

JAERI-M

9 9 8 1

NEANDC(J)-80/U

INDC(JAP)-67/L

EVALUATION OF NEUTRON NUCLEAR
DATA FOR SCANDIUM-45

February 1982

Yoshiaki OKA*, Tsuneo NAKAGAWA** and Yasuyuki KIKUCHI

日本原子力研究所
Japan Atomic Energy Research Institute

JAERI-M レポートは、日本原子力研究所が不定期に公刊している研究報告書です。
入手の問合せは、日本原子力研究所技術情報部情報資料課（〒319-11茨城県那珂郡東海村）あて、お申しこしください。なお、このほかに財団法人原子力弘済会資料センター（〒319-11 茨城県那珂郡東海村日本原子力研究所内）で複写による実費頒布をおこなっております。

JAERI-M reports are issued irregularly.

Inquiries about availability of the reports should be addressed to Information Section, Division of Technical Information, Japan Atomic Energy Research Institute, Tokai-mura, Naka-gun, Ibaraki-ken 319-11, Japan.

©Japan Atomic Energy Research Institute, 1982

編集兼発行 日本原子力研究所
印 刷 いばらき印刷株

JAERI-M 9981

Evaluation of Neutron Nuclear Data for ^{45}Sc

Yoshiaki OKA*, Tsuneo NAKAGAWA** and Yasuyuki KIKUCHI

Division of Physics, Tokai Research Establishment, JAERI

(Received January 27, 1982)

Evaluation of neutron nuclear data for ^{45}Sc was performed in the energy range of thermal to 20 MeV. Evaluated quantities are the total, elastic and inelastic scattering, capture, $(n,2n)$, (n,p) and (n,α) reaction cross sections, resonance parameters and angular distributions of emitted neutrons. Resonance parameters are recommended below 100 keV. Particular care was paid for the minimum value of the total cross section near 2 keV, since a mono-energetic neutron filter is now under design by using scandium metal at Fast Neutron Source Reactor YAYOI of The University of Tokyo. Optical and statistical model calculations are performed for the smooth cross sections above resonance region. The results were compiled in the ENDF/B format and they will be stored in the second version of Japanese Evaluated Nuclear Data Library JENDL-2.

Keywords: Evaluation, Scandium-45, Neutron Cross Sections, Resonance Parameters, Angular Distribution, Optical Model, Total Cross Section Minimum, Mono-energetic Filter.

* Nuclear Engineering Research Laboratory, The University of Tokyo

** Data Bank, OECD-Nuclear Energy Agency

^{45}Sc の中性子核データの評価

日本原子力研究所東海研究所物理部
岡 芳明^{*}・中川庸雄^{**}・菊池康之

(1982年1月27日受理)

^{45}Sc の中性子核データを熱中性子領域から20 MeVにわたり評価した。評価した量は、全断面積、弹性散乱、非弹性散乱、捕獲、 $(n, 2n)$, (n, p) , (n, α) 反応断面積、共鳴パラメータおよび放出粒子の角度分布である。共鳴パラメータは100 keV以下の領域で与えた。現在東京大学工学部付属原子力工学研究施設の高速中性子源炉「弥生」において金属Scを用いた単色中性子フィルターを設計しているので、2 keV近傍の全断面積の極小値には特に注意を払った。共鳴領域より上の滑らかな断面積は光学および統計模型に基き評価した。今回の評価結果はENDF/B フォーマットにまとめ、JENDL-2に格納される。

* 東京大学工学部付属原子力工学研究施設

** Data Bank, OECD-Nuclear Energy Agency

Contents

1. Introduction	1
2. Resonance Energy Region	2
2.1 Total Cross Section near 2 keV	2
2.2 Resonance Parameters	2
2.3 Thermal Cross Sections	4
2.4 Connection with the Smooth Cross Section	4
3. Fast Energy Region	5
3.1 Total Cross Section and Optical Model	5
3.2 Capture, Elastic and Inelastic Scattering Cross Section	5
4. Concluding Remarks	6
Acknowledgment	7
References	8

目 次

1. 序論	1
2. 共鳴エネルギー領域	2
2.1 2 keV近傍の全断面積	2
2.2 共鳴パラメータ	2
2.3 熱中性子断面積	4
2.4 滑らかな断面積との接続	4
3. 高速エネルギー領域	5
3.1 全断面積と光学模型	5
3.2 捕獲, 弹性および非弾性散乱断面積	5
4. 結語	6
謝辞	7
参照文献	8

1. Introduction

There is a deep minimum in the total neutron cross section of scandium-45 near 2 keV due to the interference between the resonance and potential scattering. As natural scandium consists of only scandium-45, a mono-energetic neutron filter can be designed with scandium metal for use in measurement of cross sections, energy calibration of neutron detectors and biomedical irradiation^{1,2,3)}. However, no evaluated neutron cross sections of scandium are available at present. Only the (n,γ) cross section was evaluated and presented in the ENDF/B-IV dosimetry file. Even the minimum value near 2 keV has not been well determined.³⁾

There is a project to construct a scandium filter at Fast Neutron Source Reactor YAYOI of The University of Tokyo for biomedical irradiation. The poor knowledge of scandium cross section makes it difficult to estimate the irradiation dose. Hence a new evaluation was made on scandium cross sections. Though much effort was devoted to the evaluation of the minimum near 2 keV, the evaluation was made from 10^{-5} eV to 20 MeV so that the evaluated data should be included in Japanese Evaluated Nuclear Data Library Version 2 (JENDL-2).

The evaluation of the data in the resonance energy region is described in Chapter 2. Chapter 3 reports the result of the fast energy region. Concluding remarks are given in Chapter 4.

2. Resonance Energy Region

2.1 Total Cross Section near 2 keV

There still remains considerable uncertainty in the total cross section value at the minimum near 2 keV.

The value of 0.085 barn based on the early measurements were denied by Liou et al.⁴⁾ who reported that the minimum value of 0.71 ± 0.03 barns at 2.05 keV. On the other hand, Razbudey et al.⁵⁾ reported the value of 0.27 ± 0.07 barns from their reactor beam measurements.

Recently Fujita and Yamamuro³⁾ reported the value of 0.25 ± 0.05 barns which obtained by using a linear accelerator at Research Reactor Institute, Kyoto University (KUR). Later Fujita informed us⁶⁾ that 0.23 ± 0.02 barns was most probable value at 2 keV and his data agreed with those by Liou et al. except in the energy range between 0.5 keV and 3 keV. The present evaluation was based on this result.

2.2 Resonance Parameters

In the present evaluation, we considered the resonance parameters deduced by Liou et al.⁴⁾ from their transmission measurements and those by Kenny et al.⁷⁾ from their capture measurements.

Liou et al. gave the Γ_n and J values for 18 s-wave resonances up to 20.78 keV including two negative ones and the $g\Gamma_n$ values for 5 p-wave resonances. Kenny et al. gave the values of the capture areas and of Γ_γ for many s- and p-wave resonance up to 100 keV.

For the s-wave resonances, we adopted the parameters of Liou et al. up to 20.78 keV assuming the Γ_γ value of 0.41 eV and those of Kenny et al. from 21 keV to 95 keV. The parameters of the two negative resonances were adjusted as will be described later. As to the p-wave

resonances, the present evaluation is based on the resonance areas reported by Kenny et al. except for the lowest 2 levels at 460 eV and 1.06 keV where the parameters of Liou et al. were adopted with the assumed Γ_γ value of 0.41 eV. Kenny et al. also reported the $g\Gamma_\gamma$ values. For most of levels, however, the values of Γ_n became negative when deduced from the reported values of the capture resonance areas and $g\Gamma_\gamma$. Hence we assumed Γ_γ value of 0.5 eV and deduced the Γ_n values.

In the present work, the resonance parameters of the two negative resonances as well as the nuclear radius were so adjusted that the calculated total cross section agreed with the data of Fujita⁶⁾ between 0.5 and 3 keV and that the calculated thermal cross sections agreed with those recommended in BNL-325, 3rd edition⁸⁾. This adjustment was made by using Neutron Data Evaluation System NDES⁹⁾. The finally obtained values are

$$J = 4, E_0 = -330 \text{ eV}, \Gamma_n = 36.7 \text{ eV}, \Gamma_\gamma = 0.41 \text{ eV}$$

$$J = 3, E_0 = -650 \text{ eV}, \Gamma_n = 101.0 \text{ eV}, \Gamma_\gamma = 0.41 \text{ eV}$$

$$R = 4.55 \text{ fm}$$

The resonance parameters are summarized in Table I. The total cross sections calculated from these parameters are presented in Figs. 1 ~ 4 together with the experimental data by Liou et al.

2.3 Thermal Cross Sections

The calculated thermal cross sections are

$$\sigma_t = 51.0 \text{ barns } (50.5 \pm 2.3 \text{ barns}),$$

$$\sigma_s = 25.0 \text{ barns } (24.0 \pm 2.0 \text{ barns}),$$

$$\text{and } \sigma_c = 26.0 \text{ barns } (26.5 \pm 1.0 \text{ barns}).$$

which agree well with the values of BNL-325⁸⁾ appeared in the parentheses.

2.4 Connection with the Smooth Cross Section

From the staircase plot of the resonance levels shown in Figs. 5 and 6, it can be concluded that some resonances are missing above 90 keV. Hence the upper limit of resonance energy region was determined to be 90 keV.

3. Fast Energy Region

The cross sections are calculated in this energy region with the optical and statistical models.

3.1 Total Cross Section and Optical Model

The optical potential parameters were determined by taking account of the following two conditions:

- (1) The s-wave strength function in low energy region should be $(5.1 \pm 0.9) \times 10^{-4}$ which is recommended in BNL-325, 3rd edition.
- (2) The total cross sections measured by Foster and Glasgow¹⁰⁾ ($2.308 \sim 14$ MeV) and by Barnard et al.¹¹⁾ ($0.2 \sim 1.409$ MeV) should be well reproduced.

The obtained optical potential parameters are presented in Table II.

The calculated s-wave strength function is 5.1×10^{-4} at 1 keV and agrees very well with the recommended value in BNL-325. The calculated total cross section also agrees very well with the measured data as shown in Fig. 7. This implies the reliability of the present optical model. The calculated cross section was adopted in the present work.

3.2 Capture, Elastic and Inelastic Scattering Cross Section

The capture, elastic and inelastic scattering cross sections were calculated with the statistical model code CASTHY¹²⁾. The neutron transmission coefficient was calculated with the optical potential parameters described before. The γ -ray strength function was so determined that the calculated capture cross section agreed with the measured data by Kenny et al.⁷⁾; 32 mb at 100 keV. The level scheme was taken from Table of Isotope, 7th edition¹³⁾ and is shown in Table III.

The level density parameters were taken from the recommendation by Gilbert and Cameron¹⁴⁾.

The (n,p), (n, α) and (n,2n) reaction cross sections were taken into account as competing processes. The (n,p) and (n, α) cross sections were taken from the compilation by Alley and Lessler¹⁵⁾ and the (n,2n) cross sections were evaluated on the basis of the measurements by Holub and Cindro¹⁶⁾. The adopted cross sections are given in Table IV. The presently evaluated capture cross section is shown in Fig. 8 with some measured data.

4. Concluding Remarks

Evaluation of neutron nuclear data of scandium-45 have been performed in the energy range of 10^{-5} eV to 20 MeV, and these data will be stored in JENDL-2. The presently evaluated data are shown in Table V with ENDF/B format.

The primary motive of the present evaluation is to know the total cross section near 2 keV. Hence we adopted the calculated total cross section in the fast energy region instead of following the remaining resonance structure in hundred keV region. The ignorance of the structure in this region makes ignorance of the self-shielding factor and may result in some errors in the neutron transport calculation as was pointed out¹⁷⁾ in the case of the iron data of JENDL-1. This problem should be investigated in future.

Acknowledgment

The authors wish to express their thanks to M. Hachya of Mitsui Engineering and Shipbuilding Co., Ltd. for summarizing the nuclear data of scandium-45. They also acknowledge Y. Fijita and K. Kobayashi of KUR for their communicating the preliminary cross section data. Careful typewriting by H. Terakado is much appreciated.

References

- 1) Brugger R. M., and Simpson O. D.: "Resonance Window Filters of Neutrons for Research and Development", Proc. Symp. Irradiation Facilities for Research Reactors, Teheran, Nov. 6 - 10, 1972. STI/PUB/316. IAEA, Vienna.
- 2) Mill A. J. and Harvey J. R.: "Reactor- and Accelerator-Based Filtered Beams", RD/B/N4776, Central Electricity Generating Board, 1980.
- 3) Fujita Y. and Yamamuro N.: J. At. Energy Soc. Jpn., 23, 85 (1981) [in Japanese].
- 4) Liou H. I., Chrien R. E., Block, R. C. and Kobayashi K.: Nucl. Sci. Eng., 67, 326 (1978).
- 5) Razbudey V. F., Muravitsky A. V., Vertebnyi V. P. and Kiriluk A. L.: "Nuclear Cross Sections for Technology", Proc. Int. Conf., Knoxville, Oct. 22 - 26, 1979, p.890, NBS Special Publication 594 (1980).
- 6) Fujita Y.: Private communication (1981).
- 7) Kenny M. J., Allen B. J. and Macklin R. L.: Aust. J. Phys., 30, 605 (1977).
- 8) Mughabgab S. F. and Garber D. I.: "Neutron Cross Sections, Vol. 1, Resonance Parameters", BNL-325, 3rd Edition (1973).
- 9) Nakagawa T.: J. At. Energy Soc. Jpn., 22, 559 (1980) [in Japanese].
- 10) Foster G. D. and Glasgow D. W.: Phy. Rev., C3, 576 (1971).
- 11) Barnard E., Devilliers J. A. M., Reitmann D. and Tepel J. W.: Z. Phys., 245, 36 (1971).
- 12) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 13) Lederer C. M. and Shirley V. S., (Editor): "Table of Isotopes", 7th Edition, p.116, A Wiley-Interscience Pub. (1978).
- 14) Gilbert A. and Cameron A. G. W.: Can. J. Phys., 43, 1446 (1965).
- 15) Alley W. E. and Lessler R. M.: Nucl. Data Tables, All, 648 (1973).
- 16) Holub E and Cindro N.: Z. Phys., A289, 421 (1979).

- 17) Kawai M., Yamano N. and Koyama K.: "Nuclear Cross Sections for Technology", Proc. Inst. Conf., Knoxville, Oct. 22 - 26, 1979, p.586, NBS Special Publication 594 (1980).
- 18) Chou M., Fröhner F. H., Kazerouni M., Muller K. N. and Rohr G.: "Nuclear Data for Reactors", Conf. Proceedings, Helsinki, 15 - 19 June 1970, Vol. 1, p.619, IAEA (1970).
- 19) Booth R., Ball W. P. and MacGregor M. H.: Phys. Rev., 112, 226 (1958).
- 20) Perkin J. L.: J. Nucl. Energy, 17, 349 (1963).

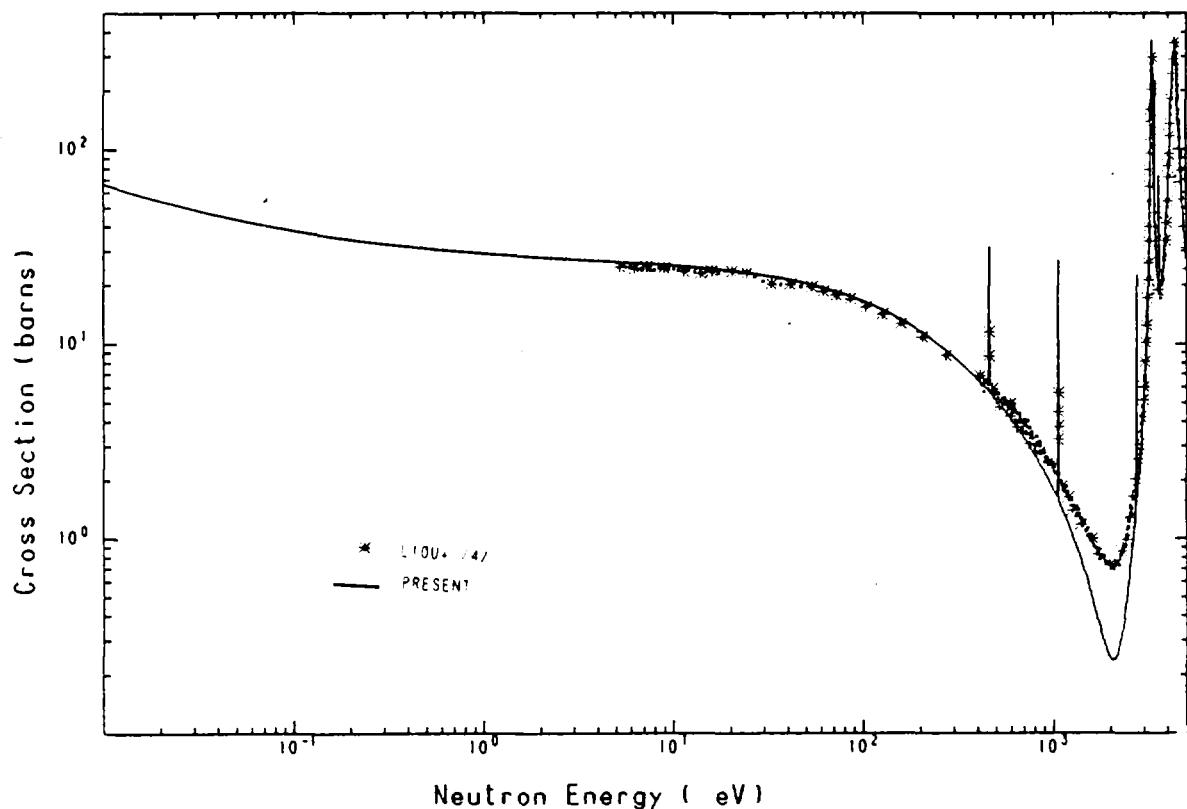


Fig. 1 The total cross section of ^{45}Sc calculated from the present resonance parameters with the measured data by Liou et al.⁴⁾ in the energy range below 5 keV.

