# Program ELIESE－1 

FORTRAN－Il Program for Analyses of Elastic and Inelastic Scattering Cross Sections

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## Preface

One day, Mr. Re :urcher visited Miss Eliese Janudac and had a conversation with her about recent research worts in science.

Mr. Researcher; "ilmost all researchers today are using the electronic computer. This is, seems to me, quite nor:ense."

Eliese; "Why ?"
Mr. Researcher; "Deciuse, the electronic computer does work very fast in numerical computation, but it's incompetent and it's also unkind. So then every researcher should spend much time and much money io computing work, not to his orm research work."

Eliese, with a puzzled look; "I don't understand what you're going to say! What's the reason for incompetence of electronic computer ?"
"Well," Mr. Researcher explained, "Suppose Mr. A has written a source program with several mistakes which are quite trivial, for example, a comma was missed or a period was used instead of a comma, so on. The electronic computer points out the program error for the first mistake and stops to work, so that Mr. A can correct it but not the others. In other words, the computer points out every program error in every run of compiling process. Similar problems happen in also writing the input data. So I would say that the only a few percent of all machine running time is actually used for real computing work."

Eliese; "Oh my goodness! Your saying is based on your own way! You are not saying that the researcher's mistake should be corrected by himself, but that the electronic computer should correct the researcher's error. I don't think it's fair !"

Mr. Researcher: "You're probably right! But ......"
Eliese; "Wait! I would emphasize that every people should read carefully the computer manual or the program manual in order to avoid the mistakes. Now, here is a manual for the Program ELIESE-1. I would like to recummend it to all who are going to use ELIESE-1."

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## I. Introduction

This is the manual of IBM-T090 code named as ELIESE-1, which can be used for calculations of any kinds of cross sections for elastic and inelastic scattering of neutrons, protons and alpha particles by means of optical model and of Hauser-Feshbach's method in compourd nuclear process. The Program ELIESE-1 has been prepared by a working group on fast neutron cross sections, as one of the 1963 projects of Japanese Nuclear Data Committee which is an ad-hoc committee of the Atomic Energy Society of Japan. The members of the working group, contributors to ELIESE-1, are composed of people from several labnratories, universities and companies in Japan, so that it should be emphasized that the completion of ELIESE-1 is due to an excellent collaboratior of such people.

Although the similar programs are available by request at the present time, ELIESE-1 has some advantages in working with the cross section evaluation. These advantages may be seen in the detailed description of ELIESE-1 on succeeding sections. It, however, does not imply that the Program ELIESE-1 is the best one, but that many improvements have been included taking account of user's convenience. The policy in making the code was that every user could use it with more results but with less pains. This is reflected in ELIESE-1 as the fact, for example, that it is quite easy to prepare the input data by means of relative address. In order to find the unexpected errors if any in ELIESE-1, the calculated results were compared carefully with those by other programs, ABACUS-2, etc., for typical examples. The comparison of the resuits by ELIESE-1 with those by other codes will be given in a later section where the running time and the stability against mesh size are also illustrated. It is expected, however, that further improvements might be required in the next step of code development. Some of the medifications are already under planning, and more refined program will be available in near future as Program ELIESE-n.

As mentioned in the first paragraph, the Program ELIESE-1 is used in calculating the cross sections oi elastic scattering and of inelastic scattering leaving a few of the low-lying excited states because of the characteristics oi optical model and Hauser-Feshbach's method. Originally, however, it has been required to calculate the cross sections of inelastic scatteriag exciting also the higher excited levels. In these cases, the effects of competing processes play an important role. With the Program ELIESE-1, it is possible to take account of the competition between nucleon emitting processes. For example, ( $n, p$ ) reaction can be included as the only competing process in calculating the cross sections of ( $n, n^{\prime}$ ). As the competing processes in above example, the inclusion of ( $n, \gamma$ ) and ( $n, \alpha$ ) reactions seems to be one of the important subjects in preparing the Program ELIESE-2.

In sections 2 and 3 of this manual, the mathematical descriptions of optical model and of Hacser-Fentbach's method are given. It is not our objective to mention the physical view point but to explain the formulas used in ELIESE-1. The methods of numerical evaluation of formulas described in sections 2 and 3 are explained in section 4. Following sections, 5 to S , are devoted to describing the Program ELIESE-1 itself. Brief explanations about sub-routines and symbols used in ELIESE-1 are given in sections 5 and 7, respectively. Section 6 is used in explaining the method of preparing the input data for initial case and for succeeding cases. The list of the Program ELIESE-1 appears in section 8. Typical examples of calculated results using ELIESE-1


Although all the members of the working group on fast neutron cross sections should be responsible for Frogram ELIESE-1, the present manual has been prepared by not all but a few members listed below:

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## 2. Mathematical Description of Shape

## Elastic Scattering Process

This section is dew :-d to describing the analysis of the elastic scattering process in terms of the optical porential moient so we are not concerned with the physical problems but with the mathematical description of the optical model. The optical potential is a very useful tool not only in analying the scattering phenomena but in understanding the nuclear reactions by means of distorted wave approxination or of compound nucleus model.

In ELIESE-1, the calculations are restricted to only neurrons, protons and alnha particles since the masses of these particles are already set in the Program. Cross sections, energies and lengths are expressed in units of milli-barns, MeV and fermis, respectively.

## 2. 1 Schroedinger equations

Basic radial Schroedinger equations of this program, in center of mass system, are written as

$$
\begin{align*}
& \left\{\frac{d^{2}}{d r^{2}}-\frac{l(l+1)}{r^{2}}+k^{2}+\mathfrak{M}_{c}(r) \div l \mathfrak{M}_{\mathrm{so}}(r)-\mathfrak{B}_{\mathrm{Cou}:}(r)\right\} \hat{Q}_{l}^{(+)}(r)=0  \tag{2.1}\\
& \left\{\frac{d^{2}}{d r^{2}}-\frac{l(l+1)}{r^{2}}+k^{2}+\mathfrak{B}_{\mathrm{c}}(r)-(l \div 1) \mathfrak{M}_{\mathrm{so}}(r)-\mathfrak{B}_{\mathrm{Coul}}(r)\right\} \varphi_{l}^{(-)}(r)=0 \tag{2.2}
\end{align*}
$$

where $\mathfrak{V}_{c}(r)$, $\mathfrak{V}_{5}(r)$ and $\mathfrak{B}_{\operatorname{cov1}}(r)$ are the central, spin-orbit and Coulomb potentials, respectively: The wave functions $\varphi_{1}^{(+)}(r)$ and $\varphi_{l}^{(-)}(r)$ are the radial wave functions correnponding to spin up and spin down. For alpha particles, spin-orbit force is zero, then eq. (2. 2) is identical to eq. (2.1). Wave number $k$ in eqs. (2.1) and (2.2) is defined by

$$
\begin{equation*}
k=\left(2 \mu E / \hbar^{2}\right)^{1 / 2} \tag{2,3}
\end{equation*}
$$

where $\mu$ and $E$ are reduced mass and relative energy between an incident particle and a target nucleus, respectively, and are given as follows;

$$
\begin{align*}
& \mu=\frac{m M}{m+M}  \tag{2.4}\\
& E=\frac{M}{m \div M} E_{0} \tag{2.5}
\end{align*}
$$

where $m$ and $M$ are masses of incident particle and target nucleus and $E_{0}$ is the energy in laboratory system.

