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### UNFOLDING OF NEUTRON SPECTRA FROM ACTIVATION

DATA USING THE RFO1 AND RFO7 CODES

L. Turi and A. Fischer Hungarian Academy of Sciences Central Physics Research Institute Budapest

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IAEA NUCLEAR DATA SECTION, KÄRNTNER RING 11, A-1010 VIENNA

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## ABSTRACT

The authors describe two methods for unfolding neutron spectra from activation data. The RFOl code can be used only with threshold detectors, but the use of the RFO7 code involves no such limitations; if suitable foils are used, neutron spectra can be unfolded over the whole energy range at one time.

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### Introduction

Knowledge of the energy distribution of neutrons plays an important part in the study of different reactor types.

The use of activation foils to measure neutron spectra has a potential that is not shared by other methods; the foils are small in size and not normally sensitive to temperature change. They are used to measure spectra as a function of position; moreover, such measurements provide information on the entire energy range at one time. The latter fact is of particular importance in that the results of measurements conducted in different energy ranges can therefore be normalized with respect to one another, and detailed energy distributions determined by other methods in various energy ranges can be fitted into the approximate spectrum obtained from the activation data. It should be noted that in processing the data we do not take into account the fact that the measurement was made with foils; the processing technique can be applied whenever one measures the rate of interaction between neutrons and matter (in fission chambers, BF, counters, semiconductor detectors and so on). For the sake of simplicity we will henceforth always use the expression "foil activation".

When applying the foil activation method the values one measures are certain integrals of the products of flux and foil cross-sections. The spectrum unfolded from these data is somewhat arbitrary, since we have only a small quantity of data available - namely, the measured foil activities. The spectrum should satisfy the activation equations (1)

$$A_{i} = \int_{O}^{\infty} \phi(E) \Sigma_{i}(E) dE \qquad (1)$$

where A<sub>i</sub> is the measured reaction rate in the i-th foil;

 $\phi(\mathbf{E})$  is the spectrum as a function of energy;

 $\Sigma_i(E)$  is the energy-dependent cross-section for the reaction occurring during activation of the i-th foil.

There is, of course, an infinite number of spectra satisfying these equations. Hence, some more initial information is required to determine the spectrum. It can be said that, on the whole, the more measured data we have, the less initial information is required. However, the microstructure of a spectrum depends greatly on the initial information, which is therefore of great importance and is usually given in the form of an initial spectrum. Methods of processing activation data can be divided into two groups. The first group comprises methods where it is assumed that one is dealing with a spectrum given in a simple analytical form (Maxwellian distribution, I/E, fission spectrum, some polynomial or certain combinations of these) and that it is only the parameters of this analytical form that are unknown. A method of this kind was first applied by Lanning  $\sqrt{-1}$ , who expanded a spectrum in an orthonormalized system of functions. The limits of applicability of this method were studied by Gold  $\sqrt{-2}$ .

In the thermal neutron region, the commonest method is the use of a Laguerre polynomial as the orthonormalized system of functions. If the spectrum is expanded in a series and only the first few terms are considered, the theoretical spectrum closely approximates the actual spectrum. In the fast and epithermal neutron region one cannot determine categorically the form in which the solution should be sought, particularly when the entire neutron energy region is taken into account. In such cases, we therefore consider it better to apply the methods belonging to the second group.

The second group comprises methods with which the spectrum is determined purely numerically by means of iteration. A method of this kind was used in Ref. [-4] for the initial measurements of a fast neutron spectrum; it was assumed that the cross-section of threshold detectors was described by means of functions whose values were equal to zero up to a threshold energy, and to certain constants above that threshold. From the foil activities the integral flux was determined for each threshold energy (this quantity is taken to mean a certain flux integral between the threshold energy and infinity), after which the spectrum was determined by differentiation. The values of  $\sigma_i(E)$  available at that time were only very approximate and more accurate calculations were therefore not possible.

