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**A Computer Code based on Hauser-Feshbach and
Moldauer Theory for Nuclear Cross Section Calculations**

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Abstract

The report describes a computer code which is based on Hauser-Feshbach and Moldauer theory. It considers the calculation of compound elastic, inelastic, (n,p) and (n,α) cross sections as one-step process and $(n,2n)$, (n,np) and (n,pn) cross sections as a two-step process. The competition of photons with particles for emission is included in the second step of the reaction only. The available calculations of the elastic and inelastic scattering cross sections with similar codes are compared with the calculations based on the present code.

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1. Introduction

The calculations of nuclear reactions are in general very difficult to carry out partly due to the lack of exact knowledge of nuclear potential and partly due to the involvement of a large number of nucleons in such reactions. The most popular potential used in nuclear reaction calculations is the optical model complex potential [1,2]. The real part of this complex potential gives shape elastic or potential scattering cross section and the imaginary part gives compound elastic and non-elastic cross sections. The nuclear reaction models that represent gradually an increasing degree of complexity of involvement of nucleons in a reaction are direct reaction, pre-equilibrium reaction and fully equilibrated compound nucleus reaction [3-7]. The equilibrium processes taking place through door way states are treated statistically using multistep statistical compound nucleus theories [8-9]. Similarly more complicated direct processes are calculated using multistep statistical direct reaction theories [10]. However, the contribution of pre-equilibrium and multistep statistical processes is small compared with fully equilibrated compound nucleus process in the neutron energy range of 0-14 MeV relevant to fission and fusion technology. The expertise in nuclear reaction calculations using the compound nucleus reaction model is highly desirable. The present code describes a computer code developed by the author for nuclear reaction calculations. It uses Hauser-Feshbach and Moldauer theory [11-12] which is based on the concept of fully equilibrated compound nucleus model. According to this model the incident particle is captured by the target nucleus. It shares its energy with all other nucleons of the nucleus and a thermodynamical equilibrium is attained. A fraction of particles possessing energies in excess of their binding energies have a probability of escape and compete with each other including photons for emission from the nucleus. Hauser and Feshbach showed that if the process of formation and decay of the compound nucleus are assumed independent then the use of reciprocity theorem allows the cross sections in all allowed exit channels to be calculated. The calculation requires the transmission coefficients for the incident channels and all allowed exit channels which are computed using appropriate optical model parameters. The present code can be used for the computation of compound elastic, inelastic, (n,p) and (n, α) cross sections as a one-step process and (n,pn), (n,np) and (n,2n) cross sections as a two-step process. The code has a provision for computation of elastic and inelastic scattering cross sections with width fluctuation correction using Moldauer theory. The competition of photons with particle emission has only been considered in the second step of the reaction for the emission of second particle. The reported calculations of elastic and inelastic nuclear scattering cross sections by similar codes have been compared with calculations carried out using the present code. The theoretical details of the code are presented in the following sections.

2.0 Theoretical Formulation

2.1 Hauser-Feshbach Theory

The expression for differential nuclear cross sections on the basis of Hauser-Feshbach is written as follows:

$$\sigma(\theta, n, m) = \frac{\pi \lambda^2}{(2i_n + 1)(2I_n + 1)} \sum_{JP} \left[\frac{\sum_{\ell' j'} \sum_{\ell j} (\sum (2\ell + 1) A_J(\ell j \ell' j' | \theta) T_{\ell}^n T_{\ell'}^m)}{\sum_{\ell'' j'' q} T_{\ell''}^q} \right] \quad (1)$$

where q labels all the allowed outgoing channels, n refers to the incident channel and m refers to the exit channel for which calculation is desired. The spins of the channels are restricted as follows.

$$\begin{aligned} |J - \ell| \leq j \leq J + \ell & \quad \text{where} \quad |I_n - i_n| \leq j \leq I_n + i_n \\ |J - \ell'| \leq j' \leq J + \ell' & \quad \text{where} \quad |I_m - i_m| \leq j' \leq I_m + i_m \\ |J - \ell''| \leq j'' \leq J + \ell'' & \quad \text{where} \quad |I_q - i_q| \leq j'' \leq I_q + i_q \end{aligned} \quad (2)$$

