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MEASUREMENT OF DOUBLE DIFFERENTIAL

NEUTRON EMISSION CROSS SECTIONS AT

14.1 MEV FOR Ca, Mn, Co and W

December 1989

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日本原子力研究所 Japan Atomic Energy Research Institute

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Measurement of Double Differential Neutron Emission Cross Sections at 14.1 MeV for Ca, Mn, Co and W

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> > (Received November 28, 1989)

Using the neutron TOF spectrometer at OKTAVIAN, double differential neutron emission cross sections at 14.1 MeV were measured for Ca, Mn, Co and W which are of interest for shielding and structural material elements of fusion reactors. Data were obtained for 16 angle points from 15 to 160 deg in the LAB system for each element, covering the secondary neutron energy region from 0.5 MeV to 15 MeV. Statistics and energy resolution of obtained data are satisfactory.

The double differential cross sections in the LAB system were once converted to those in the center-of-mass system and integrated over scattering angle to obtain neutron emission spectra. Angle-differential cross sections were obtained for the elastic and discrete-inelastic scatterings whose peaks in DDX spectra could be resolved. The measured DDX data are so numerous that only their graphs are shown in this report. However, the graphs and numerical tables are given for the neutron emission spectra and the angle-differential cross sections.

In the graphs, preliminary comparisons are made with evaluated data (ENDF/B-IV and JENDL-3T). The ENDF/B-IV data for Ca are satisfactory in the high energy region, but overestimate the experimental values in the

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low energy region. The JENDL-3T data for Mn reproduce well the angleintegrated neutron emission spectrum, though underestimation is seen in the 6-13 MeV region. It is noted that ENDF/B-IV underestimates the emission spectrum of Co in the 3-13 MeV region. The ENDF/B-IV data for W do not agree at all with the experimental spectral patterns.

Keywords: Double Differential Neutron Emission Cross Section, 14.1 MeV, TOF Experiment, Ca, Mn, Co, W, JENDL-3T, ENDF/B-IV JAERI - M 89 - 214

Ca, Mn, Co, Wの 14.1 MeVにおける中性子放出二重微分断面積の測定

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(1989年11月28日受理)

中性子遮蔽材及び短構造村元素として重要なCa, Mn, Co, Wについて、14 MeV 中性子人 射に対する中性子放出二重微分断面積が阪大オクタビアンのTOF分析装置を用いて測定された。 散乱角度は15°から160°にわたり16点である。二次中性子エネルギー範囲は0.5 MeVから15 MeVである。統計精度・エネルギー分解能ともに良好なデータを得られた。

- 得られた二重微分断面積を重心系に直し、角度積分して中性子放出スペクトルデータが導出された。

二重微分断面積のエネルギースヘクトルで、ヒークとして分離することができた弾性散乱と離 散車弾性散乱については、角度微分断面積が導出された。二重微分断面積は大量のデータとなっ たので、本報ではグラフのみを与えている。放出スヘクトルと角度微分断面積については、グラ フと数値表を与えている。

評価核データ(ENDF B-W, JENDL-3T)との予備的比較が行なわれた。その結果, Ca については、低エネルギーではENDF B-Wの過大評価がみられるが、高エネルギー側では実 験を良く再現している。Mnについては、JENDL-3Tは放出スペクトルをかなり良く再現して いるが 6~13 MeV領域で少し過小評価となっている。Coについては、ENDF B-Wは3~13 MeVで放出スペクトルを大きく過小評価している。Wについては、ENDF B-Wのデータは実 験とスペクトルパターンが全く一致しない

本報告書は日本原子力研究所から昭和63年度委託研究で行われた成果をまとめたものである。 東海研究所:**〒**319-11 茨城県那珂郡東海村白方字白根2-4

• 大阪大学

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1. Introduction

Double differential neutron emission cross sections (DDX) are of importance in fusion applications, namely not only for the neutronics calculations of blankets and shields but also for the calculational estimations of primary knock-on atom spectra and kerma factors. Neutroninduced nuclear reactions with incident energy around 14 MeV generally show the competing process between the direct, the precompound and the compound processes which reflected in the energy spectral shapes of DDX or emission spectrum. The DDX data have been therefore utilized also to the assessment of nuclear model codes for evaluation works.

In this report, measurements and results are described for Ca, Mn, Co and W. The DDX data of Ca are required as fundamental nuclear data for shielding designs using ordinary or low-activation (lime-stone) concrete, due to scarce experimental data. Tungsten is a candidate of the ITER inboard shield, whose available neutron data have large uncertainties and therefore new experimental data are strongly required. The DDX data of medium-heavy nuclei (Mn and Co) are of particular interest to assessing "standard" nuclear model codes. The data of angle-integrated neutron emission spectra and angle differential cross sections which can be obtained from the DDX data are also useful for the evaluation or code-assessing tasks. Therefore, measurements were carried out for a wide range of scattering angles (15-160 deg). Preliminary comparisons are made with a few evaluated nuclear data, e. g., ENDF/B-IV¹) and JENDL-3T².

2. Experiment

The details of our experimental method are described elsewhere^{3,4)}. A brief explanation is as follows: The pulsed D-T neutron source of OKTAVIAN³⁾ is used with 2 ns pulse width and 1 MHz repetition frequency. A neutron TOF spectrometer has an 8.3 m long collimated flight path fixed in the 85 deg direction against the OKTAVIAN beam line. A 10 inch diam. \times 10 cm thick NE213 detector is used as a main neutron detector with two (low- and high-gain) parallel pulse shape discrimination circuits. A scattering sample is set at 17 cm from the center of a TiT target (2 cm diam.) and moved along the 17 cm R arc when we change the

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scattering angle. Incident neutron energy is 14.1 + 0.2 MeV, which was determined by observing the peak-energies of the elastic scatterings of many elements.

Cylindrical metallic rods are used for the scattering samples. Seven pellets of calcium metal (3 cm diam. × 1 cm thick) are packed with aluminum cooking foil to form the cylindrical sample (7 cm long). The effect of the aluminum foil has been proved to be ignored by background runs with and without the empty aluminum foil at sample position. The sizes of the Mn and W samples are 3 cm diam. × 7 cm long. For Co, a 2.5 cm diam. × 7 cm long metallic cylinder is used.

The calibration of the DDX values is made in usual way; the scattered neutron peaks of H(n, n) reaction are measured with a 1.5 cm diam. × 5 cm long polyethylene sample at the 7 angles (20-50 deg in LAB angle) and peak-area at each angle is normalized to be equal to the corresponding differential cross section of hydrogen.

Data processing procedure is described elsewhere⁴) in detail. For multiple scattering correction⁵), the DDX data calculated from evaluated nuclear data were used; ENDF/B-IV for Ca, Co and W, and JENDL-3T for Mn. Since the correction is considerably dependent on the spectral shapes of the used nuclear data, we will have to reprocess the Co DDX data using improved data (JENDL-3 final version) when more accurate data are required. For W, the neutron emission spectra by ENDF/B-IV are so different from the measured ones that we can not make correction and have to show the uncorrected data in this report: we may estimate the correction for W to be within 10-15 %.

3. Results

3.1 DDX

Results for Ca are shown in Fig. 1 through Fig. 15. In a spectrum at each angle, we can resolve six discrete inelastic scattering peaks (3.736-3.904 MeV sum peak, 4.492 MeV peak, 6.285 MeV peak, 6.510-7.536 MeV sum peak, 7.760-8.540 MeV sum peak and 9.6 MeV peak) and an elastic scattering peak (the most right-hand peak). Significant angular dependence is seen down to low emission energy where ENDF/B-IV overestimates the measured DDX. In the energy region higher than about 5 MeV, the ENDF/B-IV data reproduce the measured spectral patterns though delicate differences are seen.