Over the past few years, the availability of more exact cross-section values and the use of computers have made it possible to develop more accurate methods based on these principles. A typical example is the SAND-I code developed by McElroy and co-workers [-4]. The SAND-II code, also developed by McElroy and co-workers, is based on different principles [-5]. Both these methods have been adapted by us for use with our ICT-1905 computer.

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As the SAND-I code is described in detail in Ref. [4], we give only a brief description of the RFOl code in this report. The RFO7 code developed by us is similar to the SAND-II code (of which only a very short description is available) only as far as the main features are concerned.

Further on we describe the RFO1 and RFO7 codes developed by us. It should be noted that the sphere of application of the former is limited (it is used only with threshold detectors), whereas there is no limitation of this kind in the case of the RF07 code; moreover, the RF07 code gives considerably better results, so that, apart from certain special cases (for example, when no initial information on the spectrum is available), it is better to use the RFO7 code. The entire energy region can be divided into a maximum of 500 points. The initial spectrum can be given in analytical or numerical form; in the latter case, it can be given for The initial spectrum actually considered will consist of arbitrary points. During the calculations, the initial straight lines joining these points. spectrum is varied until the deviation of the measured from the theoretical activities is less than a value specified in the input data.

### RF01 code

Each iterative step consists of the following operations:

1. Determination of the reaction rate for each foil from the given iteration spectrum and cross-sections:

$$B_{i}^{(k)} = \int_{0}^{\infty} \phi^{(k)}(E) \Sigma_{i}(E) dE / i = 1, 2, ..., I /$$
(2)

where  $B_i^{(k)}$  is the reaction rate for the i-th foil as calculated at the k-th iterative step;

 $\phi^{(k)}(E)$  is the spectrum at the k-th iterative step;

I is the number of foils.

2. Assignment of a threshold energy to each foil (this value is taken to be the energy above which 95% of all reactions occur in the given spectrum) in accordance with the following equation:

$$\int_{E_{i}}^{\infty} \phi^{(k)}(E) \Sigma_{i}(E) dE = \beta \int_{O}^{\infty} \phi^{(k)}(E) \Sigma_{i}(E) dE$$
(3)

where E<sub>ithr</sub> is the threshold energy of the i-th foil as determined from Eq. (3);

 $\beta = 0.95.$ 

### 3. Determination of the integral flux for each foil:

$$\Phi_{i}^{(k)} = \int_{E_{ithr}}^{\infty} \phi^{(k)}(E) dE$$
(4)

4. Determination of the new integral flux:

$$\Phi_{\mathbf{i}}^{(\mathbf{k}+1)} = \Phi_{\mathbf{i}}^{(\mathbf{k})} - \frac{A_{\mathbf{i}}}{B_{\mathbf{i}}^{(\mathbf{k})}}$$
(5)

# 5. Determination of the new spectrum by differentiation of the curve fitted to the points denoting the integral flux values.

The most difficult stage of the method is the fitting of the curve to the integral points. McElroy first carried out this operation by hand. With the method we have developed, use is made of parabolas passing through three integral points. Subsequently, when differentiating, only the segment of the parabola between the first and second points is used. The curve derived in this fashion is broken, but that does not greatly spoil the shape of the spectrum, and after the sixth or seventh iterative step the curve, when corrected manually, gives approximately the same values of  $B_i^{(k)}$  as an uncorrected broken curve.

The RFOL code has two substantial disadvantages: first, the integral flux is determined only at as many points as there were irradiated foils; second, if the threshold energies in two foils are close together or coincide, some of the information is lost, for the integral flux is determined only at one point by means of two foils.