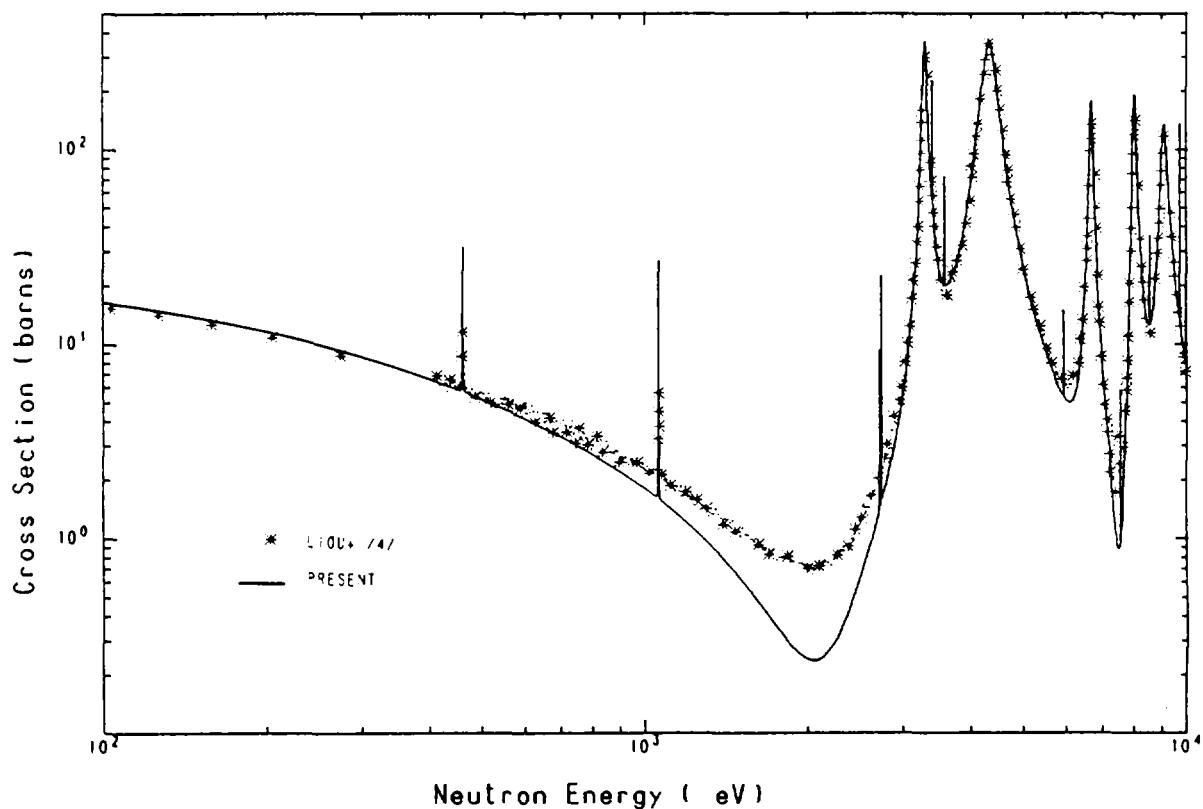


Fig. 2 The total cross section of ^{45}Sc calculated from the present resonance parameters with the measured data by Liou et al.⁴⁾ in the energy range between 100 eV and 10 keV.

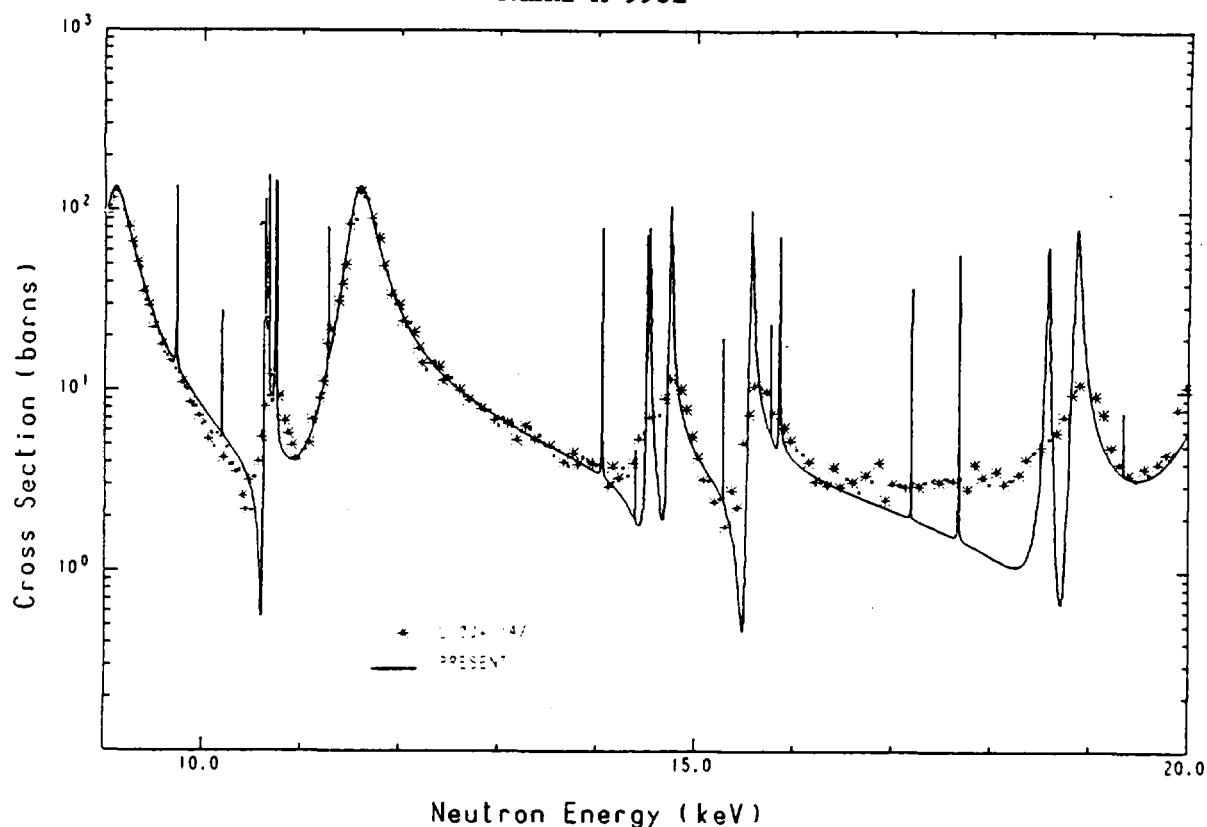


Fig. 3 The total cross section of ^{45}Sc calculated from the present resonance parameters with the measured data by Liou et al.⁴⁾ in the energy range between 9 and 20 keV.

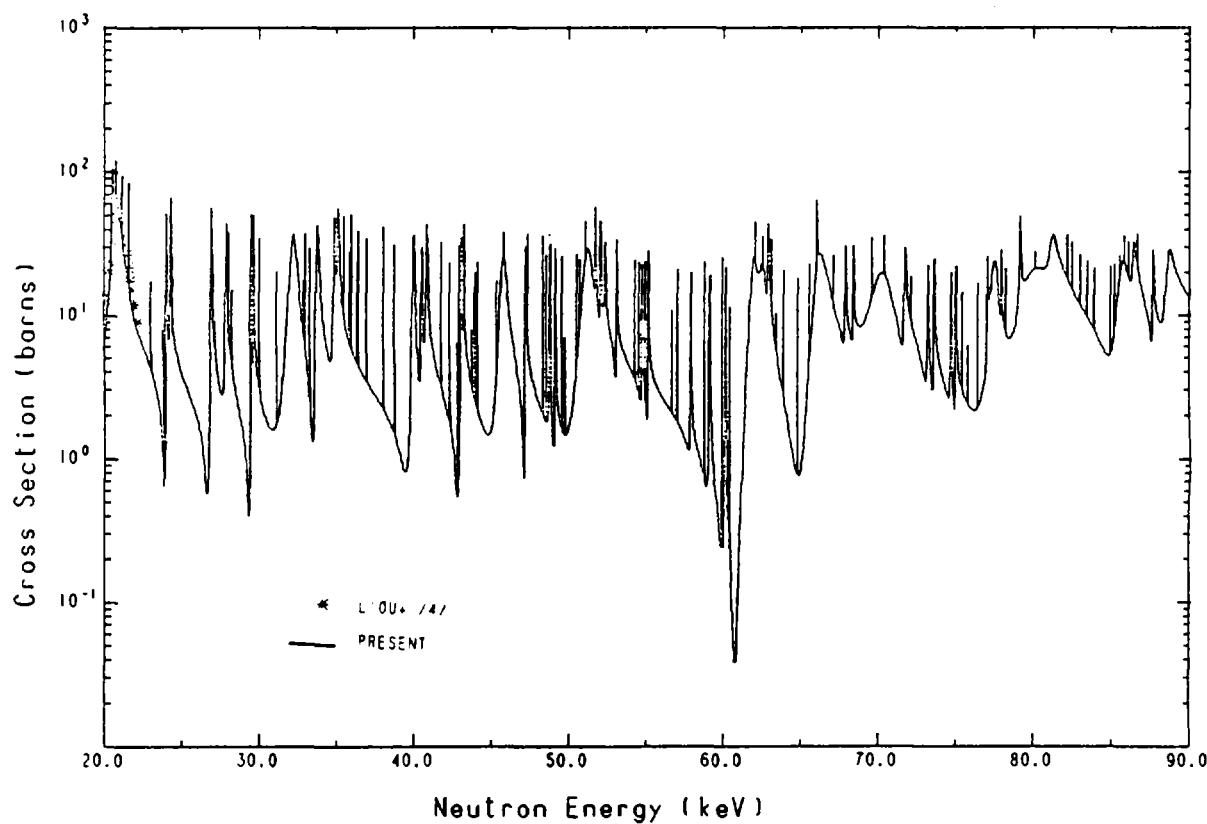


Fig. 4 The total cross section of ^{45}Sc calculated from the resonance parameters in the energy range from 20 to 90 keV.

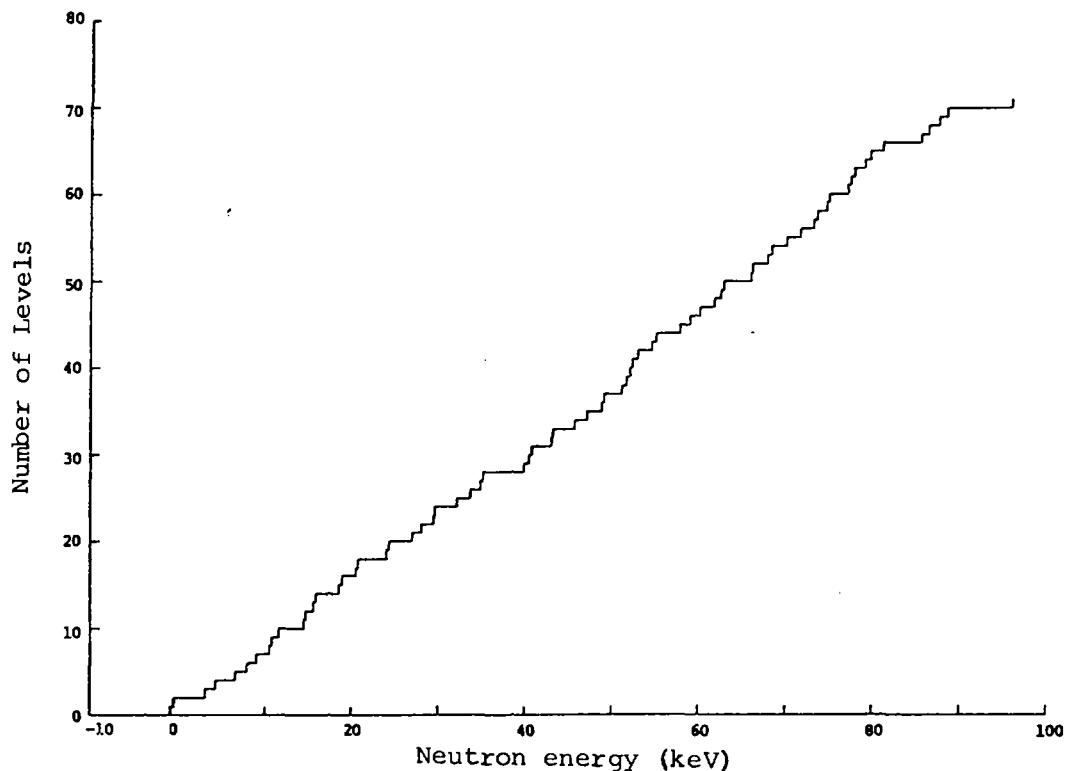


Fig. 5 Stair case plot of the s-wave resonance level sequence for ^{45}Sc .

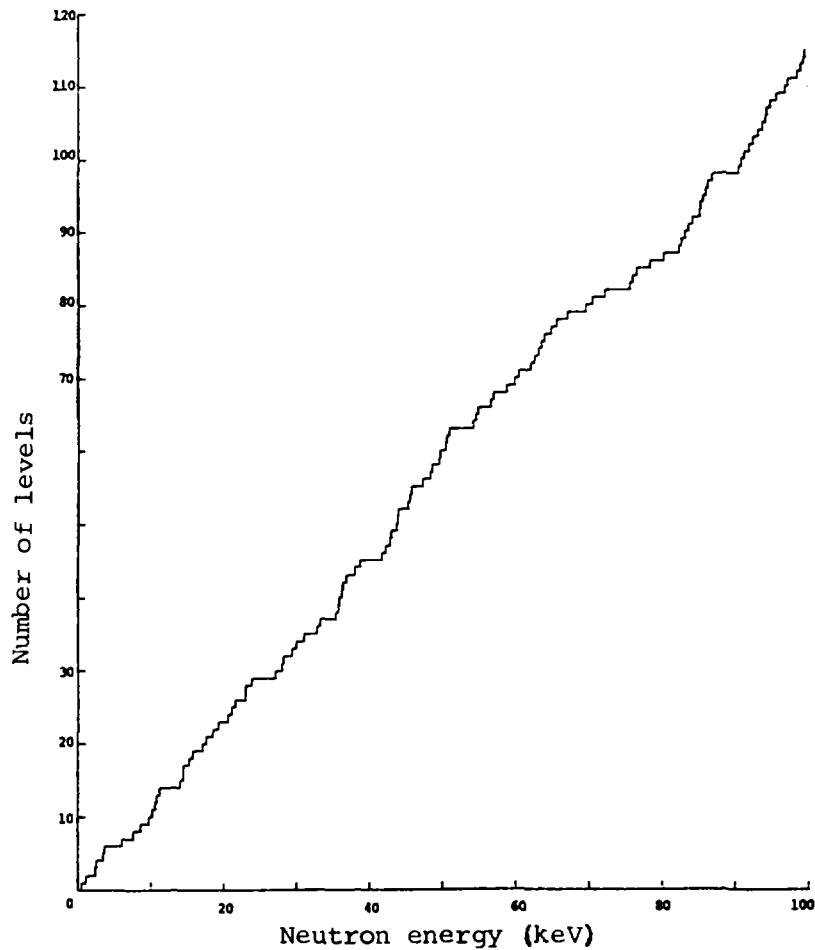


Fig. 6 Stair case plot of the p-wave resonance level sequence for ^{45}Sc .

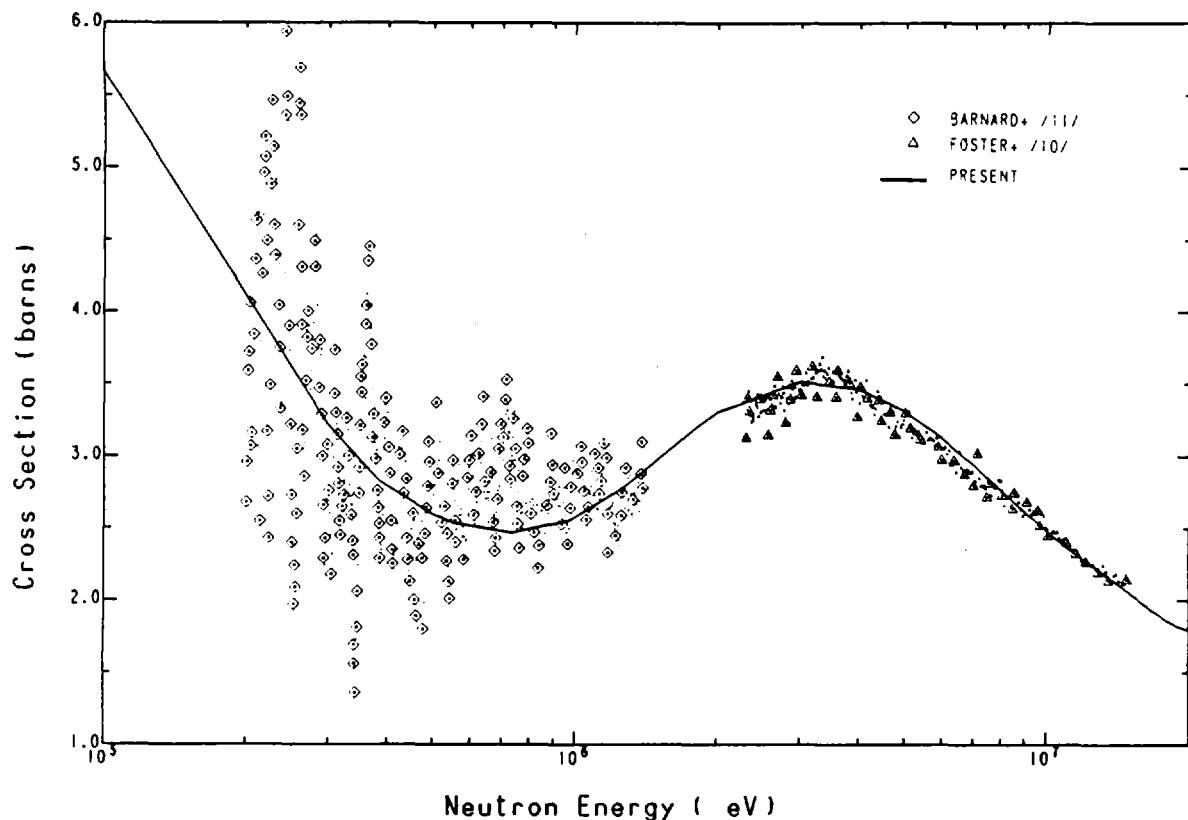


Fig. 7 The total cross section of ^{45}Sc calculated from the present optical potential parameters and the experimental values by Barnard et al.¹¹⁾ (0.2 - 1.4 MeV) and by Foster and Glasgow¹⁰⁾ (2.5 - 1.5 MeV).

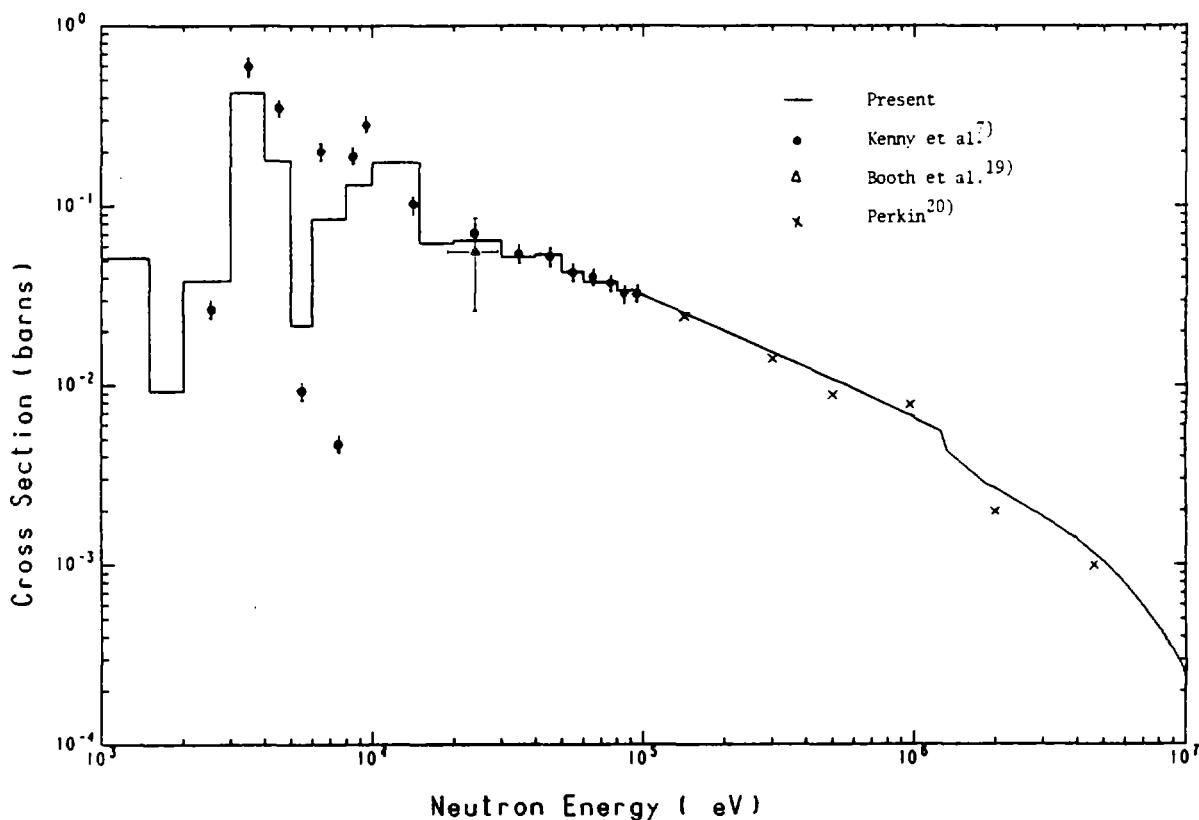


Fig. 8 The capture cross sections of ^{45}Sc . The average values are given in the resonance region.