Results for Mn are shown in Fig. 16 through Fig. 31 compared with JENDL-3T. Three peaks of the discrete inelastic scatterings (0.984, 2.822, and 4.41 MeV levels) and the elastic scattering peak could be resolved.

Results for Co are shown in Fig. 32 through Fig. 47 compared with ENDF/B-IV. We can see the resolved peaks of the elastic scattering and of the two discrete inelastic scatterings (1.099 and 4.086 MeV levels).

Results for W are shown in Fig. 48 through Fig. 63 compared with ENDF/B-IV. Except for the elastic scattering peak, no distinct peaks of the inelastic scatterings are seen at any angle though delicate structures are observed in the 9-13 MeV region.

3.2 Angle-Integrated neutron emission spectra (EDX)

Results for Ca are shown in Fig. 64 and Fig. 65 for the LAB and the CM system, and numerical values for the CM system are given in Table 1(1).

Results for Mn are shown in Fig. 66 and Fig. 67. Numerical values are given in Table 1(2).

Results for Co are shown in Fig. 68 and Fig. 69. Numerical values are given in Table l(3).

Results for W are shown in Fig. 70 and Fig. 71. Numerical values are given in Table 1(4).

3.3 Angle-differential cross sections (SDX)

Results for Ca are shown in Figs. 72, 73, 74 and 75, together with fitted curves using Legendre polynomials and evaluated curves of ENDF/ B-IV. Numerical values are given in Table 2(1) and 2(2).

Results for Mn are shown in Figs. 76, 77 and 78. Fitting with the Legendre polynomials and the JENDL-3T curves are also shown. Numerical values are given in Table 2(3).

Results for Co are shown in Figs. 79 and 80. Numerical values are given in Table 2(4).

Results for W are shown in Figs. 81 and 82, for the elastic scattering, the inelastic continuum (integration of DDX within the 5.5-11

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MeV region) and the (n, 2n) neutron emissions. For the (n, 2n) reaction, the DDX values are integrated within the 0-5.5 MeV region. Numerical values are given in Table 2(5).

4. Discussion

4.1 Calcium

As shown in Fig. 1 through Fig. 15, the calculated curves of ENDF/ B-IV reproduce the measured DDX curves as a whole. Speaking the local agreements, ENDF/B-IV underestimates the measured values in the 4-11 MeV at forward angles (15-50 deg). Below 3 MeV the measured data show the forward enhancement of the neutron emission while the ENDF/B-IV data give isotropic angular distribution and therefore overestimate the experimental values at the angles greater than 60 deg.

Looking at the angle-integrated neutron emission spectrum in the CM system shown in Fig. 65, the ENDF/B-IV data reproduce very well the measured values in the energy region above 4 MeV while significant (by 30-50 %) overestimation is seen below 4 MeV.

As for the single differential cross sections of the elastic scattering shown in Fig. 72, ENDF/B-IV overestimates 2 times the experimental values at the backward angles (110-150 deg), though the angular distribution resembles one another. For the resolved discrete inelastic scatterings shown in Figs. 73 through 75, the underestimation of ENDF/B-IV is pointed out at the forward angles for the 3.736-3.904 and 4.492 MeV levels.

4.2 Manganese

DDX: As shown in Fig. 16 through 31, the calculated DDXs by JENDL-3T reproduce the overall spectral shapes of the experimental ones but the significant underestimations at the forward angles (15-80 deg) should be pointed out. At the backward angles (90-160 deg), very good agreement is seen except for the elastic scattering peaks at the backward angles (100-160 deg). The angular distribution of the pre-equilibrium neutron emission shall be taken into account to fill the large differences at the forward angles. Seeing the angle-integrated neutron emission spectrum shown in Fig. 67, we can say that the underestimation of JENDL-3T is obvious in the 6-13 MeV region. We see a distinct peak around 9.5 MeV of the measured spectrum, which is attributed to the excitation of one phonon state of octapole vibration (excitation energy 4.41 MeV). A hump at 6-7 MeV may be due to the excitation of the low energy octapole vibration (two phonon state). A shoulder at 11.5 MeV can correspond to the 1.884 MeV level excitation.

For the differential elastic scattering cross sections shown in Fig. 76, the considerable underestimation of JENDL-3T is seen at the forward angles (15-30 deg) while overestimating about twice at the backward angles (100-160 deg). For the 0.984 MeV level excitation, fairly good agreement is seen as shown in Fig. 77 as far as the angle-dependence is concerned. As shown in Fig. 78, the JENDL-3T cross sections for the 2.822 MeV level should be doubled though their shapes of angular distribution curve agree with the measured one. Since the cross section of 4.41 MeV level seems to be large, it is recommended to include this level into the evaluations.

4.3 Cobalt

As shown in Fig. 32 through Fig. 47, the measured spectral shapes and the angular distribution of DDX are very different from those of ENDF/B-IV; especially in the 3-13 MeV region and at the forward angles, the used nuclear models seem to have problems, i. e., the direct collective excitation of the inelastic scattering and the preequilibrium neutron emission are not taken into account or are treated uncorrectly.

The results of the angle-integrated emission spectrum shown in Fig. 69 lead us to a similar conclusion.

The differential cross sections of the elastic scattering are shown in Fig. 79. At the backward angles (70-160 deg), ENDF/B-IV is 2-3 times larger than the experimental values. Overestimation over the whole angle and the difference of the distribution shape may suggest us the necessity of the reestimation of optical parameters. No comparisons with the evaluated curves are made for the 1.099 and 4.086 MeV levels, and the analyses with DWUCK4 are desirable.

- 5 -

4.4 Tungsten

Obviously the drastic underestimation of ENDF/B-IV in the 5-13 MeV region shows the ignorance of the direct and preequilibrium neutron emissions. Basically we can apply the EGNASH⁶) + DWUCK4⁷) analysis for the evaluation tasks. However, the measured DDX spectra in the 5-13 MeV region show us the existence of so many discrete levels of the direct excitations. Natural tungsten contains 5 isotopes, so that the energy spectrum may be monotonous in this region. In the case of Ta^8 which is mono-isotopic, we have observed the quite similar monotonous spectra of DDX in the corresponding energy region. Therefore we can speculate that the many direct excitations with similar magnitudes are possible for these heavy mass elements (from Ta to W). This situation requires us laborious calculations of the direct process neutron emissions.

The differential cross sections of the elastic scattering are shown in Fig. 81 compared with ENDF/B-IV. The measured data are larger on an average than those of ENDF/B-IV at the backward angles (90-160 deg). As shown in Fig. 82, a slight forward-enhancement of (n, 2n) neutrons is seen and the integrated (n, 2n) cross section of the experiment is about 15 % smaller than that of ENDF/B-IV.

Acknowledgment

The authors appreciate the operation crew of OKTAVIAN. The appreciation is also due to the continuous support of this work by Dr. S. Igarasi, Dr. T. Asami and Dr. Y. Kikuchi of JAERI Nuclear Data Center.