### RF07 code

Each iterative step consists of the following operations:

1. Determination of the reaction rates from the given spectrum:

$$B_{i}^{(k)} = \sum_{n=1}^{N} \phi_{n}^{(k)} \Sigma_{i,n} \Delta E_{n} / i = 1, 2, \dots, I /$$
(6)

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where  $\phi_n^{(k)}$  is the flux in the n-th energy range at the k-th step;  $\Sigma_{i,n}$  is the cross-section for the i-th reaction in the n-th energy range;

 $\Delta E_n$  is the width of the n-th energy range;

N is the number of energy ranges.

It should be noted that this formula corresponds to formula (2). The quantities appearing in formula (6) are of the group type, but the ranges are narrow and the quantities can therefore be calculated by means of simple formulas, which we will not consider here.

2. Determination of the weight factor for each foil and each range:

$$W_{i,n}^{(k)} = \frac{1}{\frac{(k)}{B_{i}^{(k)}}} \phi_n^{(k)} \Sigma_{i,n} \Delta E_n \qquad (1 = 1, 2, \dots, 1; n = 1, 2, \dots, N/ n = 1,$$

3. Determination of the correction factor for each range:

$$C_{n}^{(k)} = \frac{N}{I} \sum_{i=1}^{I} \left( W_{i,n}^{(k)} - \frac{A_{i} - B_{i}^{(k)}}{A_{i}} \right)$$
(8)

4. Determination of the new flux for each range:

$$\phi_{n}^{(k+1)} = \phi_{n}^{(k)} \left( 1 + c_{n}^{(k)} \right)$$
(9)

After each iterative step the flux is normalized in such a way that the sum of the squares of the deviations of the measured and computed activity ratios from unity, i.e. the expression

$$\sum_{i=1}^{I} \left( \frac{B_i^{(k)}}{A_i} - 1 \right)^2$$

is at a minimum. If the flux is multiplied by a number f in each energy range, each activity increases by a factor f, so that this number should be determined in such a way as to satisfy the condition

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$$\sum_{i=1}^{I} \left( \frac{f B_{i}^{(k)}}{A_{i}} - 1 \right)^{2} = \min \left( 10 \right)$$

If we differentiate this expression with respect to f, we get, after simple transformations

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$$\mathbf{f} = \frac{\frac{\mathbf{I}}{\sum_{i=1}^{\mathbf{I}} \frac{\mathbf{B}_{i}^{(K)}}{\mathbf{A}_{i}}}{\sum_{i=1}^{\mathbf{I}} \left(\frac{\mathbf{B}_{i}^{(K)}}{\mathbf{A}_{i}}\right)^{2}}$$
(11)

This means that one should calculate this quantity after each step, and then multiply the flux by it.

Detailed examination of the code algorithm shows clearly that at those points where the cross-section of all the detectors used is zero the spectrum varies only as a result of normalization, since the detectors do not carry any information about these ranges.

The applications of the code and some of its properties, and also the interpretation of the results obtained with it, are discussed by us in detail in Ref.  $\sqrt{-6}$ .

The cross-sections used for the calculations are recorded on RFSP-LIBRARY tape. The cross-sections of the cadmium-covered foils were calculated with the aid of a separate code. The data on the magnetic tape can be supplemented or altered as new data are received. Table 1 shows the designations of those reactions for which we have the cross-sections on tape. For the code we use RFSP-LIBRARY tape and one auxiliary magnetic tape. The input data can be inserted on 8-track punched tape or on punched cards.

Using the code, we first seek data on the foil cross-sections; after appropriate processing, these data are then recorded on the auxiliary magnetic tape. During the rest of the operation only the auxiliary tape is used. If there are no data on a particular foil (or foils) on the RFSP-LIBRARY tape, the code indicates this fact and calculates only with the data on the remaining foils. If there are no data on any of the foils, the code reads the available data for the problem being solved and then begins reading the data relating to the next problem.

### Input data for programmes

All the lines of input data are compiled in accordance with the rules for the FORTRAN format. The sequence for these lines is as follows:

1st type: 211, 12 MI = 1 - New problem;
3 - End of punched tape.
NANAL = 1 - The initial spectrum is given in
analytical form;
2 - The initial spectrum is given in
numerical form.
KIRAJZ - The number of iterations after which
the results should be printed out.
The results of the first and last
iterations are printed out irrespective
of this.