## 2. 2 Polentiof form and porameters

2.2.1 Central nuclear patential

In the optical model, we can write the central nuclear potential as

$$
\begin{equation*}
\mathfrak{B}_{c}(r)=\mathfrak{B}_{C R}(r) \div i \mathfrak{W}_{\mathrm{cl}}(r), \tag{2.6}
\end{equation*}
$$

where $\mathfrak{B}_{\mathrm{CR}}(r)$ is the real part and $\mathfrak{M}_{\mathrm{ct}}(r)$ is the imaginary part, respectively.
i) Real part $\mathfrak{B}_{\mathrm{CR}}(r)$

We assume Woods-Saxion form for $\mathfrak{B}_{c \mathrm{c}}(r)$ and represent as

$$
\begin{equation*}
\mathfrak{B}_{C R}(r)=\frac{2 \mu}{\hbar^{2}} V_{C} \tilde{f}_{C R}(r), \tag{2.7}
\end{equation*}
$$

where $\boldsymbol{F}_{c z}(\boldsymbol{r})$ is the shape function written as

$$
\begin{equation*}
\mathfrak{S}_{\mathrm{CR}}(r)=\frac{1}{1 \div \exp \left\{\left(r-R_{0}\right) / a_{0}\right\}} \tag{2.8}
\end{equation*}
$$

and $V_{c}$ is the well depth parameter expressed by

$$
\begin{equation*}
V_{c}=V_{c, a} \div V_{c, 1}\left(E-1.2 Z Z^{\prime} e^{2} / R_{c}\right) \div\left(V_{\bullet y, 0} \div V_{a r a, 1}-E\right)(N-Z) / A \tag{2.9}
\end{equation*}
$$

This well deptly parameter $F_{c}$ is asssumed to be linear form in the energy including the symmetric term for charged particles. The parameter $R_{0}$ in eq. (2.8) is the nuclear radius at which potential depth becomes half value of the maximum. With the conventional nuclear radius parameter $\pi_{0}^{-}$and mass number $A$, we have

$$
\begin{equation*}
R_{0}=r_{0} A^{1 / 3} \tag{2,10}
\end{equation*}
$$

The parameter as in eq. (2.8) is the diffuseness parameter of nuclear surface.
ii) Imaginary part $\mathfrak{R}_{\mathrm{ci}}(r)$

Imaginary part of the central nuclear potential $\mathrm{Rer}_{\mathrm{cr}}(\mathrm{r})$ is represented as

$$
\begin{equation*}
\mathfrak{s}_{c I}(r)=\frac{2 \mu}{k^{2}}\left(W_{1} \tilde{\Psi}_{c 1}(r)+W_{s} \tilde{\psi}_{c s}(r)\right) \tag{2.11}
\end{equation*}
$$

The first term in parentheses stands for the volume absorption of the incident particle and the second term for the surface absorption. Shape functions $\mathfrak{W} c ı(r)$ and $\mathfrak{F} c s(r)$ are respectively written as

$$
\begin{align*}
& \mathfrak{F}_{\mathrm{ct}}(r)= \begin{cases}1 ; & \text { Uniform } \\
\frac{1}{1 \div \exp \left\{\left(r-R_{\mathrm{I}}\right) / a_{1}\right\}} ; & \text { Woodsfaxon }\end{cases}  \tag{2.12}\\
& \mathcal{F}_{c s}(r)= \begin{cases}\operatorname{Exp}\left\{-\left[\left(r-R_{\mathrm{s}}\right) / b\right]^{2}\right\} ; & \text { Gaussian } \\
\frac{4 \cdot \exp \left\{\left(r-R_{\mathrm{s}}\right) / b\right\}}{\left[1 \div \exp \left\{\left(r-R_{\mathrm{s}}\right) / b\right\}\right\}^{2}} ; & \text { Derivative Woods-Saxon }\end{cases}
\end{align*}
$$

Radial parameter $R_{t}$ is defined in the same way as $R_{0}$ with parameter $r_{1}$ instead of $r_{0}$

$$
\begin{equation*}
\mathrm{s}_{2}=r_{1} A^{1 / 3} \tag{2.14}
\end{equation*}
$$

Parameter $R_{\mathrm{s}}$ is defined by

$$
R_{s}=R_{0} \div C_{R}
$$

where $C_{R}$ is any constant value which determines the position of the center of surface potential.
Well depth parameters $W_{1}$ and $W_{s}$ in eq. (2.11) are assumed to be linear form with respect to the energy,

$$
\begin{equation*}
W_{1}=W_{1,0} \div W_{1,1} \cdot E \tag{2.15}
\end{equation*}
$$

and

$$
\begin{equation*}
W_{s}=W_{s, 0} \div W_{s, 1} \cdot E . \tag{2.16}
\end{equation*}
$$

A remark is necessary with regard to uniform volume absorption potential. In adding this volume absorption potential to any surface absorption potential, joining point of these two potentials is defined by

$$
\begin{equation*}
r_{\mathrm{tc}}=R_{\mathrm{s}}-b V \overline{\ln \left(W_{\mathrm{s}} / W_{\mathrm{s}}\right)} \quad \text { for Gaussian } \tag{2.17}
\end{equation*}
$$

and

$$
\begin{equation*}
r_{\mathrm{Ic}}=R_{\mathrm{s}}+b \ln \alpha \text { for Derivative Woods-Saxon } \tag{2.18}
\end{equation*}
$$

where $\alpha$ is

$$
\begin{equation*}
\alpha=\left\{2 W_{\mathrm{s}}-W_{1}-2 V \overline{W_{\mathrm{s}}^{2}-W_{\mathrm{s}} \cdot W_{\mathrm{t}}}\right\} / W_{\mathrm{t}} \tag{2.19}
\end{equation*}
$$

Therefore, in the case of uriform volume absorption plus any surface absorption, we must represent the imaginary part of the nuclear central potential as

$$
\begin{align*}
\mathfrak{B}_{c I}(r) & =\frac{2 \mu}{\hbar^{2}} W_{I} \tilde{\Psi_{c I}(r) ;} & & r \leq r_{1 c}  \tag{2.20}\\
& =\frac{2 \mu}{\hbar^{2}} W_{\leq} \tilde{\Psi}_{c s}(r)^{n} ; & & r>r_{1 c} \tag{2.21}
\end{align*}
$$

### 2.2.2 Spin-orbit potenticl

Spin-orbit force is written in the Thomas form,
where $C_{s o}$ is defined with $z-$ meson mass

$$
\begin{equation*}
C_{\text {so }}=(\pi / m=c)^{2} \tag{2.23}
\end{equation*}
$$

Here $c$ is the light velocity and $m=$ is defined by

$$
\begin{equation*}
m_{\mathrm{x}}=\frac{1}{3}\left(n_{z^{+}} \div m_{z^{-}} \div m m_{\mathrm{i}}^{0}\right) \tag{2.24}
\end{equation*}
$$

Well depth parameters are the same form as (2.9), (2.15) and (2 16), and are written as

$$
\begin{gather*}
V_{\mathrm{so}}=V_{\mathrm{so}, 0}+V_{\mathrm{so}, 1} E  \tag{2.25}\\
W_{\mathrm{so}}=W_{\mathrm{so}, 0} \div W_{\mathrm{so}, 1} E \tag{2.26}
\end{gather*}
$$

### 2.2.3 Coulomb potential

Coulomb potential in the interior region is defined with the assumption of uniform charge distribution, and therefore represented as

$$
\begin{align*}
\dot{\mathfrak{N}}_{\mathrm{con}:}(r) & =\frac{2 \mu}{\hbar^{2}} \frac{Z Z^{\prime} e^{2}}{2 R_{\mathrm{c}}}\left(3-\frac{r^{2}}{R_{c}^{2}}\right) ; r \leq R_{\mathrm{c}}  \tag{2.27}\\
& =\frac{2 \mu}{\hbar^{2}} \frac{Z Z^{\prime} e^{2}}{r} \tag{2.28}
\end{align*}
$$

where $R_{\mathrm{C}}$ is written with parameter $r_{\mathrm{c}}$ as

$$
\begin{equation*}
R_{\mathrm{C}}=r_{\mathrm{C}} A^{2 / 3} \tag{2.29}
\end{equation*}
$$

In the Program ELIESE-1, sign is used for the parameter $r_{c}$ in order to discriminate the kind of the incident particles.

We now integrate the eqs. (2.1) and (2.2) numerically, as explained in section 4. They are cornected smoothly to their asymptotic solutions at the matching point.

## 2. 3 Matching radius

In this sub-section, we intead to explain the definition of the matching radius $r_{\text {ss }}$. At this point, we may consider the wave functions to have their symptotic forms, that is, the value of each potential must be negligible order of magntude in comparison with incident enersy. Thus, the matching radius $r_{x}$ is defined as the maximum value of the solutions of the following equations,

$$
\begin{align*}
& \frac{1}{k^{2}} \mathfrak{V}_{\mathrm{CR}}\left(r_{\mathrm{M}}\right) \leq 10^{-4},  \tag{2.30}\\
& \frac{1}{k^{2}} \mathfrak{V}_{\mathrm{Cl}}\left(r_{\mathrm{M}}\right) \leq 10^{-4} \tag{2.31}
\end{align*}
$$

and the condition $r_{M} \geq R_{c}$.