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Table 1(1)	Angle-integrated	neutron emission	spectrum	in	the	ſМ
V - V	system with En =	14 1 MoV for Ca	Spectrum		the	Uni
	System with the	14.1 Heve TUP Ud				

SUBENTRY	00021003	880201			00021003
COMMENT	TWO DATA SET DATA OBTAINE	S ARE GIVËN D FROM RAW	DDX DATA .	IN LEFT HAD	00021003 2 00021003 3 ND SIDE: 00021003 4
	DATA OBTAINE IN RIGHT HAN	D FROM CORF D SIDE	ECTED DDX I	DATA WITH M	USCC3 CODE 00021003 5 00021003 6
REACTION	(20-CA-0(N,S IN THE CENTE	(T)DE) S R-OF-MASS S	ECONDARY NE	UTRON SPEC	TRUM 00021003 7 00021003 8
COMMON	8 1	5			00021003 9
MEV 14 10000					00021003 12
ENDCOMMON DATA	5 6	66			00021003 14 00021003 15
E-MAX MEV	E-MIN D MEV B	ATA D /MEV B	ATA-ERR D /MEV B	ATA L VMEV 1	DATA-ERR 00021003 16 B/MEV 00021003 17
14 20000 14 00000	14.00000 13.80000	9 95E-02 3 11E-01	2.98E-03 3.84E-03	9 27E-02 3 01E-01	2.95E-0300021003 18 3.82E-0300021003 19
13 80000	13.40000	7 14E-01 1.27E+00	4 66E-03 5 27E-03	1 23E-01	4.71E-0300021003 20 5.30E-0300021003 21
13.20000	13.00000	6 07E-01	4 66E-03 3 58E-03	6.16E-01	3 56E-0300021003 23 2 65E-0300021003 23
12 80000	12.60000	1 22E-01 6 19E-02	2 20E-03 2 05E-03	1 22E-01 6 22E-02	2 15E-0300021003 25 2.00E-0300021003 26
12.40000	12.20000 12.00000	3 62E-02 2 37E-02	1.93E-03 1.88E-03	3 66E-02 2 40E-02	1.88E-0300021003 27 1.83E-0300021003 28
12.00000	11 80000 11 60000	1 57E-02 1 24E-02	1 85E-03 1 78E-03	1 60E-02 1 27E-02	1 79E-0300021003 29 1 72E-0300021003 30
11 60000	11 40000	5 30E-03 1 96E-03	1 71E-03 1 66E-03	5 46E-03 2 02E-03	1 67E-0300021003 31 1 62E-0300021003 32
	10.80000	2 22E-03	1 52E-03	2 24E-03	1 52E-0300021003 33 1 52E-0300021003 34 1 46E-0300021003 35
10 60000	10 40000	9 96E-03 1 80E-02	1 42E-03 1 42E-03	1 01E-02 1 82E-02	1 42E-0300021003 36 1 43E-0300021003 37
10 20000	10.00000 9.80000	4 09E-02 8 27E-02	1 49E-03 1 65E-03	4 12E-02 8 34E-02	I 50E-0300021003 38 I 66E-0300021003 39
9 60000 9 80000	9.60000 9.40000	9 75E-02 5 65E-02	I G8E-03 I 54E-03	9 80E - 02 5 G3E - 02	1 69E-0300021003 40 1 53E-0300021003 41
9 40000 9 20000	9.20000	3 55E-02 4 42E-02	1 45E-03 1 51E-03	3 SOE-02 4.01E-02	1.43E=0300021003 42 1.42E=0300021003 43
9 00000 8 80000 8 60000	8.60000	2.41E-02	1 57E-03 1 55E-03	1.63E-02	1.19E-0300021003 44 1.19E-0300021003 45
8.40000	8.20000	1 60E-02 2 36E-02	1 48E-03	1 12E-02	1 23E-0300021003 47 1 30E-0300021003 47
8 00000	7.80000	2 38E-02 2 12E-02	1 52E-03 1 52E-03	1 84E-02 1 74E-02	1.32E-0300021003 49 1.37E-0300021003 50
7.60000	7 40000 7 20000	2 68E-02 3 30E-02	1 54E-03 1 57E-03	2.37E-02 3.01E-02	1 44E-0300021003 51 1 48E-0300021003 52
7 20000 7 00000	7.00000 6.80000	3 21E-02 4 01E-02	1 59E-03 1 64E-03	2 97E-02 3 62E-02	1 49E-0300021003 53 1 48E-0300021003 54
G 80000 G 60000	6.60000 6.40000	5 38E-02 5 00E-02	69E-03	4 74E-02 4 27E-02	1.50E-0300021003 55 1.45E-0300021003 56
6.40000	6 00000	3.65E-02 3.83E-02	1.68E-03	3 37E-02 3 54E-02	1.44E-0300021003 57 1.47E-0300021003 58
5 80000	5 60000	3 85E~02 3 71E-02	1 70E-03	3 29E-02 3 29E-02	1 49E-0300021003 60 1 50E-0300021003 61
5 40000	5.20000 5.00000	3 96E-02 3 82E-02	1 74E-03 1 74E-03	3 43E-02 3 03E-02	I.47E-0300021003 62 I.42E-0300021003 63
5.00000 4.80000	4 80000 4 60000	3 51E-02 4 08E-02	1.75E-03 1.77E-03	2.59E-02 3.08E-02	1 38E-0300021003 64 1 39E-0300021003 65
4.60000 4.40000	4.40000 4.20000	4 47E-02 4 76E-02	1.76E-03 1.77E-03	3.40E-02 3.73E-02	1.40E-0300021003 66 1.43E-0300021003 67
4.20000	3 80000	5 09E-02 5 24E-02 5 82E-02	1 77E-03	3 97E-02 3.89E-02	1 42E-0300021003 68 1 42E-0300021003 69
3 60000	3.40000	6.10E-02 6.87E-02	1 81E-03	4.70E-02 5.37E-02	1 47E-0300021003 71 1 52E-0300021003 72
3 20000	3.00000	7.80E-02 9.41E-02	1 94E-03 2 06E-03	6 29E-02 7 80E-02	I 62E-0300021003 73 I 73E-0300021003 74
2.80000 2.60000	2.60000 2.40000	1.06E-01 1.20E-01	2 20E-03 2 37E-03	8 72E-02 9 43E-02	1.86E-0300021003 75 1.91E-0300021003 76
2.40000 2.20000	2.20000 2.00000	1.52E-01 1.58E-01	2 52E-03 2 71E-03	1.17E-01 1.26E-01	1.97E-0300021003 77 2.19E-0300021003 78
2 00000 1.80000		1.71E-01 1.79E-01	2 92E-03 3 28E-03 3 92E-03	1 43E-01 1 47E-01 1 57E-01	2.43E+0300021003 79 2.70E+0300021003 80 3.25E+0300021003 81
1.40000	1.20000	1.94E-01 2 43E-01	5 20E-03	1 G1E-01 1 97F-01	4 37E-0300021003 82 9 39E-0300021003 83
ENDDATA ENDSUBENTRY ENDENTRY	70 85 3				00021003 84 0002100399999 0002199999999