 2nd type: 12
 NSIG

 3rd type: [2A8, 2E12.5]

- Number of foils used.

- The first two data items indicate the foil designation. This designation must agree with that given in Table 1. The designation is followed by the measured reaction rates in the spectrum being studied and the calibration spectrum. The calibration spectrum need not be read, but if the foils have not been calibrated, we have to give absolute foil activities for one atom.

This type is read NSIG times.

- Any text in two lines with 60-60 alphanumerical symbols in each.
- Maximum number of iterations;
- Permissible error in the activities. Iteration terminates when

 $\sum_{i=1}^{I} \frac{1}{A_{i}} \left| B_{i}^{(k)} - A_{i} \right| \leq DMEG$ 

4th type: 2 [7A8, A4]

5th type: 14, E14.5

LEPMAX

DMEG

6th type: 2E12.5, I6 **ALSO** - Lower energy limit in MeV; FELSÖ - Upper energy limit in MeV; NOSZT - Number of energy intervals. The intervals on a logarithmic scale are distributed uniformly. 7th type: 4E12.5 CK1 - Parameters of calibration flux. EMAXW1, CK2, CK3 CK1, CK2 and CK3 are amplitudes of Maxwellian and I/E spectra and fission spectrum, while EMAXWl is the maximum energy of the Maxwellian spectrum. If the foils are not calibrated, the values of these parameters need not be given, but a place has to be left empty for them. - The parameters of the initial spectrum 8th type: 4E12.5 CK11, EMAXW11, CK12, are in the same sequence as in the case CK13 of the 7th type. This type is read only when NANAL = 1. 9th type: I4 - The number of energy points at which NENBE the initial spectrum is given. This type is read only when NANAL = 2. 10th type: / 6E12.5 7 - Altogether 2 x NENBE numbers.

The code then begins the calculation, in the course (in accordance with the KIRAJZ value) and after the completion of which it prints out the result and goes on to read data relating to the next problem.

order.

the KIRAJZ value.

only when NANAL = 2.

 $E_{T}, \phi_{O}(E_{T}), E_{2}, \phi_{O}(E_{2}), etc.$ 

The energies must follow in descending

times as required for consistency with

This type is read as many

It is also read

### Print-out of results

After the input data have been issued as first-iteration results, the code prints out the normalized initial spectrum; the spectrum is then

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printed out after each KIRAJZ iteration. The measured and calculated reaction rates, their ratios and percentage deviations, are also printed out. The spectrum is displayed schematically on a logarithmic scale.

The Appendix contains a set of input data and a photocopy of results printed out by the RFO7 code.

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# Table 1

## Reactions recorded on RFSP-LIBRARY tape and their energy limits

	_
U235/NF/FPCD	0,7.10 <sup>-8</sup> - 18 MeV
U233/NF/FP-CD	<b>1</b> ,0,10 <sup>-8</sup> - 18
PU239/NF/FP_CD	0,6.10 <sup>-8</sup> - 18
NA23/NG/NA24-CD	0,5.10 <sup>-8</sup> - 18
MG24/NP/NA24	0,05 - 18
IN115/NN/IN115M	0,05 - 18
832/NP/P32	0,05 - 18
AL27/NP/MG27	0,05 - 18
AL27/NHE/NA24	0,05 - 18
RH103/NN/RH103M	0,05 - 18
FE56/NP/MN56	0,05 - 18
N158/NP/C058	0,05 - 18
P31/NP/SI31	0,05 - 18
PU239/NF/FP	0,5.10 <sup>-10</sup> - 10 <sup>-5</sup>
DY164/NG/DY165	0,33.10 <sup>-10</sup> -10 <sup>-5</sup>
LU176/NG/LU177	$0,5.10^{-10} - 10^{-5}$
EU151/NG/EU152	$0,5.10^{-10} - 10^{-5}$
IN115/NG/IN116	$0,5.10^{-10} - 10^{-5}$
AU197/NG/AU198	0,5.10 <sup>-10</sup> - 2.10 <sup>-5</sup>
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## REFERENCES