Table I Resonance parameters of ^{45}Sc

ENERGY (KEV)	L	J	TOTAL WIDTH (EV)	NEUTRON WIDTH*	GAMMA WIDTH*	MISCELLANEOUS**	REFERENCE ***
-0.65 -0.5 ± 0.05	0 0	3 3	101.41 89 ± 11	101.0 9.9 ± 1.5	0.41	CNO= 4.0 ± 0.5	JENDL-2 78L1OU+
-0.33 -0.22 ± 0.04	0 0	4 4	37.11	36.7 9.9 ± 1.5	0.41	CNO= 0.67 ± 0.10	JENDL-2 78L1OU+
0.4606 0.4606 ± 0.0004	1 1	3.5	0.5044	0.0044 0.0044 ± 0.0004	0.5		JENDL-2 78L1OU+
1.0604 1.0604 ± 0.0010	1 1	3.5	0.51	0.01 0.0100 ± 0.0014	0.5		JENDL-2 78L1OU+
2.715 2.715 ± 0.003	1 1	3.5	0.508	0.008 0.008 ± 0.002	0.5	ARG= 7.1 ± 0.7	JENDL-2 77KENNY+
2.737 2.737 ± 0.003	1 1	3.5	0.522	0.022 0.022 ± 0.002	0.5	ARG= 19.9 ± 2.0	JENDL-2 77KENNY+
3.295 3.300 ± 0.015 3.295 ± 0.012	0 0 0	3	75.41	75.0 80 ± 10 75 ± 5	0.41 0.62 ± 0.06	ARG= 396 ± 40	JENDL-2 77KENNY+ 78L1OU+
3.404 3.404 ± 0.003	1 1	3.5	0.871	0.371	0.5 0.186 ± 0.018	ARG= 133.8 ± 13.4	JENDL-2 77KENNY+
3.582 3.582 ± 0.004	1 1	3.5	0.58	0.08 0.080 ± 0.008	0.5	ARG= 54.8 ± 5.5	JENDL-2 77KENNY+
4.33 4.326 ± 0.050 4.330 ± 0.018	0 0 0	4	340.41	340.0 320 ± 40 340 ± 20	0.41 0.71 ± 0.07	ARG= 352 ± 35	JENDL-2 77KENNY+ 78L1OU+
5.943 5.943 ± 0.006	1 1	3.5	0.522	0.022 0.022 ± 0.002	0.5	ARG= 9.2 ± 0.9	JENDL-2 77KENNY+
6.684 6.700 ± 0.020 6.684 ± 0.020	0 0 0	3	130.41	130.0 125 ± 25 130 ± 14	0.41 0.65 ± 0.07	ARG= 207 ± 21	JENDL-2 77KENNY+ 78L1OU+
7.377 ± 0.025	1			0.8 ± 0.4			78L1OU+
7.56 7.560 ± 0.008 7.458 ± 0.025	1 1 1	3.5	0.514	0.014 0.014 ± 0.002 0.8 ± 0.4	0.5	ARG= 4.8 ± 0.5	JENDL-2 77KENNY+ 78L1OU+
7.548 ± 0.025	1			0.50 ± 0.30			78L1OU+
8.023 8.038 ± 0.030 8.023 ± 0.025	0 0 0	4	145.41	145.0 140 ± 30 145 ± 15	0.41 0.64 ± 0.06	ARG= 168 ± 17	JENDL-2 77KENNY+ 78L1OU+
8.558 8.558 ± 0.009	1 1	3.5	0.586	0.086 0.086 ± 0.008	0.5	ARG= 24.6 ± 2.5	JENDL-2 77KENNY+
9.070 ± 0.009	0			40 ± 10	0.96 ± 0.10	ARG= 217 ± 22	77KENNY+
9.092 9.080 ± 0.040 9.092 ± 0.030	0 0 0	3	300.41	300.0 250 ± 50 300 ± 20	0.41 0.82 ± 0.12	ARG= 193 ± 30	JENDL-2 77KENNY+ 78L1OU+
9.725 9.725 ± 0.010	1 1	3.5	3.03	2.53	0.5 0.368 ± 0.036	ARG= 91.8 ± 9.2	JENDL-2 77KENNY+
10.189 10.189 ± 0.010	1 1	3.5	0.598	0.098 0.098 ± 0.010	0.5	ARG= 23.4 ± 2.3	JENDL-2 77KENNY+
10.625 10.625 ± 0.035	0 0	3	10.41	10.0 10 ± 3	0.41		JENDL-2 78L1OU+
10.662 10.662 ± 0.011	1 1	5.0	4.63	3.83	0.8 0.800 ± 0.080	ARG= 182.5 ± 18.3	JENDL-2 77KENNY+
10.735 10.735 ± 0.035	0 0	4	6.41	6.0 6 ± 2	0.41		JENDL-2 78L1OU+
10.74 10.740 ± 0.011	1 1	5.0	1.711	0.911	0.8 0.516 ± 0.052	ARG= 116.6 ± 11.7	JENDL-2 77KENNY+
11.265 11.265 ± 0.011	1 1	3.5	1.093	0.593	0.5 0.240 ± 0.024	ARG= 51.5 ± 5.2	JENDL-2 77KENNY+
11.575	0	4	290.41	290.0	0.41		JENDL-2

Table I (cont.)

ENERGY (KEV)	L	J	TOTAL WIDTH (EV)	NEUTRON WIDTH*	GAMMA WIDTH*	MISCELLANEOUS**	REFERENCE ***
11.580 ± 0.050	0	4		300 ± 50	0.86 ± 0.09	ARG = 158 ± 16	77KENNY+ 78LIOU+
11.575 ± 0.050	0	4		290 ± 20			
14.05	1	3.5	2.15	1.65	0.5		JENDL-2
14.050 ± 0.014	1				0.338 ± 0.034	ARG = 58.4 ± 5.8	77KENNY+
14.39	1	3.5	0.5153	0.0153	0.5		JENDL-2
14.390 ± 0.014	1				0.012 ± 0.002	ARG = 2.2 ± 0.2	77KENNY+
14.5	1	5.0	1.62	0.82	0.8		JENDL-2
14.500 ± 0.015	1				0.490 ± 0.050	ARG = 82.1 ± 8.2	77KENNY+
14.525	0	3	20.41	20.0	0.41		JENDL-2
14.525 ± 0.060	0	3		20 ± 4			78LIOU+
14.74	0	4	26.41	26.0	0.41		JENDL-2
14.820 ± 0.015	0			35	0.52 ± 0.05	ARG = 75.3 ± 7.5	77KENNY+ 78LIOU+
14.740 ± 0.060	0	4		26 ± 5			
15.28	1	3.5	0.621	0.121	0.5		JENDL-2
15.280 ± 0.015	1			0.122 ± 0.012		ARG = 19.2 ± 1.9	77KENNY+
15.56	0	4	28.41	28.0	0.41		JENDL-2
15.623 ± 0.016	0			30	0.67 ± 0.07	ARG = 92.1 ± 9.2	77KENNY+ 78LIOU+
15.560 ± 0.060	0	4		28 ± 5			
15.763	1	3.5	0.632	0.132	0.5		JENDL-2
15.763 ± 0.016	1			0.132 ± 0.014		ARG = 20.5 ± 2.1	77KENNY+
15.85	0	3	5.41	5.0	0.41		JENDL-2
15.850 ± 0.060	0	3		5 ± 2			78LIOU+
17.192	1	3.5	0.899	0.399	0.5		JENDL-2
17.192 ± 0.017	1				0.20 ± 0.02	ARG = 27.6 ± 2.8	77KENNY+
17.677	1	3.5	1.73	1.23	0.5		JENDL-2
17.677 ± 0.018	1				0.318 ± 0.032	ARG = 43.0 ± 4.3	77KENNY+
18.504	1	3.5	0.51	0.01	0.5		JENDL-2
18.504 ± 0.019	1			0.010 ± 0.002		ARG = 13.9 ± 1.4	77KENNY+
18.58	0	3	32.41	32.0	0.41		JENDL-2
18.580 ± 0.080	0	3		32 ± 6			78LIOU+
18.87	0	4	62.41	62.0	0.41		JENDL-2
19.17	4			60			70CHO+
19.084 ± 0.019	0	{ 4 }		60	0.69 ± 0.07	ARG = 86.0 ± 8.6	77KENNY+ 78LIOU+
18.870 ± 0.080	0	4		62 ± 10			
19.341	1	3.5	0.532	0.032	0.5		JENDL-2
19.341 ± 0.019	1			0.032 ± 0.004		ARG = 4.0 ± 0.4	77KENNY+
20.5	0	4	80.41	80.0	0.41		JENDL-2
20.80	4			60			70CHO+
20.644 ± 0.021	0	{ 4 }		100	0.83 ± 0.12	ARG = 86.1 ± 8.6	77KENNY+ 78LIOU+
20.500 ± 0.090	0	4		80 ± 14			
20.726	1	3.5	3.4	2.9	0.5		JENDL-2
20.726 ± 0.021	1				0.374 ± 0.038	ARG = 44.0 ± 4.4	77KENNY+
20.78	0	3	710.41	710.0	0.41		JENDL-2
20.95	3			800			70CHO+
20.933 ± 0.200	0	{ 3 }		700 ± 200	0.60 ± 0.20	ARG = 49.2 ± 4.9	77KENNY+ 78LIOU+
20.780 ± 0.100	0	3		710 ± 60			
21.114	1	3.5	2.74	2.24	0.5		JENDL-2
21.114 ± 0.021	1				0.360 ± 0.036	ARG = 41.4 ± 4.1	77KENNY+
21.58	1	5.0	2.36	1.86	0.5		JENDL-2
21.580 ± 0.022	1				0.476 ± 0.048	ARG = 53.7 ± 5.4	77KENNY+
23.015	1	3.5	0.644	0.144	0.5		JENDL-2
23.015 ± 0.023	1			0.144 ± 0.014		ARG = 15.3 ± 1.5	77KENNY+
23.065	1	3.5	0.512	0.012	0.5		JENDL-2
23.065 ± 0.023	1			0.012 ± 0.002		ARG = 1.4 ± 0.14	77KENNY+
23.838	1	3.5	0.572	0.072	0.5		JENDL-2
23.838 ± 0.024	1			0.072 ± 0.008		ARG = 7.4 ± 0.74	77KENNY+
24.01	0	3	61.087	60.0	1.087		JENDL-2

JAERI-M 9981

Table I (cont.)

ENERGY (KEV)	L	J	TOTAL WIDTH (EV)	NEUTRON WIDTH*	GAMMA WIDTH* (EV)	MISCELLANEOUS**	REFERENCE ***
24.18 24.010± 0.024		3 0 (3)		60 (60)	1.087± 0.109	ARG= 83.1 ± 8.3	70CHO+ 77KENNY+
24.315 24.48 24.315± 0.024	0	4 4 0 (4)	60.462	60.0 60 (60)	0.462 0.462± 0.046	ARG= 45.5 ± 4.6	JENDL-2 70CHO+ 77KENNY+
26.925 27.12 26.925± 0.027	0	4 4 0 (4)	90.9	90.0 90 (90)	0.9	ARG= 62.0 ± 6.2	JENDL-2 70CHO+ 77KENNY+
27.19 27.190± 0.027	1	3.5 1	0.534	0.034 P 0.034± 0.004	0.5	ARG= 3.0 ± 0.3	JENDL-2 77KENNY+
27.9 28.12 27.900± 0.028	0	3 3 0 (3)	110.811	110.0 110 (110)	0.811 0.811± 0.081	ARG= 53.9 ± 5.4	JENDL-2 70CHO+ 77KENNY+
28.04 28.040± 0.028	1	3.5 1	1.069	0.569	0.5 0.234± 0.024	ARG= 20.3 ± 2.0	JENDL-2 77KENNY+
28.235 28.235± 0.028	1	3.5 1	0.638	0.138 P 0.138± 0.014	0.5	ARG= 11.9 ± 1.2	JENDL-2 77KENNY+
29.41 29.410± 0.029	1	3.5 1	0.898	0.398	0.5 B 0.196± 0.020	ARG= 16.1 ± 1.6	JENDL-2 77KENNY+
29.48 29.480± 0.029	0	4 0 (4)	30.613	30.0 30	0.613 0.613± 0.061	ARG= 49.0 ± 4.9	JENDL-2 77KENNY+
29.63 29.85 29.630± 0.030	0	3.5 4 0	50.723	50.0 100 50	0.723 B 0.723± 0.072	ARG= 51.8 ± 5.2	JENDL-2 70CHO+ 77KENNY+
30.01 30.010± 0.030	1	3.5 1	1.507	1.007	0.5 B 0.294± 0.030	ARG= 23.8 ± 2.4	JENDL-2 77KENNY+
31.135 31.135± 0.031	1	3.5 1	0.853	0.353	0.5 B 0.184± 0.018	ARG= 14.2 ± 1.4	JENDL-2 77KENNY+
32.18 32.40 32.180± 0.032	0	3 3 0 (3)	570.917	570.0 570 (570)	0.917 0.917± 0.092	ARG= 53.1 ± 5.3	JENDL-2 70CHO+ 77KENNY+
32.84 32.840± 0.033	1	3.5 1	0.644	0.144 P 0.144± 0.014	0.5	ARG= 10.6 ± 1.1	JENDL-2 77KENNY+
32.94 32.940± 0.033	1	5.0 1	1.779	0.979	0.8 B 0.532± 0.054	ARG= 39.3 ± 3.9	JENDL-2 77KENNY+
33.28 33.280± 0.033	1	3.5 1	1.394	0.894	0.5 B 0.284± 0.028	ARG= 20.6 ± 2.1	JENDL-2 77KENNY+
33.73 34.0 33.730± 0.034	0	3 3 0 (3)	200.866	200.0 190 200	0.866 0.866± 0.087	ARG= 47.9 ± 4.8	JENDL-2 70CHO+ 77KENNY+
34.86 34.860± 0.035	0	3.5 0	100.689	100.0 100	0.689 B 0.689± 0.070	ARG= 42.7 ± 4.3	JENDL-2 77KENNY+
35.08 35.3 35.080± 0.035	0	4 4 0 (4)	150.543	150.0 280 150	0.543 0.543± 0.054	ARG= 28.9 ± 2.9	JENDL-2 70CHO+ 77KENNY+
35.47 35.470± 0.036	1	5.0 1	1.93	1.43	0.5 B 0.448± 0.044	ARG= 30.7 ± 3.1	JENDL-2 77KENNY+
35.8 35.800± 0.036	1	3.5 1	1.101	0.601	0.5 B 0.242± 0.024	ARG= 16.3 ± 1.6	JENDL-2 77KENNY+
35.955 35.995± 0.036	1	5.0 1	3.76	3.26	0.5 B 0.524± 0.052	ARG= 35.4 ± 3.5	JENDL-2 77KENNY+
36.31 36.310± 0.036	1	3.5 1	0.979	0.479	0.5 B 0.214± 0.022	ARG= 14.4 ± 1.4	JENDL-2 77KENNY+
36.39 36.390± 0.037	1	3.5 1	4.35	3.85	0.5 B 0.388± 0.038	ARG= 26.0 ± 2.6	JENDL-2 77KENNY+
36.93 36.930± 0.037	1	3.5 1	2.61	2.11	0.5 B 0.356± 0.036	ARG= 23.4 ± 2.3	JENDL-2 77KENNY+

JAERI-M 9981

Table I (cont.)

ENERGY (KEV)	L	J	TOTAL WIDTH (EV)	NEUTRON WIDTH*	GAMMA WIDTH** (EV)	MISCELLANEOUS***	REFERENCE ***
38.0 38.000± 0.038	1 1	5.0	2.55	2.05	0.5 0.486± 0.048	ARG= 31.1 ± 3.1	JENDL-2 77KENNY+
38.73 38.730± 0.039	1 1	3.5	2.65	2.15	0.5 0.356± 0.036	ARG= 22.4 ± 2.2	JENDL-2 77KENNY+
39.98 40.37 39.980± 0.040	0 4 0 (4)	4	181.067	180.0 130 180	1.067 1.067± 0.107	ARG= 63.9 ± 6.4	JENDL-2 70CHO+ 77KENNY+
40.5 40.77 40.500± 0.041	0 3 0 (3)	3	101.276	100.0 100 (100)	1.276 1.276± 0.128	ARG= 75.1 ± 7.5	JENDL-2 70CHO+ 77KENNY+
40.815 41.15 40.815± 0.041	0 4 0 (4)	4	110.639	110.0 110 (110)	0.639 0.639± 0.064	ARG= 29.1 ± 3.0	JENDL-2 70CHO+ 77KENNY+
41.74 41.740± 0.042	1 1	3.5	3.65	3.15	0.5 0.380± 0.038	ARG= 22.1 ± 2.2	JENDL-2 77KENNY+
42.3 42.300± 0.042	1 1	3.5	1.424	0.924	0.5 0.286± 0.028	ARG= 16.4 ± 1.6	JENDL-2 77KENNY+
42.79 42.790± 0.043	1 1	3.5	0.612	0.112 0.112± 0.012	0.5	ARG= 6.4 ± 0.6	JENDL-2 77KENNY+
42.9 42.900± 0.043	1 1	3.5	4.266	3.81	0.456 0.456± 0.046	ARG= 20.3 ± 2.0	JENDL-2 77KENNY+
43.05 43.35 43.050± 0.043	0 4 0 (4)	4	101.068	100.0 170 100	1.068 1.068± 0.107	ARG= 46.0 ± 4.6	JENDL-2 70CHO+ 77KENNY+
43.215 43.215± 0.043	0 0	3.5	31.074	30.0 30	1.074 1.074± 0.107	ARG= 51.8 ± 5.2	JENDL-2 77KENNY+
43.71 43.710± 0.044	1 1	3.5	0.59	0.09 0.090± 0.010	0.5	ARG= 5.0 ± 0.5	JENDL-2 77KENNY+
43.92 43.920± 0.044	1 1	3.5	1.102	0.602	0.5 0.242± 0.024	ARG= 13.3 ± 1.3	JENDL-2 77KENNY+
44.08 44.080± 0.044	1 1	3.5	1.544	1.044	0.5 0.298± 0.030	ARG= 16.4 ± 1.6	JENDL-2 77KENNY+
45.3 45.300± 0.045	1 1	3.5	0.915	0.415	0.5 0.198± 0.020	ARG= 10.7 ± 1.1	JENDL-2 77KENNY+
45.57 45.570± 0.046	1 1	3.5	0.632	0.132 0.132± 0.014	0.5	ARG= 7.1 ± 0.7	JENDL-2 77KENNY+
45.73 45.15 45.730± 0.046	0 3 0 (3)	3	480.521	480.0 480 (480)	0.521 0.521± 0.052	ARG= 21.3 ± 2.1	JENDL-2 70CHO+ 77KENNY+
45.78 45.780± 0.046	1 1	3.5	0.814	0.314	0.5 0.168± 0.016	ARG= 9.0 ± 0.9	JENDL-2 77KENNY+
47.18 47.60 47.180± 0.047	0 3 0 (3)	3	60.053	60.0 180 60	0.053 0.053± 0.054	ARG= 27.1 ± 2.7	JENDL-2 70CHO+ 77KENNY+
47.31 47.310± 0.047	1 1	5.0	1.94	1.44	0.5 0.450± 0.046	ARG= 23.1 ± 2.3	JENDL-2 77KENNY+
48.31 48.310± 0.048	1 1	5.0	4.57	4.07	0.5 0.538± 0.054	ARG= 27.1 ± 2.7	JENDL-2 77KENNY+
48.53 48.530± 0.049	1 1	5.0	2.23	1.43	0.8 0.622± 0.062	ARG= 31.1 ± 3.1	JENDL-2 77KENNY+
48.79 48.790± 0.049	0 0 (4)	4	40.478	40.0 40	0.478 0.478± 0.048	ARG= 23.3 ± 2.3	JENDL-2 77KENNY+
49.12 49.17 49.120± 0.049	0 0 0	3.5 4	40.361	40.0 160 40	0.361 0.361± 0.036	ARG= 17.5 ± 1.8	JENDL-2 70CHO+ 77KENNY+
49.54 49.540± 0.050	1 1	5.0	2.278	1.48	0.798 0.798± 0.080	ARG= 30.8 ± 3.1	JENDL-2 77KENNY+

Table I (cont.)