Where I_n and i_n are the spins of the target and the incident particle. I_m and i_m are the spins of the residual and outgoing particles of interest for calculations. I_q and i_q are spins of the residual nuclei and outgoing particles in all the allowed channels for a given compound nucleus state having spin J and parity P . The lower summation depends only on J and P . It is calculated only once for each set of these parameters and it is done in a subroutine of the main programme.

The angle integrated cross section from channel n to m is given by

$$\sigma = \frac{\pi \lambda^2}{(2i_n + 1)(2I_n + 1)} \left[\frac{(2J + 1) \sum_{\ell \ell' j j'} T_{\ell}^n T_{\ell'}^m}{\sum_{\ell'' j'' q} T_{\ell''}^q} \right] \quad (3)$$

The coefficient $A_J(\ell j | \ell' j' | \theta)$ is given by

$$A_J(\ell j | \ell' j' | \theta) = \frac{(2\ell' + 1)(2J + 1)^2}{4\pi} \left| \sum_L C(\ell \ell L; 000) W(JJ \ell \ell; L_j) C(\ell' \ell' L; 000) W(JJ \ell' \ell'; L_j') P_L(\cos \theta) \right| \quad (4)$$

where C and W denote Clebsch-Gordan coefficient and Racah coefficient respectively. The L is defined by $0 \leq L \leq \min(2\ell, 2\ell', 2J)$ such that it is even. Both C and W are calculated using the recurrence relationships [13].

$$C(\ell\ell L+2;000) = \left(\frac{L+1}{L+2} \right) \left[\frac{(2L+5)(2\ell+L+2)(2\ell-L)}{(2L+1)(2\ell+L+3)(2\ell-L-1)} \right]^{\frac{1}{2}} C(\ell\ell L;000) \quad (5)$$

with

$$C(\ell\ell 0;000) = (-1)^\ell \left(\frac{1}{2\ell+1} \right)^{\frac{1}{2}} \quad (6)$$

$$W(JJ\ell\ell; L+2, j) = F(\ell LJ) \frac{K_{L+2}(Jj\ell)}{K_L(Jj\ell)} W(JJ\ell\ell; Lj) \quad (7)$$

where

$$F(\ell LJ) = \left[\frac{(2J+L+3)(2J+L+2)(2\ell+L+3)(2\ell+L+2)}{(2J-L)(2J-L-1)(2\ell-L)(2\ell-L-1)} \right]^{-\frac{1}{2}}$$

$$\text{and } W(JJ\ell\ell; 0j) = (-1)^{\ell+J-j} \left[\frac{1}{(2J+1)(2\ell+1)} \right]^{\frac{1}{2}} \quad (8)$$

$K_L(Jj\ell)$ is defined by

$$K_{L+1} = \left(\frac{2L+1}{L+1} \right) K_L K_L - L(2L+1) K_L - \frac{L}{L+1} \left[(2J+1)^2 - L^2 \right] \left[(2\ell+1)^2 - L^2 \right] K_{L-1} \quad (9)$$

$$\text{with } K_0 = 1 \text{ and } K_1 = -2[j(j+1) - J(J+1) - \ell(\ell+1)] \quad (10)$$