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Table 1(2)	Angle-integrated system with En =	neutron emission 14.1 MeV, for Mn	spectrum	in	the	СМ
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SUBENTRY	00020003	881201				00020003	1
COMMENT	TWO DATA SET DATA OBTAINE	S ARE GIVE D FROM RAW	N. DDX DATA ,	IN LEFT HAI	ND SIDE.	00020003	2 3 4
REACTION	DATA OBTAINE IN RIGHT HAN (25-MN-55(N)	D FROM CORI D SIDE SCTI DEI	SECONDARY	DATA WITH MU	JSCC3 CODE	00020003	5
ENDBIB	IN THE CENTE	R-OF-MASS	SYSTEM	NEUTRON SPEC	LIKUM	00020003	8 9
COMMON EN	1	5				00020003	10
14.1000 ENDCOMMON	0 5					00020003	12
DATA E-MAX	E-MIN D	68 4 TA [ATA-ERR I	ATA D	ATA-ERR	00020003	i 5 1 6
14.60000 14.40000	мех В, 0 14.40000 0 14.20000	MEY 1 1.02E-02 4.75E-02	6.39E-04 1.19E-03	0/MEV E 1.23E∽02 0.00E+00	7.82E-04 1.36E-03	00020003	17
14.20000	0 14.00000 0 13.80000	2.22E-01 8.08E-01	1.98E-03 2.63E-03	2.69E-01 9.91E-01	2.20E-03 3.08E-03	00020003	2021
13 60000) 13.40000	1.59E+00 1.64E+00 9.59E-01	3.18E-03 2.47E-03	2 02E+00 1 17E+00	3.91E-03 3.84E-03 2.94E-03	00020003	2 Z 2 3 2 4
13 20000) 13.00000) 12.80000) 13.60000	4 12E-01 2 01E-01	1.80E-03 1.44E-03	4 93E-01 2 36E-01	2.08E-03 1.63E-03	00020003	25 26
12.60000	12.40000	9 07E-02 6 14E-02	1 16E-03 1 07E-03	1.09E-01 7.44E-02	1.35E-03 1.25E-03	00020003	28 29
12.20000) 12.00000) 11.80000	4.32E-02 3.81E-02	1.01E-03 9.85E-04	5.24E-02 4.62E-02	1.18E-03 1.16E-03	00020003	30 31
11.60000	11.40000	3 25E-02 2 81E-02	9.33E-04 9.08E-04	3.94E-02 3.41E-02	1.11E-03 1.08E-03	00020003	33 33 34
11.20000		2 34E-02 2 38E-02	8.87E-04 8.69F-04	2 81E-02 2 86E-02	1.06E-03 1.04E-03	00020003	35 36
10.80000	10.40000	2 53E-02 2 42E-02 2 27E-02	8 54E-04 8 42E-04	2 88E-02 2 71E-02	1.04E-03 1.02E-03	00020003	37 38 39
10.20000	10.00000 9.80000	2 41E-02 2 73E-02	8.50E-04 8.67E-04	2 86E-02 3 24E-02	1.01E-03 1.03E-03	00020003	40
9 60000 9 60000 9 40000	9.40000 9.20000	4 36E-02 4 72E-02	9 27E-04 9 51E-04	5 16E-02 5 47E-02	1.11E-03 1.12E-03	00020003	42 43 44
9 20000 9 00000	9.00000 8 80000	4 21E-02 3 75E-02	9 28E-04 9 14E-04	4 28E-02 3 68E-02	9.56E-04 9.38E-04	00020003	45 46
8 60000 8 60000 8 40000	8.40000 8.20000	3 79E-02 3 82E-02 3 76E-02	9.21E-04 9.21E-04 9.25E-04	3 92E-02 3 94E-02	9.67E-04 9.82E-04	00020003	47 48 49
8 20000 8 00000	8.00000 7.80000	4.09E-02 4.37E-02	9.29E-04 9.41E-04	4 32E-02 4 66E-02	9 97E-04 1.01E-03	00020003	50 51
7 60000 7 60000 7 40000	7 . 40000 7 . 20000	4.03E-02 5.20E-02 5.72E-02	9 53E-04 9 53E-04 9 64E-04	5.60E-02 6.16E-02	1.04E-03 1.05E-03	00020003	53 54
7 20000 7 00000	7 00000 6.80000	6 03E-02 6 26E-02	9.66E-04 9.66E-04	6 62E-02 6 90E-02	1.06E-030	00020003	55 56
6 60000	6 40000 6 20000	6 72E-02 6 86E-02	9 69E-04 9 69E-04 9 62E-04	7.34E-02 7.52E-02	1 07E-030	0020003	58 59
6 20000 6 00000	6 00000 5 80000	7 33E-02 7 59E-02	9 74E-04 9 77E-04	8 0GE-02 8 38E-02	1 08E-030 1 09E-030	0020003	60 61
5.80000 5.60000 5.40000	5.40000 5.20000	7.76E-02 8.20E-02 8.78E-02	9.84E-04 9.92E-04 1.01E-03	8.60E-02 9.12E-02 9.75E-02	1.11E-030 1.13E-030)0020003)0020003)0020003	62 63 64
5.20000 5.00000	5 00000 4 80000	9.39E-02 1.02E-01	1 02E-03 1 04E-03	J 04E-01 1.13E-01	1.14E-03(1.16E-030	0020003	65 66
4.80000 4.60000 4.40000	4.40000 4.20000	1.17E-01 1.25E-01	1.07E-03 1.07E-03 1.09E-03	1.29E-01 1.39E-01	1 18E-030 1 21E-030	0020003	68 69
4 20000	4.00000 3.80000	1 36E-01 1 45E-01	1 1 E - 03 1 1 5 E - 03	1 51E-01 1 60E-01	1.23E-030 1.26E-030	0020003	70 71
3.80000 3.60000 3.40000	3.40000 3.20000	1 67E-01 1 87E-01	1 20E-03	1 82E-01 2 04E-01	1 31E-030	0020003	73 74
3 20000 3 00000	3.00000 2.80000	2 . 11E-01 2 . 45E-01	1 32E-03 1 40E-03	2 28E-01 2 64E-01	1.42E-030 1.50E-030	0020003	75 76 77
2.60000	2.40000 2.20000	3.32E-01 4.01E-01	1.59E-03 1.68E-03	3 39E-01 4 07E-01	1.61E-030	0020003	78 79
2 20000	2.00000 1.80000	4.56E-01 5.10E-01 5.92E-01	1.78E-03 1.88E-03 2.08E-03	4.73E-01 5.34E-01 6.14E-01	1.82E-030 1.97E-030 2.16E-030	0020003	80 81 82
1.60000	1.40000	6 76E-01 7 55E-01	2 38E-03 2 87E-03	6.90E-01 7.58E-01	2.43E-030 2.88E-030	0020003 0020003	83 84
1 20000 ENDDATA	1.00000	7.93E-01	4.04E-03	7.82E-01	3.99E-030	0020003	85 86
ENDENTRY	3				0	0020999999	999

Table 1(3)	Angle-integrated system with En =	neutron emission 14.1 MeV. for Co	spectrum	in	the	СМ
	System with En	14.1 /// 101 00				