ENERGY (KEV)	L	J	TOTAL WIDTH (EV)	NEUTRON WIDTH * (EV)	GAMMA WIDTH * (EV)	MISCELLANEOUS **	REFERENCE ***
49.75 49.750± 0.050	1 1	3.5 ,	0.626 0.126± 0.012	0.126 0.126± 0.012	0.5	ARG= 4.9 ± 0.5	JENDL-2 77KENNY+
50.5 50.500± 0.051	1 1	3.5	2.42	1.92 0.348± 0.034	0.5 0.348± 0.034	ARG= 16.8 ± 1.7	JENDL-2 77KENNY+
50.685 50.685± 0.051	1 1	3.5	1.228	0.728 0.260± 0.026	0.5 0.260± 0.026	ARG= 12.5 ± 1.3	JENDL-2 77KENNY+
51.05 51.050± 0.051	1 1	3.5	2.12	1.62 0.336± 0.034	0.5 0.336± 0.034	ARG= 16.0 ± 1.6	JENDL-2 77KENNY+
51.16 51.16 51.160± 0.051	0 0 0	4 4 (4)	841.3 840 (840)	840.0 1.300± 0.013	1.3	ARG= 46.4 ± 4.6	JENDL-2 70CHO+ 77KENNY+
51.685 51.685± 0.052	0 0	3.5	40.352	40.0 40	0.352 0.352± 0.035	ARG= 14.7 ± 1.5	JENDL-2 77KENNY+
52.025 52.025± 0.052	0 0	3.5	40.521	40.0 40	0.521 0.521± 0.052	ARG= 21.5 ± 2.1	JENDL-2 77KENNY+
52.33 52.18 52.330± 0.052	0 0 0	3 3 (3)	70.418 100 70	70.0 0.418± 0.04	0.418 0.418± 0.04	ARG= 14.9 ± 1.5	JENDL-2 70CHO+ 77KENNY+
53.075 53.075± 0.053	0 0	3.5	40.248	40.0 40	0.248 0.248± 0.25	ARG= 10.0 ± 1.0	JENDL-2 77KENNY+
54.255 54.255± 0.054	1 1	5.0	2.03	1.23 0.583± 0.058	0.8 0.583± 0.058	ARG= 26.3 ± 2.6	JENDL-2 77KENNY+
54.525 54.525± 0.054	1	3.5	2.45	1.95 0.348± 0.034	0.5 0.348± 0.034	ARG= 15.6 ± 1.6	JENDL-2 77KENNY+
54.73 54.83 54.730± 0.055	0 0 0	3 3 (3)	41.76 220 40	40.0 1.760± 0.176	1.76	ARG= 57.7 ± 5.8	JENDL-2 70CHO+ 77KENNY+
54.92 54.920± 0.055	1 1	5.0	2.04	1.24 0.590± 0.060	0.8 0.590± 0.060	ARG= 26.1 ± 2.6	JENDL-2 77KENNY+
55.125 55.125± 0.055	0 0	3.5	40.39	40.0 40	0.39 0.390± 0.039	ARG= 15.1 ± 1.5	JENDL-2 77KENNY+
56.655 56.655± 0.057	1 1	3.5	0.781	0.281 0.158± 0.016	0.5 0.158± 0.016	ARG= 6.8 ± 0.7	JENDL-2 77KENNY+
57.01 57.010± 0.057	1 1	5.0	1.95	1.15 0.570± 0.058	0.8 0.570± 0.058	ARG= 24.3 ± 2.4	JENDL-2 77KENNY+
57.89 57.68 57.890± 0.058	0 0 0	3 3 (3)	35.487 220 35	35.0 0.487± 0.049	0.487	ARG= 17.9 ± 1.8	JENDL-2 70CHO+ 77KENNY+
58.76 58.760± 0.059	1 1	5.0	2.95	2.15 0.706± 0.070	0.8 0.706± 0.070	ARG= 29.2 ± 2.9	JENDL-2 77KENNY+
59.11 59.77 59.110± 0.059	0 0 0	3 3 (3)	51.047 1640 50	50.0 1.047± 0.105	1.047	ARG= 37.3 ± 3.7	JENDL-2 70CHO+ 77KENNY+
59.92 59.920± 0.060	1 1	5.0	2.7	2.2 0.492± 0.130	0.5 0.492± 0.130	ARG= 20.0 ± 2.0	JENDL-2 77KENNY+
60.14 60.140± 0.060	0 0	3.5	40.681	40.0 40	0.681 0.681± 0.068	ARG= 24.0 ± 2.4	JENDL-2 77KENNY+
60.42 60.420± 0.060	1 1	3.5	0.973	0.473 0.214± 0.022	0.5 0.214± 0.022	ARG= 8.6 ± 0.9	JENDL-2 77KENNY+
61.89 61.84 61.890± 0.062	0 0 0	4 4 (4)	520.7 520 (520)	520.0 0.700± 0.070	0.7	ARG= 26.9 ± 2.7	JENDL-2 70CHO+ 77KENNY+
62.025 62.025± 0.062	1 1	3.5	3.174	2.84 0.334± 0.034	0.334 0.334± 0.034	ARG= 10.3 ± 1.0	JENDL-2 77KENNY+
62.49 62.54 62.490± 0.062	0 0 0	3 3 (3)	571.0 570 (570)	570.0 1.000± 0.100	1.0 1.000± 0.100	ARG= 29.8 ± 3.0	JENDL-2 70CHO+ 77KENNY+

JAERI-M 9981

Table I (cont.)

ENERGY (KEV)	L	J	TOTAL WIDTH (EV)	NEUTRON WIDTH* (EV)	GAMMA WIDTH* (EV)	MISCELLANEOUS**	REFERENCE ***
62.5 62.500± 0.063	1 1	3.5 ,	1.171	0.671	0.5 0.254± 0.026	ARG= 9.8 ± 0.9	JENDL-2 77KENNY+
62.85 62.850± 0.063	0 0	3.5	100.548	100.0 100	0.548 0.548± 0.055	ARG= 18.8 ± 1.9	JENDL-2 77KENNY+
63.05 63.050± 0.063	1 1	3.5	4.602	4.11	0.492 0.492± 0.050	ARG= 14.9 ± 1.5	JENDL-2 77KENNY+
63.4 63.400± 0.063	1 1	3.5	0.632	0.132 0.132± 0.014	0.5	ARG= 5.1 ± 0.5	JENDL-2 77KENNY+
63.85 63.850± 0.064	1 1	5.0	2.05	1.25	0.8 0.592± 0.060	ARG= 22.5 ± 2.3	JENDL-2 77KENNY+
64.78 64.780± 0.065	1 1	5.0	2.04	1.24	0.8 0.588± 0.030	ARG= 22.1 ± 2.2	JENDL-2 77KENNY+
65.52 65.520± 0.066	1 1	5.0	2.28	1.48	0.8 0.628± 0.062	ARG= 23.3 ± 2.3	JENDL-2 77KENNY+
66.0 66.000± 0.066	0 0	3.5	40.287	40.0 40	0.287 0.287± 0.029	ARG= 9.3 ± 0.9	JENDL-2 77KENNY+
66.1 65.94 66.100± 0.066	0 0 (4)	4	1041.8	1040.0 1040 (1040)	1.8	ARG= 50.8 ± 5.1	JENDL-2 70CHO+ 77KENNY+
67.05 67.050± 0.067	1 1	3.5	1.438	0.938	0.5 0.286± 0.028	ARG= 10.4 ± 1.0	JENDL-2 77KENNY+
67.85 67.850± 0.069	0 0	3.5	76.504	75.0 75	1.504 1.504± 0.150	ARG= 46.8 ± 4.7	JENDL-2 77KENNY+
68.375 68.375± 0.068	0 0	3.5	51.435	50.0 50	1.435 1.435± 0.144	ARG= 44.0 ± 4.4	JENDL-2 77KENNY+
69.555 69.555± 0.070	1 1	5.0	5.37	4.37	1.0 0.984± 0.098	ARG= 34.4 ± 3.4	JENDL-2 77KENNY+
70.11 70.11 70.110± 0.070	0 0 (3)	3	1690.6	1690.0 1690 (1690)	0.6	ARG= 16.0 ± 1.9	JENDL-2 70CHO+ 77KENNY+
70.375 70.375± 0.071	1 1	5.0	2.28	1.48	0.8 0.628± 0.066	ARG= 21.7 ± 2.5	JENDL-2 77KENNY+
71.7 71.76 71.760± 0.072	0 0 (4)	4	151.606	150.0 410 150	1.606 1.606± 0.210	ARG= 53.3 ± 5.5	JENDL-2 70CHO+ 77KENNY+
72.115 72.115± 0.072	1 1	3.5	0.947	0.447	0.5 0.208± 0.022	ARG= 7.0 ± 0.9	JENDL-2 77KENNY+
73.2 73.18 73.200± 0.073	0 0 (3)	3	70.951	70.0 350 70	0.951 0.951± 0.140	ARG= 24.0 ± 2.9	JENDL-2 70CHO+ 77KENNY+
73.6 73.600± 0.074	0 0	3.5	60.281	60.0 60	0.281 0.281± 0.028	ARG= 8.2 ± 1.0	JENDL-2 77KENNY+
74.7 74.90 74.700± 0.075	0 0 (3)	3	61.177	60.0 150 60	1.177 1.177± 0.153	ARG= 28.9 ± 2.9	JENDL-2 70CHO+ 77KENNY+
75.0 75.000± 0.075	0 0	3.5	46.54	45.0 45	1.54 1.540± 0.200	ARG= 42.9 ± 4.3	JENDL-2 77KENNY+
75.43 75.430± 0.075	1 1	3.5	1.294	0.794	0.5 0.270± 0.210	ARG= 8.7 ± 1.2	JENDL-2 77KENNY+
75.78 75.780± 0.076	1 1	3.5	0.63	0.13 0.130± 0.016	0.5	ARG= 4.2 ± 0.4	JENDL-2 77KENNY+
76.42 76.420± 0.076	1 1	3.5	2.34	1.84	0.5 0.346± 0.038	ARG= 11.0 ± 1.4	JENDL-2 77KENNY+
77.025 77.15 77.025± 0.077	0 0 (4)	4	50.522	50.0 250 50	0.522 0.522± 0.068	ARG= 16.1 ± 2.1	JENDL-2 70CHO+ 77KENNY+
77.5	0	3	600.498	600.0	0.498		JENDL-2

JAERI-M 9981

Table I (cont.)

ENERGY (KEV)	L	J	TOTAL WIDTH (EV)	NEUTRON WIDTH *	GAMMA WIDTH *	MISCELLANEOUS **	REFERENCE***
77.55 77.500± 0.078	0	3 (3)		600 1600	0.498± 0.063	ARG= 12.0 ± 1.6	70CHO+ 77KENNY+
77.925 77.85 77.925± 0.078	0	4 4 (4)	40.824	40.0 150 40	0.824 0.824± 0.125	ARG= 24.9 ± 3.0	JENDL-2 70CHO+ 77KENNY+
78.215 78.215± 0.078	1	5.0 1	1.89	1.09	0.8 0.560± 0.064	ARG= 17.4 ± 2.0	JENDL-2 77KENNY+
79.15 79.00 79.150± 0.079	0	3 3 (3)	100.827	100.0 200 100	0.827 0.827± 0.125	ARG= 24.9 ± 3.0	JENDL-2 70CHO+ 77KENNY+
79.8 79.80 79.800± 0.500	0	3 3 (3)	2802.0	2800.0 2800 (2800)	2.0 2.0 ± 1.0	ARG= 50.6 ± 25	JENDL-2 70CHO+ 77KENNY+
80.1 80.100± 0.080	1	3.5 1	0.809	0.309	0.5 0.192± 0.040	ARG= 5.1 ± 1.0	JENDL-2 77KENNY+
81.2 81.10 81.200± 0.081	0	4 4 (4)	600.28	600.0 600 (600)	0.28 0.280± 0.090	ARG= 8.3 ± 2.8	JENDL-2 70CHO+ 77KENNY+
82.18 82.180± 0.082	1	5.0 1	6.42	5.42	1.0 1.022± 0.114	ARG= 30.2 ± 3.8	JENDL-2 77KENNY+
82.48 82.480± 0.083	1	5.0 1	3.45	2.65	0.8 0.744± 0.084	ARG= 21.9 ± 2.8	JENDL-2 77KENNY+
83.005 83.005± 0.083	1	5.0 1	4.34	2.84	1.5 1.190± 0.132	ARG= 34.8 ± 4.0	JENDL-2 77KENNY+
83.00		4		150			70CHO+
83.45 83.450± 0.084	1	5.0 1	4.18	2.68	1.5 1.164± 0.130	ARG= 33.9 ± 4.0	JENDL-2 77KENNY+
83.9 83.900± 0.084	1	5.0 1	2.08	1.28	0.8 0.596± 0.072	ARG= 17.3 ± 2.1	JENDL-2 77KENNY+
84.95 84.950± 0.085	1	5.0 1	2.16	1.66	0.5 0.466± 0.058	ARG= 13.3 ± 1.6	JENDL-2 77KENNY+
85.205 85.205± 0.085	1	3.5 1	5.47	4.97	0.5 0.400± 0.050	ARG= 11.4 ± 1.4	JENDL-2 77KENNY+
85.525 85.525± 0.086	1	3.5 1	0.947	0.447	0.5 0.208± 0.026	ARG= 5.9 ± 0.8	JENDL-2 77KENNY+
85.6 85.60 85.600± 0.086	0	4 4 (4)	850.35	850.0 850 (850)	0.35 0.350± 0.052	ARG= 9.8 ± 1.5	JENDL-2 70CHO+ 77KENNY+
85.84 85.840± 0.086	1	3.5 1	2.11	1.61	0.5 0.336± 0.042	ARG= 9.5 ± 1.1	JENDL-2 77KENNY+
86.105 86.105± 0.086	1	3.5 1	4.606	4.14	0.466 0.466± 0.058	ARG= 10.4 ± 1.2	JENDL-2 77KENNY+
86.4 86.00 86.400± 0.086	0	3 3 (3)	275.51	275.0 650 275	0.51 0.510± 0.078	ARG= 14.2 ± 2.1	JENDL-2 70CHO+ 77KENNY+
86.675 86.675± 0.087	1	3.5 1	6.61	6.11	0.5 0.404± 0.052	ARG= 11.4 ± 1.3	JENDL-2 77KENNY+
87.65 87.650± 0.088	0	3.5 0	77.934	75.0 75	2.934 2.934± 0.440	ARG= 69.5 ± 5.0	JENDL-2 77KENNY+
88.6 88.60 88.600± 0.089	0	3 3 (3)	550.9	550.0 550 (550)	0.9 0.900± 0.140	ARG= 18.9 ± 3.0	JENDL-2 70CHO+ 77KENNY+
90.24 90.240± 0.090	1	5.0 1	2.03	1.23	0.8 0.588± 0.074	ARG= 15.8 ± 1.8	JENDL-2 77KENNY+
90.20		4		120			70CHO+
90.575	1	5.0	4.71	3.21	1.5		JENDL-2

JAERI-M 9981

Table I (cont.)