<u></u> 1_7	LANNING, W.D., Trans. Am. Nucl. Soc. 6 (1963) 35.
<u>[2]</u>	GOLD, R., Nucl. Sci. Eng. 20 (1964) 493.
<u>[3]</u>	HUGHES, D.J., Pile Neutron Research, Cambridge (Mass.) (1953).
<u>_4_7</u>	McELROY, W.N. et al., Nucl. Sci. Eng. 27 (1967) 533.
<u>[5]</u>	McELROY, W.N. et al., AFWL-TR-67-41 (September 1967).
<u>[</u> 6 <u>]</u>	FISCHER, A., TURI, L., to be published.

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```
22 2
 5
PU239(NF)FP
                 8.76059E 02
DY164(NG)DY165
                1.80564E+03
LU176(NG)LU177
                 4.21792E+03
                 2.46769E+03
EU151 (NG)EU152
IN115(NG)IN116
                 6.08475E+02
   - TEST CASE FOR REPORT -
- 15 JULY 1970. -
 100
       0.01000E 00
 1.00000E-09 3.00000E-06
                          100
 0.0
             0.0
                         0.0
                                     0.0
  39
 3.
        E-06 1.7
                   E-02 2.75
                               E-06 1.925 E-02 2.2
                                                       E-06 2.32
                                                                   E-02
 1.9
        E-06 2.68
                   E-02 1.6
                               E-06 3.19
                                           E-02 1.4
                                                       E-06 3.64
                                                                   E-02
        E-06 4.25
                   E-02 1.05
                               E-06 4.85
 1.2
                                           E-02 0.9
                                                       E-06 5.67
                                                                   E-02
 0.85109E-06 6.8781 E-02 0.68412E-06 6.8781 E-02 0.68411E-06 9.1563 E-02
 0.51234E-06 9.1563 E-02 0.51233E-06 1.2353 E-01 0.38482E-06 1.2353 E-01
 0,38481E-06 1.658 E-01 0.27553E-06 1.658 E-01 0.27552E-06 2.4184 E-01
 0.21278E-06 2.4184 E-01 0.21277E-06 3.4906 E-01 0.17104E-06 3.4906 E-01
 0.17103E-06 4.8664 E-01 0.13385E-06 4.8664 E-01 0.13384E-06 8.3368 E-01
 0.10121E-06 8.3368 E-01 0.10120E-06 1.3658 E 00 7.31180E-08 1.3658 E 00
 7.31170E-08 2.139 E-00 4.95890E-08 2.139 E 00 4.95880E-08 2.6911 E-00
 3.0614 E-08 2.6911 E 00 3.06130E-08 2.684 E 00 1.7853 E-08 2.687 E 00
 1.7852 E-08 2.1198 E 00 9.1081 E-09 2.1198 E 00 9.1080 E-09 1.318 E 00
 4.0481 E-09 1.318 E 00 4.0480 E-09 2.8335 E-01 1.0 E-09 2.8335 E-01
3
```

Set of input data

• • • RFO7 + + +

- TEST CASE FOR REPORT -

 PU239(NF)FP
 R.76059E
 02