## 2. 4 Asymptotic form of wave function

Asymtotic expression for wave function consists of the incoming and outgoing parts. Well known expression is
where $x_{1}^{(t)}(\rho)$ is defined with the spherical Neumann and Bessel functions (or Whitaker functions) multiplied by their argument, $\rho=k r$. The wave functions $u_{l}^{(+2)}(\rho)$ and $u_{i}^{(-)}(\rho)$ stand for the outgoing and incoming waves, respectively:

$$
\begin{equation*}
u_{l}^{[s]}(\rho)=G_{l}(\rho) \doteq i F_{2}(\rho) \tag{2.33}
\end{equation*}
$$

In eq. (2.32), $J_{l}^{(x)}$ is called the scattering amplitude and is related with the scattering phase shift $\delta_{b}^{\left({ }^{(2)}\right.}$ as

$$
\begin{equation*}
\eta_{l}^{(=)}=\exp \left(2 i \delta_{l}^{(x)}\right) \tag{2.34}
\end{equation*}
$$

This amplitude is the most important quantity and can be obtained by joining the interior wave function to its asymptotic wave function smoothly at $\rho_{\mathrm{M}}=k r_{\mathrm{s}}$.

The maximum angular momentum $l_{\text {max }}$ is defined $b$; the following condition,

$$
\begin{equation*}
\left(G_{l}\left(\rho_{s}\right) / G_{0}\left(\rho_{s}\right)\right)^{2}>10^{6} \tag{2.35}
\end{equation*}
$$

In the case of neutron, the condition (2.35) means that the penetrabilities of the partial waves effective to the process are larger than $10^{-6}$.

Next, we describe the method of obtaining the inregular solutions of asymptotic wave equacions, $G_{l}(\rho)$ 's. They are derived by the recurrence formulas)

$$
\begin{align*}
& G_{l+1}\left(\rho_{\mathrm{M}}\right)=\frac{l \div 1}{\sqrt{\eta^{2} \div(l+1)^{2}}}\left\{(2 l \div 1)\left(\frac{\eta}{l(l+1)} \div \frac{1}{\rho_{\mathrm{M}}}\right) G_{l}\left(\rho_{\mathrm{M}}\right)\right. \\
&\left.-\frac{1}{l}\left(\eta^{2} \div l^{2}\right)^{1 / 2} G_{i-1}\left(\rho_{\mathrm{M}}\right)\right\} \tag{2.36}
\end{align*}
$$

where $p$ is Coulomb parameter defined by

$$
\begin{equation*}
\eta=\frac{\mu Z Z^{\prime} e^{2}}{\pi^{2} k} \tag{2.37}
\end{equation*}
$$

For the neutron, $\eta$ is, of course, zero, and

$$
\begin{align*}
& \mathrm{G}_{0}\left(\rho_{\mathrm{M}}\right)=\cos \rho_{\mathrm{M}}  \tag{2.38}\\
& \mathrm{G}_{\mathrm{L}}\left(\rho_{\mathrm{N}}\right)=\frac{1}{\rho_{\mathrm{M}}} \cos \rho_{\mathrm{M}} \div \sin \rho_{\mathrm{M}} \tag{2.39}
\end{align*}
$$

If an incident particle is proton or alpha particle, we must find $G_{0}(\rho)$ and $G_{0}{ }^{\prime}(\rho)$ at the asymptotic radius $\rho_{A}$ (see section 4). Asymptotic radius $\rho_{A}$ is defined by ${ }^{3}$ )

$$
\begin{align*}
\rho_{A} & =2 \eta & ; & \text { for } \eta \geq 4  \tag{2.40}\\
& =2 \eta \div 9 ; & & \text { for } \eta<4 . \tag{2.41}
\end{align*}
$$

The Coulomb wave equation for s-wave.

$$
\begin{equation*}
\frac{d^{2} G_{0}}{d \rho^{2}} \div\left(1-\frac{2 \pi}{\rho}\right) G_{0}=0 \tag{2.42}
\end{equation*}
$$

is integrated from $\rho_{\mathrm{A}}$ to $\rho_{\mathrm{s}}$. Using $G_{0}\left(r_{\mathrm{M}}\right)$ and $G_{0}{ }^{\prime}\left(\rho_{\mathrm{M}}\right)$, we obtain $G_{1}\left(\rho_{\mathrm{m}}\right)$ from

$$
\begin{equation*}
G_{1}\left(\rho_{\mathrm{M}}\right)=\frac{1}{V r_{i}^{2}-1}\left\{\left(\eta \div \frac{1}{\rho_{\mathrm{M}}}\right) G_{0}\left(\rho_{\mathrm{N}}\right)-G_{v}^{\prime}\left(\rho_{\mathrm{M}}\right)\right\} \tag{2.43}
\end{equation*}
$$

Now we have had $G_{0}\left(\rho_{\mathrm{M}}\right)$ and $G_{1}\left(\rho_{\mathrm{M}}\right)$. Thus any $G_{l}\left(\rho_{\mathrm{M}}\right)$ is obtained by the eq. (2.36).
Regular wave functions $F_{i}\left(\rho_{M}\right)$ 's are obtained by means of well known Stegux and Abravowitz's downward recurrence method ${ }^{33}$. In section 4, we shall explain this method in detail.

Derivatives of $G_{s}\left(D_{\mathrm{s}}\right)$ and $F_{l}\left(\rho_{\mathrm{N}}\right)$ may be obtained from the formula

$$
\begin{equation*}
X_{l^{\prime}}\left(\rho_{\mathrm{sz}}\right)=\frac{1}{2-1}\left\{\left(\frac{(l \div 1)^{2}}{\rho_{\mathrm{N}}} \div n\right) X_{1}\left(\rho_{\mathrm{M}}\right)-\left((l \div 1)^{2} \div 7^{2}\right)^{1 / 2} X_{8+1}\left(\rho_{\mathrm{N}}\right)\right\} \tag{2.44}
\end{equation*}
$$

where $X_{l}\left(\rho_{M}\right)$ stands $f_{1}$. aither $G_{l}\left(\rho_{\mathrm{s}}\right)$ or $F_{1}\left(\rho_{\mathrm{M}}\right)$.

## 2. 5 Scattering amplitude

Scattering amplitude $: i{ }^{r=3}$ is given by the formula

$$
\begin{equation*}
x_{14}^{(x)}=\frac{f_{t}^{(-)}-\left(\rho_{1}-i s_{l}\right)}{\left.f_{i}^{(=)}-\Lambda_{l} \div i s_{l}\right)} \frac{u_{l}^{(-)}\left(\rho_{\mathrm{M}}\right)}{u_{l}^{(+)}\left(\rho_{\mathrm{s}}\right)} \tag{2.45}
\end{equation*}
$$

where $f_{i}^{(s)}$ is the logarithmic derivative of the interior wave function defined at $r=r_{u}$,

$$
\begin{equation*}
f_{2}^{(x)}=r_{:}\left[\frac{d c_{2}^{(x)}}{d r} / \varphi_{2}^{(x)}\right]_{r_{N}} \tag{2.46}
\end{equation*}
$$

Correspondiag quantity for the incoming and outgoing wave functions in the asymptatic region is

$$
\begin{equation*}
\Delta_{l} \pm i s_{l}=\rho_{\mathrm{M}}\left[\frac{d u_{l}^{(s)}}{d \rho} / u_{l}^{(t)}\right] o_{s_{N}} \tag{2.47}
\end{equation*}
$$

## 2. 3 Cross sections

We have defined $l_{\text {mas }}$ hy the formula $\{2.35)$. This $l_{\text {mas }}$ is somewhat larger than the largest value of the angular momenta which contribute effectively to the cross soctions. This latter value of the angular momentum is indicated by a notation $l_{\text {max }}$, and defined by the condition

$$
\begin{equation*}
\sigma_{c}{ }^{\left(l_{\max } C\right)} \mid \sum_{t=0}^{\theta_{\tan } \mathrm{C}^{-1}} \sigma_{\mathrm{c}}^{(1)} \leq 10^{-4} \tag{2.48}
\end{equation*}
$$

where $\sigma_{\mathrm{c}}{ }^{[1 /}$ is the partial cross section of the formation of compound nucleus. This cross section is obtained by using the transmission coefficient

$$
\begin{equation*}
T_{i}^{(s)}(E)=1-\left|r_{i}(土)\right|^{2}, \tag{2.49}
\end{equation*}
$$

and is written as

$$
\begin{equation*}
\sigma_{c}^{(l)}=\frac{\bar{\sigma}^{2}}{k^{2}}\left\{(l+1) T_{i}^{(+)}+l T_{i}^{(-)}\right\} \times 10 \tag{2.50}
\end{equation*}
$$

Cross section of the formation of compound nucleas is then

$$
\begin{equation*}
\sigma_{\mathrm{c}}=\sum_{l=0}^{\operatorname{man}^{2} c} \sigma_{\mathrm{c}}{ }^{(l)} . \tag{2.51}
\end{equation*}
$$

Elastic scattering and total cross sections for neutrons are calfulated b; the formulas
and

$$
\begin{equation*}
\sigma_{t}=\sigma_{e} \div \sigma_{c} \tag{2.53}
\end{equation*}
$$

Formulas (2.52) and (2.53) cannot be used for the charged particles, because of the Coulomb scattering.