2.2 Moldauer Theory

For low incident energies the compound nucleus is characterized by low density of levels and a small number of exit channels. The correlations of partial widths necessitates computation of width fluctuation correction to the cross sections calculated using Hauser-Feshbach theory. Moldauer gave the following formula for nuclear cross sections on the basis of compound nucleus cross section model [14]

$$\sigma(\theta, n, m) = \frac{\pi \lambda^2}{(2I_n + 1)(2i_n + 1)} \sum_{JP} \left[\frac{\sum_{\ell'j'} \left(\sum_{\ell j} (2\ell + 1) A_J(\ell j | \ell' j' | \theta) T_{\ell}^n T_{\ell'}^m \right) C_{nm} G_{nm}}{\sum_{\ell''j''q} T_{\ell''}^q} \right] \quad (11)$$

where

$$G_{nm} = \int_0^{\infty} dx \Pi_q \left(1 + \frac{2}{v_q} x \frac{\langle \Gamma_{uq} \rangle}{\langle \Gamma_u \rangle} \right)^{-\left(\frac{1}{2} v_q + \delta_{nq} + \delta_{mq}\right)} \quad (12)$$

$$\text{and } C_{nm} = 1 + \frac{2 \delta_{nm\ell\ell'jj'}}{v_q} \quad \begin{array}{l} \delta_{nm\ell\ell'jj'} = 1 \\ \text{for } n = m, \ell = \ell', j = j' \\ \text{otherwise it is zero} \end{array} \quad (13)$$

The expression for G_{nm} in terms of transmission coefficients becomes

$$G_{nm} = \int_0^{\infty} dx \Pi_q \left(1 + \frac{2}{v_q} x \frac{T_{\ell''}^q}{T} \right)^{-\left(\frac{1}{2} v_q + \delta_{nq} + \delta_{mq}\right)} \quad (14)$$

where $T = \sum_{\ell''} T_{\ell''}^q$

v_q is the degree of freedom that characterizes the distribution of partial widths. The value of v_q is given by [15]

$$v_q = 1.78 + (T_{\ell}^{1.212} - 0.78) \exp(-0.228T) \quad (15)$$

where T_{ℓ} is the transmission coefficient in the incident channel ℓ through which compound nucleus is formed in the state having spin and parity J^{π} .

The G_{nm} is written as

$$G_{nm} = \int_0^{\infty} \frac{dx}{\left(1 + \frac{2x}{v_q} \frac{T_{\ell}^n}{T}\right) \left(1 + \frac{2x}{v_q} \frac{T_{\ell}^m}{T}\right) \Pi_q \left(1 + \frac{2x}{v_q} \frac{T_{\ell}^q}{T}\right)^{v_q/2}} \quad (16)$$

The integral is evaluated [16] by putting

$$y = \frac{1}{1 + \frac{2x}{v_q} \frac{T_{\max}}{T}} \quad \text{or} \quad x = \frac{v_q T}{2T_{\max}} \left(\frac{1}{y} - 1 \right) \quad (17)$$

where T_{\max} is the maximum transmission coefficient in the reaction.

The transformed integral becomes

$$G_{nm} = \frac{v_q T}{2T_{\max}} \int_0^1 \frac{dy}{y^2 \left[1 + \frac{T_{\ell}^n}{T_{\max}} \left(\frac{1}{y} - 1 \right) \right] \left[1 + \frac{T_{\ell}^m}{T_{\max}} \left(\frac{1}{y} - 1 \right) \right] \Pi_q \left[1 + \frac{T_{\ell}^q}{T_{\max}} \left(\frac{1}{y} - 1 \right) \right]^{v_q/2}} \quad (18)$$

This integral is evaluated numerically by Simpson's Rule.

2.3 Particle Transmission Coefficients

The transmission coefficients of neutrons, protons, and alpha-particles required for Hauser-Feshbach calculations can be read as a part of input data or calculated internally with the help of a subroutine based on the optical model code [17] by feeding appropriate optical model parameters. If opted the code uses global optical model parameters recommended by Becchetti and Greenless [18] for the calculations of transmission coefficients.