	SUBENTRY BIB COMMENT	THO	00 .D	019003 ATA SET	S A	881 RE_C	201 8 VE	N.							000	019003 019003	1223
	REACTION	DAT DAT IN	A A R1 -C	OBTAINE OBTAINE GHT HAN		ROM I ROM (IDE	CAN COR	RECI	ED DD		ATA NTA	WITH I	AND MUSC FCTR	C3 COD	E 000	019003	4 5 6 7
		ÌÑ	ТЙ	E CENTE	R-O	F-MAS	55' 5	รังรัว	EM						000	019003	8 9 10
	EN MEV			·											000	019003	11
	ENDCOMMON DATA	,		5 6	_		69	_							000	19003	13 14 15
	E-MAX MEV 14 60000	E-M MEV	IN IA	D/ B.	ATA /Me	۷ ۹05-	02	DATA B/ME 5	-ERR V 30F-(DA B/ DA	ATA ME'	V 855-02	DAT B/M	A-ERR EV 6.51E-4	000 000 000⊾0)19003)19003)19003	16 17 18
	14 40000)	4	20000	4 2	33E- 66E-	02	Ĩ	20E-0	3	53	29E-02 37E-01	2	1.32E- 2.17E-	03000	19003	19 20
	13.80000)	13	. 60000	1	41E+ 22E+	00	2 3 2	-46E-0 -07E-0 -80E-0)3)3)3	1	88E+00		3.98E- 3.57E-	03000	19003	21 22 23
	13.40000		3	20000	52	- 66E- - 28E-	01	1	-98E-0 -41E-0)3)3)3	72	31E-01 92E-01		2.45E-0 1.69E-0	03000 03000	19003	24 25 26
	12 80000		2	60000	8	63E- 15E-	02	i 1	07E-0	3	1	08E-01		1.29E- 1.29E-	03000	19003	27
	12.40000 12.20000 12.00000	1	2	00000 80000	6 4 3	67E- 64E- 09E-	02 02 02	1 9 8	- 40E-0 77E-0) 3) 4) 4	8 5 4	38E-02 92E-02 01E-02		1 25E-(1 17E-(1 09E-()3000)3000)3000	19003	29 30 31
	00008 00008 11 40000	1	1.	60000 40000 20000	2	-15E- 69E- 21E-	02 02 02	8	38E-0 16E-0 86F-0	14 14	22.	82E-02 22E-02 57E-02		1.04E-(1.02E-(9.85E-()3000)3000)4000	19003 19003	32 33 34
	11.20000	1	0	00000	8	89E- 15E-	03	1711	61E-C	4	1.	15E-02 04E-02		9 55E-0 9 31E-0	4000	19003	35
	10 60000	1	0.0	40000 20000	1	10E- 41E-	02	77	29E-0 09E-0	4	1	35E-02 73E-02		9.15E-0 8.87E-0	4000	19003	38 39
	10 20000 10 00000 9 80000	1	0. 9. 9	00000 80000 60000	2222	15E- 99E- 69E-	02 02 02	7 7 7	27E-0 48E-0 29E-0	4	3	65E-02 69E-02 32E-02		9.06E-0 9.32E-0 9.08E-0	4000	19003 19003 19003	40 41 42
	9 60000 9 40000		9. 9.	40000	222	45E- 68E-	02	777	10E-0 04E-0	4	3.	04E-02 19E-02	8	8 83E-0 8 54E-0 7 84E-0	4000	19003	43 44 45
	9.00000 9.00000 8.80000		8. 8.	80000	2.	80E-	02	7	04E-0 09E-0	4 4	2.2	88E-02 73E-02		7.66E-0	4000	19003	46 47
	8-60000 8-40000 8-20000		8 - 8 - 8 -	40000 20000 00000	2.	87E-0 94E-0 06E-0	02 02 02	7 7 7	11E-0 24E-0 18E-0	4 4 4	3.3.	01E-02 15E-02 29E-02	8	/-88E-0 3-07E-0 3-09E-0	4000 4000 4000	19003 19003 19003	48 49 50
	8.00000 7.80000		7. 7.	80000	3.	02Ē~(03E-)		777	31E-0 33E-0	4	3.	26E-02 34E-02	800	3.26E-0 3.33E-0	4000	19003	51
	7 40000 7 40000 7 20000		7 . 7 . 7 .	20000	3.00	43E-0)2)2)2	7 7 7	47E-0 57E-0	4 4 4	3.4	76E-02 08E-02	500	52E-0 63E-0	4000	19003	54 55
	7.00000 6.80000 6.60000		6. 6.	80000 60000 40000	3 4.	88E-(25E-(41F-()2)2)2	7	58E-0 64E-0 71E-0	4 4 4	4.4.	34E-02 75E-02 86E-02	ມ	3.61E-0 3.66E-0 3.72E-0	4000 4000 4000	19003 19003 19003	56 57 58
	6.40000 6.20000		6. 6.	20000	4.5.	67E-(15E-($\frac{1}{2}$	7 - 7 - 8	77E-0 95E-0	4	5.5	14E-02 66E-02 95E-02	899	8.80E-0 .00E-0	4000	9003	59 60
	5.80000		5.	60000	5.	80E-0 32E-0	2	8.	26E-0 49E-0	4	6	41E-02 93E-02	9	30E-0	4000	9003	62 63
	5 40000 5 20000 5 00000	1	5. 5. 4.	20000 00000 80000	Б 7. 8.	90E-0 52E-0 17E-0)2)2)2	8. 9.	92E-0	4 4 4	8 8	22E-02 82E-02	9 1	86E-0	40001	9003	65
	4 80000		4.	60000 40000 20000	9. 9.	10E-0 74E-0 05E-0)2)2	9. 9. 9.	44E-0- 67E-0- 927-0-	1 1 1	9.	68E-02 03E-01 13E-01	1	02E-0 04E-0	30001 30001 30001	9003	68 69
	4 20000 4 00000		4.	00000	1.	13E-0		1.	01E-0: 03E-0:	3	1.	23E-01 29E-01	1	10E-0	30001	9003	70 71 72
	3 60000 3 40000		3.	40000	1	37E-0 51E-0		1.	09E-0: 13E-0:	3	1	52E-01 71E-01	i	21E-0	30001	9003 9003	73 74
	3.20000 3.00000 2.80000		3.0	00000 80000 60000	1.	68E~0 91E~0 17E~0		1.	17E-03 24E-03 27E-03	3	1 2 2	95E-01 22E-01 52E-01	1	44E-0	30001	9003 9003 9003	75 76 77
	2 60000 2 40000			40000	222	49E-0 96E-0	1	1.	36E-03 41E-03	3	2.1	83E-01 34E-01	1	55E-03 59E-03	30001	9003 9003 9003	78 79 80
	2.00000 2.00000 1.80000		2 (. 8 . 6	80000 50000	3. 4.	34E-0 93E-0 64E-0	1	1.	64E-03 85E-03	5	4.4	46E-01 20E-01	12	87E-03	0001	9003 9003	81 82
	1.60000 1.40000			40000 20000 00000	5. 6. 7.	38E-0 19E-0 41E-0	1 1 1	2 . 2 . 4 .	14E-03 73E-03 59E-03	5	5.8	88E-01 34E-01 76E-01	2 2 4	.35E-03 .92E-03 .77E-03	0001	9003 9003	83 84 85
E	I 00000	(5.8	80000	8	85Ē-Ŏ	i	i.	40Ē-02	2	9	22E-01	i	45E-03	0001	9003 9003 900399	86 87 999
Ē	NDENTRY			3											0001	9999999	999

Table 1(4) Angle-integrated neutron emission spectrum in the CM system with En = 14.1 MeV, for W