Differential elastic scattering cross section for neutrons is calculated as follows,

$$
\begin{equation*}
\frac{d \sigma_{e}}{d \Omega}=\left\{|A(\theta)|^{2}+|B(0)|^{2}\right\} \times 10 \tag{2.54}
\end{equation*}
$$

where

$$
\begin{equation*}
A(\theta)=\frac{i}{2 k} \sum_{l=0}^{l_{a n} c}\left\{(l+1)\left(1-\eta_{l}^{(+)}\right)+l\left(1-\eta_{l}^{(-)}\right)\right\} P_{l}(\cos \theta), \tag{2.55}
\end{equation*}
$$

and

$$
\begin{equation*}
B(\theta)=\frac{1}{2 k} \sum_{j=0}^{l_{\max } c}\left\{\Gamma_{1}^{(-)}-\pi_{l^{k}}^{k+)}\right\} P_{1}^{1}\{\cos \theta) \tag{2.55}
\end{equation*}
$$

Coefficient of the Legendre expansion of the formula (2.54) is necessary for the reaztor calculations, and is expressed by the formula

$$
\begin{align*}
& \times \mathfrak{R e}\left[\left(1-T_{1_{2}}^{j_{1}}\right)\left(1-T_{1_{2}}^{j_{2}}\right) *\right\} \times 10, \tag{257}
\end{align*}
$$

where $Z$ is the $Z$-coefficient given by Blatt and Biedenarari), and is xipressed in a general form

$$
\begin{align*}
Z\left(l_{1} j_{1} l_{2} j_{2} ;\right. & s L)=(-i)^{-l_{2}+l_{2}+L}\left(2 l_{1} \div 1\right)^{1 / 2}\left(2 l_{2} \div 1\right)^{1 / 2} \\
& \times\left(2 j_{1} \div 1\right)^{1 / 2}\left(2 j_{2} \div 1\right)^{1 / 2}\left(l_{1} l_{2} 00 \mid L 0\right) W\left(I_{1} j_{1} l_{2} j_{2} ; s L\right) \tag{2.57-1}
\end{align*}
$$

The $Z$-coefficient above does not vanish if the following conditions are satisfied: Conditions

1. $l_{2} \div l_{2} \div L=$ even
$\left.\begin{array}{ll}\text { 2. } & |l-s| \leq j \leq l \div s \\ \text { 3. } & \left|l_{2}-L\right| \leq l_{2} \leq l_{1} \div L\end{array}\right\}$
2. $\left|j_{1}-L\right| \leq j_{2} \leq j_{1} \div L \mid$

In eq. (2.57-1), $W\left(I_{1} j_{1} l_{2} j_{2} ; s L\right)$ is so-called Racah coelficient ${ }^{5)}$ and is given as

$$
\begin{align*}
& W(a b c d ; e f)=[(a \div b-e)!(a \div e-b)!(b \div e-a)!(c \div d-e)!(c \div e-d)! \\
& \times(d \div e-c)!(a \div c-f)!(a \div f-c)!(c \div f-a)!(b \div d-f)!(b \div f-d)! \\
& \times(d \div f-b)!][(a \div b \div e \div 1)!(c \div d \div e \div 1)!(a \div c \div f \div 1)!(b \div d \div f \div 1)!\})^{2} \\
& \times \sum_{z}(-)^{2}(a \div b \div c \div d \div 1-z)!1\{(a \div b-e-z)!(c \div d-e-z)!(a \div c-f-z)! \\
& \times(b \div d-f-z)!z!(c \div f-a-d \div z)!(e \div f-b-c \div z)!] . \tag{2.57-3}
\end{align*}
$$

In eq. (2.57), $r_{s}^{(t)}$ is expressed by $r_{i}{ }^{i}$, corresponding to $j=l=1 / 2$.
For elastically scattered protons, diferential cross section is also given by the formula (2.54), but $A(\theta)$ and $B(\theta)$ are somewhat different from (2.55) and (2.56). The corresponding expressions are
and

$$
\begin{equation*}
\left.B(\theta)=\frac{1}{2 k} \sum_{i=0}^{b_{\cot } c} e^{e_{i} \theta_{i}\left[r_{1}(-)\right.}-r_{t}^{(+1)}\right] \cdot P_{1}^{1}(\cos \theta) . \tag{2.59}
\end{equation*}
$$

Coulomb scattering amplitude $f_{c}(\theta)$ is given by

$$
\begin{equation*}
f_{\mathrm{c}}(\theta)=\frac{-\eta}{2 k \sin ^{2}(\theta / 2)} \exp \left[-i T_{\mathrm{c}} \ln \left(\sin ^{2}(\theta / 2)\right) \div 2 i \sigma_{0}\right] \tag{2.60}
\end{equation*}
$$

Phase shift of the Coulomb scattering $\sigma_{l}$ is given by the recurrence relation

$$
\begin{equation*}
e^{2 i \sigma_{l}}=\frac{(l+i \eta)(l-1+i \eta) \cdots \cdots(1+i \eta)}{(l-i \eta)(l-1-i \eta) \cdots \cdots(1-i \eta)} e^{i a a_{0}} \tag{2.61}
\end{equation*}
$$

where

$$
\begin{gather*}
\sigma_{0}=-\eta+\frac{\eta}{2} \ln \left(16 \div r_{1}^{2}\right) \div \frac{7}{2} \tan ^{-1}\left(\frac{r}{4}\right)-\left[\tan ^{-1} \because \tan ^{-i}\left(\frac{n}{2}\right) \div \tan ^{-1}\left(\frac{\eta}{3}\right)\right] \\
-\frac{\ddot{\eta}_{i}}{12\left(16+\eta^{2}\right)}\left[1+\frac{r^{2}-48}{30\left(16 \div r_{i}^{2}\right)^{2}}+\frac{r^{4}-160 r^{2} \div 1250}{105\left(16 \div r^{2}\right)^{4}}\right] \tag{2.62}
\end{gather*}
$$

Sometimes we are interested in the Rutherford ratio of the elastically scattered protons. Cross section of the Rutherford scattering is

$$
\begin{equation*}
\left(\frac{d \sigma_{E}}{d Q}\right)_{R}=\tilde{E}^{\prime} \theta_{j}:=\times 10 \tag{2.63}
\end{equation*}
$$

and then Rutherford ra" withe cross sition is defined by the formula

$$
\left(\frac{d \sigma_{\mathrm{E}}}{d Q}\right)_{\mathrm{R} \cdot \mathrm{se}}=\frac{d \sigma_{\mathrm{E}}}{d Q} /\left(\frac{d \sigma_{\mathrm{s}}}{d \Omega}\right)_{\mathrm{R}}
$$

When aipha partici: E , ini incicent particle, we can write the scattering amplitude

$$
\begin{equation*}
\left.\eta_{1}^{(+2}=y_{1}^{( }\right)=3: \tag{2.65}
\end{equation*}
$$

and therefore

$$
\begin{align*}
& \left.A(\theta)=f_{c} \theta\right) \div \frac{i}{2 k} \sum_{i=0}^{l} e^{2 i \theta_{l}(2 l \div 1)\left(1-\eta_{2}\right) P_{l}(\cos \theta)}  \tag{2.66}\\
& B(\theta)=0 . \tag{2.67}
\end{align*}
$$

## 2. 7 Chi square deviation

Experimental and calculsted angular distributions of scattered particles may be compared by means of the chi square deviation,

$$
\begin{equation*}
x_{\sigma}^{2}=\sum_{\theta}\left[\frac{\sigma^{\operatorname{sn}(\theta)-a \sigma^{e x}(\theta)}}{\Delta \sigma^{\mathrm{ex}}(\theta)}\right]^{2} \tag{2.68}
\end{equation*}
$$

where $a$ is a normalization factor which is a measure of the discrepancy of the absolute values between experimental and calculated cross sections, and is given by

$$
\begin{equation*}
a=\frac{\sum\left[\frac{\sigma^{\operatorname{ex}}(\theta)-\sigma^{\mathrm{th}}(\theta)}{\left(\lambda \sigma^{\operatorname{ex}}(\theta)\right)^{2}}\right]}{\sum\left[\sigma^{\left.\operatorname{ex}(\theta) / \Delta \sigma^{\operatorname{ex}}(\theta)\right]^{2}}\right.} \tag{2.69}
\end{equation*}
$$

where $0^{\text {ex }}(\theta)$ and $\sigma^{\text {th }}(\theta)$ are experimental and calculated differential cross sections, and $\Delta \sigma^{e x}(\theta)$ is the experimental error in differential cross section. In our program, it is also possible to calculate the chi square deviation setting $a$ to unity.