2.4 Photons Transmission Coefficients

The gamma-ray transmission coefficient $T_{XL}^{\gamma}(E)$ of multipole-type XL and transition energy E is related to gamma-ray strength function $f_{XL}^{\gamma}(E)$ in the following way [19].

$$T_{XL}^{\gamma}(E) = 2\pi E^{2L+1} f_{XL}^{\gamma}(E) \quad (19)$$

where

$$f_{\lambda L}^{\gamma} = \frac{\bar{\Gamma}_{\lambda \gamma f}^{XL}}{\bar{D}_{\gamma} E^{2L+1}} \quad (20)$$

where λ refers to the initial state and f to the final state of the transition. The average gamma-ray width $\bar{\Gamma}_{\lambda \gamma f}^{XL}$ and the average level spacing \bar{D}_{λ} are given in eV and the gamma-ray energy, E , is given in MeV. Brink [20] and Axel [21] have assumed that E1 giant dipole resonance is described by a classical Lorentzian line shape and thus partial width, $\bar{\Gamma}_{\lambda \gamma 0}$ of the state λ for transition to the ground state is given by

$$\bar{\Gamma}_{\lambda \gamma 0} = \frac{8.67 \times 10^{-8} \bar{D}_{\lambda} \sigma_0 E^4 \Gamma_g^2}{[E^2 - E_g^2]^2 + E^2 \Gamma_g^2} \quad (21)$$

where σ_0 is the peak resonance cross section and equals $13A/\Gamma_g$ mb. The transition energy E , the giant dipole resonance energy E_g and the resonance width Γ_g are in MeV. The average level spacing \bar{D}_{λ} and width $\bar{\Gamma}_{\lambda \gamma 0}$ are in eV. The above expression holds for a unit spin of the state λ and a zero spin of the ground state. In order to generalize the above expression to arbitrary spin-values, we rewrite the above expression in the following form:

$$\bar{\Gamma}_{\lambda \gamma 0} = 8.67 \times 10^{-8} \times 3 \left(\frac{2J_f + 1}{2J_i + 1} \right) \frac{\bar{D}_{\lambda} E^4 \sigma_0 \Gamma_g^2}{(E - E_g)^2 + E^2 \Gamma_g^2} \quad (22)$$

The gamma-ray transmission coefficient becomes

$$T_{EI}^{\gamma}(E) = 2\pi \frac{\bar{\Gamma}_{\lambda \gamma 0}}{\bar{D}_{\lambda}} = 2.125 \times 10^{-5} \left(\frac{2J_f + 1}{2J_i + 1} \right) \frac{A \Gamma_g E^4}{(E - E_g)^2 + E^2 \Gamma_g^2} \quad (23)$$

The calculated values of the transmission coefficients for E1 transitions are normalized using a measured value of the gamma-ray width. The measured E1 transition width is also used to normalize the widths calculated on the basis of single particle model [22-23]. The following expressions have been used for calculation of widths on the basis of the single particle model [22].

$$\begin{aligned}
\Gamma_{\lambda\gamma f}(E1) &= 6.8 \times 10^{-8} E^3 A^{2/3} \frac{D_\lambda}{D_0} \\
\Gamma_{\lambda\gamma f}(M1) &= 2.1 \times 10^{-8} E^3 \frac{D_\lambda}{D_0} \\
\Gamma_{\lambda\gamma f}(E2) &= 4.9 \times 10^{-14} E^5 A^{4/3} \frac{D_\lambda}{D_0}
\end{aligned} \tag{24}$$

where $\Gamma_{\lambda\gamma f}$ and D_λ are in eV and the gamma-ray energy E and D_0 in MeV. A value of 15 MeV for D_0 has been used.

2.5 Energy Level Densities

The knowledge of energy level densities is needed in nuclear cross section calculations involving energy regions where the number of levels is high and the information on their spins and parities is poor. The energy level densities play a very crucial role in these calculations. There are two types of energy level density formulas currently being used in the nuclear cross section calculations. Both of these have been included in the present code. The details of these formulas are given in the following sections.