SUB BIB Com	ENTRY MENT	(T¥O DAT/	0023003 2 DATA SE 0BTAIN	IS A ED F	890601 8 RE GIVE ROM RAV	N. DD	X DATA	. IN	LEFT H	AND S	DE.	00023003 00023003 00023003 00023003	1 2 3 4
REA	CTION	DAT/ IN F (74-	\ OBTAINI RIGHT HAI ∙₩-0{N,S(ED F ND S CT),	ROM COP SIDE. DE) S	REC ECO	TED DDX NDARY NI	DAT Eutr	A WITH I	MUSCC Trum	3 CODE	00023003 00023003 00023003	5 6 7
END Comi EN	B I B HON	INI	HE CENTI 8 1	ER-C	DF-MASS	SYS	TEM					00023003 00023003 00023003 00023003	8 9 10 11
END END	14 10000 COMMON	E-141	56		7 2	DAT		DAT		D. T.		00023003 00023003 00023003 00023003	12 13 14 15
ŇEŸ	5.00000 4.80000	MEV	4 80000 4 60000	1/ме 1 3	V 83E-10 24F-02	В/М І	EV 45E-03	В/м	EV 6.40E-10 4.36E-02	B/ME	V 99E~0	00023003	17
1	4 60000 4 40000 4 20000	1	4 40000 4 20000 4 00000	2021	19E-01 09E-01 02E+00		55E-0 91E-0 42E-0		2 95E-01 1 22E+0C 2 71E+0C		86E-0 38E-0 10E-0	300023003 300023003 300023003	20 21 22
 	4 00000 3 80000 3 60000 3 40000	 	3 80000 3 60000 3 40000 3 20000	2 6 2	38E+00 50E+00 20E-01 54E-01	1	2.57E-03 08E-03 .45E-03		3.12E+00 1.88E+00 7.44E-01 3.02E-01) 3) 2]	25E-0 50E-0 65E-0	300023003 300023003 300023003 300023003	23 24 25 26
1	3 20000 3 00000 2 80000		3 00000 2 80000 2 60000	1 9 7	45E-01 80E-02 50E-02	8	3.99E-04 3.17E-04 72E-04		1 78E-01 1 24E-01 9 53E-02	1 9 9	04E-0 66E-0 20E-0	300023003 400023003 400023003	27 28 29
1 1 1	2 60000 2 40000 2 20000	1	2 40000 2 20000 2 00000	6 5 4	01E-02 00E-02 32E-02	7 7 6	37E-04	(7 71E-02 5 46E-02 5 49E-02	8 8 8	92E-0- 60E-0- 22E-0-	100023003 100023003 100023003	30 31 32
1 1 1	$ \begin{array}{c} 2 & 00000 \\ 1 & 80000 \\ 1 & 60000 \\ 1 & 40000 \end{array} $	1	1 60000	3 3 3 3	62E-02 62E-02 70E-02	0 0 0 0	30E-04 30E-04 17E-04		4 93E-02 4 48E-02 1 45E-02 1 57E-02	777	87E~04 57E~04 41E~04 32E~04	100023003 100023003 100023003	33 34 35 36
1	1 20000 1 00000 0 80000	i 1 1	1 00000 0 80000 0 60000	3 3 3	65E-02 64E-02 66E-02	555	95E-04 94E-04 94E-04	4	53E-02 52E-02 56E-02	7 7 7	29E-04 28E-04 34E-04	00023003	37 38 39
1	0 60000 0 40000 0 20000	1 1 1	0 40000 0 20000 0 00000 0 80000	3339	7GE-02 88E-02 85E-02	5 6 5 5	99E-04 01E-04 98E-04	444	1.68E-02 86E-02 86E-02	777	41E-04 53E-04 52E-04	00023003	40 41 42
ſ	9 80000 9 60000 9 40000		9.60000 9.40000 9.20000	333	70E-02 61E-02 63E-02	56	96E-04 00E-04 09E-04	74216	60E-02 56E-02 50E-03	7 4 1	37E-04 49E-04 32E-04	00023003	43 44 45 46
	9 20000 9 00000 8 80000		00000 8 80000 8 60000	3 3	55E-02 55E-02 47E-02	6 6	09E-04 14E-04 1GE-04	455	46E-03 98E-03	1.	29E-04 59E-04 73E-04	00023003 00023003 00023003	47 48 49
	8 40000 8 40000 8 20000	1	8 40000 8 20000 8 00000	3.3	44E-02 50E-02 42E-02	6 6 6	23E-04 30E-04 36E-04	8	10E-03 36E-03 15E-02	22.3	18E-04 39E-04 29E-04	00023003	50 51 52
	7 80(00 7 60000 7 40000		60000 40000 20000	3.3	31E-02 42E-02 44E-02	6 6	49E-04 54E-04 57E-04	1	57E-02 86E-02 18E-02	4 · 4 · 5	27E-04 85E-04 27E-04	00023003 00023003 00023003	54 55 56
,	7.20000 7.00000 6.80000	(00000	3.3.	43E-02 57E-02 68E-02	6 6	54E-04 55E-04 54E-04	5,5,0,0	27E-02 64E-02 07E-02	5 5. 6.	30E-04 95E-04 50E-04	00023003 00023003 00023003	57 58 59
	5.60000 5.40000 5.20000	6 6	20000 00000 00000	3.3.	68E-02 63E-02 82E-02 87E-02	6666	.54E-04 .63E-04 .78E-04 .89E-04	333	.20E-02 .32E-02 .65E-02 .90E-02	6. 7. 7. 7	56E~04 02E~04 50E~04 88E~04	00023003 00023003 00023003	60 61 62 63
	5 80000 5 60000 5 40000	2 4 2 4 2 4 2	40000	3 4 4	91E-02 17E-02 47E-02	6 7 7	99E-04 12E-04 25E-04	4 4 4	15E-02 56E-02 96E-02	8 8 8	11E-04 37E-04 63E-04	00023003 00023003 00023003	64 65 66
	5 20000 5 00000 4 80000	5 4 4	00000 80000 60000	4 5 5	70E-02 07E-02 62E-02	7 7 7	37E-04 55E-04 72E-04	5 5 6	28E-02 80E-02 57E-02	8 9 9	78E-04 08E-04 45E-04	00023003 00023003 00023003	67 68 69
• • •	4 60000 4 40000 4 20000	444	.40000 20000 .00000	6. 7. 8.	18E-02 13E-02 10E-02	7 8 8	87E-04 14E-04 32E-04	7 8 9	36E-02 61E-02 88E-02	9. 1. 1.	72E-04 01E-03 04E-03	00023003 00023003 00023003	70 71 72 72
	3 80000 3 60000 3 40000	32,33	60000 40000 20000	J. . .	08E-01 28E-01 51E-01	8 9 9	74E-04 14E-04 57E-04	1	36E-01 62E-01 93E-01	1.	12E-03(18E-03(24E-03(0023003 0023003 0023003	74 75 76
	20000 00000 80000	322	00000 80000 60000	122	85E-01 23E-01 79E-01	1.	02E-03 09E-03 20E-03	223	40E-01 91E-01 57E-01	1.	34E-03(45E-03(55E-03(0023003	77 78 79
	2.60000 2.40000 2.20000	2221	. 40000 . 20000 . 00000	3. 4. 5.	56E-01 52E-01 60E-01	1.	34E-03 43E-03 57E-03 75E-03	45.	52E-01 83E-01 36E-01	1.1	74E-030 87E-030 08E-030	0023003	80 81 82 82
2 	80000 60000 40000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	60000 40000 20000	8	82E-01 11E+00 42E+00	2223	00E-03 3GE-03 01E-03	1.	16E+00 44E+00 81E+00	2 (55E-030 55E-030 58E-030	0023003	84 85 86
i 1 C	20000	1 0 0	00000 80000 60000	1222	84E+00 54E+00 40E+00	4.	42E-03 05E-02 39E-02	1.001	29E+00 09E+00 79E+00	5 5 1	4E-030 8E-020 2E-020	0023003	87 88 89
ENDDA ENDSL ENDEN	TA BENTRY ITRY		76 91 3								0 0 0	0023003 002300399 0023999999	90 999 999