## 2. 8 Legendri: polynomiols

Legendre polynomials are computed by the following relations,

$$
\begin{align*}
& P_{0}(\cos \theta)=1  \tag{2.70}\\
& P_{l}(\cos \theta)=\cos \theta  \tag{2.71}\\
& P_{l+1}(\cos \theta)=\frac{1}{l \div 1}\left\{(2 l \div 1) \cos \theta \cdot P_{l}(\cos \theta)-l P_{t-1}(\cos \theta)\right\},  \tag{2.72}\\
& P_{l}^{\prime}(\cos \theta)=\frac{l+1}{\sin \theta}\left\{\cos \theta \cdot P_{l}(\cos \theta)-P_{l+1}(\cos \theta)\right\} \tag{2.73}
\end{align*}
$$

2. 9 Transfermation of the cross sections from center of moss system (CMS) to lobsratory system (LAB)
i) Angles

Let us define the parameter $\gamma$ as follows,

$$
\begin{equation*}
\gamma=\left(\frac{m m^{\prime}}{M \vec{M} M^{\prime}}\right)^{1 / 2}\left(\frac{E}{E^{\prime}}\right)^{1 / 2}, \tag{2.74}
\end{equation*}
$$

where primed quantities are referred to those of final stage and the energies are in center of mass system. Relations between the scatering angles in CMS and I.AB ar?

$$
\begin{equation*}
\cos \theta_{L}=\frac{\gamma+\cos \theta_{\mathrm{c}}}{\left(1+2 \gamma \cos \theta_{\mathrm{c}}+\gamma^{2}\right)^{1 / 2}} \tag{2.75}
\end{equation*}
$$

or

$$
\begin{equation*}
\tan \theta_{L}=\frac{\sin \theta_{C}}{\gamma+\cos \theta_{C}} \tag{2.76}
\end{equation*}
$$

ii) Cross sentions

Relation between angular distributions in CMS and LAB is $\quad \xi^{-}$

$$
\begin{equation*}
\because \quad\left(\frac{d \sigma}{d \Omega}\right)_{L}=\frac{\left(1+2 \gamma \cos \theta_{c}+\gamma^{2}\right)^{3 / 2}}{\left|1+\gamma \cos \theta_{c}\right|}\left(\frac{d \sigma}{d \Omega}\right)_{c} \tag{2.77}
\end{equation*}
$$

## 2. 10 Recurrence formula for Coulomb phase factor $\exp \left(2 i \sigma_{i}\right)$

Relation given by the formula (2.61) can be separated into real and imaginary parts;

$$
\begin{align*}
& \mathfrak{R e}\left(e^{2 i \sigma_{l+1}}\right)=\left[\frac{(l+1)^{2}-\eta^{2}}{(l+1)^{2}+\eta^{2}} \mathfrak{R e}\left(e^{\left.2 i \sigma_{l}\right)}\right]-\left[\frac{2 \eta(l+1)}{(l+1)^{2}+\eta^{2}} \mathfrak{J m}\left(e^{2 i 0 l}\right)\right],\right.  \tag{2.76}\\
& \Im \mathrm{m}\left(e^{2 i \sigma_{l+1}}\right)=\left[\frac{(l+1)^{2}-\eta^{2}}{(l+1)^{2}+\eta^{2}} \Im \mathrm{~m}\left(e^{2 i \sigma_{l}}\right)\right] \div\left[\frac{2 \eta(l+1)}{(l+1)^{2} \div \eta^{2}} \Re \mathrm{R}\left(e^{\left.2 i \sigma_{i}\right)}\right] .\right. \tag{2.79}
\end{align*}
$$

For the s-wave phase shift, $\sigma_{0}$ has been given by the formula (2.62) and then one can obtain the Coulornb phase shift associated with any l-value, using the above recurrence relations.

## 3. Mathematical Description of Campound Nuclear Process -Hauser-Feshbach's Method ${ }^{\text {() }}$

## 1 -

In this section, we consider the nuclear process via the compound nucleus formation, in the case of the incident and outgoing particles being neutrons. Target and residual nuclei are spacified by their spin $I$, parity $\pi$ and excitation energy $\varepsilon\left(=E-E^{\prime}\right)$. Now we consider the case of the inelastic scattering of neutrons which will be expressed as ( $\left.E I \pi \rightarrow E^{\prime} I^{\prime} \pi^{\prime}\right)$.

## 3. 1 Angular distribution of the inelostic scattering process

Angular distribution of the inelastically scattered neutrons is calculated by the following formula

$$
\begin{equation*}
\frac{d \sigma\left(E I \pi \rightarrow E^{\prime} I^{\prime} \pi^{\prime}\right)}{d \Omega}=\sum_{L=0}^{2 \sum_{\operatorname{mac}}} B_{L}\left(E I \pi \rightarrow E^{\prime} I^{\prime} \pi^{\prime}\right) P_{L}(\cos \theta) \tag{3.1}
\end{equation*}
$$

where

$$
\begin{align*}
B_{L}\left(E I \pi \rightarrow E^{\prime} I^{\prime} \pi^{\prime}\right)=\frac{1}{8 k^{2}} \frac{(-)^{I-I^{\prime}}}{(2 I+1)} \sum_{j \bar{\pi}}^{J \pi} \frac{(2 J+1)^{2}}{\sigma_{J \pi}} \sum_{j l} \omega_{\Pi}(\pi l) \tau_{l^{*}} j(E I J L) \\
\times \sum_{j j^{\prime}} \omega_{\Pi}\left(\pi^{\prime} l^{\prime}\right) \tau_{l^{\prime} x^{\prime} j^{\prime}}\left(E^{\prime} I^{\prime} J L\right) \times 10 . \tag{3.2}
\end{align*}
$$

Here $J$ and $\Pi$ are spin and parity of the compound system, and $\omega_{\Pi}(=l)$ is introduced by taking account of parity conservation,

$$
\begin{equation*}
\omega_{\Pi}(\pi l)=\frac{1}{2}\left|\Pi \div(-)^{t} \pi\right| \tag{3.3}
\end{equation*}
$$

In eq. (3.2), $\tau_{l \pi}{ }^{j}(E I J L)$ is

$$
\begin{equation*}
\tau_{l_{\pi}}{ }^{j}(E I J L)=T_{t^{i}}(E I \bar{\pi}) Z\left(l j l j ; \frac{1}{2} L\right) W(j J j J ; I L) \tag{3.4}
\end{equation*}
$$

where $T_{t}{ }^{i}(E I \pi)$ is the same quantity given by the formula (2.49), and Z-coefficient and Racah coefficient are mentioned in eqs. (2.57-1) to (2.57-3). In the final state, as the reciprocal process, $\Gamma_{y^{\prime}} j^{\prime}\left(E^{\prime} I^{\prime} \pi^{\prime}\right)$ is calculated with emitted neutron energy and angular momentum. In the denominator of the formuia (3.2), $\sigma_{J \Pi}$ is the sum of $T_{i}^{j}$ corresponding to all possible nuclear states;

In general, we should take all possible nuclear reactions into account, such as ( $n, p$ ), $(n, \alpha)$, ( $n, \gamma$ ) and so on, but in our program ( $n, p$ ) process can only be considered as a competing process. Besides, the contributions from highly excited levels which are in continuum region, are not included in this program. We intend to improve these points in future.