2.5.1 Gilbert-Cameron Composite Formula

The density of levels per MeV of energy E , spin J at high energies is given by [24]

$$\rho_2(E, J) = \frac{1}{24\sqrt{2}} \frac{\exp(2\sqrt{aU})}{\sigma^3 a^{1/4} U^{5/4}} (2J + 1) \exp\left(-\frac{(J + 1/2)^2}{2\sigma^2}\right) \tag{25}$$

where

$$\begin{aligned}
U &= E - U_0 = E - P(z) - P(N) \\
\sigma^2 &= 0.0888 (aU)^{1/2} A^{2/3}
\end{aligned}$$

Here $P(z)$ and $P(N)$ are pairing energies listed by Gilbert and Cameron [24]. The value of the level density parameter a (MeV^{-1}) is calculated from the following expression for the undeformed nuclei.

$$a/A = 0.00917S + 0.142 \tag{26}$$

and for deformed nuclei it is given by

$$a/A = 0.00917S + 0.120 \tag{27}$$

where S is given by

$$S = S(z) + S(N)$$

$S(z)$ and $S(N)$ are shell corrections in MeV tabulated by Gilbert and Cameron. The level density per MeV, of all J's is given by

$$\rho_2 = \frac{1}{12\sqrt{2}} \frac{\exp(2\sqrt{au})}{\sigma a^{1/4} U^{5/4}} \quad (28)$$

The nuclear temperature τ in MeV is given by

$$\frac{1}{\tau} = \frac{dp_2}{dU} = \sqrt{\frac{a}{U}} - \frac{5}{4} \frac{1}{U} \quad (29)$$

The above formulas for level density are used for energies greater than E_x (MeV) where

$$E_x = U_x + P(z) + P(N)$$

$$\text{and } U_x = 2.5 + 150/A \quad (30)$$

Below E_x the following simple formula for level density is used.

$$\rho_1(E) = \frac{1}{T} \exp\left(\frac{E - E_0}{T}\right) \quad (31)$$

$$\text{The temperature } T \text{ and } E_0 \text{ are determined by fitting } \rho_2 \text{ and } \rho_1 \text{ at } E = E_x \quad (32)$$

$$T = \tau(U_x)$$

and

$$E_0 = E_x - T \log_e(T \rho_2(U_x)) \quad (33)$$

2.5.2 Back-shifted Fermi-gas Model Formula

The back-shifted Fermi-gas model formula is based on two empirically fitted parameters a and Δ . The level density formula is given by [25].

$$\rho(U, J) = \frac{1}{24\sqrt{2}} \frac{\exp[2(a(U - \Delta))^{1/2}]}{\sigma^3 a^{1/4} (U - \Delta + t)^{5/4}} (2J + 1) \exp\left(\frac{-J(J + 1)}{\sigma^2}\right) \quad (34)$$

and the total density ρ per MeV is given by

$$\rho(U) = \frac{1}{12\sqrt{2}} \frac{1}{\sigma a^{1/4}} \frac{\exp[2(a(U - \Delta))^{1/2}]}{(U - \Delta + t)^{5/4}} \quad (35)$$

The thermodynamic temperature t in MeV is given by

$$U - \Delta = at^2 - t$$

σ is the spin cut-off parameter and it is given by

$$\sigma^2 = g \langle m_j^2 \rangle - t$$

Here $\langle m_j^2 \rangle$ is the average squared projection of spins and g is the density of single particle states near the Fermi level. From theoretical arguments σ^2 is expected to approach at high excitations the value

$$\sigma_{\text{rigid}}^2 = I_{\text{rigid}} \frac{t}{\hbar^2} = 0.0150 A^{5/3} t \quad (38)$$

where $I_{\text{rigid}} = 2/5 MR^2$ is the rigid body moment of inertia and a nucleus radius $1.25 A^{1/3}$ fm is assumed.

3.0 Comparison with other Codes

The differential elastic and inelastic scattering cross sections of 3.3 MeV neutrons scattered from ^{58}Ni calculated using the present code are compared with the available calculations of ABAREX code [26] in table 1. The ABAREX code calculations given in the laboratory system have been converted to the centre-of-mass system. As the calculated cross sections are symmetric about 90 degree in the centre-of-mass system, cross sections for comparison have been included only upto 90 degree. The Hauser-Feshbach calculations are given under the columns headed by H.F. The cross sections corrected for width fluctuation are given in the columns under Moldauer. The integrated elastic and inelastic scattering cross sections of different levels are listed in table 2. The following optical model parameters with derivative Woods-Saxon form factor for imaginary potential and Thomas form factor for the spin orbit potential have been used.