 0.0000F-01

 DY164(NG)DY165
 1.80564E
 03
 0.00000F-01

 LU176(NG)LI1177
 4.21792E
 03
 0.00000F-01

 LU176(NG)LI1177
 4.21792E
 03
 0.00000F-01

 LU176(NG)LI1177
 4.21792E
 03
 0.00000F-01

 LU15(NG)LI1152
 2.46769E
 03
 0.00000F-01

Number of foils

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Number of steps 100 Number of division 100 points 1.000E-02 3.0005-06 MFV Energy limits 1.000E-00 ES 3.0005-06 MFV

Non-calibrated foils

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Results printed out by the RFO7 programme (I)

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R F 0 7	
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Number of iterations: 1

Differential flux printout 1 Point-wise

	96	¥	÷	35	ŝ	Ŷ	× ×	÷	ž	ý	£	Ś	÷	5	ŗ	5	š		::	77
(3)3.	1 "013E (	1.0135	1.0136 1	6.71CE	1 2012 Y	7.5755 1	1.5755 (	0.598E	5 K17F 1	7.6445 (	ANSE (	1 3640 4	1 3745 1	8, 443E (	4.455 1	3.272E	2,0025	1 377F (	2,139F C	1 3520 9
ja.	1.382E-09	2.0715-00	3.1036-09	60-3079.7	6.055E-09	1.0445-08	1.5645-08	2.3435+08	3.511E-08	5,260E-98	7. 232E-08	1.1816-07	1.7596-07	- 20-315-07-	3.9776-67	5.9525-07	8.018E-07	1.3365+06	2.002E-05	3.0006+06
	9 U	90	90	90	9 ¢	90	90	9 U	9 Ú	9ü	ŝ	90	90	5 C	9 C	ŝ	ŝ	ŝ	. 70	9 Ú
(3)3	12:0°3F	1.013F	1.01%E	4.710F	24 JE	7.575F	7.575E	9.5005	9.6175	9.617E	7.6445	3026°2	1.730E	8.643E	5.925F	3.272E	2,458E	1.483E	9.902E	6,825E
<b>5</b>	1.2755-09	1.9105-09	2.8615-09	4.287F-19	6-4227 9	9.6245-09	1.4475-08	2.1615-08	3.234F-A8	6.852E-08	7.269F-08	1. n80 E-07	1.4326-07	2.4455-07	3.6645-07	5.49AF-07	B. 2256-07	1.232E-06	1.8475-06	2.767E-06
	96	90	00	٩u	90	۶ů	. 90	.90	°°	çõ	92	śċ	÷0	50	50	S	50	50	ŝ	30
F(F)	1.0135	1.0135	1.0135	1.0135	4.74 nF	4.74AF	7.575E	9.603.9	9.5925	9.6175	7.6446	4 . RAJE	1 739 =	8.6435	5,0255	4.455	2.45PF	1 609F	3220 1	7.3885
<b>14</b> 1	1,1755-00	1 7615-00	2 639E-09	3.9545-60	5.925F=10	8.878E-00	1.330F-08	1.903E-AA	2.986E-08	4.475E-0R	6.705E-03	1.0055-07	1.505E-67	2.2555-07	3.3795-117	5.063E-07	7 5845-07	1 137E-06	1.7635-04	2.552E-06
	90	90	ŝ	90	50	9 U	ۍ د	90	9 U	ç Ç	9 u	9 U	90	9 U	ŝ	ŝ	s c	ŝ	ŝ	40
F (E)	1.0136	1.0135	1.013E	1.013E	4.7105	4.710E	7.575F	9.6025	0.594F	9.617F	7.6445	4.2815	1.735 5	1.2675	5.92E	4.4155	2.458F	1.7365	1.1635	7.8965
<b>L</b> .	1.0845-09	4 425F-09	2.4344-09	3 447 - n9	5.4054-09	8 1381-09	1 227F-08	1 A38F-08	2 754F-08	4.1271-08	80-128: 9	9.7651-08	1 3885-07	2 ndnr-07	3. 17 07	6 c 701 - 07	6 cu7c=07	1 0485-06	1. 7.15-06	2. 3565-06
	90	.90	90	20	05	90	90	90	00	90	.90	9ù	0 0	90	05	ĉ	02	5	50	70