## 3. 2 Exce:tation function

By integrating the eq. (3.1) over the angles, the excitation function is obtained as

$$
\begin{equation*}
\sigma\left(E I \pi \rightarrow E^{\prime} I^{\prime} \pi^{\prime}\right)=4 \pi B_{0}\left(E I \pi \rightarrow E^{\prime} I^{\prime} \pi^{\prime}\right) \tag{3.6}
\end{equation*}
$$

where $B_{0}\left(E I \pi \rightarrow E^{\prime} I^{\prime} \pi^{\prime}\right)$ is

$$
\begin{align*}
& B_{0}\left(E I \pi \rightarrow E^{\prime} I^{\prime} \pi^{\prime}\right)=\frac{1}{8 k^{2}} \frac{1}{(2 I+1)} \sum_{J \pi} \frac{2 J+1}{\sigma J \Pi} \sum_{j!} \omega_{\Pi}(\pi l) T_{l^{j}}(E I \pi) \tag{3.7}
\end{align*}
$$

Total inelastic scattering cross section is then

$$
\begin{equation*}
\sigma_{\mathrm{ia}}(E I \Rightarrow)=\frac{T}{E \Gamma^{\prime} z^{\prime}} \sigma\left(E I \approx \rightarrow E I^{\prime} 二^{\prime}\right) \tag{3.8}
\end{equation*}
$$

## 3. 3 Conmpound elastic s=attering cross section

Compound elastic scattering cross section is defined by setting ( $E^{\prime} I^{\prime} \mathbf{L}^{\prime}$ ) equal to ( $E 1=$ ). Then, angular ci.tritution of the compound elastic process is

$$
\begin{equation*}
-\frac{\sigma_{c x}(E I=)}{a!}=\sum_{L=0}^{\Gamma_{i} c} B_{I}\left(E I-j P_{I}(\cos \theta)\right. \tag{3.9}
\end{equation*}
$$

where -

$$
\begin{equation*}
E_{i}(E I \pi)=\frac{10}{8 k^{2}(2 I+1)} \sum_{j \bar{I}} \frac{1}{\sigma_{J I}}\left[(2 J \div 1) \sum_{j^{T}} \omega_{I I}(\bar{I} l)=_{i_{\pi}} j(E I J L)\right]^{2} \tag{3.10}
\end{equation*}
$$

Integrating this ara the angles, we obtain the compound elastic scattering cross section.

$$
\begin{equation*}
\sigma_{i t}(E I \pi)=4=B_{0}(E I \Delta), \tag{3.11}
\end{equation*}
$$

where

In these calculations, we must take care of the relations between angular momenta. The selection rules on the anguiar momenta are as follows:
i) $L=$ even and $0 \leq L \leq \operatorname{Min}\left(2 l_{\text {max }}, 2 l^{\prime}{ }_{\text {max }}\right)$.
ii) $J_{\text {mia }}=0$, if $I$ is half odd integer.

$$
=1 / 2, \quad \text { if } I \text { is integer. }
$$

iii) $J_{\min } \leq J \leq \operatorname{Min}\left(l_{\max } \div I \div \frac{1}{2}, l_{\operatorname{maxC}} \div I^{\prime}+\frac{1}{2}\right)$
iv) $|J-I| \leq j \leq J \div I \leq l_{\text {mace }} \div \frac{1}{2}$.

$$
\left|J-I^{\prime}\right| \leq j^{\prime} \leq J \div I^{\prime} \leq l_{\max }^{\prime} \div \frac{1}{2}
$$

v) $\left|j-\frac{1}{2}\right| \leq l \leq j+\frac{1}{2} \leq l_{\text {mas }}$.

$$
\left|j^{\prime}-\frac{1}{2}\right| \leq l^{\prime} \leq j^{\prime} \div \frac{1}{2} \leq l^{\prime}=a x c
$$

## 4. Methods of Numerical Calculations

1-"
4. 1 Basic constants

Some basic constants set in the program are

$$
\begin{align*}
& m_{\pi}=1.005952 \\
& m_{p}=1.007593 \\
& m_{a}=4.003570  \tag{4.0}\\
& C_{s 0}=(1.42926)^{2} \\
& \left(\frac{2 \mu_{0}}{\hbar^{2}}\right)^{1 / 2}=0.2157135  \tag{4.1}\\
& \frac{2 \mu_{0} e^{2}}{\hbar^{2}}=0.0635747  \tag{4.2}\\
& \frac{2 \mu_{n}}{\hbar^{2}} C_{50}=0.0977178  \tag{4.3}\\
& \eta=\frac{\mu Z Z^{\prime} e^{2}}{\hbar^{2} k}=\frac{Z Z^{\prime} e^{2}}{\sqrt{2} \hbar}\left(\frac{\mu}{E}\right)^{1 / 2}=0.157452 Z Z^{\prime}\left(\frac{\mu}{E}\right)^{1 / 2} . \tag{4.4}
\end{align*}
$$

## 4. 2 Initizi values of wave functions

In numerical integration of Schroedinger equations, we must have the values of the wave functions at first two mesh points as the starting values of the functions. We can obtain these values by power series expansion of the functions;

$$
\begin{equation*}
\varphi_{1}^{(x)}(r)=\sum_{n=0}^{\infty} a_{n, 4} 4^{(t)} r^{n+l+1} \tag{4.5}
\end{equation*}
$$

Relations between expansion coeffcients are

$$
\begin{align*}
& a_{n, i^{(x)}}=\frac{-1}{n(2 l+n+1)}\left\{\left(k^{2}-\mathfrak{B}_{\mathrm{c}}(r)-\frac{3 k \eta}{R_{\mathrm{c}}}\right) a_{n-2, i^{(x)}}\right. \\
&+\frac{k \eta}{R_{\mathrm{c}}^{3}} a_{\left.n-4,1^{(x)}-b_{l}^{(2)} \mathfrak{T}_{\mathrm{so}}(r) a_{n-1, i^{(n)}}\right\}} \tag{4.6}
\end{align*}
$$

where

$$
\begin{align*}
& b_{l}^{(+)}=l,  \tag{4.7}\\
& b_{l}^{(-)}=-(l+1) \tag{4.8}
\end{align*}
$$

- and

$$
\begin{equation*}
\tilde{\mathfrak{Q}}_{\mathrm{so}}(r)=\frac{2 \mu}{\hbar^{2}} C_{s_{0}} \frac{1}{a_{0}}\left(V_{\mathrm{so}} \div i \mathrm{IV}_{\mathrm{s}_{0}}\right) \frac{\exp \left[\left(r-R_{0}\right) / a_{0}\right]}{\left(1 \div \exp \left[\left(r-R_{0}\right) / a_{0} \mid\right]^{2}\right.} \tag{4.9}
\end{equation*}
$$

In eq. (4.6), we assume that the potential values at these mesh points are nearly constant. In particular, Gaussian and derivative Woods-Saxon potential values at these mesh points are reset to the constant values in the program. First four values of the expansion coefficients are

$$
\begin{align*}
& a_{1,} l^{(*)}=\frac{-1}{2(l+1)} b_{l}^{(s)} \tilde{\mathfrak{M}}_{50}(r) a_{0, l}(s), \tag{4.10}
\end{align*}
$$

$$
\begin{align*}
& a_{3, l^{( \pm)}}=\frac{-1}{3(2 l+4)}\left\{\left(k^{2}+\mathfrak{R}_{c}(r)-\frac{3 k_{\eta}}{R_{c}}\right) a_{1,4}^{( \pm)}+b_{l}^{( \pm)} \mathfrak{T}_{s}(r) a_{2, l}^{(t)}\right\} . \tag{4.11}
\end{align*}
$$ and

$$
\begin{align*}
& a_{4, l}^{(=)}=\frac{-1}{4(2 l \div 5)}\left\{\left(k^{2} \div \mathfrak{P}_{c}(r)-\frac{3 k \eta}{R_{c}}\right) a_{2, l^{(s)}} \div b_{l}^{\left(=2 \mathfrak{P}_{50}\right.}(r) a_{3, l}^{(s)}\right. \\
& \left.+\frac{k \eta}{R_{\mathrm{c}}{ }^{3}} a_{0,4}^{(=)}\right\}, \tag{4.13}
\end{align*}
$$

where $a_{0,2}^{( \pm)}$is a normalization constant and can be set to unity.