- 11 -

Q (dard)	elas	tic	Q= -3.736~3	. 904 MeV	Q= -4.49	2 MeV	Q= -6.285 MeV		
G LAB (deg)	$d\sigma/d\Omega(b/sr)$	error	$d\sigma/d\Omega(b/sr)$	error	$d\sigma/d\Omega(b/sr)$	error	$d\sigma/d\Omega(b/sr)$	error	
1 5	1.06E+0	3. 2E-2	7.73E~3	1.2E-3	3.57E-3	7.1E-4	1.81E-3	5.4E-4	
2 0	6.63E-1	2.0E-2	7.53E-3	7.5E-4	3.85E-3	5.8E-4	2. 99E-3	4.5E-4	
30	1.56E-1	4.7E-3	7.37E-3	5.2E-4	3.67E-3	3. 7E-4	3. 39E-3	3.4E-4	
42.5	3.61E-2	1.1E-3	6.90E-3	3.4E-4	2.90E-3	2.9E-4	3.47E-3	3.5E-4	
5 0	5.94E-2	1.8E-3	7.02E-3	3.5E-4	2.39E-3	2.4E-4	2.74E-3	2.7E-4	
60	5.26E-2	1.6E-3	6. 88E-3	3. 4E-4	2.48E-3	2. 5E-4	1.75E-3	2.6E-4	
70	2. 39E-2	7.2E-4	6.19E-3	3.1E-4	1.74E-3	2.6E-4	9. 37E-4	1.9E-4	
80	1.49E-2	5. 6E-4	4.77E-3	2.9E-4	1.69E-3	2.5E-4	6.46E-4	1.9E-4	
90	2. 07E-2	6. 2E-4	3. 79E-3	2.6E-4	1.85E-3	2.8E-4	5.77E-4	2. 0E-4	
100	2. 2 7 E-2	6. 8E-4	3. 25E-3	2.6E-4	1.42E-3	2. 1E-4	7.84E-4	2. 0E-4	
1 1 0	1.49E-2	4.5E-4	2. 53E-3	2. 3E-4	1.07E-3	2.1E-4	6.73E-4	2. 0E-4	
120	5. 37E-3	3.4E-4	2.60E-3	2. 3E-4	7.49E-4	1.9E-4	7.75E-4	1.9E-4	
1 3 0	3. 89E-3	3. 3E-4	2. 92E-3	2.6E-4	9.46E-4	1.9E-4	1.08E-3	2.2E-4	
140	3. 85E-3	3. 2E-4	2.95E-3	2. 7E-4	1.08E-3	2. 2E-4	7.65E-4	1.9E-4	
150	3. 44E-3	4.1E-4	2.92E-3	3. 5E-4	8.02E-4	2.8E-4	7.69E-4	2. 7E-4	
σ_{Total} (barn)	8.96E-1	3.6E-2	5.78E-2	2.9E-3	2.21E-2	3.3E-3	1.71E-2	2. 6E-3	

Table 2(1) Partial differential cross sections for Ca at En = 14.1 MeV

	Q= -6.510~	7.536 MeV	Q= -7.760~	8.540 MeV	Q = -9.6	MeV
O LAB (deg)	$d\sigma/d\Omega(b/sr$) error	$d\sigma/d\Omega(b/sr$) error	$d\sigma/d\Omega(b/sr)$	error
1 5	1.76E-3	4.4E-4	1.43E-3	5. 7E-4	2. 27E-3	6.8E-4
2 0	2. 28E-3	3.4E-4	3. 34E-3	6. 7E-4	2. 59E-3	5. 2E-4
30	3. 67E-3	3. 7E-4	4.20E-3	8. 5E-4	2.97E-3	5.9E-4
42.5	3. 78E-3	3.8E-4	4. G8E-3	9.4E-4	3. 31E-3	6.6E-4
50	3. 47E-3	3.5E-4	4.35E-3	8.7E-4	3.56E-3	7.1E-4
60	2.77E-3	2.8E-4	2.63E-3	5.3E-4	2. 30E-3	4.6E-4
70	2.63E-3	2.6E-4	2. 53E-3	5.1E-4	2.56E-3	5.1E-4
80	1.85E-3	2.8E-4	2.89E-3	5.8E-4	2. 02E-3	4. 0E-4
90	1.82E-3	2.7E-4	2. 69E-3	5.4E-4	1.95E-3	3.9E-4
100	1.75E-3	2.6E-4	2. G8E-3	5.4E-4	1.74E-3	3. 5E-4
110	1.35E-3	2.0E-4	1.97E-3	3.9E-4	1.70E-3	3.4E4
120	1.57E-3	2. 4E-4	2.46E-3	4.9E-4	1.73E-3	3. 5E-4
1 3 0	1.56E-3	2. 3E-4	2.18E-3	4.4E-4	1.67E-3	3.3E-4
140	1.71E-3	2.6E-4	2. 28E-3	4.6E-4	1. 47E-3	2.9E-4
150	1.95E-3	3. 7E-4	2. 61E-3	5. 2E-4	1.55E-3	4.6E-4
σ_{Total} (barn)	2.73E-2	3. 3E−3	3.74E-2	7.5E-3	2. 69E-2	5. 4E-3

Table 2(2) Partial differential cross sections for Ca at En = 14.1 MeV (continued)

	elas	tic	Q= -0.9	84 MeV	Q = -2.8	22 MeV	Q = -4.1	l MeV
O LAB (deg)	$d\sigma/d\Omega(b/sr$	> error	$d\sigma/d\Omega(b/sr$	> error	$d\sigma/d\Omega(b/sr$) error	$d\sigma/d\Omega$ (b/sr) crror
15	1.89E+0	5. 7E-2						
2 0	1.17E+0	3. 5E-2						
30	3.14E-1	9.4E-3						
4 0	7.39E-2	2. 2E-3	5. 62E-3	1.7E-3	2. 08E-3	2. 1E-4	5. 07E-3	3. 0E-4
50	5. 85E-2	1.8E-3	3. 94E-3	7.9E-4	1.95E-3	1.9E-4	4.15E-3	2.5E-4
60	2. 56E-2	7.7E-4	4.01E-3	8. 0E-4	1.50E-3	1.5E-4	5.13E-3	3. 1E-4
70	1.40E-2	4. 2E-4	2. 59E-3	3. 9E-4	1.79E-3	1.8E-4	3. 29E-3	2. 3E-4
80	2. 63E-2	7.9E-4	3.86E-3	5.8E-4	1.12E-3	1.3E-4	2. 99E-3	2.1E-4
90	3. 04E-2	9. 1E-4	3.74E-3	5.6E-4	6.77E-4	1.1E-4	2. 98E-3	2. 1E-4
100	1.94E-2	5.8E-4	2. 48E-3	3. 7E-4	6.73E-4	9.4E-5	2.94E-3	2.1E-4
1 1 0	1.07E-2	3. 2E-4	1.27E-3	1.9E-4	6.95E-4	1.0E-4	2.90E-3	2. 0E-4
120	1.04E-2	3. 1E-4	1.34E-3	2. 7E-4	8.61E-4	1.1E-4	2. 21E-3	1.5E-4
130	1.16E-2	3. 5E-4	9. 29E-4	1.9E-4			1.67E-3	1.3E-4
140	1.37E-2	4.1E-4	7.10E-4	1.4E-4			2. 68E-3	1.9E-4
150	1.52E-2	4.6E-4	9. 51E-4	1.9E-4			2. 21E-3	2. 2E-4
160	1.38E-2	5. 4E-4	5. 49E-4	2.5E-4				
σ_{Total} (barn)	1.38E+0	2. 1E-1	3. 4 2E-2	6.8E-3	1.60E-2	1.9E-3	4.12E-2	2. 9E-3