Real potential well depth	=	45.1 MeV
Real potential well radius	=	$1.2975 A^{1/3}$ fm
Real potential well diffuseness	=	0.6380 fm

Imaginary potential well depth	=	11.7 MeV
Imaginary well radius	=	$1.302 A^{1/3}$ fm
Imaginary potential well diffuseness	=	0.3344 fm
Real spin-orbit potential well depth	=	5.5 MeV
Real spin-orbit potential well radius	=	$1.005 A^{1/3}$ MeV
Real spin-orbit potential well diffuseness	=	0.65 fm

The calculations for differential elastic, inelastic and integrated cross sections of 0.072 MeV neutrons scattered from ^{238}U carried out using the present code are compared with the calculations of Wilmore code [16] in table 3. The transmission coefficients of neutrons used are also listed in table 3. There is a very good agreement between the calculations carried out using the present code and the available calculations of the ABAREX code and Wilmore code.

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Table 1. Comparison of the calculations of differential elastic and inelastic scattering cross sections of 3.3 MeV neutrons from ^{58}Ni carried out using the present code and ABAREX code. The differential cross sections are in c.m. system and given in mb/steradian.

E_x (J $^\pi$)	$\theta_{c.m.}$	H.F		Moldauer	
		ABAREX Code	PRESENT Code	ABAREX Code	PRESENT Code
0.0 (0 $^+$)	0.0	45.5	44.25	83.60	82.05
	15.0		39.61		72.84
	15.3	40.38		73.60	
	30.0		29.57		53.28
	30.5	29.55		52.95	
	45.0		20.92		37.02
	45.7	21.06		37.07	
	60.0		16.44		28.94
	60.9	16.93		29.66	
	75.0		14.86		26.14
	76.0	15.02		26.33	
	90.0		14.56		25.49
	91.0	14.40		25.22	
1.45 (2 $^+$)	0.0	44.79	44.8	37.0	37.26
	15.0		45.46		37.78
	15.3	45.43		37.57	
	30.0		46.56		38.79
	30.7	46.65		38.67	
	45.0		47.11		39.23
	45.9	46.99		39.0	
	60.0		46.56		38.70
	61.2	46.64		38.39	
	75.0		45.50		37.74
	76.3	45.22		37.45	
	90.0		44.98		37.28
	91.3	44.79		37.07	
2.459 (4 $^+$)	0.0	10.96	10.92	9.67	9.81
	15.0		11.11		9.99
	15.5	11.18		9.85	
	30.0		11.59		10.44
	31.0	11.70		10.31	
	45.0		12.18		10.98
	46.4	12.39		10.90	
	60.0		12.68		11.45
	61.7	12.99		11.43	
	75.0		12.99		11.75
	76.9	13.41		11.80	
	90.0		13.10		11.85
	92.0	13.50		11.88	
2.776 (2 $^+$)	0.0	17.57	17.66	15.20	15.39
	15.0		17.71		15.43
	15.7	17.62		15.24	
	30.0		17.81		15.51
	31.3	17.67		15.30	
	45.0		17.84		15.51
	46.8	17.62		15.25	
	60.0		17.74		15.41
	62.3	17.44		15.08	
	75.0		17.63		15.27
	77.5	17.23		14.89	
	90.0		17.56		15.20
	92.6	17.50		14.80	

Table 1 continued ...