## 4. 3 Numerical integration of wave functicits

SThe method used for numerical integration is the Fox-Goodwin's two points method. Eqs. (2.1) and (2.2) are rewritten as

$$
\begin{equation*}
\frac{d^{2} \varphi_{l}^{(t)}}{d r^{2}}=Q_{i}^{(t)}(r) \cdot \varphi_{l}^{(t)} \tag{4.14}
\end{equation*}
$$

With Fox-Goodwin's method, we can write this equation as follows;
where $h$ is the step length in this numerical integration, and $n$ indicates the mesh point. Derivative of the function is calculated by Lagrange's six points method;

$$
\begin{align*}
& \frac{d}{d r} \varphi_{l}^{(1)}(n)=\frac{1}{h}\left\{\frac{1}{60}\left(\varphi_{l}^{(1)}(n+3)-\varphi_{l}^{( \pm)}(n-3)\right)+\frac{3}{20}\left(\varphi_{i}^{( \pm)}(n-2)\right.\right. \\
&\left.\left.-\varphi_{l}^{( \pm)}(n+2)\right)+\frac{3}{4}\left(\varphi_{2}^{( \pm)}(n+1)-\varphi_{1}^{(x)}(n-1)\right)\right\} . \tag{4.16}
\end{align*}
$$

## 4. 4 External wove function $F_{l}\left(\rho_{\mathrm{M}}\right)$

In section II, we have shown the method by which the function $G_{l}\left(\rho_{s 1}\right)$ and the maximum angular momentum $l_{\text {atx }}$ are defined. Using $l_{\text {atx }}$ and $G_{l}\left(\rho_{\mathrm{s}}\right)$ for $l \leq l_{\text {atx }}$, we will explain the method ${ }^{3)}$ of the calculation of $F_{1}\left(\rho_{\mathrm{m}}\right)$ in this section.

Let

$$
\begin{align*}
& l^{(1)}=l_{\mathrm{m} \times x}+10  \tag{4.17}\\
& F_{l(1)+1}^{(1)}=0 \tag{4.18}
\end{align*}
$$

and

$$
\begin{equation*}
\bar{E}_{f^{\prime \prime}}{ }^{(1)}=10^{-36} . \tag{4.19}
\end{equation*}
$$

With these startisg values, we can obtain $F_{t}\left(\rho_{\mathrm{M}}\right)$ corresponding to lower $l$-values by the following recurrence formula;

$$
\begin{equation*}
F_{l-1}^{(1)}=\frac{l}{\sqrt{\eta^{2}+l^{2}}}\left\{(2 l+1)\left(\frac{\eta}{l(l+1)}+\frac{1}{\rho_{\mathrm{M}}}\right) F_{l}^{(1)}-\frac{1}{l+1}\left(\eta^{2}+(l+1)^{3}\right)^{1 / 2} F_{l+1}^{(1)}\right\} \tag{4.20}
\end{equation*}
$$

For $l=0$, we obtain the normalization factor by means of Wronskian's rule,

$$
\begin{equation*}
\alpha=\left(1 \div \eta^{2}\right)^{1 / 2}\left(F_{0}^{(1)} G_{2}-G_{0} F_{1}^{(1)}\right) \tag{4.21}
\end{equation*}
$$

and

$$
\begin{equation*}
F_{1}\left(\rho_{\mathrm{s}}\right)=F_{i}^{(1)}\left(\rho_{\mathrm{s}}\right) / \alpha \tag{4.22}
\end{equation*}
$$

If $F_{l}\left(\rho_{\mathrm{M}}\right)$ has the correct value, Wronskian's rule must be satisfied for $l \leq l_{\text {max }}$;

$$
\begin{equation*}
F_{l}^{\prime}\left(\rho_{\mathrm{N}}\right) G_{l}\left(\rho_{\mathrm{M}}\right)-F_{l}\left(\rho_{\mathrm{M}}\right) G_{l}^{\prime}\left(\rho_{\mathrm{N}}\right)=1 \tag{4.23}
\end{equation*}
$$

if it has not, above method is repeated by resetting $l^{(1)}$ as $l^{(1)}+5$.

## 4. 5 Coulom't wave function for $s$-wove

At $\rho=\rho_{\mathrm{M}}$, we can calculate $G_{0}$ and $G_{0^{\prime}}$ by means of the following formulas. ${ }^{22}$
i) $\eta \geq 4$

In this case, we set $\varepsilon_{A}=2 \eta$ and

$$
\begin{gather*}
G_{0}\left(\rho_{\mathrm{A}}\right)-1.293404016 \eta^{1 / 6}\left\{1 \div 0.04959570165 \eta^{-4 / 3}-0.008558888889 \eta^{-2}\right. \\
\left.\div 0.002+55109181 \eta^{-10 / 3}-0.0009108958061 \eta^{-4} \div 0.0002534684115 \eta^{-16 / 3}\right\} \tag{4.24}
\end{gather*}
$$

and

$$
\begin{gather*}
G_{0}^{\prime}\left(\rho_{A}\right)=-0.7078817734 \eta^{-1 / 6}\left\{1-0.1728260369 \eta^{-2 / 3}\right. \\
+0.0003174603174 \eta^{-2}-0.003581214850 \eta^{-8 / 3} \\
\left.+0.0003117824680 \eta^{-4}-0.0009073966427 \eta^{-1 / 1 / 3}\right\} . \tag{4.25}
\end{gather*}
$$

ii) $\eta<4$

Let $\rho_{A}=9 \div 2 \eta$ and $\varphi=\rho_{A}-\eta \cdot \ln \left(2 \rho_{A}\right) \div \sigma_{0}$, then $G_{0}$ and $G_{0}{ }^{\prime}$ are given by

$$
\begin{equation*}
G_{0}\left(\rho_{\mathrm{A}}\right)=s \cdot \cos \varphi-t \cdot \sin \varphi, \tag{4.26}
\end{equation*}
$$

and

$$
\begin{equation*}
G_{0}^{\prime}\left(\rho_{A}\right)=S \cdot \cos \varphi-T \cdot \sin \varphi, \tag{4.27}
\end{equation*}
$$

where

$$
\begin{align*}
& s=\Sigma s_{n},  \tag{4.28}\\
& t=\sum t_{n},  \tag{4.29}\\
& S=\Sigma S_{n}, \tag{4.30}
\end{align*}
$$

and

$$
\begin{equation*}
T=\Sigma T_{n} . \tag{4.31}
\end{equation*}
$$

They are calculated by means of the relations;

$$
\begin{align*}
& s_{n+1}=A_{n} s_{n}-B_{n} t_{n},  \tag{4.32}\\
& t_{n+1}=A_{n} t_{n}+B_{n} s_{n},  \tag{4.33}\\
& S_{n+1}=A_{n} S_{n}-B_{n} T_{n}-\frac{s_{n+1}}{\rho_{\mathrm{A}}}, \tag{4.34}
\end{align*}
$$

and

$$
\begin{equation*}
T_{n+1}=A_{n} T_{n} \div B_{n} S_{n}-\frac{t_{n+1}}{\rho_{\mathrm{A}}} \tag{4.35}
\end{equation*}
$$

Coefficients $A_{n}$ and $B_{n}$ are respectively given by

$$
\begin{equation*}
A_{n}=\frac{2 n \div 1}{2(n \div 1) \rho_{\mathrm{A}}} \eta \tag{4.36}
\end{equation*}
$$

and

$$
\begin{equation*}
B_{n}=\frac{n^{2}-n(n+1)}{2(n \div 1) \rho_{\mathrm{A}}} . \tag{4.37}
\end{equation*}
$$

The initial values are

$$
\begin{align*}
s_{0} & =1  \tag{4.38}\\
t_{0} & =0  \tag{4.39}\\
S_{0} & =0,  \tag{4.40}\\
T_{0} & =1-\left(\eta / \rho_{A}\right) . \tag{4.41}
\end{align*}
$$

iii) Numerical integration of $G_{0}$ and $G_{0}{ }^{\prime}$ from $\rho_{A}$ to $\rho_{\mathcal{N}}$

Wave equation for $G_{0}$ is rewritten as

$$
\begin{equation*}
\frac{d^{2} G_{0}}{d \rho^{2}}=\left(\frac{2 \eta}{\rho}-1\right) G_{0}=f(\rho) \cdot G_{0} \tag{4.42}
\end{equation*}
$$