ENERGY (KEV)	L	J	TOTAL WIDTH (EV)	NEUTRON WIDTH *	GAMMA WIDTH *	MISCELLANEOUS **	REFERENCE ***
90.575± 0.091	1				1.238± 0.144	ARG= 33.2 ± 4.2	77KENNY+
90.95	1	5.0	3.93	3.13	0.8		JENDL-2
90.950± 0.091	1				0.770± 0.094	ARG= 20.6 ± 2.6	77KENNY+
91.6	1	5.0	3.75	2.95	0.8		JENDL-2
91.600± 0.092	1				0.762± 0.094	ARG= 20.2 ± 2.6	77KENNY+
91.70		3		550			70CHO+
92.25	1	3.5	0.542	A 0.042	0.5		JENDL-2
92.250± 0.092	1			B 0.042± 0.004		ARG= 1.1 ± 0.2	77KENNY+
92.72	1	3.5	1.59	1.09	0.5		JENDL-2
92.720± 0.093	1				0.300± 0.040	ARG= 7.9 ± 1.1	77KENNY+
93.39	1	5.0	2.12	1.32	0.8		JENDL-2
93.390± 0.093	1				0.604± 0.080	ARG= 15.7 ± 2.2	77KENNY+
93.78	1	5.0	5.63	4.13	1.5		JENDL-2
93.780± 0.094	1				1.330± 0.158	ARG= 34.5 ± 4.4	77KENNY+
94.02	1	5.0	6.63	5.13	1.5		JENDL-2
94.020± 0.094	1				1.402± 0.166	ARG= 36.3 ± 4.6	77KENNY+
94.45	1	5.0	3.37	2.57	0.8		JENDL-2
94.450± 0.094	1				0.740± 0.094	ARG= 19.0 ± 2.5	77KENNY+
95.25	1	3.5	3.46	2.96	0.5		JENDL-2
95.250± 0.095	1				0.374± 0.046	ARG= 9.6 ± 1.3	77KENNY+
95.94	0	3	80.359	80.0	0.359		JENDL-2
94.40		3		800			70CHO+
95.940± 0.096	0	(3)		80	0.359± 0.054	ARG= 8.0 ± 1.2	77KENNY+
96.44	1	5.0	2.64	1.84	0.8		JENDL-2
96.440± 0.096	1				0.674± 0.080	ARG= 17.0 ± 2.4	77KENNY+
96.9	1	5.0	1.8	1.0	0.8		JENDL-2
96.900± 0.097	1				0.540± 0.070	ARG= 13.5 ± 2.9	77KENNY+
98.26	1	5.0	2.03	1.23	0.8		JENDL-2
98.260± 0.098	1				0.586± 0.072	ARG= 14.5 ± 2.1	77KENNY+
98.585	1	5.0	3.77	2.97	0.8		JENDL-2
98.585± 0.099	1				0.764± 0.094	ARG= 18.8 ± 2.5	77KENNY+
99.08	1	5.0	5.53	4.73	0.8		JENDL-2
99.080± 0.099	1				0.830± 0.110	ARG= 20.3 ± 2.7	77KENNY+
99.2	1	5.0	2.52	1.72	0.8		JENDL-2
99.200± 0.099	1				0.662± 0.086	ARG= 16.2 ± 2.3	77KENNY+
99.80		3		2000			70CHO+
100.7		4		300			70CHO+
101.0		3		400			70CHO+
102.1		4		300			70CHO+
102.3		3		350			70CHO+
104.0		4		150			70CHO+
105.7		4		150			70CHO+

* A denotes $2g\Gamma_n$

B denotes $2g\Gamma_\gamma$

** GNO = $\Gamma_n^{(o)}$ (eV)

ARG = $2\pi\lambda^2 g\Gamma_n \Gamma_\gamma / \Gamma$ (b·eV)

*** 78 LIOU+ : Ref. (4)

77 KENNY+ : Ref. (7)

70 CHO+ : Ref. (18)

Table II Optical potential parameters
(in MeV and fm)

real term	$V(En) = 56.15 - 0.2189 En$
	$r_o = 1.16$
	$a_o = 0.677$
surface term*	$W_s(En) = 8.698$
	$r_s = 1.288$
	$b = 0.310$
spin-orbit term	$V_{so} = 6.874$
	$r_{so} = 1.185$
	$a_{so} = 0.76$

* derivative Woods-Saxon type

Table III Level scheme of ^{45}Sc

level	Energy(MeV)	Spin and Parity
1	0	$7/2^-$
2	0.01240	$3/2^+$
3	0.3764	$3/2^-$
4	0.5429	$5/2^+$
5	0.7202	$5/2^-$
6	0.9391	$1/2^+$
7	0.9745	$7/2^+$
8	1.2364	$11/2^-$
9	1.3032	$3/2^+$
10	1.4334	$9/2^+$
11	1.6615	$9/2^-$
12	1.8006	$5/2^+$

Levels above 1.9 MeV were assumed to be overlapping.

Table IV (n,p), (n, α) and (n,2n) cross sections
used in the evaluation

Energy MeV	cross sections, m barn			
	(n,p)	(n, α)	(n,2n)	(n,p)+(n, α)+(n,2n)
0.5	0.0	0.0		0.0
1.0	2.0	1.0		3.0
2.0	16.0	2.5		18.5
3.0	50.0	4.0		54.0
4.0	75.0	5.0		80.0
5.0	93.0	7.0		100.0
6.0	107.0	8.0		115.0
7.0	115.0	10.0		125.0
8.0	115.0	11.0		126.0
9.0	109.0	14.0		123.0
10.0	100.0	19.0		119.0
11.0	91.0	26.0		117.0
11.5	85.5	30.0	0.0	115.5
12.0	80.0	36.0	20.0	136.0
12.5	75.0	42.0	65.0	182.0
13.0	70.0	48.0	120.0	238.0
13.5	64.5	54.0	170.0	288.5
14.0	59.0	56.0	245.0	360.0
14.5	53.5	56.0	348.0	457.5
15.0	48.0	52.0	380.0	480.0
16.0	38.0	40.0	400.0	478.0
17.0	27.0	29.5	460.0	516.5
18.0	17.0	26.5	500.0	543.5
19.0	5.0	25.0	510.0	540.0
20.0	0.0	23.5	520.0	543.5

Table V Presently evaluated nuclear data of ^{45}Sc

							MAT	MF	MT	SEQ
.....	10.....	20.....	30.....	40.....	50.....	60.....				
2.10450+ 4	4.45697+ 1		1	0	0	362145	1451		1	
0.0	+ 0	0.0	+ 0	0	1	02145	1451		2	
						2145	1451		3	
				1	451	39	2145	1451		4
				2	151	193	2145	1451		5
				3	1	17	2145	1451		6
				3	2	17	2145	1451		7
				3	4	16	2145	1451		8
				3	16	8	2145	1451		9
				3	51	16	2145	1451		10
				3	52	15	2145	1451		11
				3	53	15	2145	1451		12
				3	54	14	2145	1451		13
				3	55	14	2145	1451		14
				3	56	14	2145	1451		15
				3	57	13	2145	1451		16
				3	58	13	2145	1451		17
				3	59	12	2145	1451		18
				3	60	12	2145	1451		19
				3	61	12	2145	1451		20
				3	91	11	2145	1451		21
				3	102	17	2145	1451		22
				3	103	12	2145	1451		23
				3	107	12	2145	1451		24
				3	251	18	2145	1451		25
				4	2	200	2145	1451		26
				4	16	10	2145	1451		27
				4	51	112	2145	1451		28
				4	52	120	2145	1451		29
				4	53	102	2145	1451		30
				4	54	111	2145	1451		31
				4	55	98	2145	1451		32
				4	56	96	2145	1451		33
				4	57	98	2145	1451		34
				4	58	90	2145	1451		35
				4	59	88	2145	1451		36
				4	60	92	2145	1451		37
				4	61	84	2145	1451		38
				4	91	88	2145	1451		39
							2145	1 0		40
							2145	0 0		41
2.10450+ 4	4.45697+ 1		0	0	1		02145	2151		42
2.10450+ 4	1.00000+ 0		0	0	1		02145	2151		43
1.00000- 5	9.00000+ 4		1	2	0		02145	2151		44
3.50000+ 0	4.55000- 1		0	0	2		02145	2151		45
4.45697+ 1	0.0	+ 0	0	0	426		712145	2151		46
-3.30000+ 2	4.00000+ 0	3.71100+ 1	3.67000+ 1	4.10000- 1	0.0		+ 02145	2151		47
-6.50000+ 2	3.00000+ 0	1.01410+ 2	1.01000+ 2	4.10000- 1	0.0		+ 02145	2151		48
3.29500+ 3	3.00000+ 0	7.54100+ 1	7.50000+ 1	4.10000- 1	0.0		+ 02145	2151		49

.....10.....20.....30.....40.....50.....60.....MAT MF MT SEQ

3.63100+ 4 3.50000+ 0 9.79000- 1 4.79000- 1 5.00000- 1 0.0 + 02145 2151 160
 3.63900+ 4 3.50000+ 0 4.35000+ 0 3.85000+ 0 5.00000- 1 0.0 + 02145 2151 161
 3.69300+ 4 3.50000+ 0 2.61000+ 0 2.11000+ 0 5.00000- 1 0.0 + 02145 2151 162
 3.80000+ 4 5.00000+ 0 2.55000+ 0 2.05000+ 0 5.00000- 1 0.0 + 02145 2151 163
 3.87300+ 4 3.50000+ 0 2.65000+ 0 2.15000+ 0 5.00000- 1 0.0 + 02145 2151 164
 4.17400+ 4 3.50000+ 0 3.65000+ 0 3.15000+ 0 5.00000- 1 0.0 + 02145 2151 165
 4.23000+ 4 3.50000+ 0 1.42400+ 0 9.24000- 1 5.00000- 1 0.0 + 02145 2151 166
 4.27900+ 4 3.50000+ 0 6.12000- 1 1.12000- 1 5.00000- 1 0.0 + 02145 2151 167
 4.29000+ 4 3.50000+ 0 4.26600+ 0 3.81000+ 0 4.56000- 1 0.0 + 02145 2151 168
 4.37100+ 4 3.50000+ 0 5.90000- 1 9.00000- 2 5.00000- 1 0.0 + 02145 2151 169
 4.39200+ 4 3.50000+ 0 1.10200+ 0 6.02000- 1 5.00000- 1 0.0 + 02145 2151 170
 4.40800+ 4 3.50000+ 0 1.54400+ 0 1.04400+ 0 5.00000- 1 0.0 + 02145 2151 171
 4.53000+ 4 3.50000+ 0 9.15000- 1 4.15000- 1 5.00000- 1 0.0 + 02145 2151 172
 4.55700+ 4 3.50000+ 0 6.32000- 1 1.32000- 1 5.00000- 1 0.0 + 02145 2151 173
 4.57800+ 4 3.50000+ 0 8.14000- 1 3.14000- 1 5.00000- 1 0.0 + 02145 2151 174
 4.73100+ 4 5.00000+ 0 1.94000+ 0 1.44000+ 0 5.00000- 1 0.0 + 02145 2151 175
 4.83100+ 4 5.00000+ 0 4.57000+ 0 4.07000+ 0 5.00000- 1 0.0 + 02145 2151 176
 4.85300+ 4 5.00000+ 0 2.23000+ 0 1.43000+ 0 8.00000- 1 0.0 + 02145 2151 177
 4.95400+ 4 5.00000+ 0 2.27800+ 0 1.48000+ 0 7.98000- 1 0.0 + 02145 2151 178
 4.97500+ 4 3.50000+ 0 6.26000- 1 1.26000- 1 5.00000- 1 0.0 + 02145 2151 179
 5.05000+ 4 3.50000+ 0 2.42000+ 0 1.92000+ 0 5.00000- 1 0.0 + 02145 2151 180
 5.06850+ 4 3.50000+ 0 1.22800+ 0 7.28000- 1 5.00000- 1 0.0 + 02145 2151 181
 5.10500+ 4 3.50000+ 0 2.12000+ 0 1.62000+ 0 5.00000- 1 0.0 + 02145 2151 182
 5.42550+ 4 5.00000+ 0 2.03000+ 0 1.23000+ 0 8.00000- 1 0.0 + 02145 2151 183
 5.45250+ 4 3.50000+ 0 2.45000+ 0 1.95000+ 0 5.00000- 1 0.0 + 02145 2151 184
 5.49200+ 4 5.00000+ 0 2.04000+ 0 1.24000+ 0 8.00000- 1 0.0 + 02145 2151 185
 5.66550+ 4 3.50000+ 0 7.81000- 1 2.81000- 1 5.00000- 1 0.0 + 02145 2151 186
 5.70100+ 4 5.00000+ 0 1.95000+ 0 1.15000+ 0 8.00000- 1 0.0 + 02145 2151 187
 5.87600+ 4 5.00000+ 0 2.95000+ 0 2.15000+ 0 8.00000- 1 0.0 + 02145 2151 188
 5.99200+ 4 5.00000+ 0 2.70000+ 0 2.20000+ 0 5.00000- 1 0.0 + 02145 2151 189
 6.04200+ 4 3.50000+ 0 9.73000- 1 4.73000- 1 5.00000- 1 0.0 + 02145 2151 190
 6.20250+ 4 3.50000+ 0 3.17400+ 0 2.84000+ 0 3.34000- 1 0.0 + 02145 2151 191
 6.25000+ 4 3.50000+ 0 1.17100+ 0 6.71000- 1 5.00000- 1 0.0 + 02145 2151 192
 6.30500+ 4 3.50000+ 0 4.60200+ 0 4.11000+ 0 4.92000- 1 0.0 + 02145 2151 193
 6.34000+ 4 3.50000+ 0 6.32000- 1 1.32000- 1 5.00000- 1 0.0 + 02145 2151 194
 6.38500+ 4 5.00000+ 0 2.05000+ 0 1.25000+ 0 8.00000- 1 0.0 + 02145 2151 195
 6.47800+ 4 5.00000+ 0 2.04000+ 0 1.24000+ 0 8.00000- 1 0.0 + 02145 2151 196
 6.55200+ 4 5.00000+ 0 2.28000+ 0 1.48000+ 0 8.00000- 1 0.0 + 02145 2151 197
 6.70500+ 4 3.50000+ 0 1.43800+ 0 9.38000- 1 5.00000- 1 0.0 + 02145 2151 198
 6.95550+ 4 5.00000+ 0 5.37000+ 0 4.37000+ 0 1.00000+ 0 0.0 + 02145 2151 199
 7.03750+ 4 5.00000+ 0 2.28000+ 0 1.48000+ 0 8.00000- 1 0.0 + 02145 2151 200
 7.21150+ 4 3.50000+ 0 9.47000- 1 4.47000- 1 5.00000- 1 0.0 + 02145 2151 201
 7.54300+ 4 3.50000+ 0 1.29400+ 0 7.94000- 1 5.00000- 1 0.0 + 02145 2151 202
 7.57800+ 4 3.50000+ 0 6.30000- 1 1.30000- 1 5.00000- 1 0.0 + 02145 2151 203
 7.64200+ 4 3.50000+ 0 2.34000+ 0 1.84000+ 0 5.00000- 1 0.0 + 02145 2151 204
 7.82150+ 4 5.00000+ 0 1.89000+ 0 1.09000+ 0 8.00000- 1 0.0 + 02145 2151 205
 8.01000+ 4 3.50000+ 0 8.09000- 1 3.09000- 1 5.00000- 1 0.0 + 02145 2151 206
 8.21800+ 4 5.00000+ 0 6.42000+ 0 5.42000+ 0 1.00000+ 0 0.0 + 02145 2151 207
 8.24800+ 4 5.00000+ 0 3.45000+ 0 2.65000+ 0 8.00000- 1 0.0 + 02145 2151 208
 8.30050+ 4 5.00000+ 0 4.34000+ 0 2.84000+ 0 1.50000+ 0 0.0 + 02145 2151 209
 8.34500+ 4 5.00000+ 0 4.18000+ 0 2.68000+ 0 1.50000+ 0 0.0 + 02145 2151 210
 8.39000+ 4 5.00000+ 0 2.08000+ 0 1.28000+ 0 8.00000- 1 0.0 + 02145 2151 211
 8.49500+ 4 5.00000+ 0 2.16000+ 0 1.66000+ 0 5.00000- 1 0.0 + 02145 2151 212
 8.52050+ 4 3.50000+ 0 5.47000+ 0 4.97000+ 0 5.00000- 1 0.0 + 02145 2151 213
 8.55250+ 4 3.50000+ 0 9.47000- 1 4.47000- 1 5.00000- 1 0.0 + 02145 2151 214

	10	20	30	40	50	60	MAT	MF	MT	SEQ
0.0	+ 0 9.96365+ 5		0	0	6		02145	4	52	875
0.0	+ 0 -1.15842- 2	0.0	+ 0 -9.78641- 4	0.0	+ 0 2.59210-	82145	4	52	876	
0.0	+ 0 1.00000+ 6		0	0	6		02145	4	52	877
0.0	+ 0 -1.13606- 2	0.0	+ 0 -9.93811- 4	0.0	+ 0 3.29090-	82145	4	52	878	
0.0	+ 0 1.26414+ 6		0	0	8		02145	4	52	879
0.0	+ 0 -1.36922- 2	0.0	+ 0 -1.44007- 3	0.0	+ 0 -1.13763-	72145	4	52	880	
0.0	+ 0 2.77748- 8					2145	4	52	881	
0.0	+ 0 1.33244+ 6		0	0	8		02145	4	52	882
0.0	+ 0 -1.44516- 2	0.0	+ 0 -1.53904- 3	0.0	+ 0 -1.35797-	92145	4	52	883	
0.0	+ 0 6.32468- 9					2145	4	52	884	
0.0	+ 0 1.46556+ 6		0	0	8		02145	4	52	885
0.0	+ 0 -1.58742- 2	0.0	+ 0 -1.71498- 3	0.0	+ 0 -4.80173-	82145	4	52	886	
0.0	+ 0 1.04805- 8					2145	4	52	887	
0.0	+ 0 1.69878+ 6		0	0	8		02145	4	52	888
0.0	+ 0 -1.77976- 2	0.0	+ 0 -1.89957- 3	0.0	+ 0 -1.65480-	72145	4	52	889	
0.0	+ 0 2.09193- 8					2145	4	52	890	
0.0	+ 0 1.84100+ 6		0	0	8		02145	4	52	891
0.0	+ 0 -1.85758- 2	0.0	+ 0 -1.90705- 3	0.0	+ 0 -2.84777-	72145	4	52	892	
0.0	+ 0 4.15501- 8					2145	4	52	893	
0.0	+ 0 1.94263+ 6		0	0	8		02145	4	52	894
0.0	+ 0 -1.90669- 2	0.0	+ 0 -1.93878- 3	0.0	+ 0 -4.14436-	72145	4	52	895	
0.0	+ 0 5.78808- 8					2145	4	52	896	
0.0	+ 0 2.00000+ 6		0	0	8		02145	4	52	897
0.0	+ 0 -1.92432- 2	0.0	+ 0 -1.93172- 3	0.0	+ 0 -5.03935-	72145	4	52	898	
0.0	+ 0 6.93407- 8					2145	4	52	899	
0.0	+ 0 3.00000+ 6		0	0	8		02145	4	52	900
0.0	+ 0 -2.03256- 2	0.0	+ 0 -1.67740- 3	0.0	+ 0 -6.89750-	62145	4	52	901	
0.0	+ 0 7.85686- 7					2145	4	52	902	
0.0	+ 0 4.00000+ 6		0	0	10		02145	4	52	903
0.0	+ 0 -1.65599- 2	0.0	+ 0 -1.29931- 3	0.0	+ 0 -4.86434-	52145	4	52	904	
0.0	+ 0 4.92618- 6	0.0	+ 0 2.05288- 9			2145	4	52	905	
0.0	+ 0 5.00000+ 6		0	0	10		02145	4	52	906
0.0	+ 0 -9.78891- 3	0.0	+ 0 -1.28879- 3	0.0	+ 0 -1.78714-	42145	4	52	907	
0.0	+ 0 1.56506- 5	0.0	+ 0 1.68608- 8			2145	4	52	908	
0.0	+ 0 6.00000+ 6		0	0	12		02145	4	52	909
0.0	+ 0 -3.05191- 3	0.0	+ 0 -1.83077- 3	0.0	+ 0 -3.95154-	42145	4	52	910	
0.0	+ 0 2.79050- 5	0.0	+ 0 1.03775- 7	0.0	+ 0 1.51744- 10	2145	4	52	911	
0.0	+ 0 7.00000+ 6		0	0	12		02145	4	52	912
0.0	+ 0 2.13196- 3	0.0	+ 0 -2.78538- 3	0.0	+ 0 -6.44083-	42145	4	52	913	
0.0	+ 0 3.33561- 5	0.0	+ 0 5.06079- 7	0.0	+ 0 8.62465- 10	2145	4	52	914	
0.0	+ 0 8.00000+ 6		0	0	12		02145	4	52	915
0.0	+ 0 6.21182- 3	0.0	+ 0 -3.88184- 3	0.0	+ 0 -8.75429-	42145	4	52	916	
0.0	+ 0 2.80062- 5	0.0	+ 0 1.99842- 6	0.0	+ 0 3.75601- 9	2145	4	52	917	
0.0	+ 0 9.00000+ 6		0	0	12		02145	4	52	918
0.0	+ 0 9.67136- 3	0.0	+ 0 -4.80873- 3	0.0	+ 0 -1.04882-	32145	4	52	919	
0.0	+ 0 7.17136- 6	0.0	+ 0 6.44165- 6	0.0	+ 0 1.29588-	82145	4	52	920	
0.0	+ 0 1.00000+ 7		0	0	14		02145	4	52	921
0.0	+ 0 1.32418- 2	0.0	+ 0 -5.38915- 3	0.0	+ 0 -1.17928-	32145	4	52	922	
0.0	+ 0 -3.95926- 5	0.0	+ 0 1.74626- 5	0.0	+ 0 3.72860-	82145	4	52	923	
0.0	+ 0 1.65313- 10					2145	4	52	924	
0.0	+ 0 1.10000+ 7		0	0	14		02145	4	52	925
0.0	+ 0 1.79361- 2	0.0	+ 0 -5.66352- 3	0.0	+ 0 -1.34319-	32145	4	52	926	
0.0	+ 0 -1.30535- 4	0.0	+ 0 4.03152- 5	0.0	+ 0 9.55376-	82145	4	52	927	
0.0	+ 0 4.72131- 10					2145	4	52	928	
0.0	+ 0 1.15000+ 7		0	0	14		02145	4	52	929