5 (F)	1.0135	42 10 ·	1.0135	10135	7105	4.710F	7 5755	7.5756	C. 506F	C. 617F	7.6445	4.8815	2 9795	1 2475	5 9255	4155	3 2775	1 895F	1.267F	8.4165
44.	1.0005-09	1.4985+00	2.2455=09	3.3648-09	5.0405-09	7.5528+09	1.1321-08	1.695E=08	2.5405-08	3.8065-08	5.7031-08	8.5455+08	1.2301-07	1.9185-07	2.875F=07	4.3075-07	6.4538-07	0 4701-07	1.4495-06	2.1745-06

Measured and counted activities, activity ratios and percentage errors . B(1)/A(1) - 1.

B(I)/A(I)

8(1)

4 ( I ) A

) = 3.948F=02				
11239 (NF) FP	8.74059E 02	R.68173E 02	9. 00008E+01	-0.9002
V164 2NG 50V-65	1.805645.03	1 R8585F 03	1.04442F 00	4122 2
U176(NG)10477	4.217025 03	4.01247F 03	-9.7583E-01	#7:2617
N115CNG) [N116	6.08475F 02	A. 38400F 02	1, n40185 0n	4.9481
U151 (NG) FU152	2.407691 03	2.41241F 03	9.27400E=04	-2.2400

Results printed out by the RFO7 programme (II)

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er of iter	ations:	51										123	25/35,
erential f	lux prin	tout	1 Poin	lt-wise									
•	F(E)		ŧ.	FCES		, <b>W</b> J	F(F)	•	F(E)		w	£ (£)	·
0000000			00-0700	30.00		4 4745an0	1 1125 14	1 2745-00	1 0125	Ŷ	1.382E-09	1.0125	.90
			- 20 - 2 - 0 0	1.0125		1.7615-00	1.012F 06	1.9105-09	1 0135	90	2.0715-09	1.0136	00
2.2456+00	01.35	06 2	4345-09	1.0935	99	2.6395-09	1.0138 96	2.8615-09	1.0135	90	3.1035-09	1. 013E	06
3.3646-09	1.0135	06 3	6475-09	1.0135	90	1.954E-00	1.01.5F 06	4.287F-09	4.778F	90	4.649E-09	4.777E	90 90
5.0405-09	2795	50 00	1.057-09	4.7785	90	5 925E-00	4 780F 00	61-125-09	4 777E	ŝ	6.965E-09	4.7758	n é
7.5526-09	4.775	00	188-09	4.7726	<b>9</b> 0	8 878F=00	4.764F 06	9 424F-09	7.7325	9 U	80-377J.1	3756.6	06
1.1325-08	7 6995	1 00	227F-08	7.6785	90	1.330F-0A	7.651F 06	1.447F-08	7.6285	ŝç	1.564E+08	7.592E	ŶŨ
1.695E-08	7.561F	00	80=38F=08	9.5226	\$ C	1.9935-08	9 446F 08	2.1615-08	9.3536	0 Q	2.343E+AA	9,276F	ý Ų
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5. Zatrena	· 780F	9 90	1341-08	5.754F	90	6.7055-08	6 754F 06	7.260F-0R	6.703E	<b>6</b> 0	7 . RR2F+0A	4.55×F	96
8.5457.00	4 643F	00	2655-08	4.8125	0	1.0055-07	5.107F 06	1.0895-07	3.2576	9 U	1.1816-07	3,6168	0 6
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1.9185-07	1 2495	06 2	0401-07	1.223#	90	2555+07	8,482F 05	7.45F-07	8.544E	50	2.651F+07	R_762E	05
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4.1075-07	5 6958	1 20	470F-07	6.420F	50	5.063E-07	5.188F 05	5.49AE-07	3.34AE	S	5.952E=07	3,2365	50
6.4534-07	3 1025	05 6	997F-07	2.399 #	5	7.5865-07	2,305F 05	8.225F=07	2.395F	50	8.9185-07	2.057E	05
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