085 0.085	JENOL-2 JENOL-2 JENOL-2 JENOL-2 JENOL-2 JENOL-2 JENOL-2 JENOL-2 JENOL-2

Pu	-242

,

ENERGY (EV)	Ĺ	J	TOTAL WIDTH (MEV)	NEUTRON WIDTH (MEV)	GANNA HIDTH (MEV)	FISSION WIDTH	REFERENCE
1783.0	0	0.5	24.367	0.022	24.2	0.145	JENOL-2
1789.0	0	0.5	25-13	0.13	24.2	0.8	JENOL-2
1806-0	0	0.5	37.212	12.9	24.2	0.112	JENDL-2
1820-0	0	0.5	28.615	4.1	24.2	0.315	JENDL-2
1836.0	0	0.5	117.8	3.0	24.2	90.6	JENDL-2
1862-0	0	0.5	29.508	4.9	24.2	0.408	JENDL-2
1881-0	0	0.5	108-553	84.3	24-2	0.053	JENDL-2
1891-0	0	0.5	29.1	4.1	24.2	0.8	JENDL-2

日立高速印刷納