						MAT	MF	MT	SEQ
.....	10.....	20.....	30.....	40.....	50.....	60.....			
0.0	+ 0 2.09003- 2 0.0	+ 0 -5.73933- 3 0.0	+ 0 -1.46360- 32145 4 52						930
0.0	+ 0 -1.97717- 4 0.0	+ 0 5.74564- 5 0.0	+ 0 1.47726- 72145 4 52						931
0.0	+ 0 7.63268-10					2145 4 52			932
0.0	+ 0 1.20000+ 7	0 0	14			02145 4 52			933
0.0	+ 0 2.42593- 2 0.0	+ 0 -5.80674- 3 0.0	+ 0 -1.61653- 32145 4 52						934
0.0	+ 0 -2.79724- 4 0.0	+ 0 7.82444- 5 0.0	+ 0 2.24110- 72145 4 52						935
0.0	+ 0 1.20536- 9					2145 4 52			936
0.0	+ 0 1.25000+ 7	0 0	14			02145 4 52			937
0.0	+ 0 2.78577- 2 0.0	+ 0 -5.88272- 3 0.0	+ 0 -1.79708- 32145 4 52						938
0.0	+ 0 -3.73559- 4 0.0	+ 0 1.01514- 4 0.0	+ 0 3.33882- 72145 4 52						939
0.0	+ 0 1.86218- 9					2145 4 52			940
0.0	+ 0 1.30000+ 7	0 0	14			02145 4 52			941
0.0	+ 0 3.15141- 2 0.0	+ 0 -5.97444- 3 0.0	+ 0 -1.99431- 32145 4 52						942
0.0	+ 0 -4.74146- 4 0.0	+ 0 1.25447- 4 0.0	+ 0 4.89815- 72145 4 52						943
0.0	+ 0 2.82481- 9					2145 4 52			944
0.0	+ 0 1.35000+ 7	0 0	14			02145 4 52			945
0.0	+ 0 3.50375- 2 0.0	+ 0 -6.07949- 3 0.0	+ 0 -2.19335- 32145 4 52						946
0.0	+ 0 -5.75295- 4 0.0	+ 0 1.47911- 4 0.0	+ 0 7.09531- 72145 4 52						947
0.0	+ 0 4.22230- 9					2145 4 52			948
0.0	+ 0 1.40000+ 7	0 0	14			02145 4 52			949
0.0	+ 0 3.82597- 2 0.0	+ 0 -6.18899- 3 0.0	+ 0 -2.37889- 32145 4 52						950
0.0	+ 0 -6.70992- 4 0.0	+ 0 1.66899- 4 0.0	+ 0 1.01412- 62145 4 52						951
0.0	+ 0 6.23361- 9					2145 4 52			952
0.0	+ 0 1.45000+ 7	0 0	16			02145 4 52			953
0.0	+ 0 4.10877- 2 0.0	+ 0 -6.29043- 3 0.0	+ 0 -2.53904- 32145 4 52						954
0.0	+ 0 -7.56632- 4 0.0	+ 0 1.81013- 4 0.0	+ 0 1.43304- 62145 4 52						955
0.0	+ 0 8.99112- 9 0.0	+ 0 7.38698-11				2145 4 52			956
0.0	+ 0 1.50000+ 7	0 0	16			02145 4 52			957
0.0	+ 0 4.34869- 2 0.0	+ 0 -6.38112- 3 0.0	+ 0 -2.66983- 32145 4 52						958
0.0	+ 0 -8.30068- 4 0.0	+ 0 1.89587- 4 0.0	+ 0 2.01781- 62145 4 52						959
0.0	+ 0 1.30222- 8 0.0	+ 0 1.11264-10				2145 4 52			960
0.0	+ 0 1.60000+ 7	0 0	16			02145 4 52			961
0.0	+ 0 4.71817- 2 0.0	+ 0 -6.50119- 3 0.0	+ 0 -2.84566- 32145 4 52						962
0.0	+ 0 -9.39466- 4 0.0	+ 0 1.90440- 4 0.0	+ 0 3.90227- 62145 4 52						963
0.0	+ 0 2.66930- 8 0.0	+ 0 2.45457-10				2145 4 52			964
0.0	+ 0 1.70000+ 7	0 0	16			02145 4 52			965
0.0	+ 0 4.98522- 2 0.0	+ 0 -6.52968- 3 0.0	+ 0 -2.93814- 32145 4 52						966
0.0	+ 0 -1.00666- 3 0.0	+ 0 1.72735- 4 0.0	+ 0 7.25802- 62145 4 52						967
0.0	+ 0 5.29884- 8 0.0	+ 0 5.21334-10				2145 4 52			968
0.0	+ 0 1.80000+ 7	0 0	16			02145 4 52			969
0.0	+ 0 5.20644- 2 0.0	+ 0 -6.46870- 3 0.0	+ 0 -2.99472- 32145 4 52						970
0.0	+ 0 -1.04594- 3 0.0	+ 0 1.40771- 4 0.0	+ 0 1.28593- 52145 4 52						971
0.0	+ 0 1.01550- 7 0.0	+ 0 1.06376- 9				2145 4 52			972
0.0	+ 0 1.90000+ 7	0 0	16			02145 4 52			973
0.0	+ 0 5.42344- 2 0.0	+ 0 -6.32291- 3 0.0	+ 0 -3.05508- 32145 4 52						974
0.0	+ 0 -1.07117- 3 0.0	+ 0 9.73104- 5 0.0	+ 0 2.15067- 52145 4 52						975
0.0	+ 0 1.87504- 7 0.0	+ 0 2.08334- 9				2145 4 52			976
0.0	+ 0 2.00000+ 7	0 0	16			02145 4 52			977
0.0	+ 0 5.65836- 2 0.0	+ 0 -6.09619- 3 0.0	+ 0 -3.14435- 32145 4 52						978
0.0	+ 0 -1.09319- 3 0.0	+ 0 4.36361- 5 0.0	+ 0 3.37156- 52145 4 52						979
0.0	+ 0 3.31509- 7 0.0	+ 0 3.91862- 9				2145 4 52			980
						2145 4 0			981
2.10450+	4 4.45698+ 1	0 1	0			02145 4 53			982
0.0	+ 0 4.45698+ 1	0 2	0			02145 4 53			983
0.0	+ 0 0.0 + 0	0 0	1			342145 4 53			984

							MAT	MF	MT	SEQ
10.....	20.....	30.....	40.....	50.....	60.....				
	34	2	0	0	0	0	02145	4	53	985
0.0	+ 0 5.55081+ 5		0	0	2		02145	4	53	986
0.0	+ 0 0.0 + 0						2145	4	53	987
0.0	+ 0 7.36359+ 5		0	0	4		02145	4	53	988
0.0	+ 0 1.34045- 3 0.0		+ 0-1.45936- 5				2145	4	53	989
0.0	+ 0 9.60170+ 5		0	0	6		02145	4	53	990
0.0	+ 0 4.47259- 3 0.0		+ 0-6.17362- 5 0.0		+ 0-1.47646-	82145	4	53		991
0.0	+ 0 9.96365+ 5		0	0	6		02145	4	53	992
0.0	+ 0 5.01126- 3 0.0		+ 0-7.06901- 5 0.0		+ 0-2.03505-	82145	4	53		993
0.0	+ 0 1.00000+ 6		0	0	6		02145	4	53	994
0.0	+ 0 5.32639- 3 0.0		+ 0-7.54118- 5 0.0		+ 0-2.16589-	82145	4	53		995
0.0	+ 0 1.26414+ 6		0	0	6		02145	4	53	996
0.0	+ 0 9.44275- 3 0.0		+ 0-1.53624- 4 0.0		+ 0-1.26633-	72145	4	53		997
0.0	+ 0 1.33244+ 6		0	0	6		02145	4	53	998
0.0	+ 0 9.57672- 3 0.0		+ 0-1.56026- 4 0.0		+ 0 4.18857-	72145	4	53		999
0.0	+ 0 1.46556+ 6		0	0	6		02145	4	53	1000
0.0	+ 0 9.91654- 3 0.0		+ 0-1.73095- 4 0.0		+ 0 5.08092-	72145	4	53		1001
0.0	+ 0 1.69878+ 6		0	0	6		02145	4	53	1002
0.0	+ 0 8.29117- 3 0.0		+ 0-1.64706- 4 0.0		+ 0 9.18396-	72145	4	53		1003
0.0	+ 0 1.84100+ 6		0	0	6		02145	4	53	1004
0.0	+ 0 8.94981- 3 0.0		+ 0-1.81545- 4 0.0		+ 0 1.21525-	62145	4	53		1005
0.0	+ 0 1.94263+ 6		0	0	6		02145	4	53	1006
0.0	+ 0 9.30542- 3 0.0		+ 0-1.96816- 4 0.0		+ 0 1.51800-	62145	4	53		1007
0.0	+ 0 2.00000+ 6		0	0	6		02145	4	53	1008
0.0	+ 0 9.27810- 3 0.0		+ 0-2.01832- 4 0.0		+ 0 1.67857-	62145	4	53		1009
0.0	+ 0 3.00000+ 6		0	0	8		02145	4	53	1010
0.0	+ 0 1.02197- 2 0.0		+ 0-2.60895- 4 0.0		+ 0 6.81342-	62145	4	53		1011
0.0	+ 0-4.36214- 8						2145	4	53	1012
0.0	+ 0 4.00000+ 6		0	0	8		02145	4	53	1013
0.0	+ 0 1.22490- 2 0.0		+ 0-4.45737- 5 0.0		+ 0 2.62729-	52145	4	53		1014
0.0	+ 0 1.96523- 7						2145	4	53	1015
0.0	+ 0 5.00000+ 6		0	0	8		02145	4	53	1016
0.0	+ 0 1.64309- 2 0.0		+ 0 4.93507- 4 0.0		+ 0 6.35103-	52145	4	53		1017
0.0	+ 0 1.00553- 6						2145	4	53	1018
0.0	+ 0 6.00000+ 6		0	0	10		02145	4	53	1019
0.0	+ 0 2.19529- 2 0.0		+ 0 1.19863- 3 0.0		+ 0 9.14712-	52145	4	53		1020
0.0	+ 0 3.47306- 6 0.0		+ 0 4.26326- 9				2145	4	53	1021
0.0	+ 0 7.00000+ 6		0	0	10		02145	4	53	1022
0.0	+ 0 2.76750- 2 0.0		+ 0 1.83974- 3 0.0		+ 0 6.87882-	52145	4	53		1023
0.0	+ 0 8.90243- 6 0.0		+ 0 2.02054- 8				2145	4	53	1024
0.0	+ 0 8.00000+ 6		0	0	10		02145	4	53	1025
0.0	+ 0 3.31962- 2 0.0		+ 0 2.34384- 3 0.0		+ 0-6.60978-	62145	4	53		1026
0.0	+ 0 1.86505- 5 0.0		+ 0 8.49355- 8				2145	4	53	1027
0.0	+ 0 9.00000+ 6		0	0	12		02145	4	53	1028
0.0	+ 0 3.81284- 2 0.0		+ 0 2.74951- 3 0.0		+ 0-8.62007-	52145	4	53		1029
0.0	+ 0 3.31531- 5 0.0		+ 0 2.83046- 7 0.0		+ 0-8.67073-	102145	4	53		1030
0.0	+ 0 1.00000+ 7		0	0	12		02145	4	53	1031
0.0	+ 0 4.21879- 2 0.0		+ 0 3.12258- 3 0.0		+ 0-1.12793-	42145	4	53		1032
0.0	+ 0 5.10858- 5 0.0		+ 0 7.67261- 7 0.0		+ 0 1.15751-	92145	4	53		1033
0.0	+ 0 1.10000+ 7		0	0	12		02145	4	53	1034
0.0	+ 0 4.55679- 2 0.0		+ 0 3.53300- 3 0.0		+ 0-6.11678-	52145	4	53		1035
0.0	+ 0 7.12191- 5 0.0		+ 0 1.68650- 6 0.0		+ 0 2.61257-	92145	4	53		1036
0.0	+ 0 1.15000+ 7		0	0	12		02145	4	53	1037
0.0	+ 0 4.70417- 2 0.0		+ 0 3.75311- 3 0.0		+ 0-1.05144-	52145	4	53		1038
0.0	+ 0 8.14812- 5 0.0		+ 0 2.37068- 6 0.0		+ 0 3.79298-	92145	4	53		1039

							MAT	MF	MT	SEQ	
.....	10.....	20.....	30.....	40.....	50.....	60.....					
0.0	+ 0	1.20000+ 7		0	0	12	02145	4	53	1040	
0.0	+ 0	4.83873- 2 0.0		+ 0	3.97787- 3 0.0	+ 0	5.11811-	52145	4	53	1041
0.0	+ 0	9.14062- 5 0.0		+ 0	3.24077- 6 0.0	+ 0	5.45540-	92145	4	53	1042
0.0	+ 0	1.25000+ 7		0	0	12	02145	4	53	1043	
0.0	+ 0	4.95699- 2 0.0		+ 0	4.19761- 3 0.0	+ 0	1.19042-	42145	4	53	1044
0.0	+ 0	1.00464- 4 0.0		+ 0	4.31237- 6 0.0	+ 0	7.78811-	92145	4	53	1045
0.0	+ 0	1.30000+ 7		0	0	12	02145	4	53	1046	
0.0	+ 0	5.05990- 2 0.0		+ 0	4.40746- 3 0.0	+ 0	1.89413-	42145	4	53	1047
0.0	+ 0	1.08242- 4 0.0		+ 0	5.60825- 6 0.0	+ 0	1.10934-	82145	4	53	1048
0.0	+ 0	1.35000+ 7		0	0	12	02145	4	53	1049	
0.0	+ 0	5.14914- 2 0.0		+ 0	4.60393- 3 0.0	+ 0	2.59665-	42145	4	53	1050
0.0	+ 0	1.14414- 4 0.0		+ 0	7.15460- 6 0.0	+ 0	1.58160-	82145	4	53	1051
0.0	+ 0	1.40000+ 7		0	0	14	02145	4	53	1052	
0.0	+ 0	5.22605- 2 0.0		+ 0	4.78362- 3 0.0	+ 0	3.27567-	42145	4	53	1053
0.0	+ 0	1.18729- 4 0.0		+ 0	8.95154- 6 0.0	+ 0	2.12900-	82145	4	53	1054
0.0	+ 0	-3.57509-10					2145	4	53	1055	
0.0	+ 0	1.45000+ 7		0	0	14	02145	4	53	1056	
0.0	+ 0	5.29211- 2 0.0		+ 0	4.94548- 3 0.0	+ 0	3.93212-	42145	4	53	1057
0.0	+ 0	1.21158- 4 0.0		+ 0	1.10662- 5 0.0	+ 0	3.03449-	82145	4	53	1058
0.0	+ 0	-5.21878-10					2145	4	53	1059	
0.0	+ 0	1.50000+ 7		0	0	14	02145	4	53	1060	
0.0	+ 0	5.35400- 2 0.0		+ 0	5.09623- 3 0.0	+ 0	4.57246-	42145	4	53	1061
0.0	+ 0	1.22119- 4 0.0		+ 0	1.35115- 5 0.0	+ 0	4.60529-	82145	4	53	1062
0.0	+ 0	4.72990-11					2145	4	53	1063	
0.0	+ 0	1.60000+ 7		0	0	14	02145	4	53	1064	
0.0	+ 0	5.47302- 2 0.0		+ 0	5.36167- 3 0.0	+ 0	5.84357-	42145	4	53	1065
0.0	+ 0	1.20115- 4 0.0		+ 0	1.94850- 5 0.0	+ 0	9.30671-	82145	4	53	1066
0.0	+ 0	7.48383-11					2145	4	53	1067	
0.0	+ 0	1.70000+ 7		0	0	14	02145	4	53	1068	
0.0	+ 0	5.61066- 2 0.0		+ 0	5.60689- 3 0.0	+ 0	7.19410-	42145	4	53	1069
0.0	+ 0	1.15940- 4 0.0		+ 0	2.68961- 5 0.0	+ 0	1.84125-	72145	4	53	1070
0.0	+ 0	1.30425-10					2145	4	53	1071	
0.0	+ 0	1.80000+ 7		0	0	14	02145	4	53	1072	
0.0	+ 0	5.78459- 2 0.0		+ 0	5.85023- 3 0.0	+ 0	8.70104-	42145	4	53	1073
0.0	+ 0	1.12524- 4 0.0		+ 0	3.54520- 5 0.0	+ 0	3.51918-	72145	4	53	1074
0.0	+ 0	2.59881-10					2145	4	53	1075	
0.0	+ 0	1.90000+ 7		0	0	14	02145	4	53	1076	
0.0	+ 0	5.99972- 2 0.0		+ 0	6.09762- 3 0.0	+ 0	1.03777-	32145	4	53	1077
0.0	+ 0	1.11717- 4 0.0		+ 0	4.44747- 5 0.0	+ 0	6.43908-	72145	4	53	1078
0.0	+ 0	5.73650-10					2145	4	53	1079	
0.0	+ 0	2.00000+ 7		0	0	16	02145	4	53	1080	
0.0	+ 0	6.24826- 2 0.0		+ 0	6.34356- 3 0.0	+ 0	1.21673-	32145	4	53	1081
0.0	+ 0	1.14078- 4 0.0		+ 0	5.29948- 5 0.0	+ 0	1.10802-	62145	4	53	1082
0.0	+ 0	5.36386-10 0.0		+ 0	-2.34255-10			2145	4	53	1083
							2145	4	0	1084	
2.10450+	4	4.45698+ 1		0	1	0	02145	4	54	1085	
0.0	+ 0	4.45698+ 1		0	2	0	02145	4	54	1086	
0.0	+ 0	0.0 + 0		0	0	1	332145	4	54	1087	
	33	2		0	0	0	02145	4	54	1088	
0.0	+ 0	7.36359+ 5		0	0	2	02145	4	54	1089	
0.0	+ 0	0.0 + 0					2145	4	54	1090	
0.0	+ 0	9.60170+ 5		0	0	4	02145	4	54	1091	
0.0	+ 0	2.16972- 4 0.0		+ 0	-2.79390- 4			2145	4	54	1092
0.0	+ 0	9.96365+ 5		0	0	4	02145	4	54	1093	
0.0	+ 0	5.50534- 4 0.0		+ 0	-3.71518- 4			2145	4	54	1094