Table 2(3) Partial differential cross sections for Mn at En = 14.1 MeV

Ο LAB (deg)	elastic		Q= -1.099 MeV		Q= -4.086 MeV	
	$d\sigma/d\Omega(b/sr)$	error	$d\sigma/d\Omega(b/sr)$	error	$d\sigma/d\Omega(b/sr)$	error
15	1.6iE+0	4.8E-2				
2 0	1.01E+0	3.0E-2				
30	2. 53E-1	7.6E-3	1.95E-2	2. 3E-3	2.96E-3	2.4E-4
4 0	5. 52E-2	1.7E-3	1.20E-2	8.4E-4	3. 02E-3	2.4E-4
50	3. 30E-2	9.9E-4	7.33E-3	2.9E-4	3. 50E-3	2. 8E-4
60	1.32E-2	3. 9E-4	4.05E-3	1.6E-4	2.09E-3	1.9E-4
7 0	1.21E-2	3.6E-4	4.12E-3	2.1E-4	1.54E-3	1.5E-4
80	2. 36E-2	7.1E-4	4.22E-3	2.1E-4	1.11E-3	1.2E-4
90	2. 49E-2	7.5E-4	3. 32E-3	2.0E-4	1.68E-3	1.8E-4
100	1.11E-2	3. 3E-4	2. 03E-3	1.6E-4	1.32E-3	1.5E-4
1 1 0	6. 66E-3	2.0E-4	1.18E-3	1.3E-4	1.25E-3	1.4E-4
120	8. 52E-3	2.6E-4	6.66E-4	1.1E-4	1.41E-3	1.6E-4
1 3 0	9.19E-3	2.8E-4	7.13E-4	1.1E-4	1.14E-3	1.4E-4
140	8. 30E-3	2.5E-4	1. 01E-3	1. 3E-4	1.40E-3	1.7E-4
150	8.19E-3	2.6E-4	1.05E-3	1.9E-4	1.53E-3	2. 3E-4
160	6.80E-3	3. 3E-4	1.43E-3	2.4E-4		
σ_{Total} (barn)	1.17E+0	1.8E-1	6. G1E-2	5. 3E-3	2. 23E-2	2. 2E-3

Table 2(4) Partial differential cross sections for Co at En = 14.1 MeV

Θ _{LAB} (deg)	elastic		continuum		(n, 2n)	
	$d\sigma/d\Omega(b/sr$) error	$d\sigma/d\Omega$ (b/sr	·) error	$d\sigma/d\Omega$ (b/sr) error
15	2. 29E+0	2. 3E-1	5.67E-2	4.0E-3	3.68E-1	2.6E-2
2 0	9.81E-1	9.8E-2	4.44E-2	3. 1E-3	3. 31E-1	2. 3E-2
3 0	1.54E-1	1.5E-2	3.05E-2	2. 1E-3	3.35E-1	2. 3E-2
4 0	2.05E-1	2.1E-2	2. 67E-2	1.9E-3	3.13E-1	2. 2E-2
5 0	9.60E-2	9. GE-3	2.45E-2	1.7E-3	3.11E-1	2. 2E-2
60	3. 07E-2	3. 1E-3	1.94E-2	1.4E-3	2. 91E-1	2. 0E-2
70	3. 26E-2	3. 3 E- 3	1.63E-2	1.1E-3	2.94E-1	2. 1E-2
8 0	2. 29E-2	2. 3E-3	1.43E-2	1.0E-3	2. 58E-1	1.8E-2
90	1.15E-2	1.2E-3	1.25E-2	8.8E-4	2.74E-1	1.9E-2
100	9. 93E-3	9.9E-4	1.12E-2	7.8E-4	2.54E 1	1.8E-2
1 1 0	9.06E-3	9.1E-4	9.48E-3	6.6E-4	2.65E-1	1.9E-2
120	7.36E-3	7.4E-4	7.70E-3	5.4E-4	2.42E-1	1.7E-2
1 3 0	4.87E-3	4.9E-4	8.45E-3	5.9E-4	2. 51E-1	1.8E-2
140	5. 82E-3	5. 8E-4	8.06E-3	5.6E-4	2.63E-1	1.8E-2
150	8. 07E-3	8.1E-4	8.48E-3	5. 9E-4	2.95E-1	2. 1E-2
160	6.84E-3	6.8E-4	5.38E-3	6.5E-4	2.84E-1	2.0E-2
σ_{70101} (barn)	1.33E+0	1.3E+0	2.01E-1	1.4E-2	3. 50E+0	2.5E-1

Table 2(5) Partial differential cross sections for W at En = 14.1 MeV



Fig. 1 Double differential neutron emission cross section at 15 deg with En = 14.1 MeV, for Ca



Fig. 2 Double differential neutron emission cross section at 20 deg with En = 14.1 MeV, for Ca





Fig. 5 Double differential neutron emission cross section at 50 deg with En = 14.1 MeV, for Ca



Fig. 6 Double differential neutron emission cross section at 60 deg with En = 14.1 MeV, for Ca



Fig. 7 Double differential neutron emission cross section at 70 deg with En = 14.1 MeV, for Ca



Fig. 8 Double differential neutron emission cross section at 80 deg with En = 14.1 MeV, for Ca

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Fig. 9 Double differential neutron emission cross section at 90 deg with En = 14.1 MeV, for Ca



cross section at 100 deg with En = 14.1 MeV, for Ca



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Fig. 11 Double differential neutron emission cross section at 110 deg with En = 14.1 MeV, for Ca



Fig. 12 Double differential neutron emission cross section at 120 deg with En = 14.1 MeV, for Ca









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cross section at 20 deg with En = 14.1 MeV, for Mn







Fig. 19 Double differential neutron emission cross section at 40 deg with En = 14.1 MeV, for Mn



Fig. 20 Double differential neutron emission cross section at 50 deg with En = 14.1 MeV, for Mn



ig. 21 Double differential neutron emission cross section at 60 deg with En = 14.1 MeV, for Mn



Fig. 22 Double differential neutron emission cross section at 70 deg with En = 14.1 MeV, for Mn













Fig. 26 Double differential neutron emission cross section at 110 deg with En = 14.1 MeV, for Mn



Fig. 27 Double differential neutron emission cross section at 120 deg with En = 14.1 MeV, for Mn



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Fig. 28 Double differential neutron emission cross section at 130 deg with En = 14.1 MeV, for Mn







Fig. 30 Double differential neutron emission cross section at 150 deg with En ≈ 14.1 MeV, for Mn



cross section at 160 deg with En = 14.1 MeV, for Mn







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fig. 34 Double differential neutron emission cross section at 30 deg with En = 14.1 MeV, for Co





Fig. 36 Double differential neutron emission cross section at 50 deg with En = 14.1 MeV, for Co



Fig. 37 Double differential neutron emission cross section at 60 deg with En = 14.1 MeV, for Co

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Fig. 38 Double differential neutron emission cross section at 70 deg with En = 14.1 MeV, for Co



cross section at 80 deg with En = 14.1 MeV, for Co









Fig. 42 Double differential neutron emission cross section at 110 deg with En = 14.1 MeV, for Co



Fig. 43 Double differential neutron emission cross section at 120 deg with En = 14.1 MeV, for Co











Fig. 46 Double differential neutron emission cross section at 150 deg with En = 14.1 MeV, for Co



Fig. 47 Double differential neutron emission cross section at 160 deg with En = 14.1 MeV, for Co







14.1 MeV, for W





Fig. 51 Double differential neutron emission cross section at 40 deg with En = 14.1 MeV, for W









Fig. 54 Double differential neutron emission cross section at 70 deg with En = 14.1 MeV, for W



Fig. 55 Double differential neutron emission cross section at 80 deg with En = 14.1 MeV, for W



Fig. 56 Double differential neutron emission cross section at 90 deg with En = 14.1 MeV, for W





Fig. 58 Double differential neutron emission cross section at 110 deg with En = 14.1 MeV, for W



Fig. 59 Double differential neutron emission cross section at 120 deg with En = 14.1 MeV, for W







Fig. 61 Double differential neutron emission _ cross section at 140 deg with En = 14.1 MeV, for W



Fig. 62 Double differential neutron emission cross section at 150 deg with En = 14.1 MeV, for W



rig. 63 Double differential neutron emission cross section at 160 deg with En = 14.1 MeV, for W











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En = 14.1 MeV, for Co







Fig. 82 Angular distributions of continuuminelastic and (n, 2n) channels with En = 14.1 MeV, for W