2.902 (1 ⁺)	0.0	11.90	11.72	10.17	10.04
	15.0		11.61		9.94
	15.5	11.78		10.05	
	30.0		11.32		9.65
	31.5	11.50		9.77	
	45.0		10.91		9.26
	47.2	11.13		9.41	
	60.0		10.50		8.87
	62.6	10.76		8.61	
	75.0		10.20		8.58
	77.9	10.52		8.82	
	90.0		10.08		8.47
	93.0	10.54		8.75	
2.942 (0 ⁺)	0.0	5.50	5.52	4.59	4.60
	15.0		5.38		4.47
	15.8	5.34		4.44	
	30.0		5.01		4.13
	31.6	4.95		4.08	
	45.0		4.59		3.75
	46.3	4.54		3.70	
	60.0		4.27		3.46
	62.8	4.24		3.44	
	75.0		4.09		3.30
	78.1	4.09		3.31	
	90.0		4.03		3.26
	93.1	4.05		3.28	
3.038 (1 ⁺)	0.0	11.56	11.59	10.04	10.12
	15.0		11.60		10.12
	16.0	11.56		10.04	
	30.0		11.60		10.11
	32.0	11.54		10.03	
	45.0		11.59		10.10
	47.8	11.49		9.98	
	60.0		11.56		10.05
	63.4	11.42		9.90	
	75.0		11.53		10.01
	78.8	11.36		9.84	
	90.0		11.52		10.0
	93.9	11.32		9.81	

Table 2. Comparison of integrated elastic and inelastic scattering cross sections of 3.3 MeV neutrons from ^{58}Ni . All cross sections are in millibarns and energies of the levels are in MeV.

Level	J^π	Hauser - Feshbach		Moldauer	
		ABAREX Code	PRESENT Code	ABAREX Code	PRESENT Code
0.0	0^+	257.0	252.4	455.5	449.2
1.45	2^+	577.4	579.3	478.5	481.4
2.459	4^+	159.6	156.6	140.5	141.4
2.776	2^+	219.1	222.7	189.5	193.3
2.902	1^+	137.4	133.6	115.9	113.1
2.942	0^+	55.8	55.7	45.5	45.3
3.038	2^+	143.7	145.3	124.6	126.3

Total cross section:

ABAREX code: 1550.0 mb

Present code: 1550.0 mb

Table 3. Comparison of the elastic and inelastic scattering cross sections of 0.072 MeV neutrons from ^{238}U computed using Wilmore code and present code. The transmission coefficients in the order of $\ell=0$, $\ell=1$, etc. for the ground state are 0.23827, 0.12472, 0.00170, 0.0004 and for the first excited state are 0.15838, 0.03598, 0.00018. The differential cross sections are in millibarn per steradian and energies are in MeV.

E_x (J $^\pi$)	$\theta_{c.m.}$	Hauser - Feshbach		Moldauer		Integrated Cross Sections
		Wilmore Code	Present Code	Wilmore Code	Present Code	
0.0 (0 $^+$)	0.0	457.6	453.1	522.1	516.5	A. <u>Hauser-Feshbach</u>
	15.0	446.4	442.1	508.0	502.6	Wilmore Code : 4353 mb
	30.0	415.9	411.8	469.6	464.7	Present Code : 4310 mb
	45.0	374.2	370.5	417.4	413.0	
	60.0	332.5	329.2	365.3	361.4	B. <u>Moldauer</u>
	75.0	302.0	299.0	327.3	323.7	Wilmore Code : 4810 mb
	90.0	290.8	287.8	313.4	310.0	Present Code : 4758 mb
	0.0	70.9	70.2	41.8	41.0	A. <u>Hauser-Feshbach</u>
	15.0	72.8	72.2	42.90	42.1	Wilmore Code : 1132 mb
0.045 (2 $^+$)	30.5	78.1	77.4	45.9	45.1	Present Code : 1121 mb
	45.0	85.3	84.5	50.1	49.3	
	60.0	92.5	91.6	54.3	53.4	B. <u>Moldauer</u>
	75.0	97.7	96.8	57.3	56.4	Wilmore Code : 664 mb
	90.0	99.7	98.7	58.4	57.5	Present Code : 654 mb