							MAT	MF	MT	SEQ
.....	10.....	20.....	30.....	40.....	50.....	60.....				
0.0	+ 0 1.00000+ 6		0	0	4		02145	4	54	1095
0.0	+ 0 7.63519- 4 0.0		+ 0-3.89563- 4				2145	4	54	1096
0.0	+ 0 1.26414+ 6		0	0	6		02145	4	54	1097
0.0	+ 0 4.28031- 3 0.0		+ 0-1.21961- 3 0.0		+ 0-3.75661- 72145	4 54	1098			
0.0	+ 0 1.33244+ 6		0	0	6		02145	4	54	1099
0.0	+ 0 3.37186- 3 0.0		+ 0-1.08832- 3 0.0		+ 0-2.69877- 72145	4 54	1100			
0.0	+ 0 1.46556+ 6		0	0	6		02145	4	54	1101
0.0	+ 0 4.74375- 3 0.0		+ 0-1.41874- 3 0.0		+ 0-2.69923- 72145	4 54	1102			
0.0	+ 0 1.69878+ 6		0	0	8		02145	4	54	1103
0.0	+ 0 6.97424- 3 0.0		+ 0-1.91595- 3 0.0		+ 0-8.93512- 72145	4 54	1104			
0.0	+ 0-1.51248- 7						2145	4	54	1105
0.0	+ 0 1.84100+ 6		0	0	8		02145	4	54	1106
0.0	+ 0 7.22216- 3 0.0		+ 0-2.01109- 3 0.0		+ 0-1.14530- 62145	4 54	1107			
0.0	+ 0-2.12302- 7						2145	4	54	1108
0.0	+ 0 1.94263+ 6		0	0	8		02145	4	54	1109
0.0	+ 0 7.93519- 3 0.0		+ 0-2.15584- 3 0.0		+ 0-1.32179- 62145	4 54	1110			
0.0	+ 0-2.57784- 7						2145	4	54	1111
0.0	+ 0 2.00000+ 6		0	0	8		02145	4	54	1112
0.0	+ 0 8.22690- 3 0.0		+ 0-2.20265- 3 0.0		+ 0-1.42360- 62145	4 54	1113			
0.0	+ 0-2.85573- 7						2145	4	54	1114
0.0	+ 0 3.00000+ 6		0	0	8		02145	4	54	1115
0.0	+ 0 1.15573- 2 0.0		+ 0-2.39346- 3 0.0		+ 0-6.05241- 62145	4 54	1116			
0.0	+ 0-2.14015- 6						2145	4	54	1117
0.0	+ 0 4.00000+ 6		0	0	10		02145	4	54	1118
0.0	+ 0 1.29967- 2 0.0		+ 0-1.93836- 3 0.0		+ 0-3.15193- 52145	4 54	1119			
0.0	+ 0-1.55318- 5 0.0		+ 0-3.45960- 9				2145	4	54	1120
0.0	+ 0 5.00000+ 6		0	0	10		02145	4	54	1121
0.0	+ 0 1.58134- 2 0.0		+ 0-1.33232- 3 0.0		+ 0-1.02681- 42145	4 54	1122			
0.0	+ 0-5.84431- 5 0.0		+ 0-2.85093- 8				2145	4	54	1123
0.0	+ 0 6.00000+ 6		0	0	12		02145	4	54	1124
0.0	+ 0 2.02263- 2 0.0		+ 0-5.80343- 4 0.0		+ 0-1.91990- 42145	4 54	1125			
0.0	+ 0-1.18541- 4 0.0		+ 0-1.83773- 7 0.0		+ 0-1.96673- 102145	4 54	1126			
0.0	+ 0 7.00000+ 6		0	0	12		02145	4	54	1127
0.0	+ 0 2.52569- 2 0.0		+ 0 2.63648- 4 0.0		+ 0-2.51643- 42145	4 54	1128			
0.0	+ 0-1.59557- 4 0.0		+ 0-9.31677- 7 0.0		+ 0-1.16665- 92145	4 54	1129			
0.0	+ 0 8.00000+ 6		0	0	12		02145	4	54	1130
0.0	+ 0 3.02467- 2 0.0		+ 0 1.07502- 3 0.0		+ 0-2.97515- 42145	4 54	1131			
0.0	+ 0-1.72727- 4 0.0		+ 0-3.79620- 6 0.0		+ 0-5.26561- 92145	4 54	1132			
0.0	+ 0 9.00000+ 6		0	0	12		02145	4	54	1133
0.0	+ 0 3.44338- 2 0.0		+ 0 1.69458- 3 0.0		+ 0-3.67076- 42145	4 54	1134			
0.0	+ 0-1.73984- 4 0.0		+ 0-1.25172- 5 0.0		+ 0-1.85809- 82145	4 54	1135			
0.0	+ 0 1.00000+ 7		0	0	14		02145	4	54	1136
0.0	+ 0 3.76062- 2 0.0		+ 0 2.09406- 3 0.0		+ 0-4.59287- 42145	4 54	1137			
0.0	+ 0-1.89944- 4 0.0		+ 0-3.43876- 5 0.0		+ 0-5.49028- 82145	4 54	1138			
0.0	+ 0-2.00739-10						2145	4	54	1139
0.0	+ 0 1.10000+ 7		0	0	14		02145	4	54	1140
0.0	+ 0 4.07152- 2 0.0		+ 0 2.43460- 3 0.0		+ 0-5.36342- 42145	4 54	1141			
0.0	+ 0-2.47745- 4 0.0		+ 0-8.03361- 5 0.0		+ 0-1.41164- 72145	4 54	1142			
0.0	+ 0-5.76014-10						2145	4	54	1143
0.0	+ 0 1.15000+ 7		0	0	14		02145	4	54	1144
0.0	+ 0 4.25817- 2 0.0		+ 0 2.63640- 3 0.0		+ 0-5.57542- 42145	4 54	1145			
0.0	+ 0-2.97779- 4 0.0		+ 0-1.15415- 4 0.0		+ 0-2.18221- 72145	4 54	1146			
0.0	+ 0-9.31409-10						2145	4	54	1147
0.0	+ 0 1.20000+ 7		0	0	14		02145	4	54	1148
0.0	+ 0 4.47545- 2 0.0		+ 0 2.87317- 3 0.0		+ 0-5.63692- 42145	4 54	1149			

10.....20.....30.....40.....50.....60.....	MAT	MF	MT	SEQ
0.0	+ 0-3.61401- 4 0.0	+ 0-1.58569- 4 0.0	+ 0-3.30677-	72145	4 54 1150
0.0	+ 0-1.46975- 9			2145	4 54 1151
0.0	+ 0 1.25000+ 7	0	0	14	02145 4 54 1152
0.0	+ 0 4.71652- 2 0.0	+ 0 3.13937- 3 0.0	+ 0-5.53004-	42145	4 54 1153
0.0	+ 0-4.34458- 4 0.0	+ 0-2.07749- 4 0.0	+ 0-4.91525-	72145	4 54 1154
0.0	+ 0-2.26616- 9			2145	4 54 1155
0.0	+ 0 1.30000+ 7	0	0	14	02145 4 54 1156
0.0	+ 0 4.97046- 2 0.0	+ 0 3.42389- 3 0.0	+ 0-5.24951-	42145	4 54 1157
0.0	+ 0-5.10569- 4 0.0	+ 0-2.59450- 4 0.0	+ 0-7.18662-	72145	4 54 1158
0.0	+ 0-3.42681- 9			2145	4 54 1159
0.0	+ 0 1.35000+ 7	0	0	14	02145 4 54 1160
0.0	+ 0 5.22206- 2 0.0	+ 0 3.71146- 3 0.0	+ 0-4.80059-	42145	4 54 1161
0.0	+ 0-5.82196- 4 0.0	+ 0-3.09353- 4 0.0	+ 0-1.03664-	62145	4 54 1162
0.0	+ 0-5.10103- 9			2145	4 54 1163
0.0	+ 0 1.40000+ 7	0	0	14	02145 4 54 1164
0.0	+ 0 5.45497- 2 0.0	+ 0 3.98561- 3 0.0	+ 0-4.19879-	42145	4 54 1165
0.0	+ 0-6.42225- 4 0.0	+ 0-3.53254- 4 0.0	+ 0-1.48006-	62145	4 54 1166
0.0	+ 0-7.49491- 9			2145	4 54 1167
0.0	+ 0 1.45000+ 7	0	0	14	02145 4 54 1168
0.0	+ 0 5.65705- 2 0.0	+ 0 4.23437- 3 0.0	+ 0-3.46696-	42145	4 54 1169
0.0	+ 0-6.85962- 4 0.0	+ 0-3.88176- 4 0.0	+ 0-2.09175-	62145	4 54 1170
0.0	+ 0-1.08987- 8			2145	4 54 1171
0.0	+ 0 1.50000+ 7	0	0	16	02145 4 54 1172
0.0	+ 0 5.82494- 2 0.0	+ 0 4.45423- 3 0.0	+ 0-2.63848-	42145	4 54 1173
0.0	+ 0-7.11583- 4 0.0	+ 0-4.12769- 4 0.0	+ 0-2.92720-	62145	4 54 1174
0.0	+ 0-1.59079- 8 0.0	+ 0-1.18648-10		2145	4 54 1175
0.0	+ 0 1.60000+ 7	0	0	16	02145 4 54 1176
0.0	+ 0 6.06012- 2 0.0	+ 0 4.80156- 3 0.0	+ 0-8.39166-	52145	4 54 1177
0.0	+ 0-7.14210- 4 0.0	+ 0-4.32865- 4 0.0	+ 0-5.63282-	62145	4 54 1178
0.0	+ 0-3.24279- 8 0.0	+ 0-2.60246-10		2145	4 54 1179
0.0	+ 0 1.70000+ 7	0	0	16	02145 4 54 1180
0.0	+ 0 6.19674- 2 0.0	+ 0 5.05064- 3 0.0	+ 0 9.47351-	52145	4 54 1181
0.0	+ 0-6.71969- 4 0.0	+ 0-4.24464- 4 0.0	+ 0-1.04676-	52145	4 54 1182
0.0	+ 0-6.42047- 8 0.0	+ 0-5.51132-10		2145	4 54 1183
0.0	+ 0 1.80000+ 7	0	0	16	02145 4 54 1184
0.0	+ 0 6.28545- 2 0.0	+ 0 5.24031- 3 0.0	+ 0 2.55256-	42145	4 54 1185
0.0	+ 0-6.11321- 4 0.0	+ 0-4.02822- 4 0.0	+ 0-1.85997-	52145	4 54 1186
0.0	+ 0-1.22993- 7 0.0	+ 0-1.12361- 9		2145	4 54 1187
0.0	+ 0 1.90000+ 7	0	0	16	02145 4 54 1188
0.0	+ 0 6.36813- 2 0.0	+ 0 5.40828- 3 0.0	+ 0 3.90870-	42145	4 54 1189
0.0	+ 0-5.51349- 4 0.0	+ 0-3.80652- 4 0.0	+ 0-3.12936-	52145	4 54 1190
0.0	+ 0-2.27241- 7 0.0	+ 0-2.20066- 9		2145	4 54 1191
0.0	+ 0 2.00000+ 7	0	0	16	02145 4 54 1192
0.0	+ 0 6.47062- 2 0.0	+ 0 5.58323- 3 0.0	+ 0 5.02152-	42145	4 54 1193
0.0	+ 0-5.01502- 4 0.0	+ 0-3.65879- 4 0.0	+ 0-4.94761-	52145	4 54 1194
0.0	+ 0-4.04793- 7 0.0	+ 0-4.13912- 9		2145	4 54 1195
				2145	4 54 1196
2.10450+ 4	4.45698+ 1	0	1	0	02145 4 55 1197
0.0	+ 0 4.45698+ 1	0	2	0	02145 4 55 1198
0.0	+ 0 0.0 + 0	0	0	1	322145 4 55 1199
	32	2	0	0	02145 4 55 1200
0.0	+ 0 9.60170+ 5	0	0	2	02145 4 55 1201
0.0	+ 0 0.0 + 0				2145 4 55 1202
0.0	+ 0 9.96365+ 5	0	0	4	02145 4 55 1203
0.0	+ 0-1.05773- 2 0.0	+ 0 3.45368- 6		2145	4 55 1204

	10.....	20.....	30.....	40.....	50.....	60.....	MAT	MF	MT	SEQ
0.0	+ 0 3.50838- 2 0.0	+ 0 -3.04347- 3 0.0	+ 0 -2.26350-	32145	4 57	1480				
0.0	+ 0 -6.08299- 4 0.0	+ 0 1.03259- 4 0.0	+ 0 6.22697-	62145	4 57	1481				
0.0	+ 0 4.76783- 8 0.0	+ 0 4.90926-10		2145	4 57	1482				
0.0	+ 0 1.90000+ 7	0 0	16	02145	4 57	1483				
0.0	+ 0 3.55051- 2 0.0	+ 0 -2.78182- 3 0.0	+ 0 -2.25013-	32145	4 57	1484				
0.0	+ 0 -6.25664- 4 0.0	+ 0 8.02815- 5 0.0	+ 0 1.03472-	52145	4 57	1485				
0.0	+ 0 8.66863- 8 0.0	+ 0 9.47997-10		2145	4 57	1486				
0.0	+ 0 2.00000+ 7	0 0	16	02145	4 57	1487				
0.0	+ 0 3.61160- 2 0.0	+ 0 -2.50744- 3 0.0	+ 0 -2.23773-	32145	4 57	1488				
0.0	+ 0 -6.45027- 4 0.0	+ 0 5.34413- 5 0.0	+ 0 1.61877-	52145	4 57	1489				
0.0	+ 0 1.51755- 7 0.0	+ 0 1.75862- 9		2145	4 57	1490				
				2145	4 0	1491				
2.10450+	4 4.45698+ 1	0 1	0	02145	4 58	1492				
0.0	+ 0 4.45698+ 1	0 2	0	02145	4 58	1493				
0.0	+ 0 0.0 + 0	0 0	1	282145	4 58	1494				
	28 2	0 0	0	02145	4 58	1495				
0.0	+ 0 1.33244+ 6	0 0	2	02145	4 58	1496				
0.0	+ 0 0.0 + 0			2145	4 58	1497				
0.0	+ 0 1.46556+ 6	0 0	4	02145	4 58	1498				
0.0	+ 0 -8.13786- 3 0.0	+ 0 -5.69581- 6		2145	4 58	1499				
0.0	+ 0 1.69878+ 6	0 0	6	02145	4 58	1500				
0.0	+ 0 -1.37150- 2 0.0	+ 0 -4.39807- 5 0.0	+ 0 -9.35128-	92145	4 58	1501				
0.0	+ 0 1.84100+ 6	0 0	6	02145	4 58	1502				
0.0	+ 0 -1.53728- 2 0.0	+ 0 -8.10342- 5 0.0	+ 0 -2.41171-	82145	4 58	1503				
0.0	+ 0 1.94263+ 6	0 0	6	02145	4 58	1504				
0.0	+ 0 -1.63331- 2 0.0	+ 0 -1.13892- 4 0.0	+ 0 -4.47627-	82145	4 58	1505				
0.0	+ 0 2.00000+ 6	0 0	6	02145	4 58	1506				
0.0	+ 0 -1.67039- 2 0.0	+ 0 -1.34635- 4 0.0	+ 0 -6.06639-	82145	4 58	1507				
0.0	+ 0 3.00000+ 6	0 0	8	02145	4 58	1508				
0.0	+ 0 -1.90652- 2 0.0	+ 0 -6.41124- 4 0.0	+ 0 -5.13966-	62145	4 58	1509				
0.0	+ 0 -4.08888- 9			2145	4 58	1510				
0.0	+ 0 4.00000+ 6	0 0	8	02145	4 58	1511				
0.0	+ 0 -1.82415- 2 0.0	+ 0 -1.26047- 3 0.0	+ 0 -4.08850-	52145	4 58	1512				
0.0	+ 0 -1.03332- 7			2145	4 58	1513				
0.0	+ 0 5.00000+ 6	0 0	8	02145	4 58	1514				
0.0	+ 0 -1.45961- 2 0.0	+ 0 -2.01399- 3 0.0	+ 0 -1.70601-	42145	4 58	1515				
0.0	+ 0 -3.37169- 6			2145	4 58	1516				
0.0	+ 0 6.00000+ 6	0 0	10	02145	4 58	1517				
0.0	+ 0 -9.00343- 3 0.0	+ 0 -2.93300- 3 0.0	+ 0 -4.17028-	42145	4 58	1518				
0.0	+ 0 -1.38982- 5 0.0	+ 0 -1.57049- 9		2145	4 58	1519				
0.0	+ 0 7.00000+ 6	0 0	10	02145	4 58	1520				
0.0	+ 0 -2.87831- 3 0.0	+ 0 -3.90594- 3 0.0	+ 0 -7.00652-	42145	4 58	1521				
0.0	+ 0 -3.79165- 5 0.0	+ 0 -7.49638- 8		2145	4 58	1522				
0.0	+ 0 8.00000+ 6	0 0	10	02145	4 58	1523				
0.0	+ 0 3.17235- 3 0.0	+ 0 -4.76816- 3 0.0	+ 0 -9.25608-	42145	4 58	1524				
0.0	+ 0 -7.93775- 5 0.0	+ 0 -3.31060- 7		2145	4 58	1525				
0.0	+ 0 9.00000+ 6	0 0	12	02145	4 58	1526				
0.0	+ 0 9.31140- 3 0.0	+ 0 -5.35490- 3 0.0	+ 0 -1.04775-	32145	4 58	1527				
0.0	+ 0 -1.38196- 4 0.0	+ 0 -1.14536- 6 0.0	+ 0 -5.31991-112145	4 58	1528					
0.0	+ 0 1.00000+ 7	0 0	12	02145	4 58	1529				
0.0	+ 0 1.57402- 2 0.0	+ 0 -5.61359- 3 0.0	+ 0 -1.07746-	32145	4 58	1530				
0.0	+ 0 -2.11127- 4 0.0	+ 0 -3.21170- 6 0.0	+ 0 -2.46458-102145	4 58	1531					
0.0	+ 0 1.10000+ 7	0 0	12	02145	4 58	1532				
0.0	+ 0 2.25014- 2 0.0	+ 0 -5.60008- 3 0.0	+ 0 -1.05709-	32145	4 58	1533				
0.0	+ 0 -2.93653- 4 0.0	+ 0 -7.63222- 6 0.0	+ 0 -1.53756-	82145	4 58	1534				