This equation is integrated from $\rho_{A}$ to $\rho_{\mathrm{y}}$ by means of Fox-Goodwin's method. Therefore, we must find the initial values at two mesh points. In our program, these initial values are calcu-
lated by means of Picard's five poicts method;

$$
\begin{align*}
& \begin{aligned}
& G_{0}(1)=G_{0}(0)-h_{c} G_{0}{ }^{\prime}(0) \div \frac{1}{1440}\left\{3 5 7 f \left(0 ; G_{0}(0) \div 540 f(1) G_{0}(1)\right.\right. \\
& \sim\left.-282 f(2) G_{0}(2) \div 116 f(3) G_{0}(3)-21 f(4) G_{0}(4)\right\},
\end{aligned}  \tag{4.43}\\
& G_{*}(2)=G_{0}(0)-2 \dot{h}_{c} G_{0}{ }^{\prime}(0) \div \frac{1}{1440} h_{c}{ }^{2}\left\{848 f(0) G_{0}(0) \div 2204 f(1) G_{0}(1)\right. \\
& -480 f(2) G_{0}(2) \div 256 f(3) G_{0}(3)-48_{j}\left(4 ; G_{0}(4 j), \quad(3.4 i)\right. \\
& G_{0}(3)=G_{0}(0)-3 h_{c} G_{0}{ }^{\prime}(0) \div \frac{1}{1440} h_{c}=\left[1 3 2 3 f ^ { \prime } \left(0 ; G_{0}(0) \div 4212 f\left(1 ; G_{0}(1)\right.\right.\right. \\
& +486 f(2) G_{0}(2) \div 540 f\left(3 ; G_{0}(3)-81 f\left(4 ; G_{0}(4)\right\}, \quad(4.45 ;\right. \\
& G_{0}(4)=G_{0}(0)-4 h_{c_{0}} G_{0}{ }^{\prime}(0)+\frac{1}{1440} h_{c^{2}}\left\{1 7 9 2 f \left(0_{j}^{j} G_{0}(0)+6144 f\left(1 ; G_{0}(1)\right.\right.\right. \\
& \div 1536 f(2) G_{0}(2) \div 2045 f(3) G_{0}(3) \div 01 \text {. }  \tag{4.46}\\
& \begin{array}{r}
G_{0}(3)=G_{0}(0)-3 h_{c} G_{0}{ }^{\prime}(0) \div \frac{1}{1440} h_{c}=11323 f\left(0 ; G_{0}(0) \div 4212 f\left(1 ; G_{0}(1)\right.\right. \\
+486 f(2) G_{0}(2) \div 540 f\left(3 ; G_{0}(3)-81 f(4) G_{0}(4)\right\}, \\
G_{0}(4)=G_{0}(0)-4 h_{6} G_{0}^{\prime}(0)+\frac{1}{1440} h_{c^{2}}\left\{1 7 9 2 f \left(0 ; G_{0}(0) \div 6144 f\left(1 ; G_{0}(1)\right.\right.\right.
\end{array}
\end{align*}
$$

These are simpie algebraic equations and easily solved. Arguments of $G_{v}{ }^{\prime} n$ ) and $f(n)$ mean the $n^{\text {th }}$ mesh point and $h_{5}$ is step lergth of this numerical method. $G_{0}(3)$ and $G_{0}(4)$ are wised as initial values of Fox-Goodwin's method. Derivative at $\rho=\rho_{\mathrm{M}}$ is given by zneans of the same method as the formula (4.16).

## 5. Progrem Description

## 5. 1 Machine specifications

The Program ELIESE-1 has been writen for an IBM 7000 FORTRAN-II with a 32,768 words memory and at least two tape units.

## 5. 2 General description of the program

The Program ELIESE-1 is compesed of the main-program and 31 sub-programs. CHART 1 shows the flow-chart of ELIESE-1 main-program. The ELIESE-1 sub-programs may be divided into four classes listed below:

1. Impar Routine reats the jupct data recquined for the actual compotation. SUBROUTINE INPUT
2. Computation Routine computes cross sections and chi-square deviations for a given set of input data.

SUBROUTINE PREP SUBROUTINE ANGLE SUBROUTINE WELL SUBROUTINE SPHBES SUBROUTINE GZERO SUBROUTINE PICARD SUBROUTINE GOASMA SUBROUTINE GFLMAX SUBROUUTINE RUTEi SUBROUTINE POTEN SUBROUTINE INIT (L) SUBROUTINE INTEG (I.) SUBROUTINE ETASIG (L) SUBRÓUTINE LEGEEND SUBROUTINE A.MPAB SUBROUTINE BLL SUBROUTINE LABRAT SUBROUTINE CHIEOS SUBROUTINE CÖMPND SUBROUTINE CÖMIP (L, A) SUBROUTINE CLBGD (A)* SUBROUTINE ZETC (A)* SUBROUTTLNE WRACA (A)* SUBROUTINE ZFACT (A)*

* Function type sub-program

3. Output Routine generates the calculated results.

SUBROUTINE OUTPUT SUBROUTINE INLIST SUBRƠUTINE OUTIN SUBROUTINE ALOCK SUBROUTINE BLOCK (FAP language)
4. Check Routine finds out an overflow and/or a divide check condition. SUBROUUTINE OOFLOW (L, A)
The program assumes the presence of the following FORTRAN elementary function sub-routines:-

| LOGF (natural logarithm) | SINF (sine) |
| :--- | :--- |
| COSF (cosine) | EXPF (exponential) |
| SQRTF (square root) | ATANF (arc-tangent) |

5. 3 Detailed descriptions of the specific routines of the program
6. SUBROUTINE PREP sets up a reduced mass, a wave number, potential well depth parameters, a matching radius, Coulomb parameters and other basic quantities used in the computation.
7. SUBROUTINE ANGLES sets up angle points and angular variables.
․ SUBROUTINE WEIL compotes the potential shape functions at each menh point.
8. SUBROUTINE SPHBES generates the functions $G_{i}(p), F_{i}(\rho), G_{1}^{\prime}(\rho)$ and $F_{z}(\rho)$ Ios neutron, and determines the maximum angular momentum $I_{\text {nax }}$.
9. SUBRGUTINE GZER $\bar{O}$ computes the functions $G_{0}(\rho)$ and $G_{0}{ }^{\prime}(\rho)$ at $\rho=\rho_{\mathrm{A}}$ for charged particle.
10. SUBROUTINE PICARD computes the functions $G_{0}(\rho \div h), G_{0}(\rho \div 2 h), G_{0}(\rho \div 3 h)$ and $G_{6}(0 \div 4 \%$ for charsed particle.
11. SUBROUTINE GOASMA integrates the Coulosib wave equation for $G_{A}(\rho)$ from $p_{A}$ to $\rho_{21}$, and generates the derivative $G_{0}{ }^{\prime}\left(\rho_{\mathrm{s}}\right)$.
12. SUBROUTINE GFLIIAX generates the functions $G_{1}(\rho)$, $F_{1}(\rho), G_{1}^{\prime}(\rho)$ and $F_{1}^{\prime}(\rho$, for charged particle, and determines the maximum angular momentum $l_{\text {mor }}$.
13. SUBROUTLNE KUTH computes the Rutherford scattering amplitudes and the cross: sections.
14. SUBROUTINE PKTEN computes the potential values at each mesh point.
15. SUBROUTINE INIT (L) sets up the starting values for the numerical integration of the internal wave equations.
16. SUBROUTINE INTEG (L) integrates the internal save equations up to $\rho_{\mathrm{s}}$ and geterates the deritatires.
i3. SUBROUTINE ETASIG (L) computes the suattering amplitudes $\boldsymbol{f}_{4}{ }^{(3)}$, the penetrabilitis $T_{l^{i}}$ and the reaction cross section, and determines $l_{\text {manc. }}$
17. SUBROUTINE LEGEND generates the Legendre polynomials.
18. SUBROUTINE AMPAB computes $A(\theta), B ; \theta)$ and the differential cross section.
19. SUBROUTINE BLL computes the coefficients of the Legendre expansion of the differertial cross section for neutron scattering.
20. SUBROUTINE LABRAT transforms the differential cross sections from center of mass system to laboratory system.
21. SUBROUTINE CHISOS computes the chi-square deviation of the differential cross sections in the center of mass system.
22. SUBROUTINE COMPXD computes the cross section of the compound nuclear process by means of Halier-Feshrach's method.
23. SUBROUTINE CŌMJP (L, A) computes $\sigma_{j a}$ expresed by (3.5).