	10.....20.....30.....40.....50.....60.....	MAT	MF	MT	SEQ
0.0	+ 0 1.92534- 4 0.0	+ 0 1.53738- 5 0.0	+ 0 2.78445-	82145	4 59 1645
0.0	+ 0 4.62939-10			2145	4 59 1646
0.0	+ 0 1.50000+ 7	0	0	14	02145 4 59 1647
0.0	+ 0 5.19523- 2 0.0	+ 0 5.73673- 3 0.0	+ 0 7.81119-	42145	4 59 1648
0.0	+ 0 1.99969- 4 0.0	+ 0 1.95501- 5 0.0	+ 0 3.74180-	82145	4 59 1649
0.0	+ 0 6.62356-10			2145	4 59 1650
0.0	+ 0 1.60000+ 7	0	0	14	02145 4 59 1651
0.0	+ 0 5.23824- 2 0.0	+ 0 6.00221- 3 0.0	+ 0 8.80801-	42145	4 59 1652
0.0	+ 0 2.20393- 4 0.0	+ 0 2.93260- 5 0.0	+ 0 6.43499-	82145	4 59 1653
0.0	+ 0 2.06470-10			2145	4 59 1654
0.0	+ 0 1.70000+ 7	0	0	14	02145 4 59 1655
0.0	+ 0 5.31332- 2 0.0	+ 0 6.33329- 3 0.0	+ 0 9.94277-	42145	4 59 1656
0.0	+ 0 2.47432- 4 0.0	+ 0 4.01413- 5 0.0	+ 0 1.15410-	72145	4 59 1657
0.0	+ 0 2.89303-10			2145	4 59 1658
0.0	+ 0 1.80000+ 7	0	0	14	02145 4 59 1659
0.0	+ 0 5.42015- 2 0.0	+ 0 6.70794- 3 0.0	+ 0 1.11389-	32145	4 59 1660
0.0	+ 0 2.77973- 4 0.0	+ 0 5.08315- 5 0.0	+ 0 2.06122-	72145	4 59 1661
0.0	+ 0 3.61397-10			2145	4 59 1662
0.0	+ 0 1.90000+ 7	0	0	14	02145 4 59 1663
0.0	+ 0 5.55035- 2 0.0	+ 0 7.09549- 3 0.0	+ 0 1.23026-	32145	4 59 1664
0.0	+ 0 3.08593- 4 0.0	+ 0 6.04125- 5 0.0	+ 0 3.64634-	72145	4 59 1665
0.0	+ 0 3.81063-10			2145	4 59 1666
0.0	+ 0 2.00000+ 7	0	0	16	02145 4 59 1667
0.0	+ 0 5.69159- 2 0.0	+ 0 7.46617- 3 0.0	+ 0 1.33514-	32145	4 59 1668
0.0	+ 0 3.36189- 4 0.0	+ 0 6.81783- 5 0.0	+ 0 6.37423-	72145	4 59 1669
0.0	+ 0 9.58417-10 0.0	+ 0 1.49524-10		2145	4 59 1670
				2145	4 0 1671
2.10450+ 4 4.45698+ 1	0	1	0	02145	4 60 1672
0.0	+ 0 4.45698+ 1	0	2	0	02145 4 60 1673
0.0	+ 0 0.0 + 0	0	0	1	262145 4 60 1674
26	2	0	0	0	02145 4 60 1675
0.0	+ 0 1.69878+ 6	0	0	2	02145 4 60 1676
0.0	+ 0 0.0 + 0			2145	4 60 1677
0.0	+ 0 1.84100+ 6	0	0	4	02145 4 60 1678
0.0	+ 0 2.77001- 4 0.0	+ 0 -4.41515- 5		2145	4 60 1679
0.0	+ 0 1.94263+ 6	0	0	4	02145 4 60 1680
0.0	+ 0 7.35324- 4 0.0	+ 0 -1.47344- 4		2145	4 60 1681
0.0	+ 0 2.00000+ 6	0	0	4	02145 4 60 1682
0.0	+ 0 1.07750- 3 0.0	+ 0 -2.32804- 4		2145	4 60 1683
0.0	+ 0 3.00000+ 6	0	0	8	02145 4 60 1684
0.0	+ 0 9.11653- 3 0.0	+ 0 -2.06814- 3 0.0	+ 0 -1.92610-	62145	4 60 1685
0.0	+ 0 -4.51332- 7			2145	4 60 1686
0.0	+ 0 4.00000+ 6	0	0	8	02145 4 60 1687
0.0	+ 0 1.33868- 2 0.0	+ 0 -1.91984- 3 0.0	+ 0 -1.41443-	52145	4 60 1688
0.0	+ 0 -5.25229- 6			2145	4 60 1689
0.0	+ 0 5.00000+ 6	0	0	10	02145 4 60 1690
0.0	+ 0 1.72743- 2 0.0	+ 0 -1.25137- 3 0.0	+ 0 -6.42038-	52145	4 60 1691
0.0	+ 0 -2.85960- 5 0.0	+ 0 -9.78308- 9		2145	4 60 1692
0.0	+ 0 6.00000+ 6	0	0	10	02145 4 60 1693
0.0	+ 0 2.17313- 2 0.0	+ 0 -5.73405- 4 0.0	+ 0 -1.71179-	42145	4 60 1694
0.0	+ 0 -8.00591- 5 0.0	+ 0 -7.40653- 8		2145	4 60 1695
0.0	+ 0 7.00000+ 6	0	0	12	02145 4 60 1696
0.0	+ 0 2.65531- 2 0.0	+ 0 8.93238- 5 0.0	+ 0 -2.92329-	42145	4 60 1697
0.0	+ 0 -1.33697- 4 0.0	+ 0 -4.26419- 7 0.0	+ 0 -4.98584- 10	2145	4 60 1698
0.0	+ 0 8.00000+ 6	0	0	12	02145 4 60 1699

						MAT	MF	MT	SEQ
.....	10.....	20.....	30.....	40.....	50.....	60.....			
0.0	+ 0 3.79166- 5 0.0	+ 0 1.91035- 6 0.0	+ 0 3.09354- 92145 4 61 1810						
0.0	+ 0 1.30000+ 7	0 0	12 02145 4 61 1811						
0.0	+ 0 4.58232- 2 0.0	+ 0 3.32132- 3 0.0	+ 0 -1.18653- 42145 4 61 1812						
0.0	+ 0 4.72364- 5 0.0	+ 0 2.38337- 6 0.0	+ 0 4.57533- 92145 4 61 1813						
0.0	+ 0 1.35000+ 7	0 0	12 02145 4 61 1814						
0.0	+ 0 4.69958- 2 0.0	+ 0 3.55359- 3 0.0	+ 0 -4.84622- 52145 4 61 1815						
0.0	+ 0 5.59598- 5 0.0	+ 0 2.87437- 6 0.0	+ 0 6.74678- 92145 4 61 1816						
0.0	+ 0 1.40000+ 7	0 0	14 02145 4 61 1817						
0.0	+ 0 4.80743- 2 0.0	+ 0 3.78655- 3 0.0	+ 0 2.61769- 52145 4 61 1818						
0.0	+ 0 6.33304- 5 0.0	+ 0 3.35747- 6 0.0	+ 0 9.18703- 92145 4 61 1819						
0.0	+ 0 -2.04500-10		2145 4 61 1820						
0.0	+ 0 1.45000+ 7	0 0	14 02145 4 61 1821						
0.0	+ 0 4.90463- 2 0.0	+ 0 4.01002- 3 0.0	+ 0 1.01777- 42145 4 61 1822						
0.0	+ 0 6.86928- 5 0.0	+ 0 3.87545- 6 0.0	+ 0 1.34523- 82145 4 61 1823						
0.0	+ 0 -3.02696-10		2145 4 61 1824						
0.0	+ 0 1.50000+ 7	0 0	14 02145 4 61 1825						
0.0	+ 0 4.99299- 2 0.0	+ 0 4.21769- 3 0.0	+ 0 1.75452- 42145 4 61 1826						
0.0	+ 0 7.16489- 5 0.0	+ 0 4.45854- 6 0.0	+ 0 1.96616- 82145 4 61 1827						
0.0	+ 0 -4.43854-10		2145 4 61 1828						
0.0	+ 0 1.60000+ 7	0 0	14 02145 4 61 1829						
0.0	+ 0 5.15181- 2 0.0	+ 0 4.57531- 3 0.0	+ 0 3.12819- 42145 4 61 1830						
0.0	+ 0 7.03507- 5 0.0	+ 0 6.09459- 6 0.0	+ 0 4.45967- 82145 4 61 1831						
0.0	+ 0 -3.98364-11		2145 4 61 1832						
0.0	+ 0 1.70000+ 7	0 0	14 02145 4 61 1833						
0.0	+ 0 5.30110- 2 0.0	+ 0 4.85655- 3 0.0	+ 0 4.40435- 42145 4 61 1834						
0.0	+ 0 6.14027- 5 0.0	+ 0 8.87297- 6 0.0	+ 0 9.16044- 82145 4 61 1835						
0.0	+ 0 -8.26143-11		2145 4 61 1836						
0.0	+ 0 1.80000+ 7	0 0	14 02145 4 61 1837						
0.0	+ 0 5.46536- 2 0.0	+ 0 5.09416- 3 0.0	+ 0 5.71096- 42145 4 61 1838						
0.0	+ 0 4.96267- 5 0.0	+ 0 1.32188- 5 0.0	+ 0 1.81114- 72145 4 61 1839						
0.0	+ 0 -1.41003-10		2145 4 61 1840						
0.0	+ 0 1.90000+ 7	0 0	14 02145 4 61 1841						
0.0	+ 0 5.66096- 2 0.0	+ 0 5.31889- 3 0.0	+ 0 7.16111- 42145 4 61 1842						
0.0	+ 0 3.96036- 5 0.0	+ 0 1.91203- 5 0.0	+ 0 3.41237- 72145 4 61 1843						
0.0	+ 0 -1.83689-10		2145 4 61 1844						
0.0	+ 0 2.00000+ 7	0 0	16 02145 4 61 1845						
0.0	+ 0 5.89159- 2 0.0	+ 0 5.54727- 3 0.0	+ 0 8.79178- 42145 4 61 1846						
0.0	+ 0 3.42970- 5 0.0	+ 0 2.60494- 5 0.0	+ 0 5.99153- 72145 4 61 1847						
0.0	+ 0 -6.06495-10 0.0	+ 0 -1.50050-10	2145 4 61 1848						
			2145 4 61 1849						
2.10450+	4 4.45698+ 1	0 1	0 02145 4 91 1850						
0.0	+ 0 4.45698+ 1	0 2	0 02145 4 91 1851						
0.0	+ 0 0.0 + 0	0 0	1 242145 4 91 1852						
	24	0 0	0 02145 4 91 1853						
0.0	+ 0 1.94263+ 6	0 0	2 02145 4 91 1854						
0.0	+ 0 0.0 + 0		2145 4 91 1855						
0.0	+ 0 2.00000+ 6	0 0	4 02145 4 91 1856						
0.0	+ 0 6.45012- 4 0.0	+ 0 4.24715- 6	2145 4 91 1857						
0.0	+ 0 3.00000+ 6	0 0	8 02145 4 91 1858						
0.0	+ 0 1.32184- 2 0.0	+ 0 1.26664- 3 0.0	+ 0 3.61011- 72145 4 91 1859						
0.0	+ 0 4.32632- 8		2145 4 91 1860						
0.0	+ 0 4.00000+ 6	0 0	8 02145 4 91 1861						
0.0	+ 0 1.96467- 2 0.0	+ 0 2.25622- 3 0.0	+ 0 3.93421- 62145 4 91 1862						
0.0	+ 0 7.28118- 7		2145 4 91 1863						
0.0	+ 0 5.00000+ 6	0 0	10 02145 4 91 1864						

	10.....	20.....	30.....	40.....	50.....	60.....	MAT	MF	MT	SEQ
0.0	+ 0 2.19079- 2 0.0	+ 0 2.53387- 3 0.0	+ 0 1.77182-	52145	4 91	1865				
0.0	+ 0 3.85053- 6 0.0	+ 0 8.19103-10		2145	4 91	1866				
0.0	+ 0 6.00000+ 6	0 0	10	02145	4 91	1867				
0.0	+ 0 2.29938- 2 0.0	+ 0 2.65411- 3 0.0	+ 0 4.65438-	52145	4 91	1868				
0.0	+ 0 1.02546- 5 0.0	+ 0 5.14303- 9		2145	4 91	1869				
0.0	+ 0 7.00000+ 6	0 0	12	02145	4 91	1870				
0.0	+ 0 2.37933- 2 0.0	+ 0 2.76604- 3 0.0	+ 0 8.49383-	52145	4 91	1871				
0.0	+ 0 1.74970- 5 0.0	+ 0 2.29633- 8 0.0	+ 0 1.88315-112145	4 91	1872					
0.0	+ 0 8.00000+ 6	0 0	12	02145	4 91	1873				
0.0	+ 0 2.43782- 2 0.0	+ 0 2.86167- 3 0.0	+ 0 1.23565-	42145	4 91	1874				
0.0	+ 0 2.29608- 5 0.0	+ 0 7.72559- 8 0.0	+ 0 7.44577-112145	4 91	1875					
0.0	+ 0 9.00000+ 6	0 0	12	02145	4 91	1876				
0.0	+ 0 2.45559- 2 0.0	+ 0 2.90347- 3 0.0	+ 0 1.53369-	42145	4 91	1877				
0.0	+ 0 2.57852- 5 0.0	+ 0 2.01606- 7 0.0	+ 0 2.22623-102145	4 91	1878					
0.0	+ 0 1.00000+ 7	0 0	12	02145	4 91	1879				
0.0	+ 0 2.44786- 2 0.0	+ 0 2.90952- 3 0.0	+ 0 1.71304-	42145	4 91	1880				
0.0	+ 0 2.69152- 5 0.0	+ 0 4.24318- 7 0.0	+ 0 5.11387-102145	4 91	1881					
0.0	+ 0 1.10000+ 7	0 0	14	02145	4 91	1882				
0.0	+ 0 2.42781- 2 0.0	+ 0 2.89358- 3 0.0	+ 0 1.82214-	42145	4 91	1883				
0.0	+ 0 2.80361- 5 0.0	+ 0 7.57164- 7 0.0	+ 0 1.00175-	92145	4 91	1884				
0.0	+ 0 2.16673-12			2145	4 91	1885				
0.0	+ 0 1.15000+ 7	0 0	14	02145	4 91	1886				
0.0	+ 0 2.41561- 2 0.0	+ 0 2.88223- 3 0.0	+ 0 1.86991-	42145	4 91	1887				
0.0	+ 0 2.89628- 5 0.0	+ 0 9.63139- 7 0.0	+ 0 1.33708-	92145	4 91	1888				
0.0	+ 0 2.93430-12			2145	4 91	1889				
0.0	+ 0 1.20000+ 7	0 0	14	02145	4 91	1890				
0.0	+ 0 2.40294- 2 0.0	+ 0 2.87128- 3 0.0	+ 0 1.91683-	42145	4 91	1891				
0.0	+ 0 3.01535- 5 0.0	+ 0 1.19096- 6 0.0	+ 0 1.79325-	92145	4 91	1892				
0.0	+ 0 4.47447-12			2145	4 91	1893				
0.0	+ 0 1.25000+ 7	0 0	14	02145	4 91	1894				
0.0	+ 0 2.39109- 2 0.0	+ 0 2.86262- 3 0.0	+ 0 1.96844-	42145	4 91	1895				
0.0	+ 0 3.16526- 5 0.0	+ 0 1.43239- 6 0.0	+ 0 2.32925-	92145	4 91	1896				
0.0	+ 0 5.86365-12			2145	4 91	1897				
0.0	+ 0 1.30000+ 7	0 0	14	02145	4 91	1898				
0.0	+ 0 2.38015- 2 0.0	+ 0 2.85633- 3 0.0	+ 0 2.02263-	42145	4 91	1899				
0.0	+ 0 3.33549- 5 0.0	+ 0 1.67906- 6 0.0	+ 0 2.99485-	92145	4 91	1900				
0.0	+ 0 7.56342-12			2145	4 91	1901				
0.0	+ 0 1.35000+ 7	0 0	14	02145	4 91	1902				
0.0	+ 0 2.37008- 2 0.0	+ 0 2.85230- 3 0.0	+ 0 2.08283-	42145	4 91	1903				
0.0	+ 0 3.52934- 5 0.0	+ 0 1.92437- 6 0.0	+ 0 3.83577-	92145	4 91	1904				
0.0	+ 0 1.08950-11			2145	4 91	1905				
0.0	+ 0 1.40000+ 7	0 0	14	02145	4 91	1906				
0.0	+ 0 2.36234- 2 0.0	+ 0 2.85255- 3 0.0	+ 0 2.14866-	42145	4 91	1907				
0.0	+ 0 3.74380- 5 0.0	+ 0 2.15972- 6 0.0	+ 0 4.87606-	92145	4 91	1908				
0.0	+ 0 1.44464-11			2145	4 91	1909				
0.0	+ 0 1.45000+ 7	0 0	14	02145	4 91	1910				
0.0	+ 0 2.35725- 2 0.0	+ 0 2.85850- 3 0.0	+ 0 2.22033-	42145	4 91	1911				
0.0	+ 0 3.97597- 5 0.0	+ 0 2.38232- 6 0.0	+ 0 6.24659-	92145	4 91	1912				
0.0	+ 0 1.83300-11			2145	4 91	1913				
0.0	+ 0 1.50000+ 7	0 0	14	02145	4 91	1914				
0.0	+ 0 2.35413- 2 0.0	+ 0 2.86842- 3 0.0	+ 0 2.29293-	42145	4 91	1915				
0.0	+ 0 4.21367- 5 0.0	+ 0 2.58566- 6 0.0	+ 0 7.88952-	92145	4 91	1916				
0.0	+ 0 2.56969-11			2145	4 91	1917				
0.0	+ 0 1.60000+ 7	0 0	16	02145	4 91	1918				
0.0	+ 0 2.35262- 2 0.0	+ 0 2.89696- 3 0.0	+ 0 2.43985-	42145	4 91	1919				

	10.....	20.....	30.....	40.....	50.....	60.....	MAT	MF	MT	SEQ
0.0	+ 0 4.70577- 5 0.0	+ 0 2.93654- 6 0.0	+ 0 1.23341-	82145	4 91	1920				
0.0	+ 0 4.17216-11 0.0	+ 0 1.38985-13		2145	4 91	1921				
0.0	+ 0 1.70000+ 7	0	0	16	02145	4 91	1922			
0.0	+ 0 2.35651- 2 0.0	+ 0 2.93569- 3 0.0	+ 0 2.59771-	42145	4 91	1923				
0.0	+ 0 5.23583- 5 0.0	+ 0 3.24460- 6 0.0	+ 0 1.89148-	82145	4 91	1924				
0.0	+ 0 6.55140-11 0.0	+ 0 2.68359-13		2145	4 91	1925				
0.0	+ 0 1.80000+ 7	0	0	16	02145	4 91	1926			
0.0	+ 0 2.36309- 2 0.0	+ 0 2.97908- 3 0.0	+ 0 2.76375-	42145	4 91	1927				
0.0	+ 0 5.80449- 5 0.0	+ 0 3.52924- 6 0.0	+ 0 2.83542-	82145	4 91	1928				
0.0	+ 0 1.10686-10 0.0	+ 0 4.10851-13		2145	4 91	1929				
0.0	+ 0 1.90000+ 7	0	0	16	02145	4 91	1930			
0.0	+ 0 2.36963- 2 0.0	+ 0 3.02114- 3 0.0	+ 0 2.92704-	42145	4 91	1931				
0.0	+ 0 6.37463- 5 0.0	+ 0 3.81794- 6 0.0	+ 0 4.15425-	82145	4 91	1932				
0.0	+ 0 1.69668-10 0.0	+ 0 7.79680-13		2145	4 91	1933				
0.0	+ 0 2.00000+ 7	0	0	16	02145	4 91	1934			
0.0	+ 0 2.37638- 2 0.0	+ 0 3.06088- 3 0.0	+ 0 3.08186-	42145	4 91	1935				
0.0	+ 0 6.92862- 5 0.0	+ 0 4.12409- 6 0.0	+ 0 5.85368-	82145	4 91	1936				
0.0	+ 0 2.54156-10 0.0	+ 0 1.23070-12		2145	4 91	1937				
				2145	4 0	1938				
				2145	0 0	1939				
				0 0	0 0	1940				
				-1 0	0 0	0				